

Borehole No. **BH106**

Engineering Log - Borehole

Sheet 1 of 1
Project No: **GEOTKPAR01560AA**

Client: **BROWN CONSULTING (QLD) PTY LTD**

Date started: **12.5.2009**

Principal:

Date completed: **12.5.2009**

Project: **BELLVISTA 2**

Logged by: **DF**

Borehole Location: **REFER TO SITE PLAN**

Checked by: **RFM**

drill model and mounting: EDSON CPI Easting: 508847.031 slope: -90° R.L. Surface: 3.365
hole diameter: 100 mm Northing 7035109.224 bearing: datum: GDA94

drilling information					material substance									
method	penetration	support	water	notes samples, tests, etc	RL	depth metres	graphic log	classification symbol	material soil type: plasticity or particle characteristics, colour, secondary and minor components.	moisture condition	consistency/ density index	pocket penetro- meter kPa	structure and additional observations	
ADT	1 2 3	N			3			SM	SILTY SAND: fine to medium grained, dark grey, trace of organics.	M	L		DIST PP=150kPa DIST PP=260kPa DIST PP=300kPa	
						1		SP	SAND: fine to medium grained, pale grey and brown. ...trace of silt.	M/W	MD			
					2			SC	CLAYEY SAND: fine to medium grained, pale grey, medium plasticity fines.	M	St	X		
					2			CH	SANDY CLAY: medium to high plasticity, pale grey and red, fine to medium grained sand.		VSt	X		
					1							X		
					3				Borehole BH106 terminated at 3m				LIMIT OF INVESTIGATION	
					0									
					4									
					-1									
					5									
					-2									
					6									
					-3									
					7									
					-4									
					8									

method AS auger screwing* AD auger drilling* RR roller/tricone W washbore CT cable tool HA hand auger DT diatube B blank bit V V bit T TC bit *bit shown by suffix e.g. ADT	support M mud N nil C casing penetration 1 2 3 4  no resistance ranging to refusal water  10/1/98 water level on date shown  water inflow  water outflow	notes, samples, tests U ₅₀ undisturbed sample 50mm diameter U ₆₃ undisturbed sample 63mm diameter D disturbed sample N standard penetration test (SPT) N* SPT - sample recovered Nc SPT with solid cone V vane shear (kPa) P pressuremeter Bs bulk sample E environmental sample R refusal	classification symbols and soil description based on unified classification system moisture D dry M moist W wet Wp plastic limit WL liquid limit	consistency/density index VS very soft S soft F firm St stiff VSt very stiff H hard Fb friable VL very loose L loose MD medium dense D dense VD very dense
--	---	--	--	---

Borehole No. **BH107**

Engineering Log - Borehole

Sheet 1 of 1
Project No: **GEOTKPAR01560AA**

Client: **BROWN CONSULTING (QLD) PTY LTD**

Date started: **12.5.2009**

Principal:

Date completed: **12.5.2009**

Project: **BELLVISTA 2**

Logged by: **DF**

Borehole Location: **REFER TO SITE PLAN**

Checked by: **RFM**

drill model and mounting: EDSON CPI Easting: 508715.242 slope: -90° R.L. Surface: 3.513
hole diameter: 100 mm Northing 7034897.495 bearing: datum: GDA94

drilling information						material substance																							
method	penetration			support	water	notes samples, tests, etc	RL	depth metres	graphic log	classification symbol	material soil type: plasticity or particle characteristics, colour, secondary and minor components.	moisture condition	consistency/ density index	pocket penetro- meter kPa	structure and additional observations														
	1	2	3																										
ADT				N								M	MD																
							3			SP	SAND: fine to medium grained, pale brown, trace of silt.	M/W																	
							1			SP	SAND: fine to medium grained, pale brown and orange, with clay fines.	W																	
						ASS	2			SC	CLAYEY SAND: fine to medium grained, pale brown and red, low plasticity fines, trace of fine grained gravel.	M/W																	
							2			CH	SANDY CLAY: medium to high plasticity, pale grey and pale brown, fine to medium grained sand, trace of gravel.	M	St																
							2			CH	SANDY SILTY CLAY: high plasticity, pale grey, fine to medium grained sand.		VSt	X	DIST PP=300kPa														
							1							X	DIST PP=290kPa														
							3																						
							0				Borehole BH107 terminated at 3m				LIMIT OF INVESTIGATION														
							4																						
							-1																						
							5																						
							-2																						
							6																						
							-3																						
							7																						
							-4																						
							8																						
method AS auger screwing* AD auger drilling* RR roller/tricone W washbore CT cable tool HA hand auger DT diatube B blank bit V V bit T TC bit *bit shown by suffix e.g. ADT						support M mud N nil C casing penetration 1 2 3 4  no resistance ranging to refusal water  10/1/98 water level on date shown  water inflow  water outflow						notes, samples, tests U ₅₀ undisturbed sample 50mm diameter U ₆₃ undisturbed sample 63mm diameter D disturbed sample N standard penetration test (SPT) N* SPT - sample recovered Nc SPT with solid cone V vane shear (kPa) P pressuremeter Bs bulk sample E environmental sample R refusal						classification symbols and soil description based on unified classification system moisture D dry M moist W wet Wp plastic limit W _L liquid limit						consistency/density index VS very soft S soft F firm St stiff VSt very stiff H hard Fb friable VL very loose L loose MD medium dense D dense VD very dense					

Borehole No. **BH108**

Engineering Log - Borehole

Sheet 1 of 1
Project No: **GEOTKPAR01560AA**

Client: **BROWN CONSULTING (QLD) PTY LTD**

Date started: **12.5.2009**

Principal:

Date completed: **12.5.2009**

Project: **BELLVISTA 2**

Logged by: **DF**

Borehole Location: **REFER TO SITE PLAN**

Checked by: **RFM**

drill model and mounting: EDSON CPI Easting: 508803.648 slope: -90° R.L. Surface: 3.421
hole diameter: 100 mm Northing 7034985.015 bearing: datum: GDA94

drilling information						material substance													
method	penetration			support	water	notes samples, tests, etc	RL	depth metres	graphic log	classification symbol	material soil type: plasticity or particle characteristics, colour, secondary and minor components.	moisture condition	consistency/ density index	pocket penetro- meter kPa	structure and additional observations				
	1	2	3																
ADT				N						SM	SILTY SAND: fine to medium grained, dark grey, trace of organics.	M	L						
							3	1		SP	SAND: fine to medium grained, grey/brown, trace of silt. ...colour changing to grey/brown. ...colour changing to pale grey and pale brown.	M/W	MD						
						ASS	2	2		CL	SANDY CLAY: medium plasticity, pale grey and orange/red, fine to medium grained sand.	M	St	X					
							2	2		SP	SAND:< fine to medium grained, pale grey. ...colour changing to dark grey/dark brown.	W	MD						
							1	3		CL	SANDY CLAY: medium plasticity, pale grey, fine to medium grained sand.	M	St						
										SP	SAND: fine to medium grained, pale grey, trace of silt and clay fines.	W	MD						
							3												
							0	4			Borehole BH108 terminated at 3m				LIMIT OF INVESTIGATION				
							-1	5											
							-2	6											
							-3	7											
							-4	8											
method AS auger screwing* AD auger drilling* RR roller/tricone W washbore CT cable tool HA hand auger DT diatube B blank bit V V bit T TC bit *bit shown by suffix e.g. ADT						support M mud N nil C casing penetration 1 2 3 4  no resistance ranging to refusal water  10/1/98 water level on date shown  water inflow  water outflow				notes, samples, tests U ₅₀ undisturbed sample 50mm diameter U ₆₃ undisturbed sample 63mm diameter D disturbed sample N standard penetration test (SPT) N* SPT - sample recovered Nc SPT with solid cone V vane shear (kPa) P pressuremeter Bs bulk sample E environmental sample R refusal				classification symbols and soil description based on unified classification system moisture D dry M moist W wet Wp plastic limit W _L liquid limit				consistency/density index VS very soft S soft F firm St stiff VSt very stiff H hard Fb friable VL very loose L loose MD medium dense D dense VD very dense	

Borehole No. **BH109**

Engineering Log - Borehole

Sheet 1 of 1
Project No: **GEOTKPAR01560AA**

Client: **BROWN CONSULTING (QLD) PTY LTD**

Date started: **12.5.2009**

Principal:

Date completed: **12.5.2009**

Project: **BELLVISTA 2**

Logged by: **DF**

Borehole Location: **REFER TO SITE PLAN**

Checked by: **RFM**

drill model and mounting: EDSON CPI Easting: 508797.886 slope: -90° R.L. Surface: 3.413
hole diameter: 100 mm Northing 7034805.5 bearing: datum: GDA94

drilling information						material substance																							
method	penetration			support	water	notes samples, tests, etc	RL	depth metres	graphic log	classification symbol	material soil type: plasticity or particle characteristics, colour, secondary and minor components.	moisture condition	consistency/ density index	pocket penetro- meter kPa	structure and additional observations														
	1	2	3																										
ADT				N								M	L																
							3			SP	SILTY SAND: fine to medium grained, dark grey, trace of organics.	W	MD																
							1			SP	SAND: fine to medium grained, pale brown, trace of silt.	M/W																	
							2			SC	SAND: fine to medium grained, brown, trace of silt and clay.	M																	
							2			CL	CLAYEY SAND: fine to medium grained, pale brown/grey and red, medium plasticity fines.		St	x	DIST PP=150kPa														
							2			CH	SANDY CLAY: medium plasticity, pale grey, fine to medium grained sand.		VSt	x	DIST PP=220kPa														
							1				SANDY CLAY: medium to high plasticity, pale grey, fine to medium grained sand.			x	DIST PP=260kPa														
							3							x	DIST PP=280kPa														
							0				Borehole BH109 terminated at 3m				DIST PP=280kPa LIMIT OF INVESTIGATION														
							4																						
							-1																						
							5																						
							-2																						
							6																						
							-3																						
							7																						
							-4																						
							8																						
method AS auger screwing* AD auger drilling* RR roller/tricone W washbore CT cable tool HA hand auger DT diatube B blank bit V V bit T TC bit *bit shown by suffix e.g. ADT						support M mud N nil C casing penetration 1 2 3 4  no resistance ranging to refusal water  10/1/98 water level on date shown  water inflow  water outflow						notes, samples, tests U ₅₀ undisturbed sample 50mm diameter U ₆₃ undisturbed sample 63mm diameter D disturbed sample N standard penetration test (SPT) N* SPT - sample recovered Nc SPT with solid cone V vane shear (kPa) P pressuremeter Bs bulk sample E environmental sample R refusal						classification symbols and soil description based on unified classification system moisture D dry M moist W wet Wp plastic limit W _L liquid limit						consistency/density index VS very soft S soft F firm St stiff VSt very stiff H hard Fb friable VL very loose L loose MD medium dense D dense VD very dense					

Borehole No. **BH110**

Engineering Log - Borehole

Sheet 1 of 1
Project No: **GEOTKPAR01560AA**

Client: **BROWN CONSULTING (QLD) PTY LTD**

Date started: **16.5.2009**

Principal:

Date completed: **16.5.2009**

Project: **BELLVISTA 2**

Logged by: **DF**

Borehole Location: **REFER TO SITE PLAN**

Checked by: **RFM**

drill model and mounting: EDSON CPI Easting: 508949.336 slope: -90° R.L. Surface: 2.719
hole diameter: 100 mm Northing 7034852.051 bearing: datum: GDA94

drilling information						material substance										
method	penetration			support	water	notes samples, tests, etc	RL	depth metres	graphic log	classification symbol	material soil type: plasticity or particle characteristics, colour, secondary and minor components.	moisture condition	consistency/ density index	pocket penetro- meter kPa	structure and additional observations	
	1	2	3													
ADT				N						SM	SILTY SAND: fine to medium grained, dark grey, trace of organics.	M/W	L			
							2	1		SP	SAND: fine to medium grained, dark grey, trace of silt.	W	MD			
							1	2		SP	SAND: fine to medium grained, pale grey.					
							1	2		SC	CLAYEY SAND: fine to medium grained, pale grey, medium plasticity fines.	M				
							2	3		CH	SANDY CLAY: high plasticity, pale grey, fine to medium grained sand. ...medium to high plasticity.		VSt	x	DIST PP=250kPa	
							0	3		SC	CLAYEY SAND: fine to medium grained, pale grey, medium plasticity fines.		St	x	DIST PP=180kPa	
							3	4					MD			
											Borehole BH110 terminated at 3m				LIMIT OF INVESTIGATION	
							-1	4								
							-2	5								
							-3	6								
							-4	7								
							-5	8								
method AS auger screwing* AD auger drilling* RR roller/tricone W washbore CT cable tool HA hand auger DT diatube B blank bit V V bit T TC bit *bit shown by suffix e.g. ADT						support M mud C casing penetration 1 2 3 4  no resistance ranging to refusal water  10/1/98 water level on date shown  water inflow  water outflow		notes, samples, tests U ₅₀ undisturbed sample 50mm diameter U ₆₃ undisturbed sample 63mm diameter D disturbed sample N standard penetration test (SPT) N* SPT - sample recovered Nc SPT with solid cone V vane shear (kPa) P pressuremeter Bs bulk sample E environmental sample R refusal				classification symbols and soil description based on unified classification system moisture D dry M moist W wet W _p plastic limit W _L liquid limit			consistency/density index VS very soft S soft F firm St stiff VSt very stiff H hard Fb friable VL very loose L loose MD medium dense D dense VD very dense	

Borehole No. **BH111**

Engineering Log - Borehole

Sheet 1 of 1
Project No: **GEOTKPAR01560AA**

Client: **BROWN CONSULTING (QLD) PTY LTD**

Date started: **15.5.2009**

Principal:

Date completed: **15.5.2009**

Project: **BELLVISTA 2**

Logged by: **DF**

Borehole Location: **REFER TO SITE PLAN**

Checked by: **RFM**

drill model and mounting: EDSON CPI Easting: 509087.238 slope: -90° R.L. Surface: 1.913
hole diameter: 100 mm Northing 7034820.414 bearing: datum: GDA94

drilling information						material substance																							
method	penetration			support	water	notes samples, tests, etc	RL	depth metres	graphic log	classification symbol	material soil type: plasticity or particle characteristics, colour, secondary and minor components.	moisture condition	consistency/ density index	pocket penetro- meter kPa	structure and additional observations														
	1	2	3																										
ADT				N						SM	SILTY SAND: fine to medium grained, dark grey, trace of organics.	W	L																
								1		SP	SAND: fine to medium grained, pale grey and pale brown, trace of silt. ...colour changing to pale grey.		MD																
								1		SC	CLAYEY SAND: fine to medium grained, pale grey, medium plasticity fines.		D																
								2		CH	SANDY CLAY: high plasticity, pale grey, fine to medium grained sand. ...medium to high plasticity.	M	VSt																
								3																					
								4			Borehole BH111 terminated at 3m																		
								5																					
								6																					
								7																					
								8																					
method AS auger screwing* AD auger drilling* RR roller/tricone W washbore CT cable tool HA hand auger DT diatube B blank bit V V bit T TC bit *bit shown by suffix e.g. ADT						support M mud N nil C casing penetration 1 2 3 4  no resistance ranging to refusal water  10/1/98 water level on date shown  water inflow  water outflow						notes, samples, tests U ₅₀ undisturbed sample 50mm diameter U ₆₃ undisturbed sample 63mm diameter D disturbed sample N standard penetration test (SPT) N* SPT - sample recovered Nc SPT with solid cone V vane shear (kPa) P pressuremeter Bs bulk sample E environmental sample R refusal						classification symbols and soil description based on unified classification system moisture D dry M moist W wet Wp plastic limit W _L liquid limit						consistency/density index VS very soft S soft F firm St stiff VSt very stiff H hard Fb friable VL very loose L loose MD medium dense D dense VD very dense					

Soil Description Explanation Sheet (1 of 2)

DEFINITION:

In engineering terms soil includes every type of uncemented or partially cemented inorganic or organic material found in the ground. In practice, if the material can be remoulded or disintegrated by hand in its field condition or in water it is described as a soil. Other materials are described using rock description terms.

CLASSIFICATION SYMBOL & SOIL NAME

Soils are described in accordance with the Unified Soil Classification (UCS) as shown in the table on Sheet 2.

PARTICLE SIZE DESCRIPTIVE TERMS

NAME	SUBDIVISION	SIZE
Boulders		>200 mm
Cobbles		63 mm to 200 mm
Gravel	coarse	20 mm to 63 mm
	medium	6 mm to 20 mm
	fine	2.36 mm to 6 mm
Sand	coarse	600 μ m to 2.36 mm
	medium	200 μ m to 600 μ m
	fine	75 μ m to 200 μ m

MOISTURE CONDITION

Dry Looks and feels dry. Cohesive and cemented soils are hard, friable or powdery. Uncemented granular soils run freely through hands.

Moist Soil feels cool and darkened in colour. Cohesive soils can be moulded. Granular soils tend to cohere.

Wet As for moist but with free water forming on hands when handled.

CONSISTENCY OF COHESIVE SOILS

TERM	UNDRAINED STRENGTH S_u (kPa)	FIELD GUIDE
Very Soft	<12	A finger can be pushed well into the soil with little effort.
Soft	12 - 25	A finger can be pushed into the soil to about 25mm depth.
Firm	25 - 50	The soil can be indented about 5mm with the thumb, but not penetrated.
Stiff	50 - 100	The surface of the soil can be indented with the thumb, but not penetrated.
Very Stiff	100 - 200	The surface of the soil can be marked, but not indented with thumb pressure.
Hard	>200	The surface of the soil can be marked only with the thumbnail.
Friable	–	Crumbles or powders when scraped by thumbnail.

DENSITY OF GRANULAR SOILS

TERM	DENSITY INDEX (%)
Very loose	Less than 15
Loose	15 - 35
Medium Dense	35 - 65
Dense	65 - 85
Very Dense	Greater than 85

MINOR COMPONENTS

TERM	ASSESSMENT GUIDE	PROPORTION OF MINOR COMPONENT IN:
Trace of	Presence just detectable by feel or eye, but soil properties little or no different to general properties of primary component.	Coarse grained soils: <5% Fine grained soils: <15%
With some	Presence easily detected by feel or eye, soil properties little different to general properties of primary component.	Coarse grained soils: 5 - 12% Fine grained soils: 15 - 30%

SOIL STRUCTURE

ZONING	CEMENTING
Layers Continuous across exposure or sample.	Weakly cemented Easily broken up by hand in air or water.
Lenses Discontinuous layers of lenticular shape.	Moderately cemented Effort is required to break up the soil by hand in air or water.
Pockets Irregular inclusions of different material.	

GEOLOGICAL ORIGIN

WEATHERED IN PLACE SOILS

Extremely weathered material Structure and fabric of parent rock visible.

Residual soil Structure and fabric of parent rock not visible.

TRANSPORTED SOILS

Aeolian soil Deposited by wind.

Alluvial soil Deposited by streams and rivers.

Colluvial soil Deposited on slopes (transported downslope by gravity).

Fill Man made deposit. Fill may be significantly more variable between tested locations than naturally occurring soils.

Lacustrine soil Deposited by lakes.

Marine soil Deposited in ocean basins, bays, beaches and estuaries.

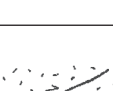
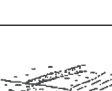
Soil Description Explanation Sheet (2 of 2)

SOIL CLASSIFICATION INCLUDING IDENTIFICATION AND DESCRIPTION

FIELD IDENTIFICATION PROCEDURES (Excluding particles larger than 60 mm and basing fractions on estimated mass)					USC	PRIMARY NAME
COARSE GRAINED SOILS More than 50% of materials less than 63 mm is larger than 0.075 mm	GRAVELS More than half of coarse fraction is larger than 2.0 mm	CLEAN GRAVELS (Little or no fines)	Wide range in grain size and substantial amounts of all intermediate particle sizes.		GW	GRAVEL
			Predominantly one size or a range of sizes with more intermediate sizes missing.		GP	GRAVEL
		GRAVELS WITH FINES (Appreciable amount of fines)	Non-plastic fines (for identification procedures see ML below)		GM	SILTY GRAVEL
			Plastic fines (for identification procedures see CL below)		GC	CLAYEY GRAVEL
	SANDS More than half of coarse fraction is smaller than 2.0 mm	CLEAN SANDS (Little or no fines)	Wide range in grain sizes and substantial amounts of all intermediate sizes		SW	SAND
			Predominantly one size or a range of sizes with some intermediate sizes missing.		SP	SAND
		SANDS WITH FINES (Appreciable amount of fines)	Non-plastic fines (for identification procedures see ML below).		SM	SILTY SAND
			Plastic fines (for identification procedures see CL below).		SC	CLAYEY SAND
FINE GRAINED SOILS More than 50% of material less than 63 mm is smaller than 0.075 mm	SILTS & CLAYS Liquid limit less than 50	IDENTIFICATION PROCEDURES ON FRACTIONS <0.2 mm.				
		DRY STRENGTH	DILATANCY	TOUGHNESS		
		None to Low	Quick to slow	None	ML	SILT
		Medium to High	None	Medium	CL	CLAY
	SILTS & CLAYS Liquid limit greater than 50	Low to medium	Slow to very slow	Low	OL	ORGANIC SILT
		Low to medium	Slow to very slow	Low to medium	MH	SILT
		High	None	High	CH	CLAY
		Medium to High	None	Low to medium	OH	ORGANIC CLAY
HIGHLY ORGANIC SOILS	Readily identified by colour, odour, spongy feel and frequently by fibrous texture.			Pt	PEAT	
• Low plasticity – Liquid Limit W _L less than 35%. • Medium plasticity – W _L between 35% and 50%.						

