



Stormwater Management Plan LOT 600 