• Low plasticity – Liquid Limit W_L less than 35%. • Medium plasticity – W_L between 35% and 50%.

COMMON DEFECTS IN SOIL

TERM	DEFINITION	DIAGRAM	TERM	DEFINITION	DIAGRAM
PARTING	A surface or crack across which the soil has little or no tensile strength. Parallel or sub parallel to layering (eg bedding). May be open or closed.		SOFTENED ZONE	A zone in clayey soil, usually adjacent to a defect in which the soil has a higher moisture content than elsewhere.	
JOINT	A surface or crack across which the soil has little or no tensile strength but which is not parallel or sub parallel to layering. May be open or closed. The term 'fissure' may be used for irregular joints <0.2 m in length.		TUBE	Tubular cavity. May occur singly or as one of a large number of separate or inter-connected tubes. Walls often coated with clay or strengthened by denser packing of grains. May contain organic matter	
SHEARED ZONE	Zone in clayey soil with roughly parallel near planar, curved or undulating boundaries containing closely spaced, smooth or slickensided, curved intersecting joints which divide the mass into lenticular or wedge shaped blocks.		TUBE CAST	Roughly cylindrical elongated body of soil different from the soil mass in which it occurs. In some cases the soil which makes up the tube cast is cemented.	
SHEARED SURFACE	A near planar curved or undulating, smooth, polished or slickensided surface in clayey soil. The polished or slickensided surface indicates that movement (in many cases very little) has occurred along the defect.		INFILLED SEAM	Sheet or wall like body of soil substance or mass with roughly planar to irregular near parallel boundaries which cuts through a soil mass. Formed by infilling of open joints.	

Appendix D

Laboratory Test Certificates

determination of emerson class number

client : **Brown Consulting (Qld) Pty Ltd**

job no : **GEOTKPAR01560AA**

principal :

laboratory : **KUNDA PARK**

project : **Bellvista 2**

date : **20/05/09**

location : **Area 1**

test report no. : **GEOTKPAR01560AA**

test procedure : **AS 1289.3.8.1**

date sampled:

material source: **Topsoil BH84**

sample number:

sample identification:

test data

air dried crumbs

time start of
test:

time dispersion
commences:

time dispersion
completed:

remoulded material

time start of
test:

time dispersion
commences:

time dispersion
completed:

material description

type of water used: **distilled**

water temperature: **20.5 ° C**

immersion of air dried crumbs

does not slake	☒		
slakes	☐		

complete dispersion	☐	①
partial dispersion	☐	②
no dispersion	☐	

swell	☐	⑦
does not swell	☒	⑧

immersion of remoulded material

disperses	☐	③
does not disperse	☐	

calcite or gypsum		
present	☐	④
absent	☐	

vigorous shaking		
disperses	☐	⑤
flocculates	☐	⑥

**Emerson
class number 8**

determination of emerson class number

client : **Brown Consulting (Qld) Pty Ltd**

job no : **GEOTKPAR01560AA**

principal :

laboratory : **KUNDA PARK**

project : **Bellvista 2**

date : **20/05/09**

location : **Area 1**

test report no. : **GEOTKPAR01560AA**

test procedure : **AS 1289.3.8.1**

date sampled:

material source: **Subsoil BH84**

sample number:

sample identification: **Depth 1.5 - 1.75m**

test data

air dried crumbs

time start of
test:

time dispersion
commences:

time dispersion
completed:

remoulded material

time start of
test:

time dispersion
commences:

time dispersion
completed:

material description

type of water used: **distilled**

water temperature: **20.5 ° C**

immersion of air dried crumbs

does not slake	☒	↓	swell	☐	⑦
slakes	☐			does not swell	☒

complete dispersion	☐	①
partial dispersion	☐	②
no dispersion	☐	

immersion of remoulded material

disperses	☐	③
does not disperse	☐	

calcite or gypsum		
present	☐	④
absent	☐	

vigorous shaking		
disperses	☐	⑤
flocculates	☐	⑥

**Emerson
class number 8**

determination of emerson class number

client : **Brown Consulting (Qld) Pty Ltd**

job no : **GEOTKPAR01560AA**

principal :

laboratory : **KUNDA PARK**

project : **Bellvista 2**

date : **20/05/09**

location : **Area 1**

test report no. : **GEOTKPAR01560AA**

test procedure : **AS 1289.3.8.1**

date sampled:

material source: **Topsoil BH107**

sample number:

sample identification:

test data

air dried crumbs

time start of
test:

time dispersion
commences:

time dispersion
completed:

remoulded material

time start of
test:

time dispersion
commences:

time dispersion
completed:

material description

type of water used: **distilled**

water temperature: **20.5 ° C**

immersion of air dried crumbs

does not slake	☒		
slakes	☐		

complete dispersion	☐	①
partial dispersion	☐	②
no dispersion	☐	

swell	☐	⑦
does not swell	☒	⑧

immersion of remoulded material

disperses	☐	③
does not disperse	☐	

calcite or gypsum		
present	☐	④
absent	☐	

vigorous shaking		
disperses	☐	⑤
flocculates	☐	⑥

**Emerson
class number 8**

determination of emerson class number

client : **Brown Consulting (Qld) Pty Ltd**

job no : **GEOTKPAR01560AA**

principal :

laboratory : **KUNDA PARK**

project : **Bellvista 2**

date : **20/05/09**

location : **Area 1**

test report no. : **GEOTKPAR01560AA**

test procedure : **AS 1289.3.8.1**

date sampled:

material source: **Subsoil BH107**

sample number:

sample identification: **Depth 2.5 - 2.75m**

test data

air dried crumbs

time start of
test:

time dispersion
commences:

time dispersion
completed:

remoulded material

time start of
test:

time dispersion
commences:

time dispersion
completed:

material description

type of water used: **distilled**

water temperature: **20.5 ° C**

immersion of air dried crumbs

does not slake	☐	↓	swell	☐	⑦
slakes	☒			does not swell	☐

complete dispersion	☐	①
partial dispersion	☐	②
no dispersion	☒	↓

immersion of remoulded material

disperses	☐	③
does not disperse	☒	↓

calcite or gypsum	☒	④
present		
absent	☐	↓

vigorous shaking	☐	⑤
disperses		
flocculates	☐	⑥

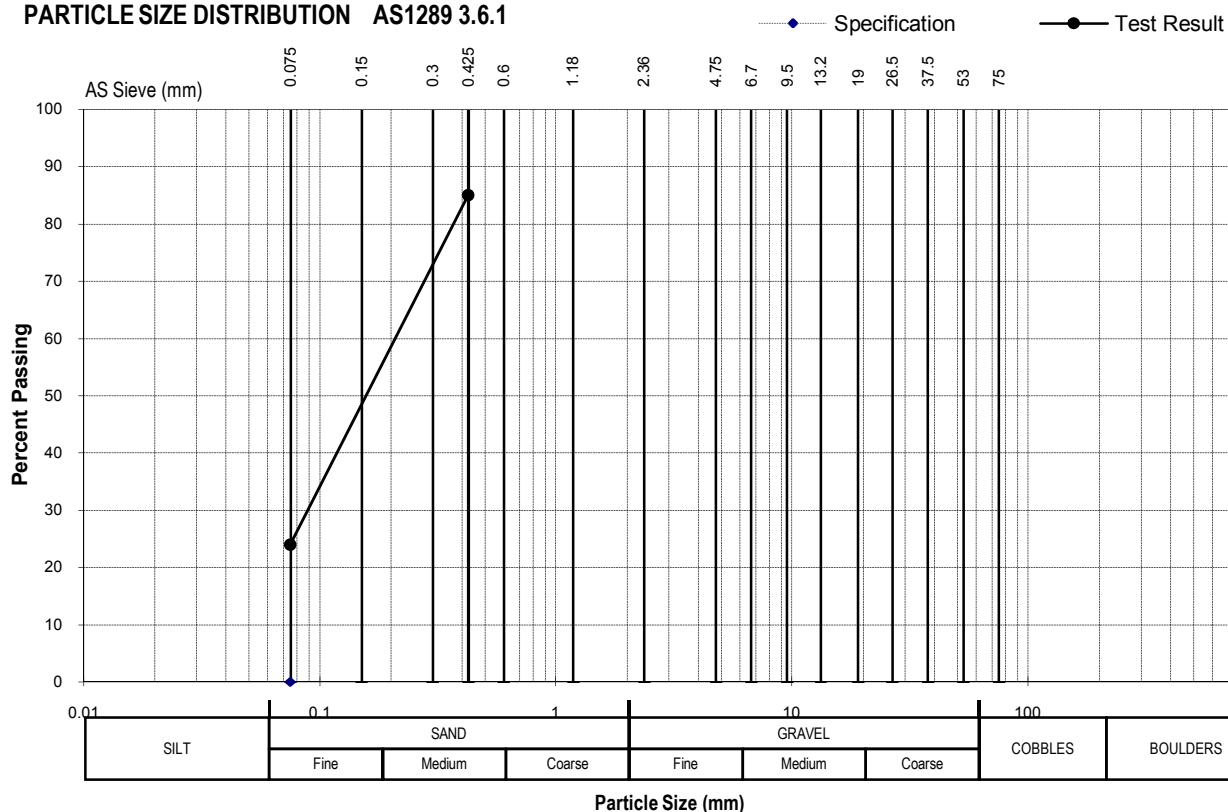
Emerson
class number

4

Client:	Brown Consulting (Qld) Pty Ltd	Job No:	GEOTKPAR01560AA	Laboratory:	Kunda Park
Principal:		Test Date:	20-May-2009	Sampled by:	MT
Project:	Bellvista 2 - Area 1	Date Sampled:		Report No:	2 of 3
Location:	REFER PLAN	Test No.:	BH 84		
Sample ID:	Subsoil 1.5m to 1.75m	Material Description			

MATERIAL CLASSIFICATION REPORT

PARTICLE SIZE DISTRIBUTION AS1289 3.6.1

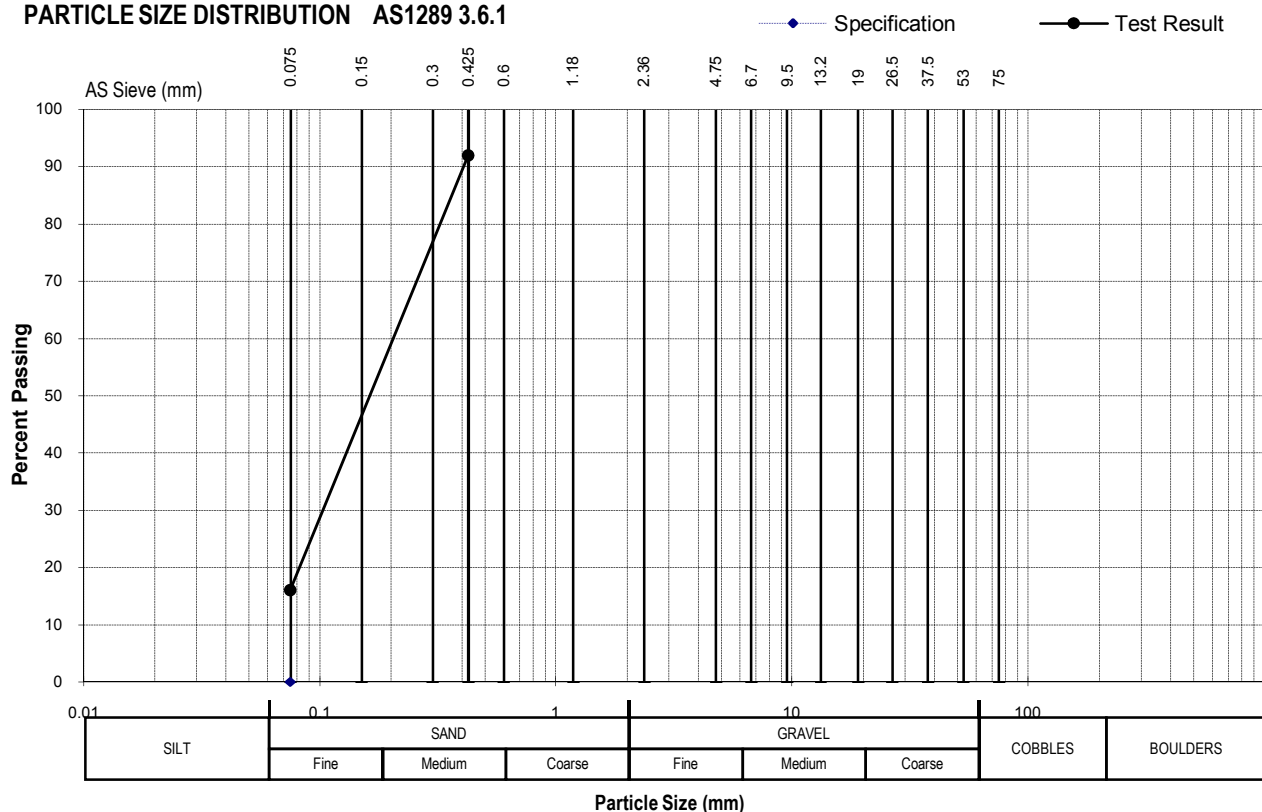


Sieve Size mm	% Passing	Specification		ATTERBERG LIMITS		Procedures
		Upper	Lower			
75				Liquid Limit	%	A
53				Plastic Limit	%	B
37.5				Plasticity Index	%	C
26.5				Linear Shrinkage	%	
19				Mould Length	mm	
13.2				Crumbling &/or Curling		
9.5				Sample History	Oven Dried ☐	Air Dried ☐
6.7				Sample Preparation	Dry Sieved ☐	Wet Sieved ☐
4.75				(A) AS 1289.3.1.1 Liquid Limit – Standard Method		
2.36				(B) AS 1289.3.2.1 Plastic Limit – Standard Limit		
1.18				(C) AS 1289.3.3.1 Plasticity Index – Standard Method		
600µm				(D) AS 1289.C4.1 Linear Shrinkage – Standard Method		
425µm	85			(NO) Not obtainable		
300µm				EMERSON CLASS NUMBER - AS 1289 3.8.1		
150µm				Emerson Class No.		
75µm	24			Water Type: Water Temperature:		
REMARKS:						

Client:	Brown Consulting (Qld) Pty Ltd	Job No:	GEOTKPAR01560AA	Laboratory:	Kunda Park
Principal:		Test Date:	20-May-2009	Sampled by:	MT
Project:	Bellvista 2 - Area 1	Date Sampled:		Report No:	1 of 3
Location:	REFER PLAN	Test No.:	BH 107		
Sample ID:	Topsoil	Material Description			

MATERIAL CLASSIFICATION REPORT

PARTICLE SIZE DISTRIBUTION AS1289 3.6.1

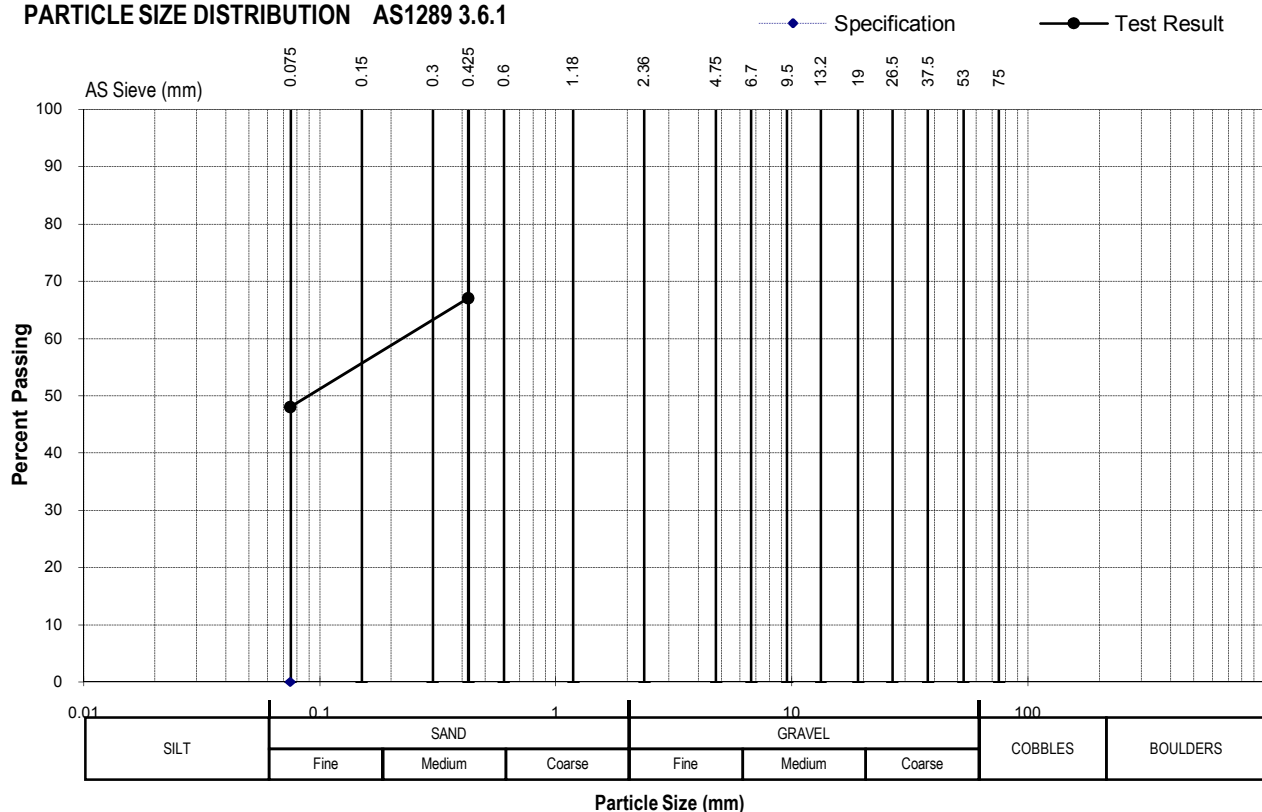


Sieve Size mm	% Passing	Specification		ATTERBERG LIMITS		Procedures
		Upper	Lower			
75				Liquid Limit	%	A
53				Plastic Limit	%	B
37.5				Plasticity Index	%	C
26.5				Linear Shrinkage	%	
19				Mould Length	mm	
13.2				Crumbling &/or Curling		
9.5				Sample History	Oven Dried ☐ Air Dried ☐	
6.7				Sample Preparation	Dry Sieved ☐ Wet Sieved ☐	
4.75				(A) AS 1289.3.1.1 Liquid Limit – Standard Method		
2.36				(B) AS 1289.3.2.1 Plastic Limit – Standard Limit		
1.18				(C) AS 1289.3.3.1 Plasticity Index – Standard Method		
600µm				(D) AS 1289.C4.1 Linear Shrinkage – Standard Method		
425µm	92			(NO) Not obtainable		
300µm				EMERSON CLASS NUMBER - AS 1289 3.8.1		
150µm				Emerson Class No.		
75µm	16			Water Type:		Water Temperature:
REMARKS:						

Client:	Brown Consulting (Qld) Pty Ltd	Job No:	GEOTKPAR01560AA	Laboratory:	Kunda Park
Principal:		Test Date:	20-May-2009	Sampled by:	MT
Project:	Bellvista 2 - Area 1	Date Sampled:		Report No:	3 of 3
Location:	REFER PLAN	Test No.:	BH 91		
Sample ID:	Subsoil 2.5m to 3.0m	Material Description			

MATERIAL CLASSIFICATION REPORT

PARTICLE SIZE DISTRIBUTION AS1289 3.6.1



Sieve Size mm	% Passing	Specification		ATTERBERG LIMITS		Procedures
		Upper	Lower			
75				Liquid Limit	%	A
53				Plastic Limit	%	B
37.5				Plasticity Index	%	C
26.5				Linear Shrinkage	%	
19				Mould Length	mm	
13.2				Crumbling &/or Curling		
9.5				Sample History	Oven Dried ☐ Air Dried ☐	
6.7				Sample Preparation	Dry Sieved ☐ Wet Sieved ☐	
4.75				(A) AS 1289.3.1.1 Liquid Limit – Standard Method		
2.36				(B) AS 1289.3.2.1 Plastic Limit – Standard Limit		
1.18				(C) AS 1289.3.3.1 Plasticity Index – Standard Method		
600µm				(D) AS 1289.C4.1 Linear Shrinkage – Standard Method		
425µm	67			(NO) Not obtainable		
300µm				EMERSON CLASS NUMBER - AS 1289 3.8.1		
150µm				Emerson Class No.		
75µm	48			Water Type: Water Temperature:		
REMARKS:						

Appendix E

Rainer Outputs

***** RAINER *****

DEPARTMENT of CONSERVATION and LAND MANAGEMENT

Date: 25/05/2009

Rainfall Intensity (mm/h) for BELLVISTA 2

1 hour, 2 years : 51.00
 12 hour, 2 years : 10.00
 72 hour, 2 years : 3.50
 1 hour, 50 years : 91.00
 12 hour, 50 years : 20.00
 72 hour, 50 years : 8.50
 Skewness : 0.12
 Geographical factor F2 : 4.39
 Geographical factor F50: 17.50

\DUR	5m	6m	10m	20m	30m	1h	2h	3h	6h	12h	24h	48h	72h	User
ARI														
1	126	118	97	71	58	39.7	25.3	19.3	12.1	7.64	5.14	3.39	2.59	0.00
2	160	150	123	90	74	51	32.4	24.8	15.7	9.92	6.76	4.50	3.46	0.00
5	196	185	152	112	91	63	40.8	31.5	20.2	12.9	9.08	6.24	4.90	0.00
10	217	204	168	124	102	70	45.8	35.5	22.9	14.8	10.5	7.37	5.85	0.00
20	247	232	191	141	116	80	53	40.9	26.5	17.2	12.5	8.83	7.07	0.00
50	285	268	221	164	134	93	62	48.0	31.4	20.5	15.1	10.9	8.78	0.00
100	314	295	244	181	148	103	68	54	35.1	23.1	17.1	12.5	10.2	0.00
User	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Estimated Rainfall Factor (R): 5540 Estimated 1:10 Storm (S10): 3580

min	Years						
	1	2	5	10	20	50	100
7	112	142	175	193	219	254	280
8	106	135	166	184	209	241	266
9	101	129	159	176	199	231	254
10	97	123	152	168	191	221	244
11	93	118	146	162	184	213	235
12	90	114	141	156	177	205	227
13	87	110	136	151	171	198	219
14	84	107	132	146	166	192	212
15	81	103	128	142	161	186	206
16	79	100	124	138	156	181	200
17	77	98	121	134	152	176	195
18	75	95	117	130	148	172	190
19	73	93	115	127	145	167	185
20	71	90	112	124	141	164	181
21	69	88	109	121	138	160	177
22	68	86	107	119	135	156	173
23	66	84	104	116	132	153	169
24	65	83	102	114	129	150	166
25	64	81	100	111	127	147	162
26	62	79	98	109	124	144	159
27	61	78	96	107	122	141	156
28	60	76	95	105	120	139	154
29	59	75	93	103	118	136	151
30	58	74	91	102	116	134	148
31	57	73	90	100	114	132	146
32	56	71	88	98	112	130	144
33	55	70	87	97	110	128	141
34	54	69	86	95	109	126	139
35	53	68	84	94	107	124	137
36	53	67	83	92	105	122	135
37	52	66	82	91	104	121	133
38	51	65	81	90	102	119	131
39	50	64	80	89	101	117	130
40	49.7	63	79	87	100	116	128
41	49.1	62	78	86	98	114	126
42	48.4	62	77	85	97	113	125
43	47.8	61	76	84	96	111	123
44	47.2	60	75	83	95	110	122
45	46.6	59	74	82	94	109	120
46	46.1	59	73	81	93	107	119
47	45.5	58	72	80	91	106	118
48	45.0	57	71	79	90	105	116
49	44.5	57	70	78	89	104	115
50	44.0	56	70	78	88	103	114
51	43.5	55	69	77	88	102	113
52	43.0	55	68	76	87	101	111
53	42.6	54	68	75	86	100	110
54	42.1	54	67	74	85	99	109
55	41.7	53	66	74	84	98	108
56	41.3	53	65	73	83	97	107
57	40.9	52	65	72	82	96	106
58	40.5	52	64	72	82	95	105
59	40.1	51	64	71	81	94	104

Appendix F

RUSLE Calculations

SWMP Commentary, Detailed Calculations

Note: These "Detailed Calculation" spreadsheets relate only to high erosion hazard lands as identified in figure 4.6 or where the designer chooses to use the RUSLE to size sediment basins. The "Standard Calculation" spreadsheets should be used on low erosion hazard lands as identified by figure 4.6 and where the designer chooses not to run the RUSLE in calculations.

1. Site Data Sheet

Site Name: Bellvista 2

Site Location: Caloundra

Precinct: Area 1

Description of Site:

Site area	Sub-catchments						Remarks
	Area 1						
Total catchment area (ha)	16						
Disturbed catchment area (ha)	16						

Soil analysis (enter sediment type if known, or laboratory particle size data)

Sediment Type (C, F or D) if known:	D	D					
% sand (fraction 0.02 to 2.00 mm)							
% silt (fraction 0.002 to 0.02 mm)							
% clay (fraction finer than 0.002 mm)							
Dispersion percentage							
% of whole soil dispersible							
Soil Texture Group	D	D					

Rainfall data

Design rainfall depth (days)	5						
Design rainfall depth (percentile)	85						
x-day, y-percentile rainfall event	57.7						
Rainfall R-factor (if known)	5540						
IFD: 2-year, 6-hour storm (if known)	15.7						

RUSLE Factors

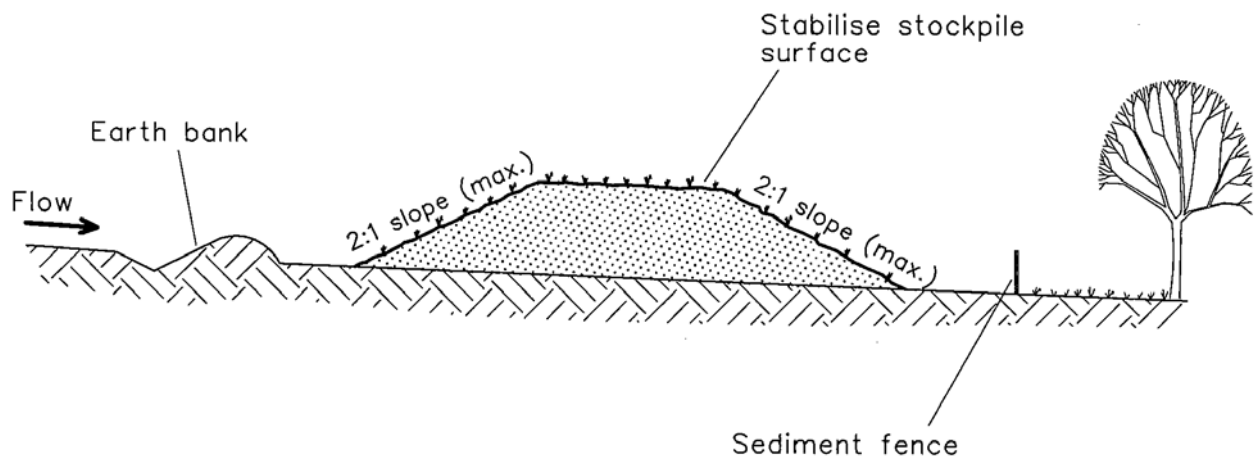
Rainfall erosivity (R-factor)	5540						Auto-filled from above
Soil erodibility (K-factor)	0.05						
Slope length (m)	80						
Slope gradient (%)	1						
Length/gradient (LS-factor)	0.19						
Erosion control practice (P-factor)	1.3		1.3	1.3	1.3	1.3	
Ground cover (C-factor)	1		1	1	1	1	

Calculations

Soil loss (t/ha/yr)	69						
Soil Loss Class	1						See Section 4.3 and Table 4-2.
Soil loss (m ³ /ha/yr)	53						
Sediment basin storage volume, m ³	145						See Sections 6.5.3 and 6.6.3

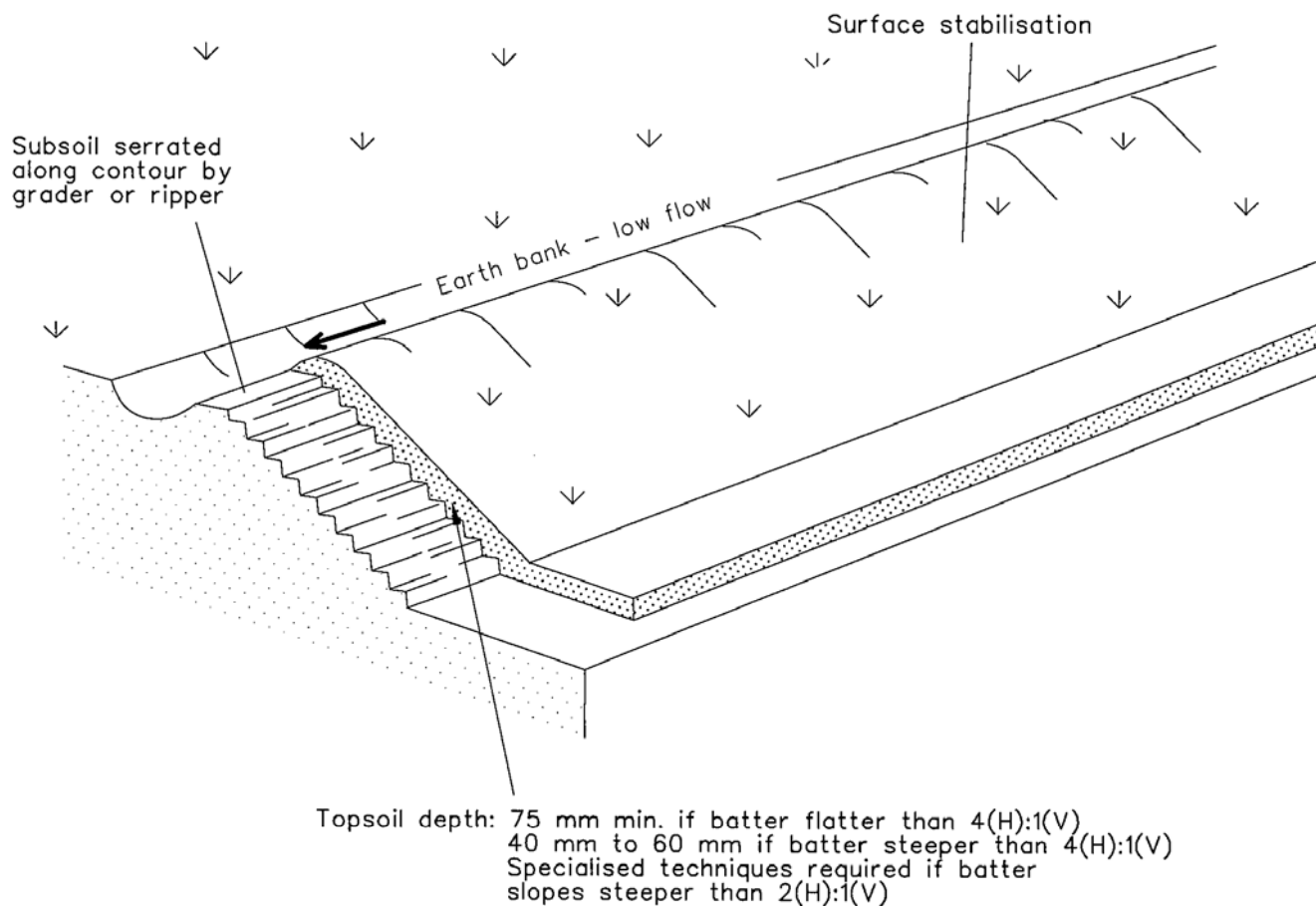
Appendix G

Standard Drawings



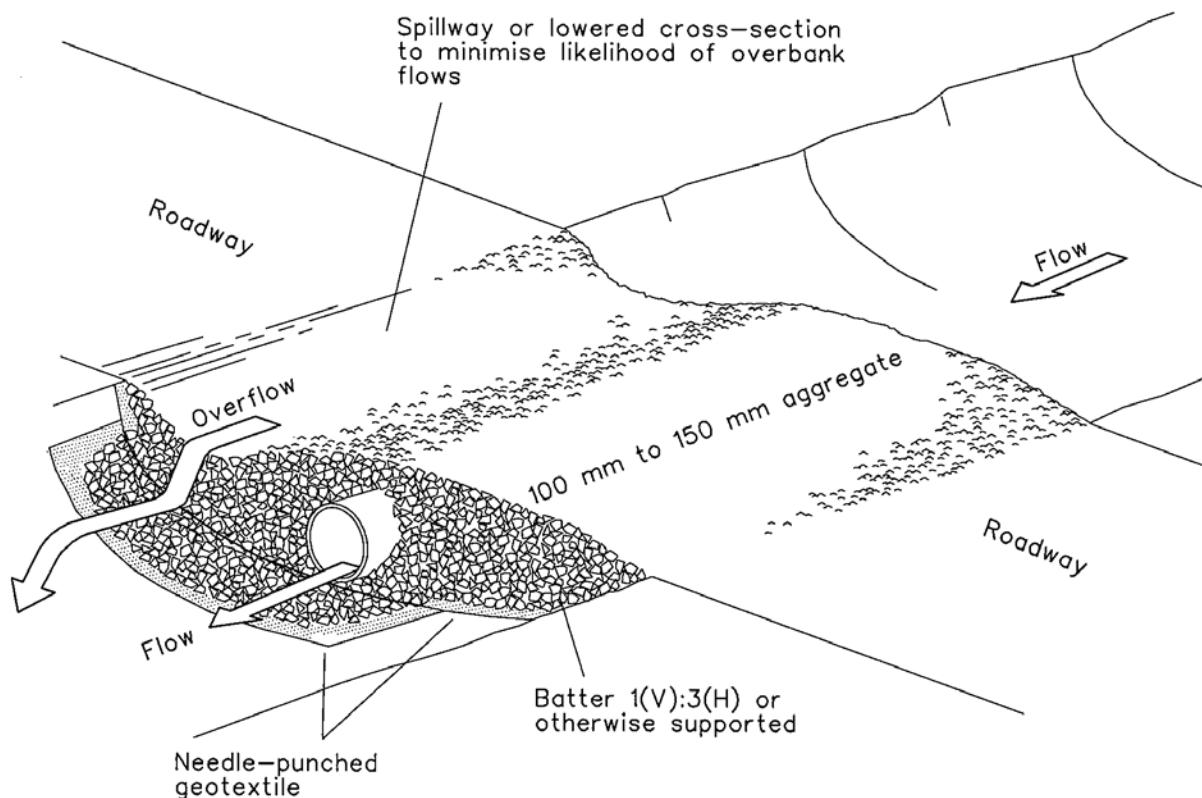
Construction Notes

1. Place stockpiles more than 2 (preferably 5) metres from existing vegetation, concentrated water flow, roads and hazard areas.
2. Construct on the contour as low, flat, elongated mounds.
3. Where there is sufficient area, topsoil stockpiles shall be less than 2 metres in height.
4. Where they are to be in place for more than 10 days, stabilise following the approved ESCP or SWMP to reduce the C-factor to less than 0.10.
5. Construct earth banks (Standard Drawing 5-5) on the upslope side to divert water around stockpiles and sediment fences (Standard Drawing 6-8) 1 to 2 metres downslope.



Construction Notes

1. Scarify the ground surface along the line of the contour to a depth of 50 mm to 100 mm to break up any hardsetting surfaces and to provide a good bond between the respread material and subsoil.
2. Add soil ameliorants as required by the ESCP or SWMP.
3. Rip to a depth of 300 mm if compacted layers occur.
4. Where possible, replace topsoil to a depth of 40 to 60 mm on lands where the slope exceeds 4(H):1(V) and to at least 75 mm on lower gradients.



Construction Notes

1. Prohibit all traffic until the access way is constructed.
2. Strip any topsoil and place a needle-punched textile over the base of the crossing.
3. Place clean, rigid, non polluting aggregate or gravel in the 100 mm to 150 mm size class over the fabric to a minimum depth of 200 mm.
4. Provide a 3-metre wide carriageway with sufficient length of culvert pipe to allow less than a 3(H): 1 (V) slope on side batters.
5. Install a lower section to act as an emergency spillway in greater than design storm events.
6. Ensure that culvert outlets extend beyond the toe of fill embankments.

Insert staples through the blanket in a 150 mm x 150 mm trench with each pattern of three staples being about 500 mm apart

Backfill and compact dirt in the 150 mm x 150 mm trench after inserting staples through the material

As an alternative to trenching, when top of slope is relatively flat extend material about 1000 mm on top of the ground and randomly insert staples through the material about 600 mm apart

Staples must be inserted through overlap material

Maximum staple spacing as specified by the manufacturer

Blanket material must overlap at least 150 mm with staples inserted through both fabrics at a maximum spacing of 1000 mm

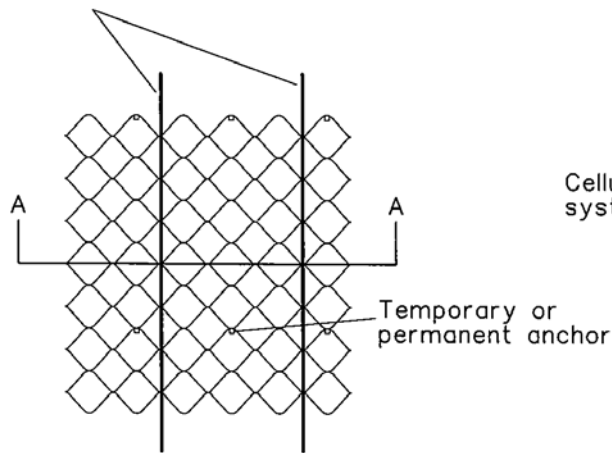
At end of slope, secure blanket material by inserting staples about 500 mm apart through the fabric

Blanket material must overlap at least 150 mm with staples inserted through both fabrics at a maximum spacing of 500 mm apart

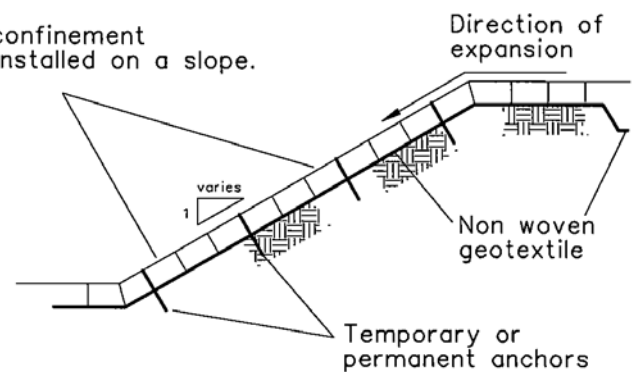
Construction Notes

1. Remove any rocks, clods, sticks or grass from the ground surface before laying the matting.
2. Spread topsoil to at least 75 mm depth.
3. Where appropriate, complete fertilising and seeding on a properly prepared seedbed (Standard Drawing 7-1) before laying the matting.
4. Ensure the fabric can be continuously in contact with the soil by grading the surface carefully first.
5. Lay the matting in "shingle-fashion" with the ends of each upstream roll overlapping the next roll downslope.
6. Ensure sufficient staples are used to maintain a good contact between the soil and the matting.

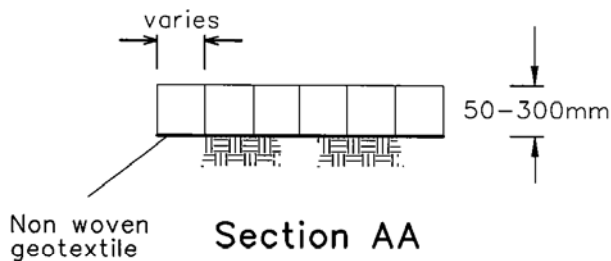
Anchor cables



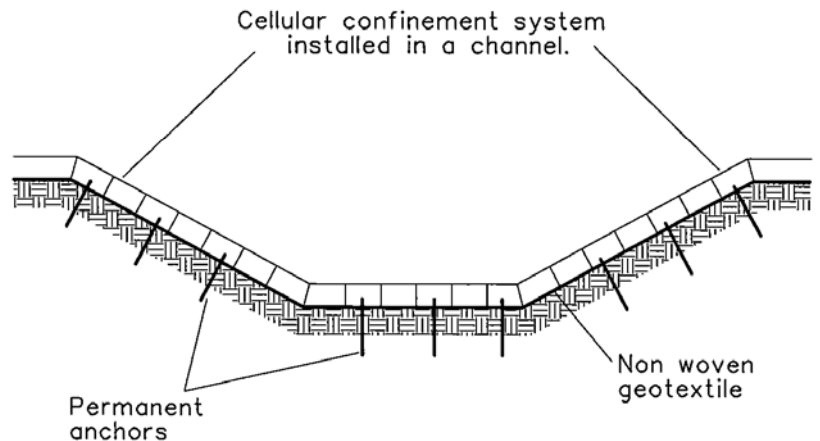
Cellular confinement system installed on a slope.



Slope Protection System



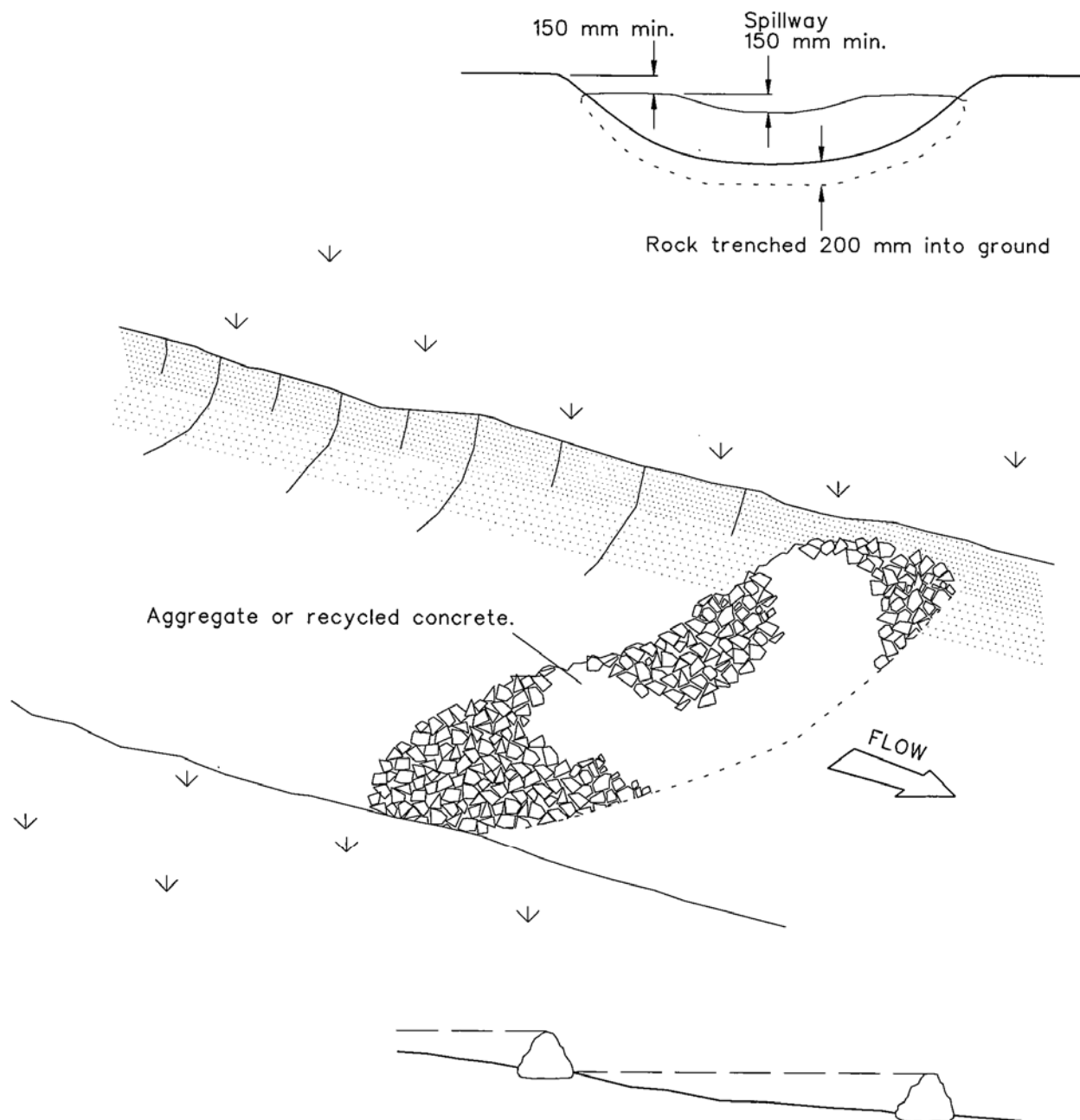
Cellular confinement system installed in a channel.



Channel Protection System

Construction Notes

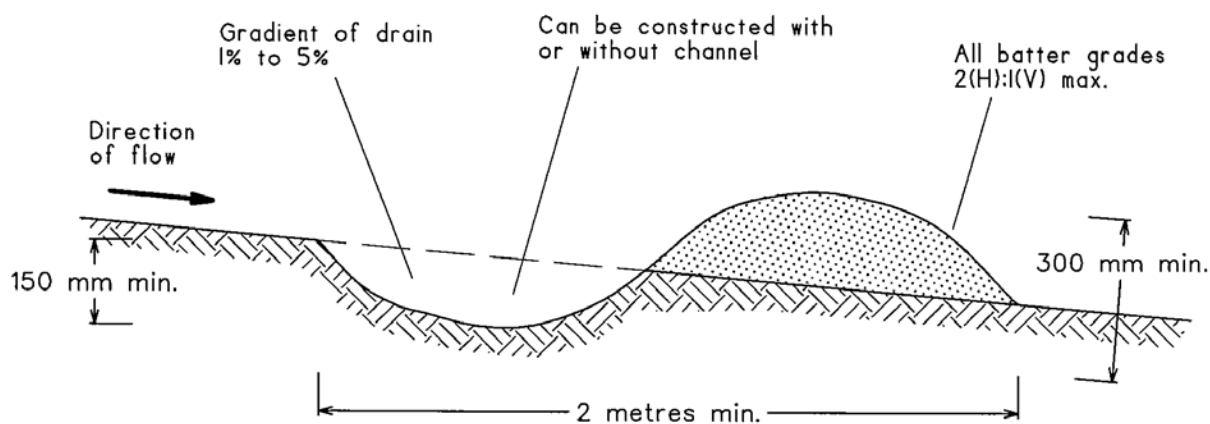
1. Undertake design only with the help of a suitably qualified geotechnical engineer.
2. Anchor systems on steep slopes to prevent sliding or movement under gravitational forces. This might include the use of high tensile, low creep cables made of polyester (not polypropylene), rope or steel wire.
3. Place thick, non woven geotextiles under the cellular confinement system to allow for lateral drainage.
4. Fill the cells with soil, rock or concrete depending on the application.



Spacing of check dams along centreline and scour protection below each check dam to be specified on SWMP/ESCP

Construction Notes

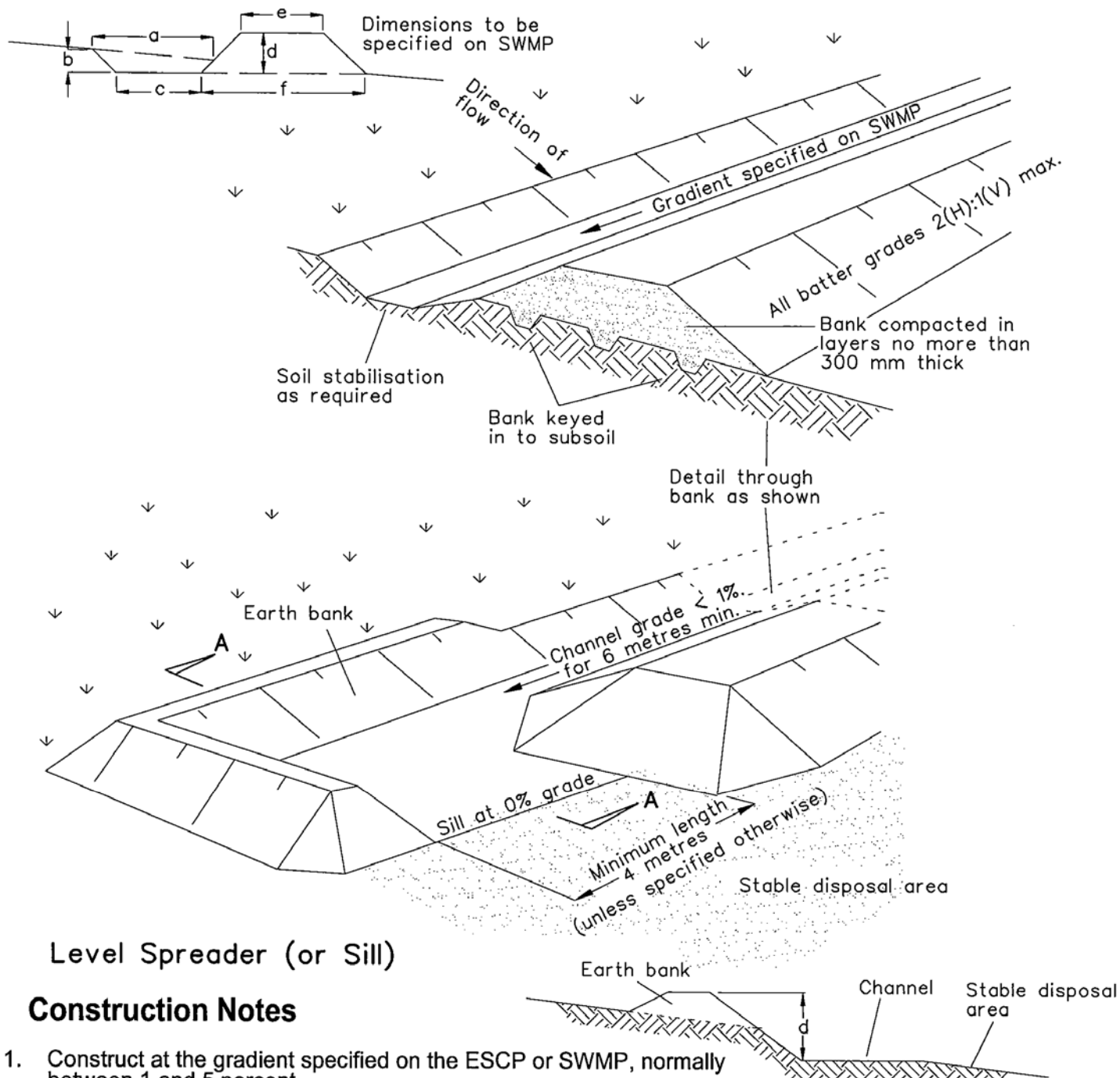
1. Check dams can be built with various materials, including rocks, logs, sandbags and straw bales. The maintenance program should ensure their integrity is retained, especially where constructed with straw bales. In the case of bales, this might require their replacement each two to four months.
2. Trench the check dam 200 mm into the ground across its whole width. Where rock is used, fill the trenches to at least 100 mm above the ground surface to reduce the risk of undercutting.
3. Normally, their maximum height should not exceed 600 mm above the gully floor. The centre should act as a spillway, being at least 150 mm lower than the outer edges.
4. Space the dams so the toe of the upstream dam is level with the spillway of the next downstream dam.



NOTE: Only to be used as temporary bank where maximum upslope length is 80 metres.

Construction Notes

1. Build with gradients between 1 percent and 5 percent.
2. Avoid removing trees and shrubs if possible - work around them.
3. Ensure the structures are free of projections or other irregularities that could impede water flow.
4. Build the drains with circular, parabolic or trapezoidal cross sections, not V shaped.
5. Ensure the banks are properly compacted to prevent failure.
6. Complete permanent or temporary stabilisation within 10 days of construction.

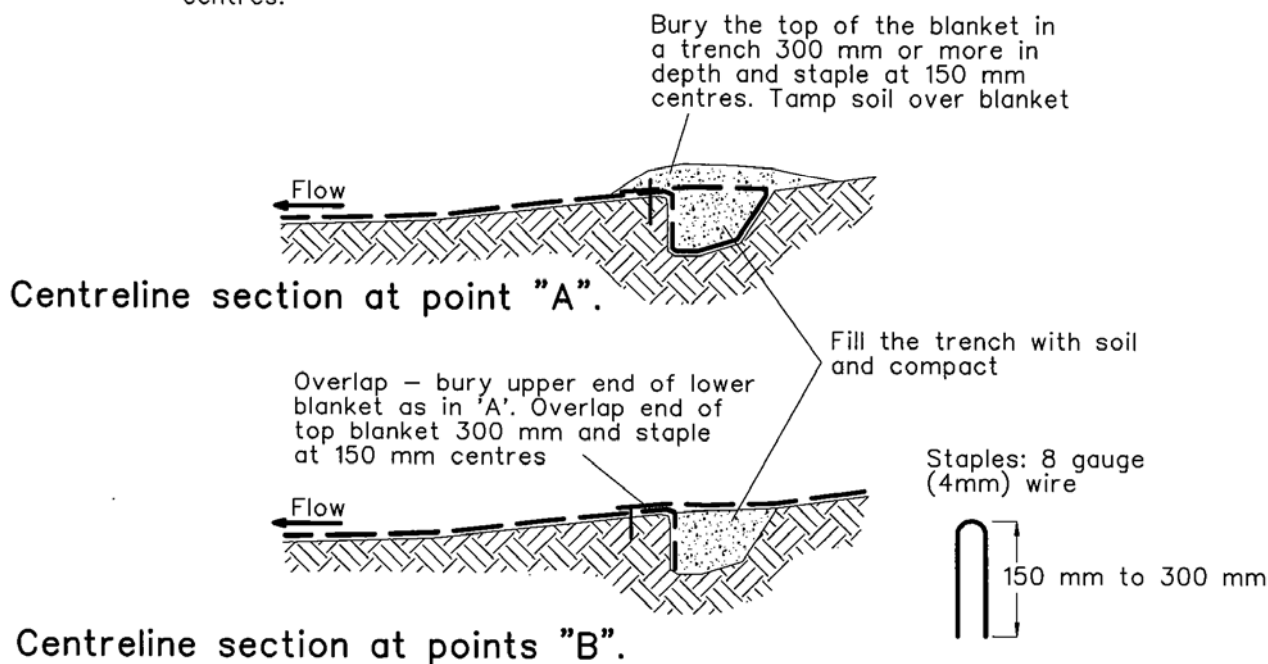
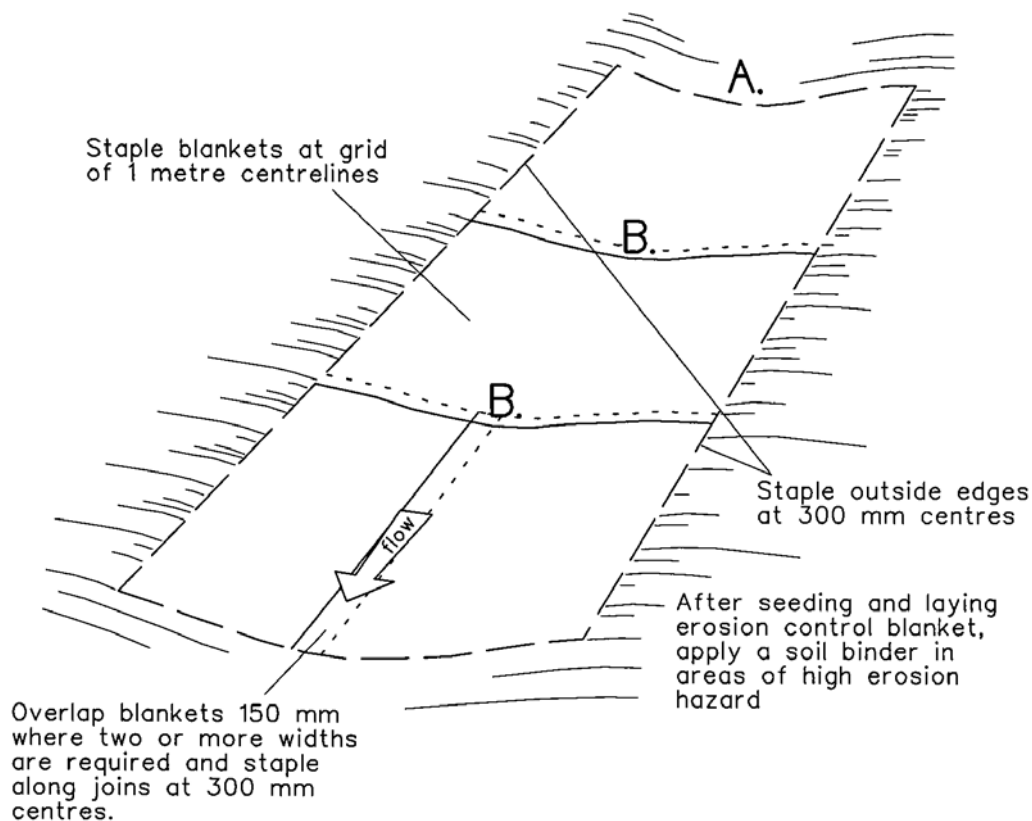


Level Spreader (or Sill)

Construction Notes

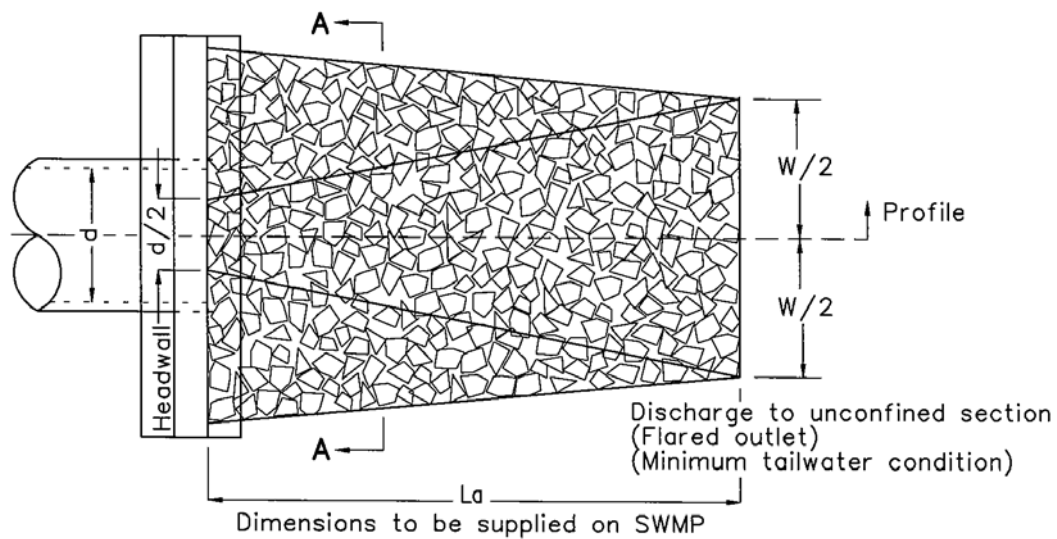
1. Construct at the gradient specified on the ESCP or SWMP, normally between 1 and 5 percent
2. Avoid removing trees and shrubs if possible - work around them.
3. Ensure the structures are free of projections or other irregularities that could impede water flow.
4. Build the drains with circular, parabolic or trapezoidal cross sections, not V-shaped, at the dimensions shown on the SWMP.
5. Ensure the banks are properly compacted to prevent failure.
6. Complete permanent or temporary stabilisation within 10 days of construction following Table 5.2 in Landcom (2004).
7. Where discharging to erodible lands, ensure they outlet through a properly constructed level spreader.
8. Construct the level spreader at the gradient specified on the ESCP or SWMP, normally less than 1 percent or level.
9. Where possible, ensure they discharge waters onto either stabilised or undisturbed disposal sites within the same subcatchment area from which the water originated. Approval might be required to discharge into other subcatchments.

Section AA

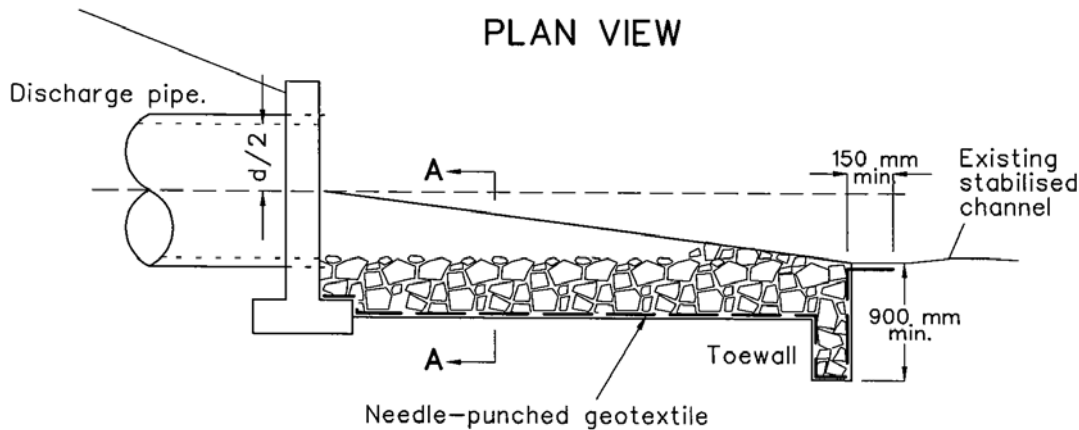


Construction Notes

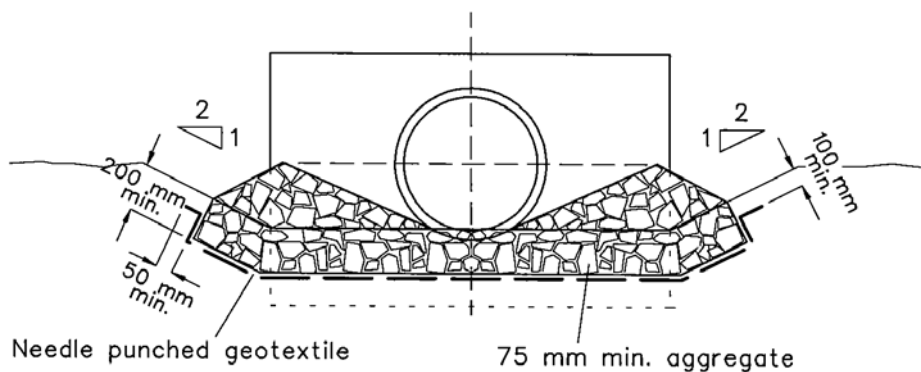
1. Remove any rocks, clods, sticks or grass from the surface before laying matting
2. Ensure that topsoil is at least 75 mm deep.
3. Complete fertilising and seeding before laying the matting.
4. Ensure fabric will be continuously in contact with the soil by grading the surface carefully first.
5. Lay the fabric in "shingle-fashion", with the end of each upstream roll overlapping those downstream. Ensure each roll is anchored properly at its upslope end (Standard Drawing 5-7b).
6. Ensure that the full width of flow in the channel is covered by the matting up to the design storm event, usually in the 10-year ARI time of concentration storm event.
7. Divert water from the structure until vegetation is stabilised properly.



PLAN VIEW



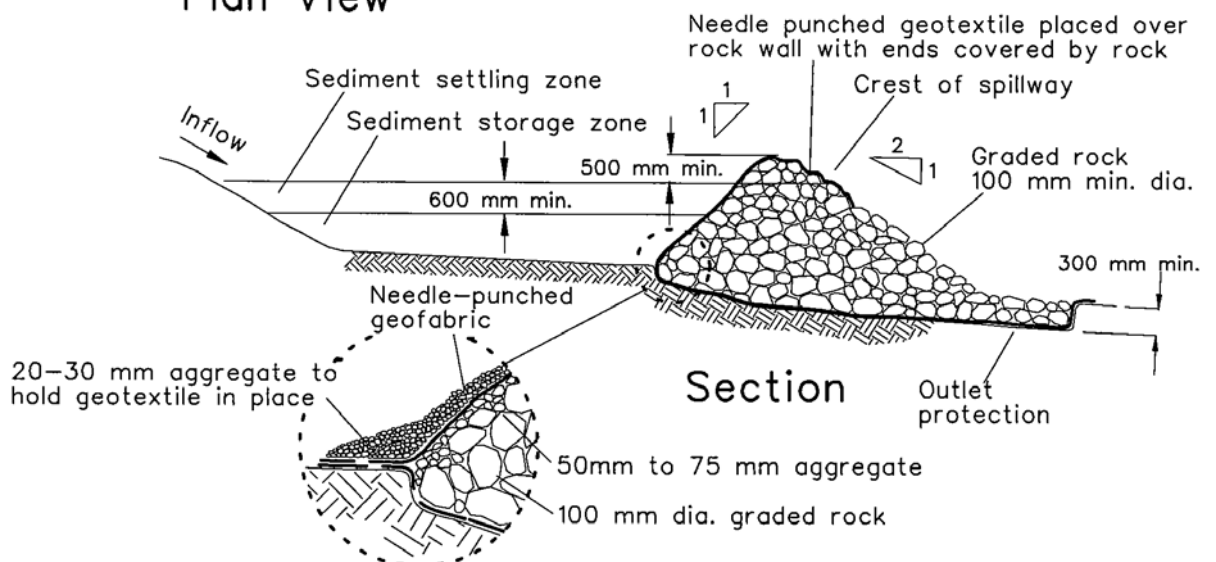
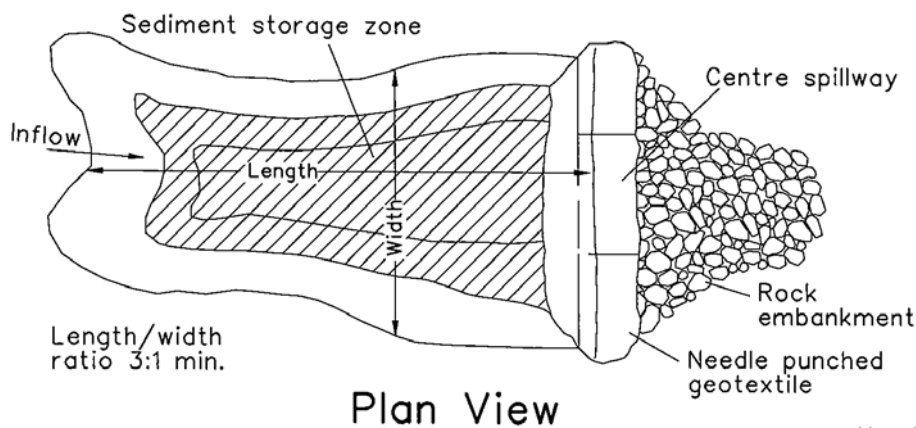
PLAN VIEW



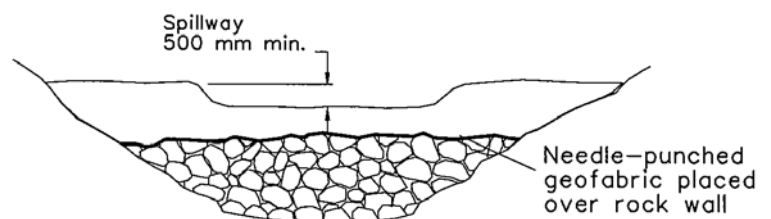
CROSS SECTION AA

Construction Notes

1. Compact the subgrade fill to the density of the surrounding undisturbed material.
2. Prepare a smooth, even foundation for the structure that will ensure that the needle-punched geotextile does not sustain serious damage when covered with rock.
3. Should any minor damage to the geotextile occur, repair it before spreading any aggregate. For repairs, patch one piece of fabric over the damage, making sure that all joints and patches overlap more than 300 mm.
4. Lay rock following the drawing, according to Table 5.2 of Landcom (2004) and with a minimum diameter of 75 mm.
5. Ensure that any concrete or riprap used for the energy dissipater or the outlet protection conforms to the grading limits specified on the SWMP.



NOTE:
Spillway width and depth, wall crest width and downstream outlet protection measures to be specified on SWMP.



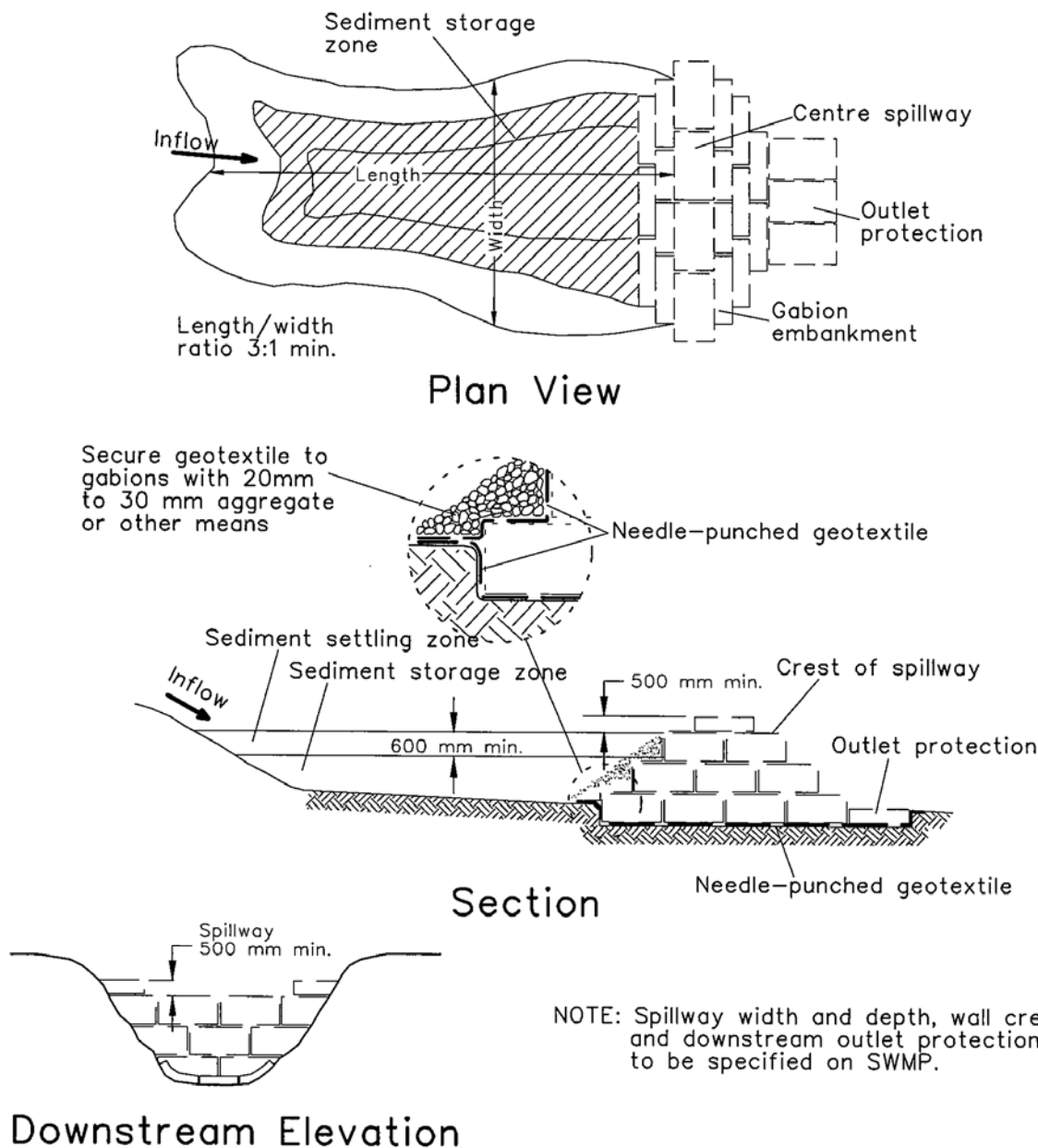
Construction Notes

1. Remove all vegetation and topsoil from under the dam wall and from within the storage area.
2. Excavate to 300 mm depth for base of the dam wall.
3. Line the excavation with a needle-punched geotextile allowing sufficient to line below the wall, and over the upstream rock and the spillway to 500 mm below the spillway exit on the downstream face.
4. Make up the wall profile and outlet protection with 100 mm (min.) diameter graded rock. Spread a layer of 50 mm to 75 mm diameter aggregate over the upstream batter for a more even surface, and add 100 mm to 150 mm of 20 mm to 30 mm gravel over the 50 mm to 75 mm diameter aggregate.
5. Lay geotextile over the upstream batter and through the spillway, fixing in place with 100 mm rock.
6. Place a "Full of Sediment" marker to show when less than design capacity occurs and sediment removal is required.
7. Replace the upstream geotextile layer each time sediment is removed

ROCK SEDIMENT BASIN

(APPLIES TO 'TYPE C' SOILS ONLY)

SD 6-1



Construction Notes

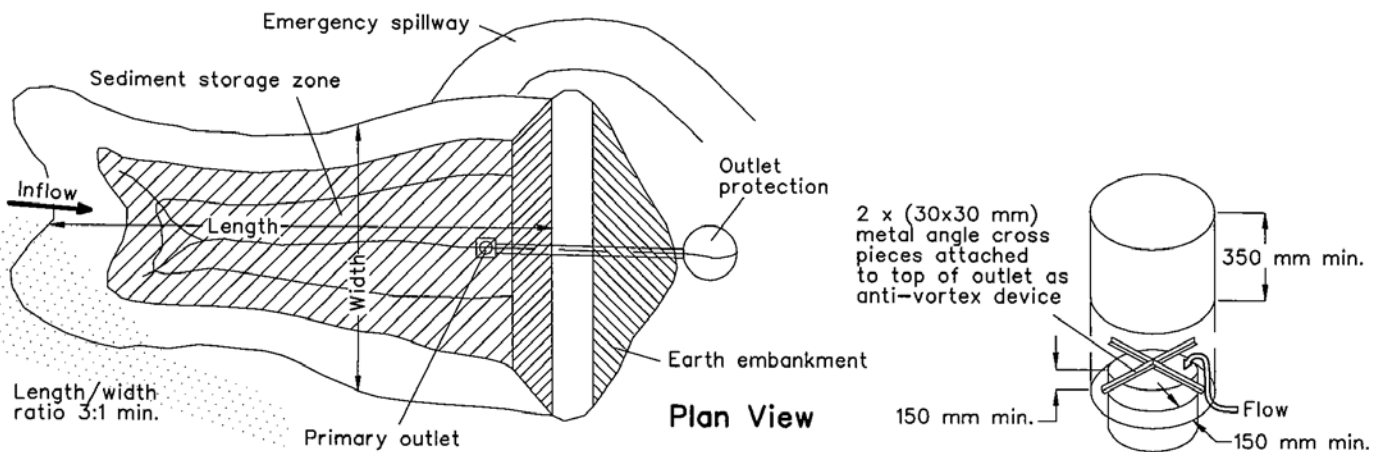
(Applies to Type C soils only)

1. Remove all vegetation and topsoil from under the dam wall and from within the storage area.
2. Excavate to 300 mm depth for the base of the dam wall and form a level platform for the gabions.
3. Line the excavation with a needle-punched geotextile allowing sufficient to line below the wall, and over the upstream gabions and spillway to 500 mm below the spillway exit on the downstream face.
4. Make up the wall profile and outlet protection with gabion units filled with graded rock as specified on the SWMP.
5. Construct a spillway 500 mm below the crest of the dam and for the width specified on the SWMP.
6. Lap the geotextile over the upstream face and through the spillway and fix it in place with the top row of gabions.
7. Cover the upstream face of the wall with 20 mm to 30 mm gravel and geotextile (Standard Drawing 6-2b)
8. Place a "Full of Sediment" marker to show when less than design capacity occurs and sediment removal is required.
9. Replace the upstream geotextile layer when sediment is removed if a dry basin is required.

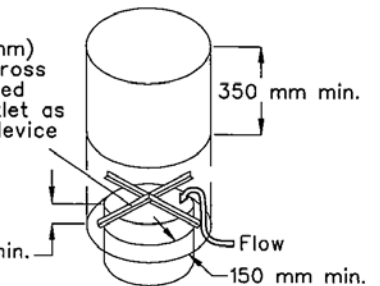
GABION SEDIMENT BASIN

(APPLIES TO 'TYPE C' SOILS ONLY)

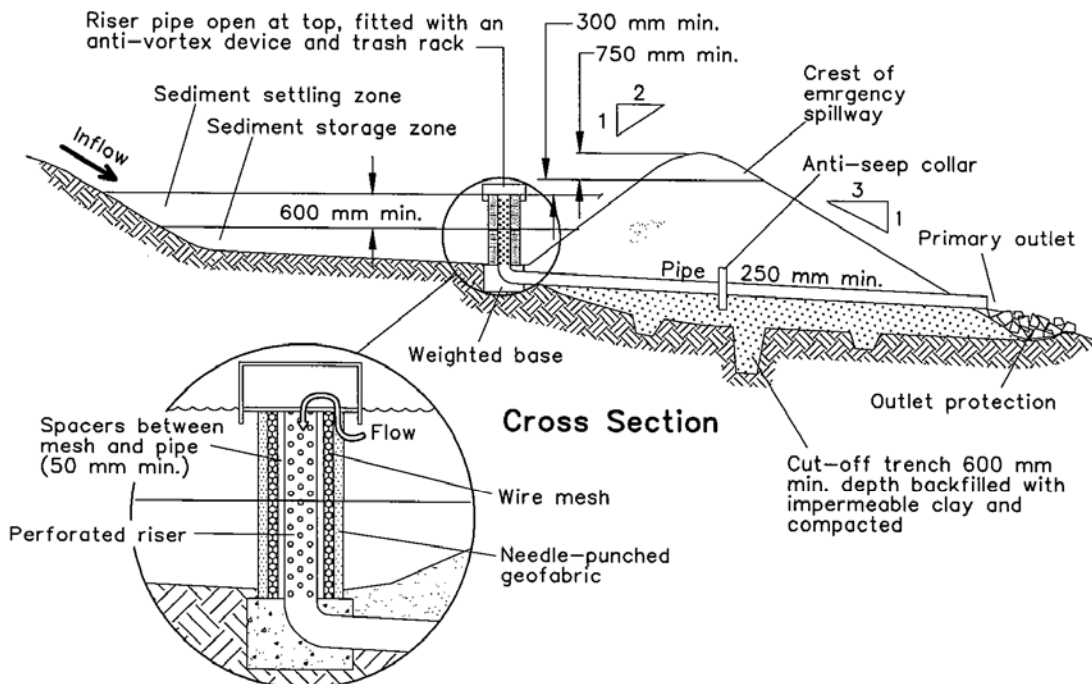
SD 6-2



2 x (30x30 mm) metal angle cross pieces attached to top of outlet as anti-vortex device

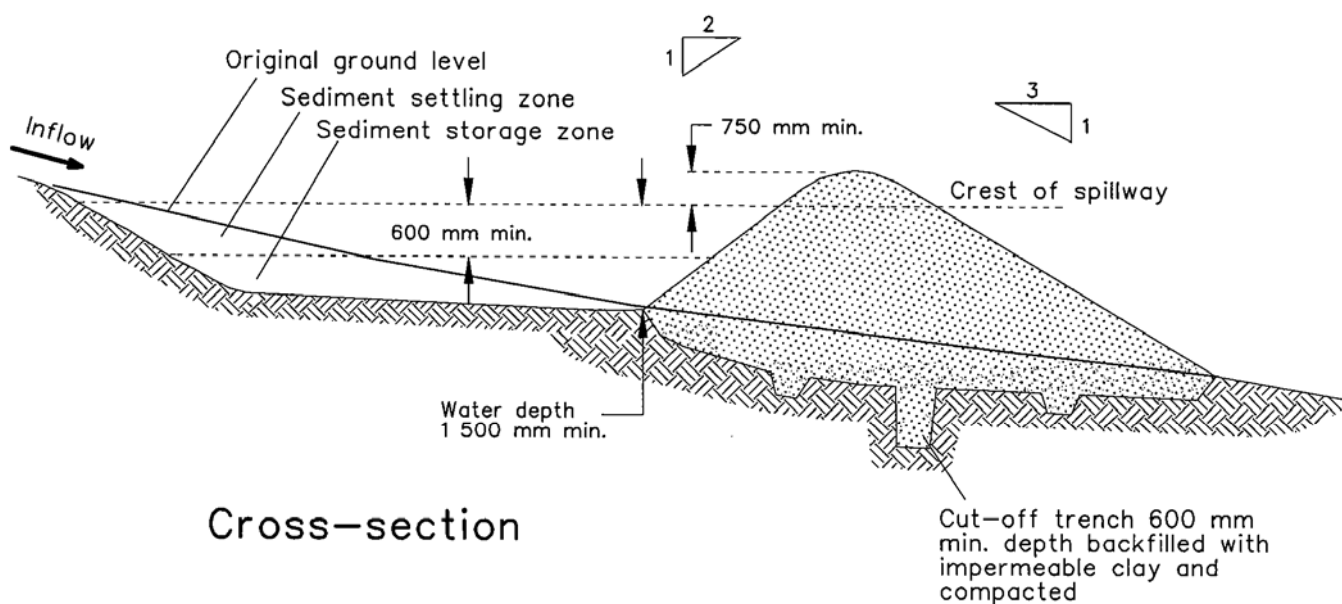
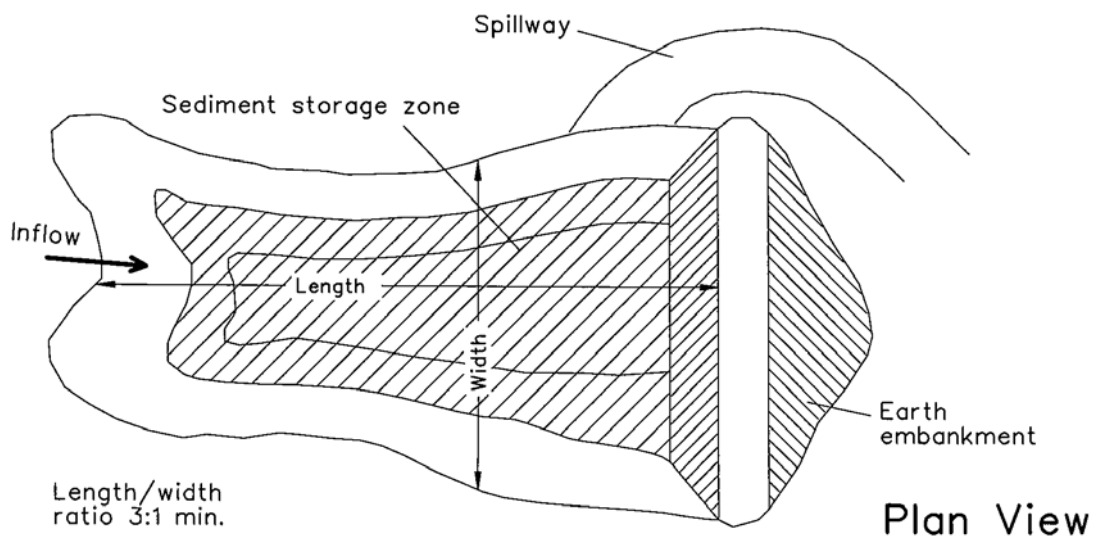


**Trash Rack/
Anti-vortex Device**



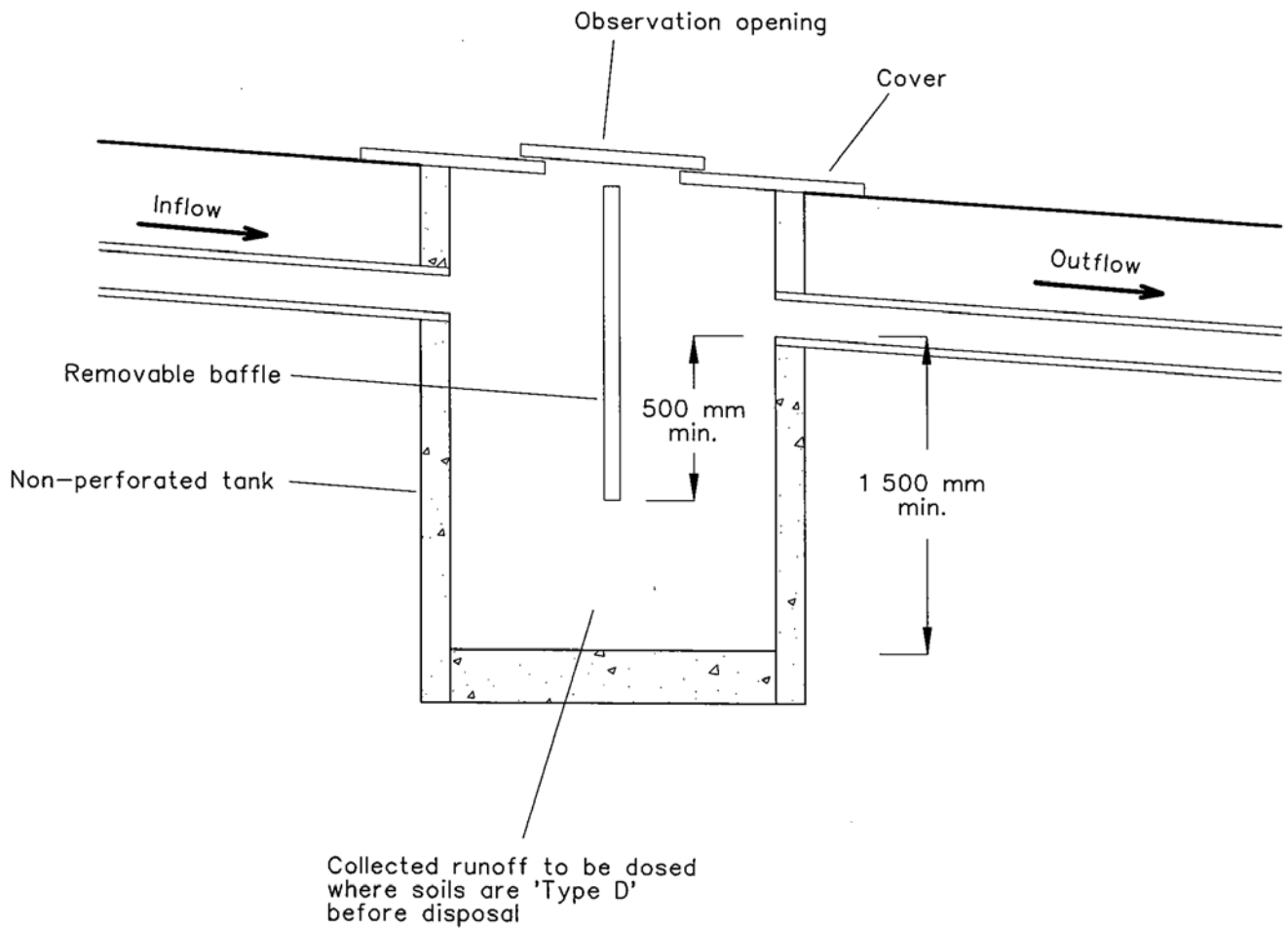
Construction Notes

1. Remove all vegetation and topsoil from under the dam wall and from within the storage area.
2. Form a cut off trench under the centreline of the embankment 600 mm deep and 1,200 mm wide, extending to a point on the watercourse wall above the riser sill level.
3. Maintain the trench free of water and recompact the materials with equipment as specified in the SWMP to 95 per cent Standard Proctor Density.
4. Select fill according to the SWMP that is free from roots, wood, rock, large stone or foreign material.
5. Prepare the site under the embankment by ripping to at least 100 mm to help bond the compacted fill to the existing substrate.
6. Spread the fill in 100 mm to 150 mm layers and compact it at optimum moisture content following the SWMP.
7. Install the pipe outlet with seepage collars as specified in the SWMP and Standard Drawing 6-3b.
8. Form batter grades at 2(H):1(V) upstream and 3(H):1(V) downstream or as specified in the SWMP



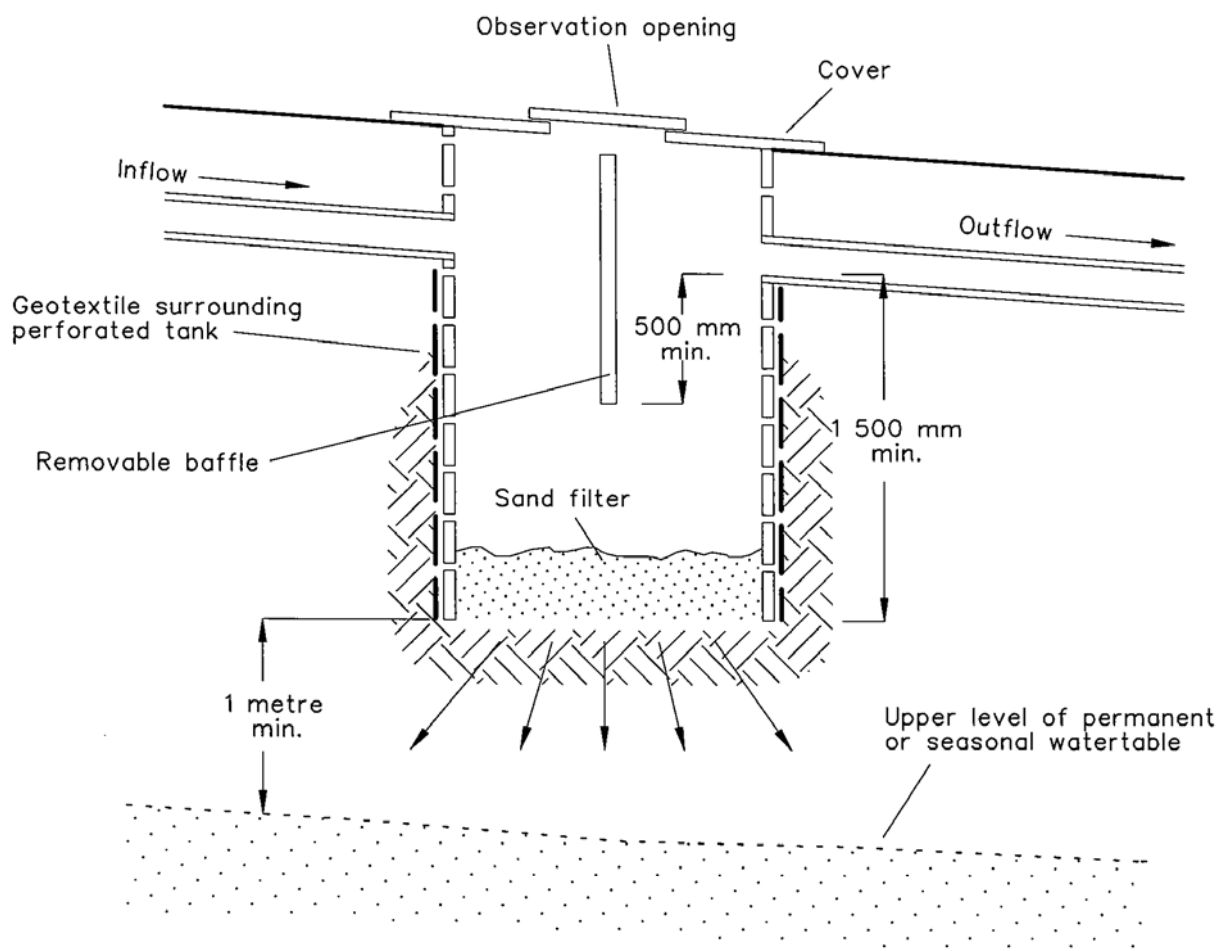
Construction Notes

1. Remove all vegetation and topsoil from under the dam wall and from within the storage area.
2. Construct a cut-off trench 500 mm deep and 1,200 mm wide along the centreline of the embankment extending to a point on the gully wall level with the riser crest.
3. Maintain the trench free of water and recompact the materials with equipment as specified in the SWMP to 95 per cent Standard Proctor Density.
4. Select fill following the SWMP that is free of roots, wood, rock, large stone or foreign material.
5. Prepare the site under the embankment by ripping to at least 100 mm to help bond compacted fill to the existing substrate.
6. Spread the fill in 100 mm to 150 mm layers and compact it at optimum moisture content following the SWMP.
7. Construct the emergency spillway.
8. Rehabilitate the structure following the SWMP.



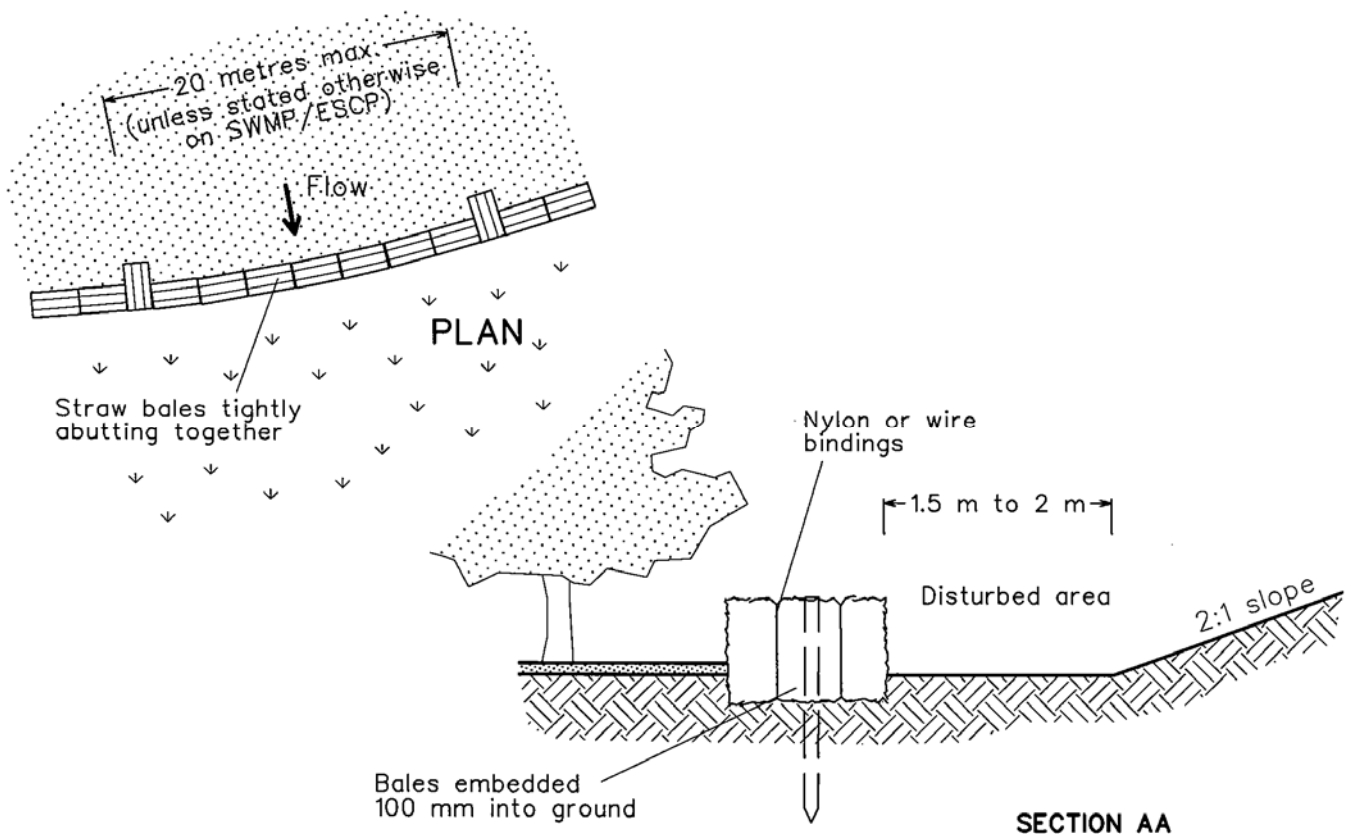
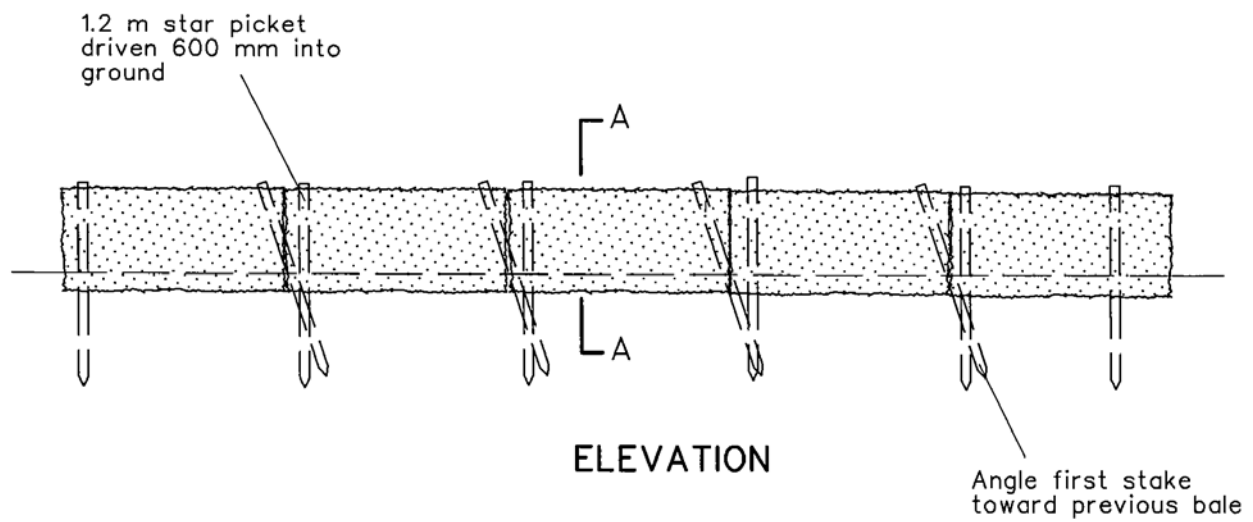
Construction Notes

1. Join the inlet to the stormwater, taking any suitable steps to remove bulky or coarse material before it can enter the tank.
2. Connect the outlet to a safe disposal area following the SWMP.
3. Install a removable baffle, central to the inflow/outflow and normal to the direction of flow, ensuring that it reaches 500 mm below the invert of the outlet pipe.
4. Install a cover over the pit with an observation port and access cover.



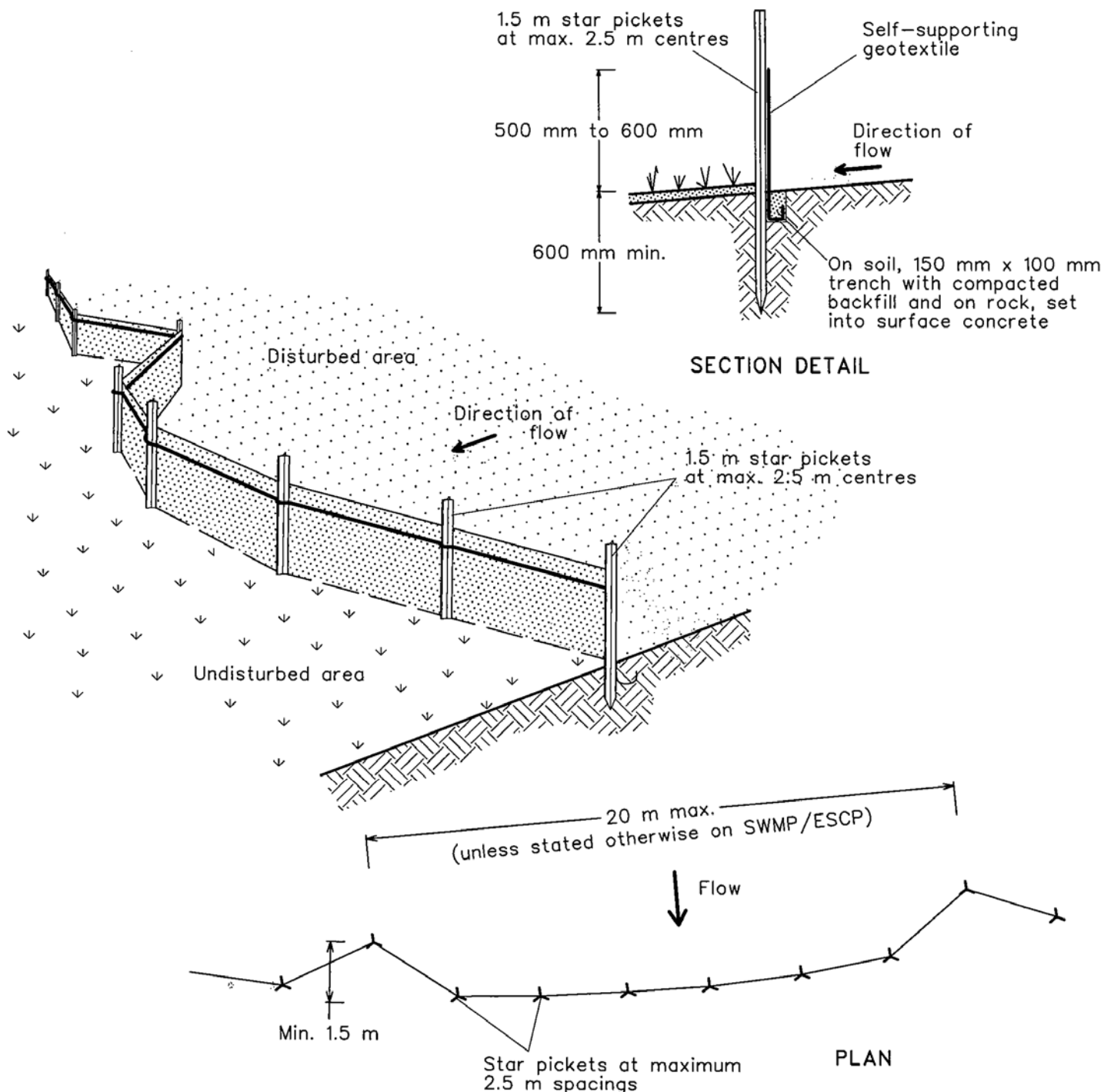
Construction Notes

1. Join the inlet to the polluted supply taking any suitable step to remove bulky material before it can enter the sump.
2. Connect the outlet to a safe disposal area following the ESCP/SWMP.
3. Place a geotextile liner on the outside of the pit.
4. Install a removable baffle, central to the inflow/outflow and normal to the direction of flow, ensuring that it reaches 500 mm below the invert of the outlet pipe.
5. Install a cover over the pit with an observation port and access cover.



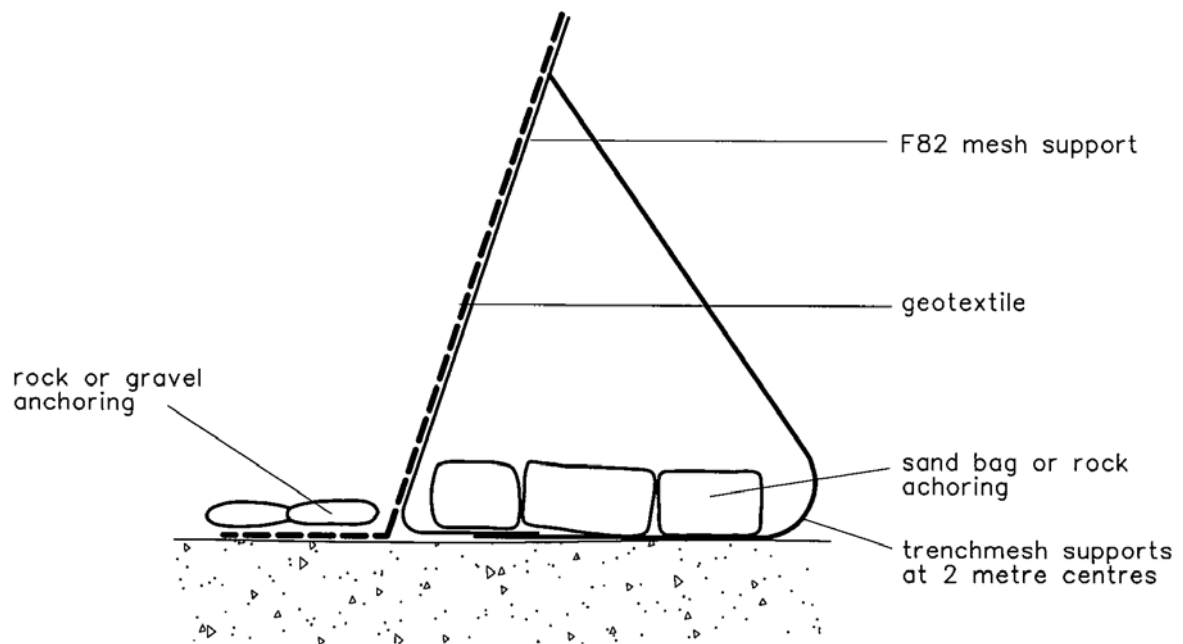
Construction Notes

1. Construct the straw bale filter as close as possible to being parallel to the contours of the site.
2. Place bales lengthwise in a row with ends tightly abutting. Use straw to fill any gaps between bales. Straws are to be placed parallel to ground.
3. Ensure that the maximum height of the filter is one bale.
4. Embed each bale in the ground 75 mm to 100 mm and anchor with two 1.2 metre star pickets or stakes. Angle the first star picket or stake in each bale towards the previously laid bale. Drive them 600 mm into the ground and, if possible, flush with the top of the bales. Where star pickets are used and they protrude above the bales, ensure they are fitted with safety caps.
5. Where a straw bale filter is constructed downslope from a disturbed batter, ensure the bales are placed 1 to 2 metres downslope from the toe.
6. Establish a maintenance program that ensures the integrity of the bales is retained - they could require replacement each two to four months.



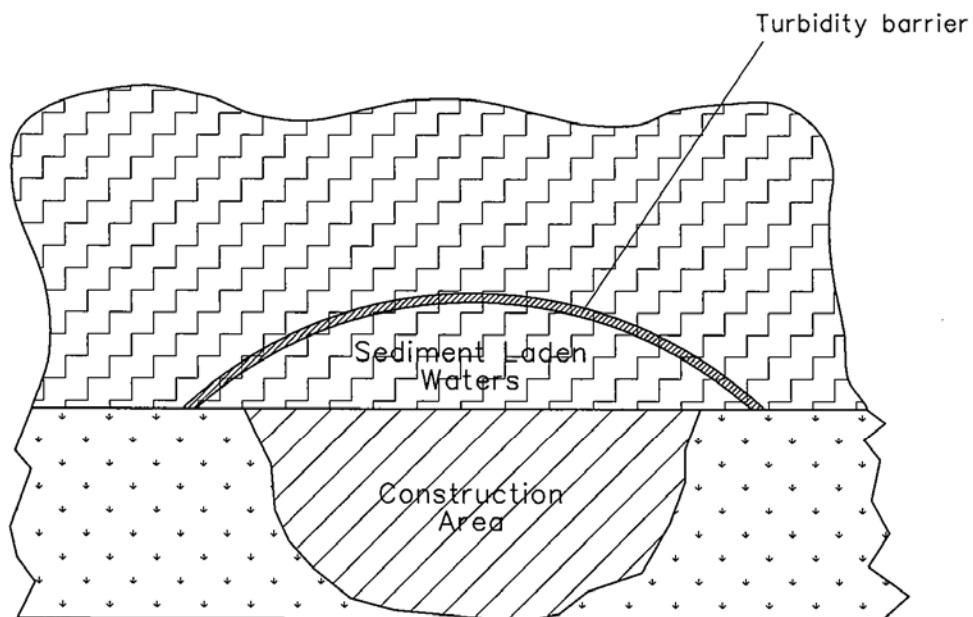
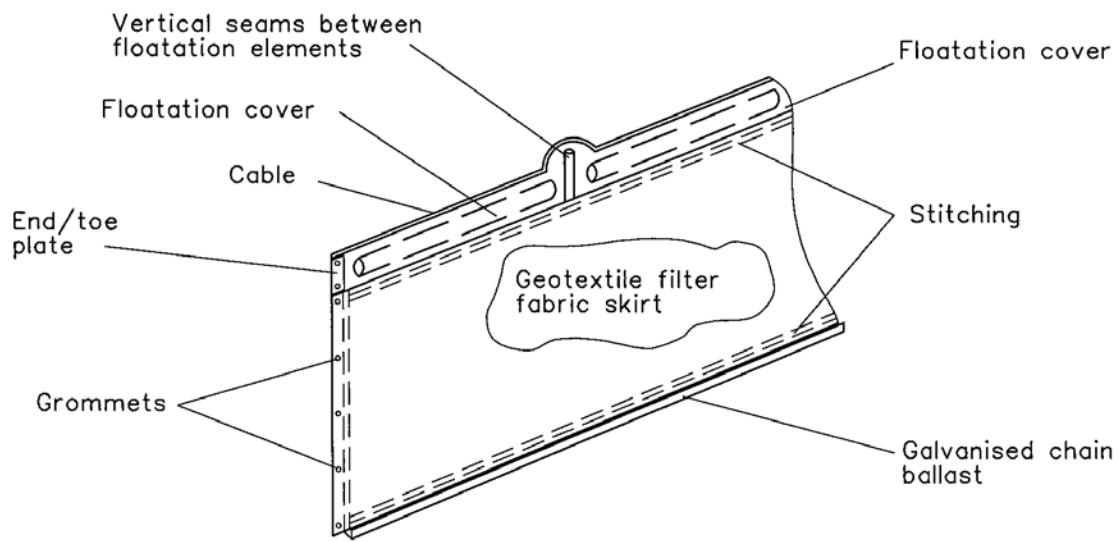
Construction Notes

1. Construct sediment fences as close as possible to being parallel to the contours of the site, but with small returns as shown in the drawing to limit the catchment area of any one section. The catchment area should be small enough to limit water flow if concentrated at one point to 50 litres per second in the design storm event, usually the 10-year event.
2. Cut a 150-mm deep trench along the upslope line of the fence for the bottom of the fabric to be entrenched.
3. Drive 1.5 metre long star pickets into ground at 2.5 metre intervals (max) at the downslope edge of the trench. Ensure any star pickets are fitted with safety caps.
4. Fix self-supporting geotextile to the upslope side of the posts ensuring it goes to the base of the trench. Fix the geotextile with wire ties or as recommended by the manufacturer. Only use geotextile specifically produced for sediment fencing. The use of shade cloth for this purpose is not satisfactory.
5. Join sections of fabric at a support post with a 150-mm overlap.
6. Backfill the trench over the base of the fabric and compact it thoroughly over the geotextile.



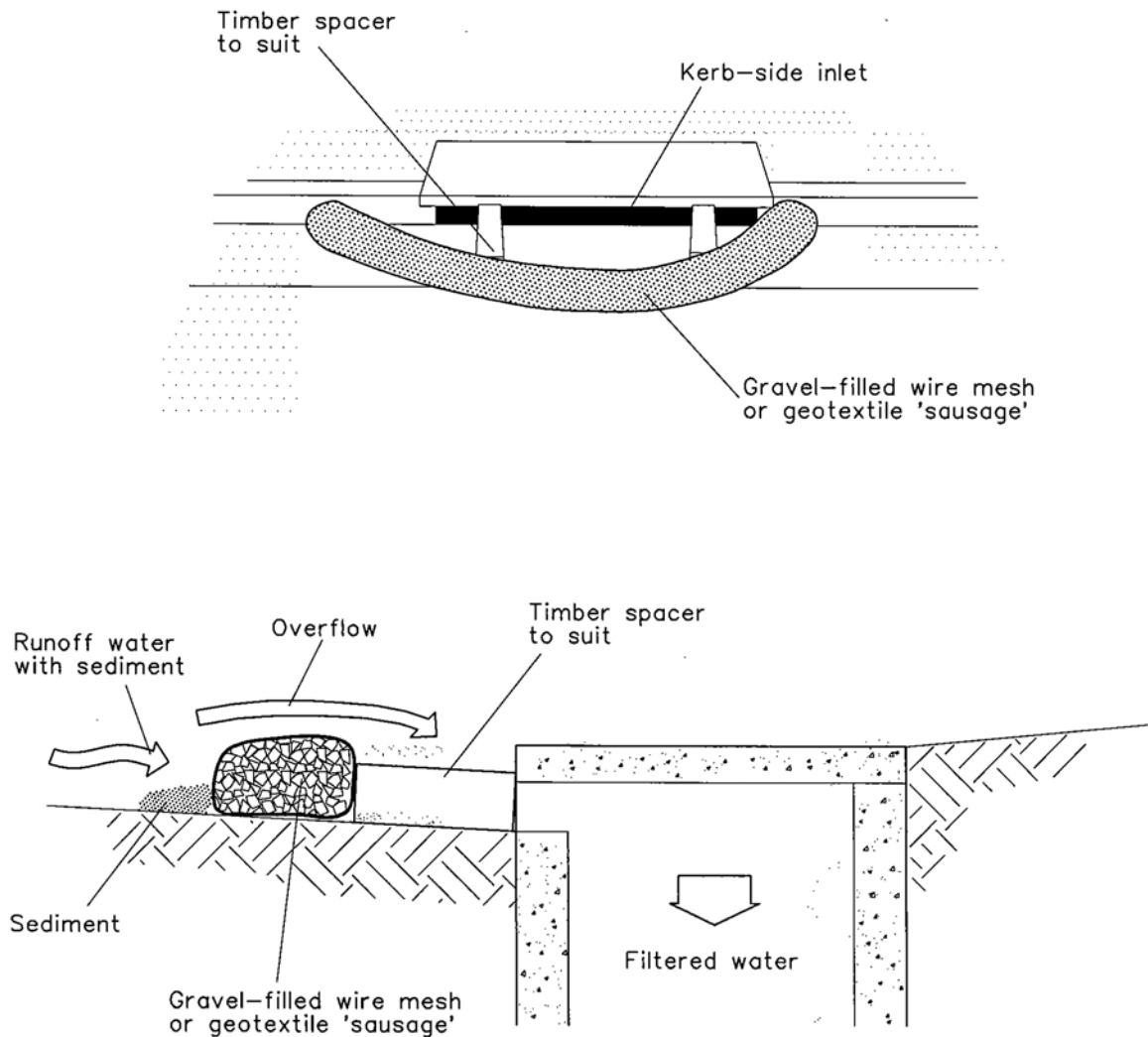
Construction Notes

1. Install this type of sediment fence when use of support posts is not desirable or not possible. Such conditions might apply, for example, where approval is granted from the appropriate authorities to place these fences in highly sensitive estuarine areas.
2. Use bent trench mesh to support the F82 welded mesh facing as shown on the drawing above. Attach the geotextile to the welded mesh facing using UV resistant cable ties.
3. Stabilise the whole structure with sandbag or rock anchoring over the trench mesh and the leading edge of the geotextile. The anchoring should be sufficiently large to ensure stability of the structure in the design storm event, usually the 10 year event.



Construction Notes

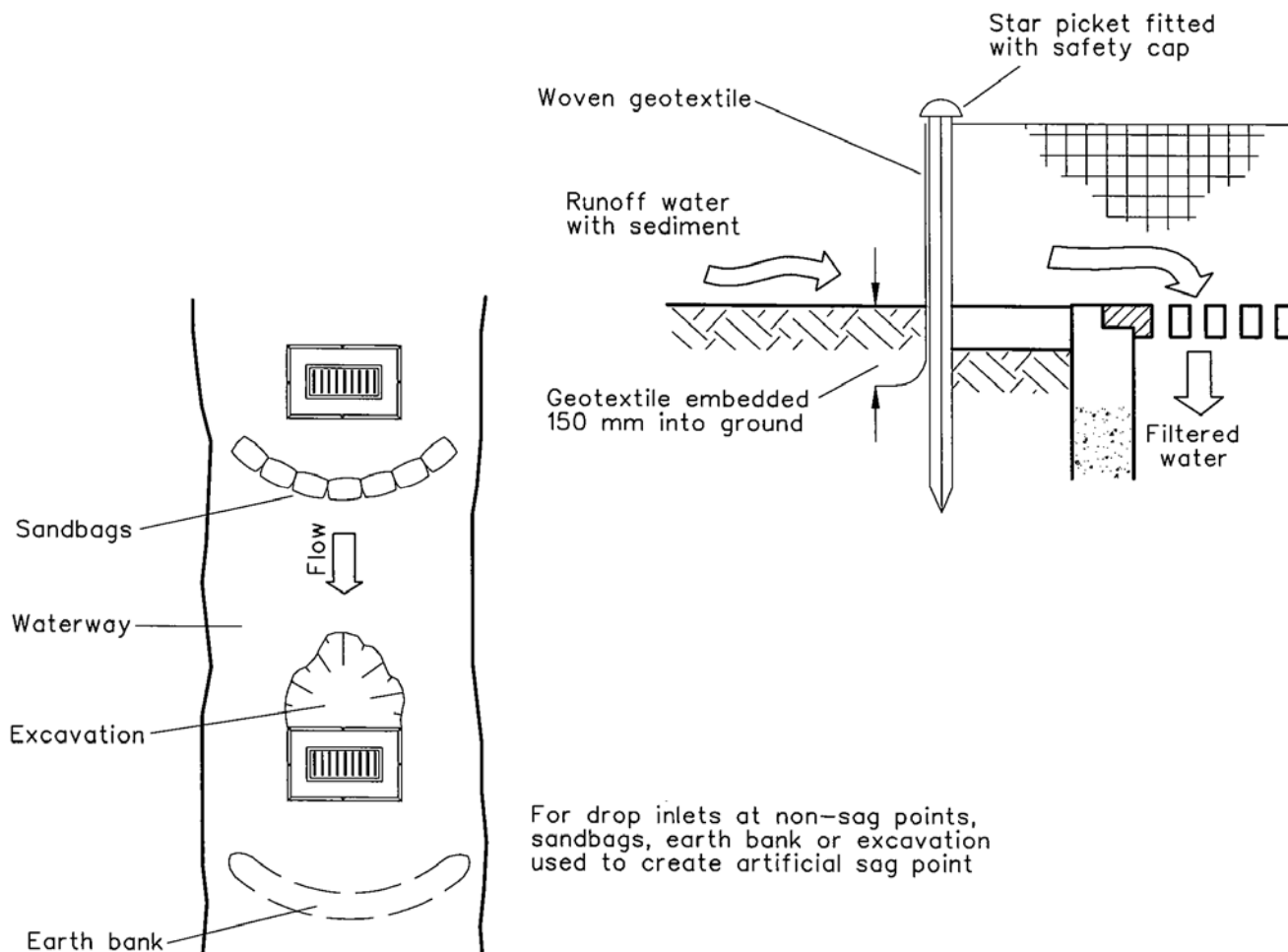
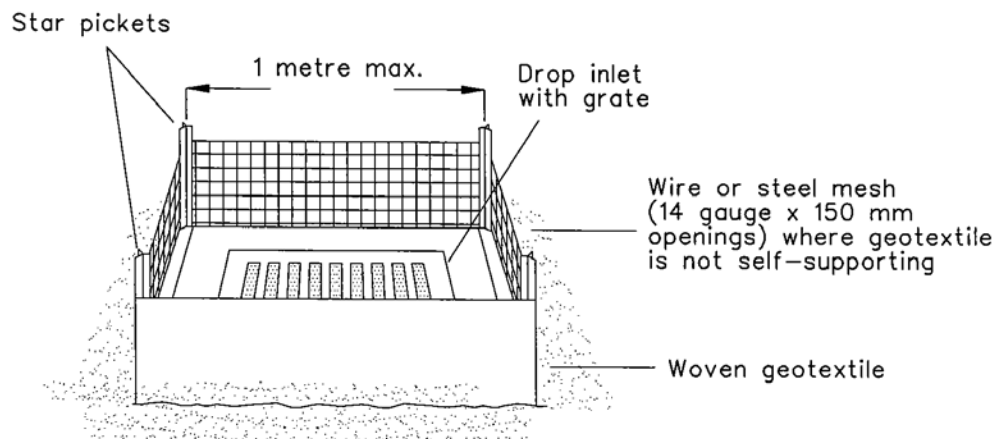
1. Use turbidity barriers only where high flows are unlikely to remove accumulated sediment and/or move the curtain significantly.
2. Where the barrier is to remain in place for more than one month, ensure the floatation cover is a UV-resistant, durable material.
3. Use only closed cell foam or foam-filled PVC piping as floatation elements. Do not use unfilled pipes.
4. Use only woven or heat-set non woven geotextiles. Needle-punched, non woven geotextiles can become fouled with debris that fray and delaminate them as they move with the waves or currents.
5. Remove captured sediment before the barrier is decommissioned.
6. In tidal areas, ensure the barrier can rise and fall without being moved from its position.



NOTE: This practice only to be used where specified in an approved SWMP/ESCP.

Construction Notes

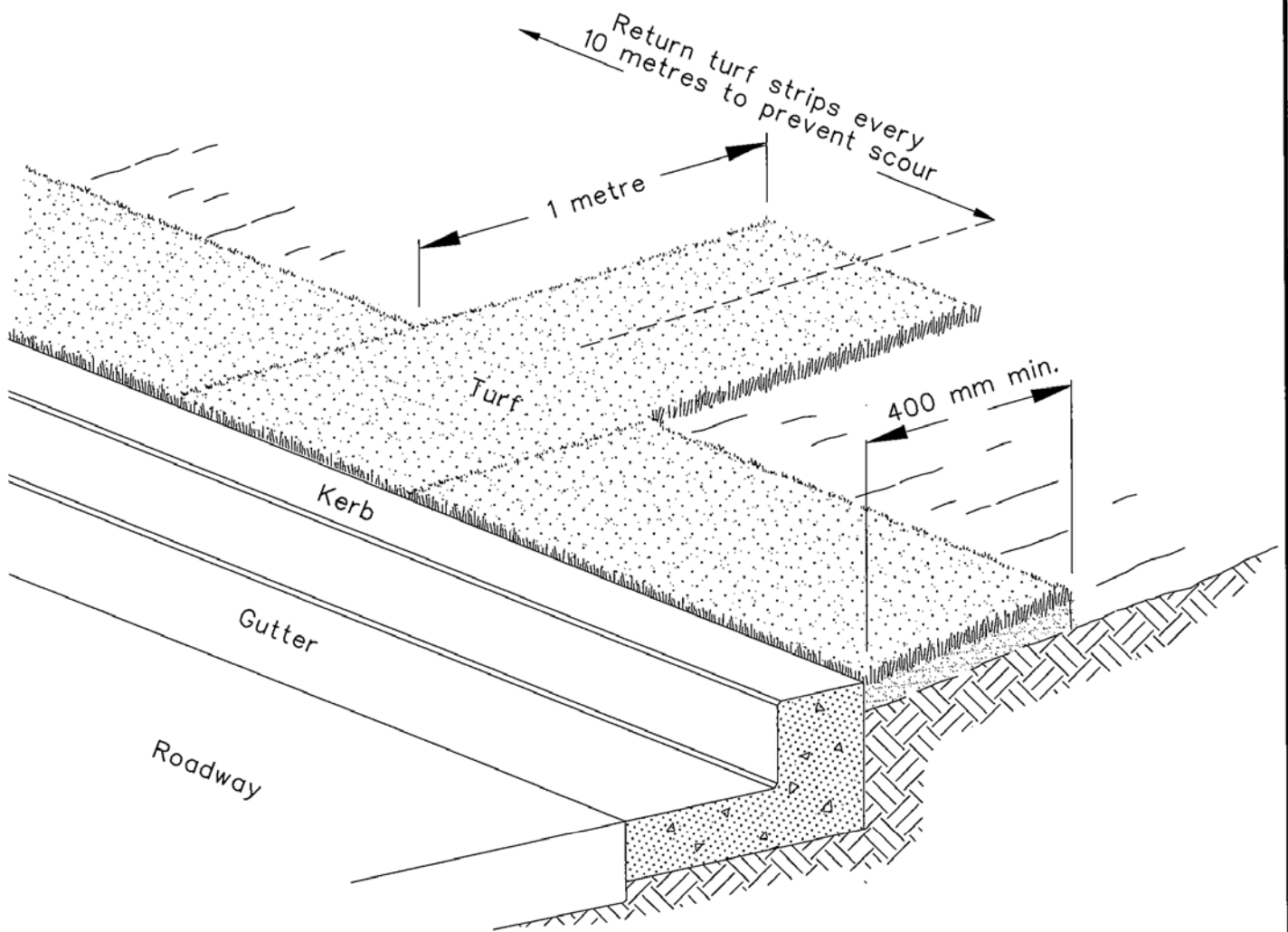
1. Install filters to kerb inlets only at sag points.
2. Fabricate a sleeve made from geotextile or wire mesh longer than the length of the inlet pit and fill it with 25 mm to 50 mm gravel.
3. Form an elliptical cross-section about 150 mm high x 400 mm wide.
4. Place the filter at the opening leaving at least a 100-mm space between it and the kerb inlet. Maintain the opening with spacer blocks.
5. Form a seal with the kerb to prevent sediment bypassing the filter.
6. Sandbags filled with gravel can substitute for the mesh or geotextile providing they are placed so that they firmly abut each other and sediment-laden waters cannot pass between.



For drop inlets at non-sag points, sandbags, earth bank or excavation used to create artificial sag point

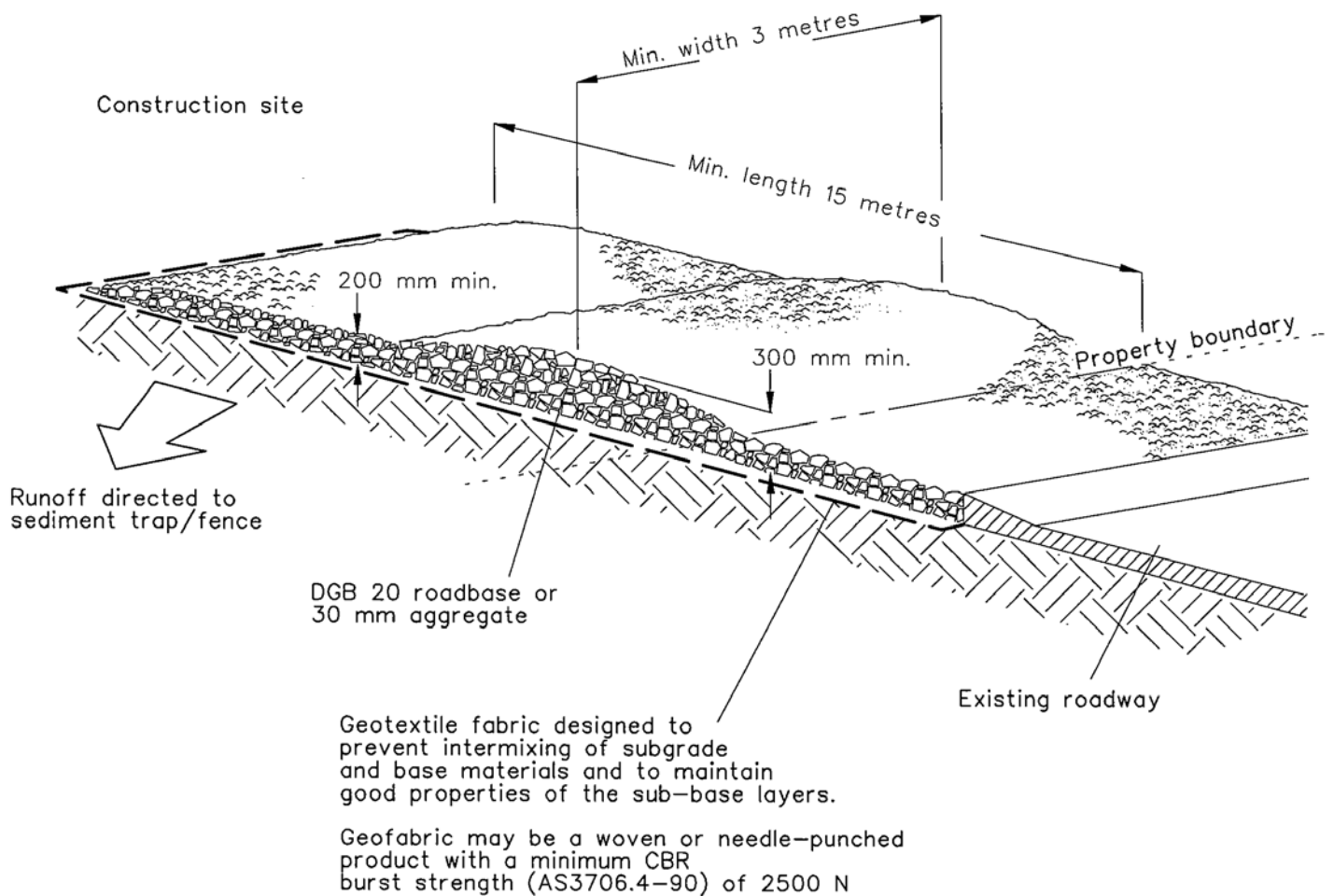
Construction Notes

1. Fabricate a sediment barrier made from geotextile or straw bales.
2. Follow Standard Drawing 6-7 and Standard Drawing 6-8 for installation procedures for the straw bales or geofabric. Reduce the picket spacing to 1 metre centres.
3. In waterways, artificial sag points can be created with sandbags or earth banks as shown in the drawing.
4. Do not cover the inlet with geotextile unless the design is adequate to allow for all waters to bypass it.



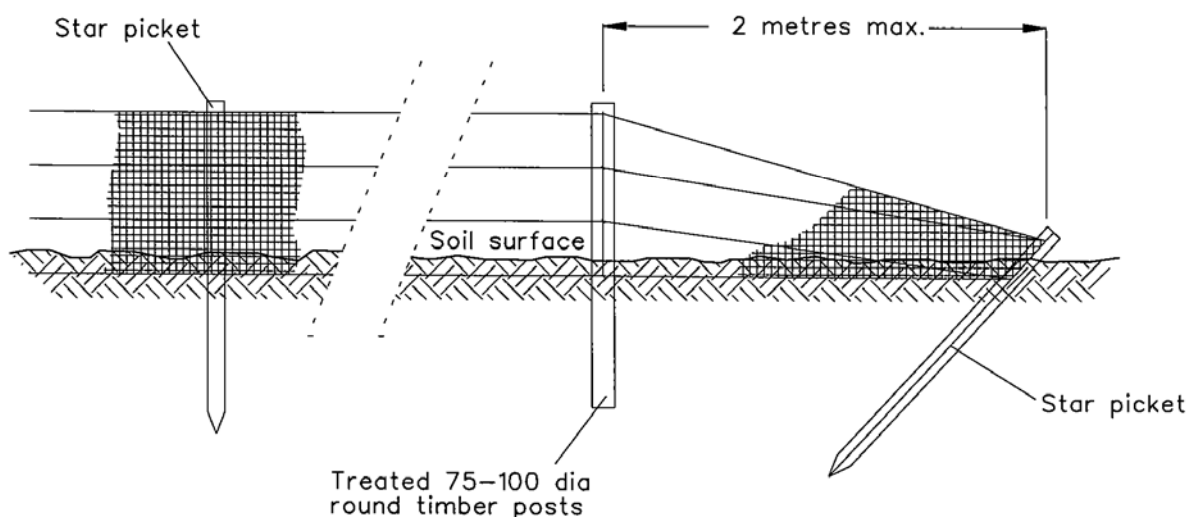
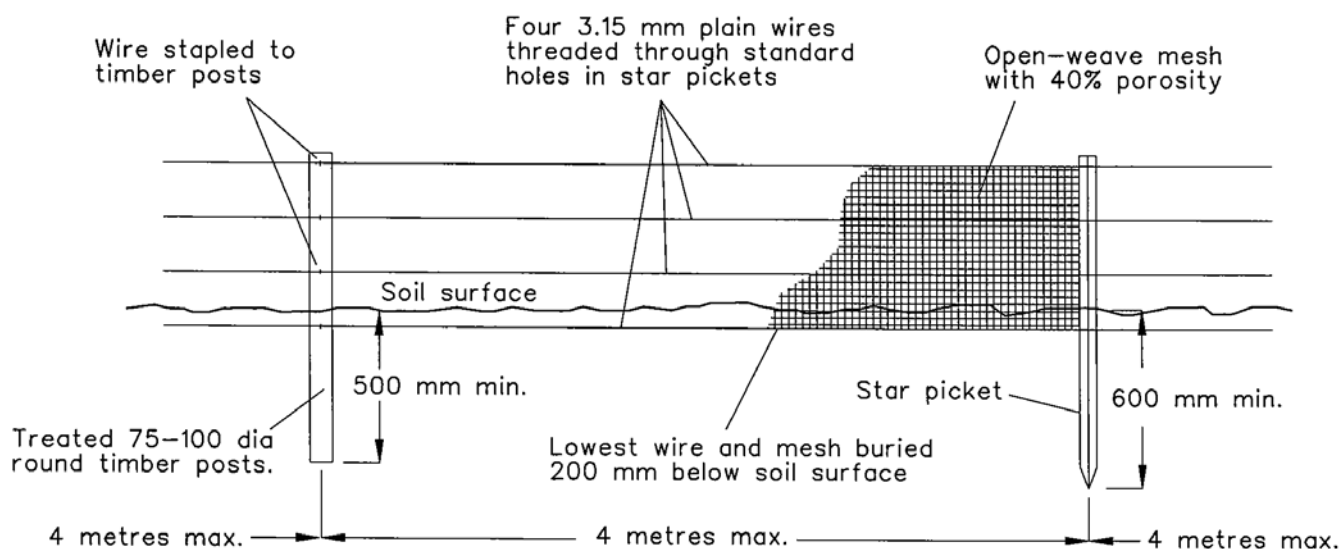
Construction Notes

1. Install a 400-mm minimum wide roll of turf on the footpath next to the kerb and at the same level as the top of the kerb.
2. Lay 1.4 metre long turf strips normal to the kerb every 10 metres.
3. Rehabilitate disturbed soil behind the



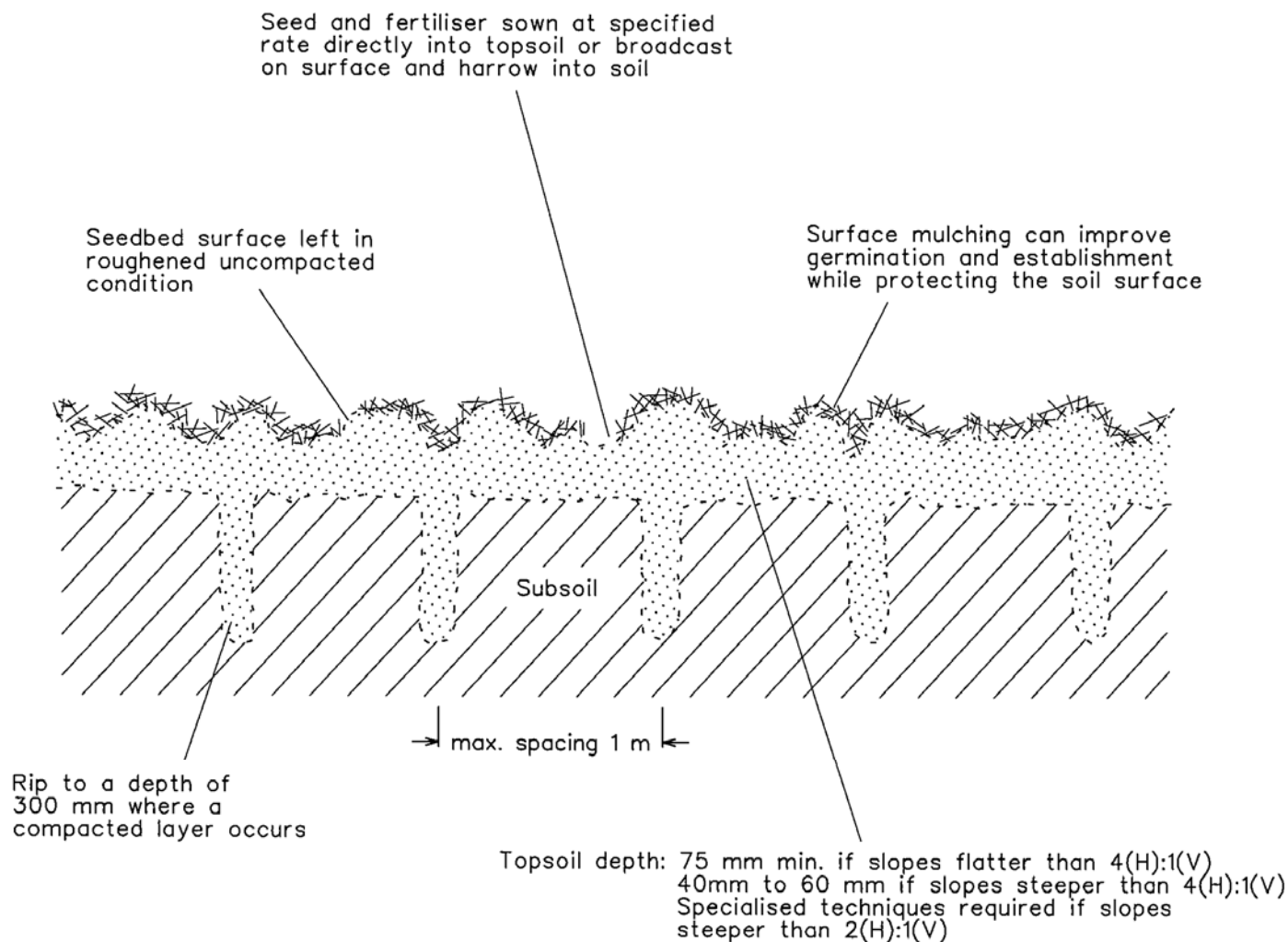
Construction Notes

1. Strip the topsoil, level the site and compact the subgrade.
2. Cover the area with needle-punched geotextile.
3. Construct a 200-mm thick pad over the geotextile using road base or 30-mm aggregate.
4. Ensure the structure is at least 15 metres long or to building alignment and at least 3 metres wide.
5. Where a sediment fence joins onto the stabilised access, construct a hump in the stabilised access to divert water to the sediment fence



Construction Notes

1. Install the fence to the height specified in the ESCP/SWMP.
2. Cut a channel 200 mm deep along the fence line.
3. Place wire and light resistant, open-weave polymer mesh with 40 percent porosity on the prevailing wind side of fence.
4. Fasten the mesh to all wires using ring fasteners at 100 mm to 150 mm intervals on top wire and 300 mm intervals on other wires.
5. Use one 75-mm to 100-mm diameter treated round timber post every 20 metres.
6. Where star pickets are used, ensure they are fitted with safety caps.



Construction Notes

1. Loosen compacted soil before sowing any seed. If necessary, rip the soil to a depth of 300 mm. Avoid rotary hoe cultivation.
2. Work the ground only as much as necessary to achieve the desired tilth and prepare a good seedbed.
3. Avoid cultivation in very wet or very dry conditions.
4. Cultivate on or close to the contour where possible, not up and down the slope.

Appendix H

High Efficiency Basin

POND OVERVIEW

Emergency spillway is to be wide, shallow and level. Where possible over the existing ground retaining the existing grass cover. Bare areas to be stabilised with concrete or similar.

Runoff Diversion Channel/Bund to ensure all flow enters at the inlet end.

Level Spreader full width of inlet end, stabilised from the beginning of the inlet to the pond invert and appropriate soft matting geotextile. Level Spreader to be 100-150mm above the invert level of the spillway.

3:1 inlet batter to be smoothed and free of voids

Manhole to act as Primary Spillway

All bare surfaces to be stabilised with vegetation

Pinned geotextile overlaid with large rock to break up flow

Extra crest width may be required to provide for machinery access for cleaning out.

FOREBAY/INLET

Construct a forebay at the pond inlet as shown - this will reduce future cleaning of the pond. Make it the same width of the pond (see below) and position it where it can be easily cleaned out by machine. The inlet slope should be a minimum of 3h:1v, smooth & level, and lined with polythene overlaid with needle punched fabric down to the permanent pool level. Ensure chemical dose point is upstream of forebay for better mixing.

POND DETAILS

Forebay. 2m x 1m x width of pond

Ensure inlet is above primary spillway level if possible

Operating volume (800 to 2000 mm)

Elevations

2750 mm

2250 mm

2000 mm

1400 mm

800 mm

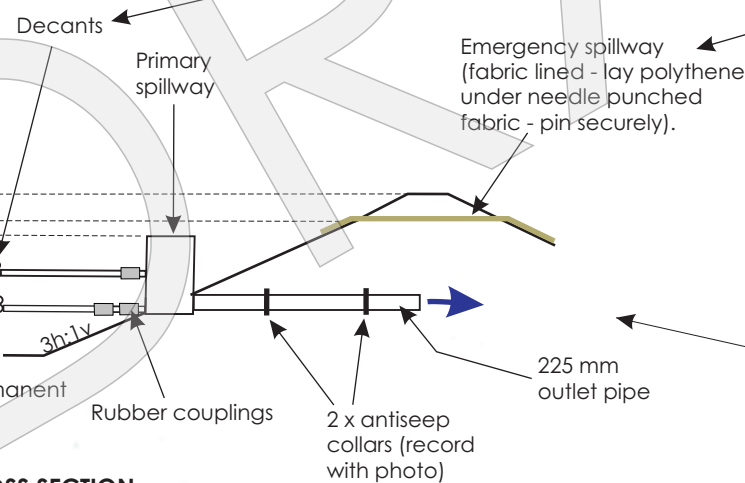
0 mm

Dead storage - permanent pool below 800 mm.

CROSS SECTION

LEVEL SPREADER

Install a 150 x 25 mm plank on its edge to act as a level spreader - see adjacent detail. It is used to spread flows the width of the pond. This is to be the width of the pond. It **must** be level & secured well with concrete. [Take care with the compaction of this area as level spreaders can be difficult to 're-level' once concrete has been laid.

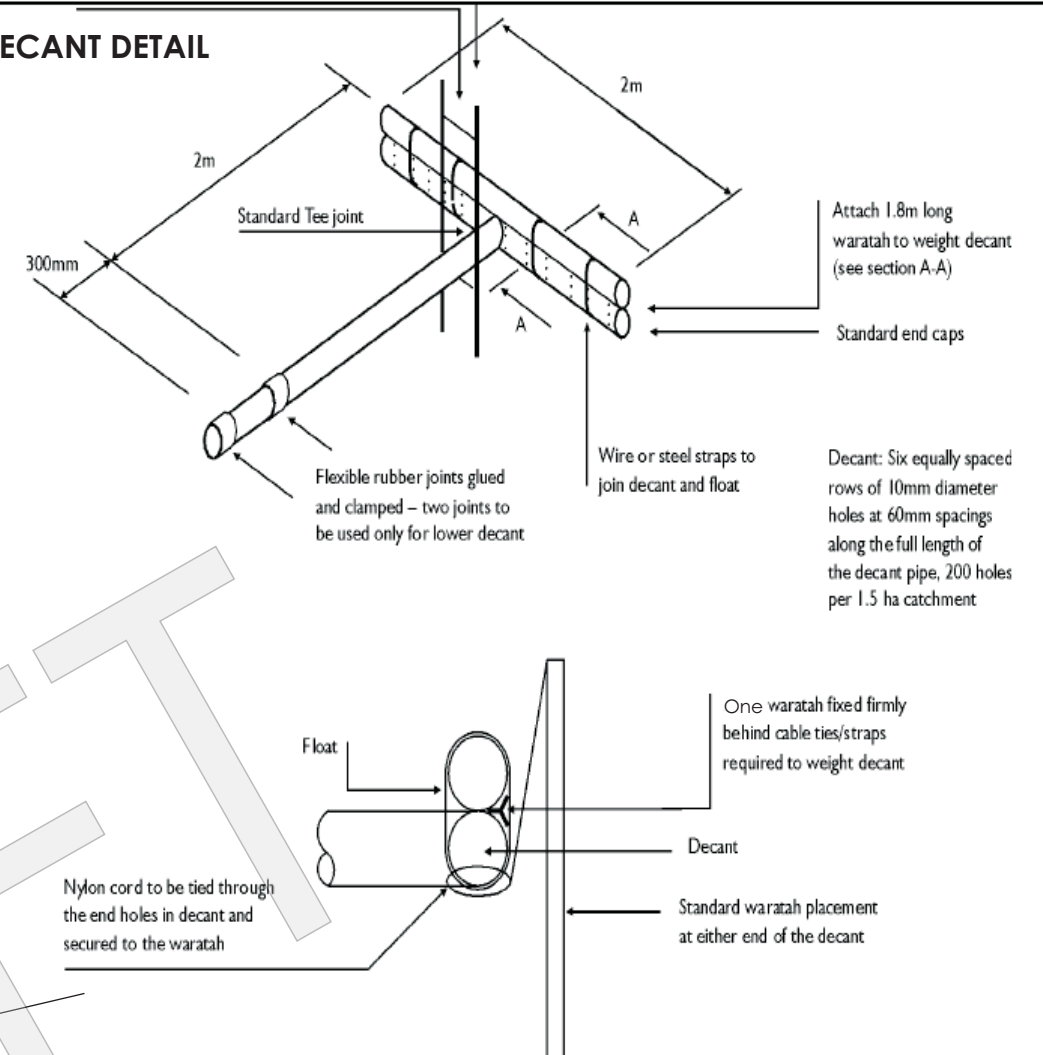


Level spreader

concrete

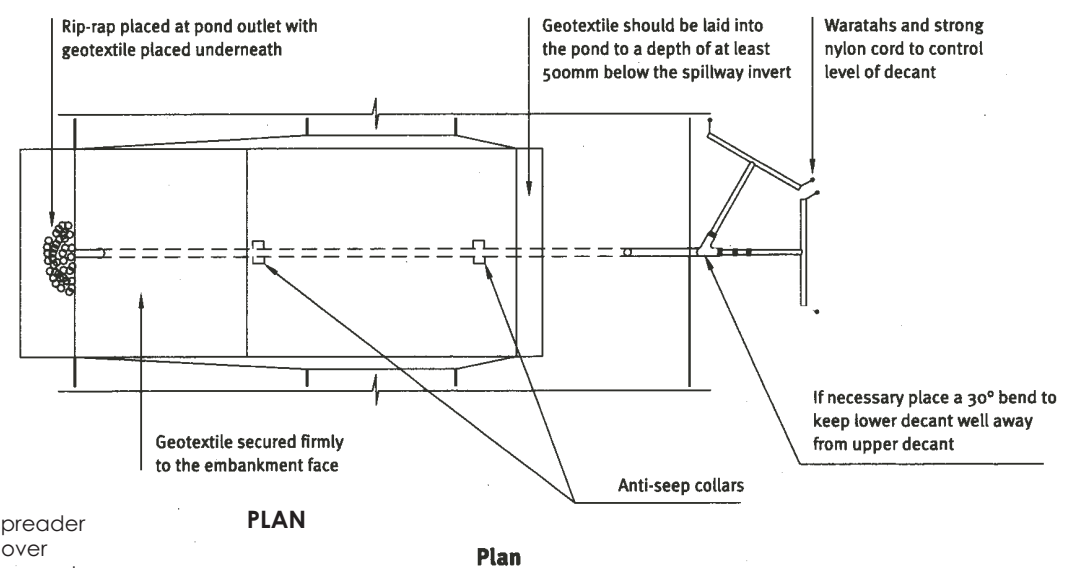
Geotextile laid to level spreader and concrete then laid over fabric and around level spreader.

DECANT DETAIL



EMERGENCY SPILLWAY

6m wide emergency spillway. Invert of spillway to be 250 mm above the invert of the primary spillway (riser). It needs to be horizontal and lined with polythene overlaid with fabric. Securely pin e.g. 0.5m centres.



Reference
TP 90: Auckland Regional Council. 1999 "Erosion and sediment control guidelines for land disturbing activities in the Auckland Region".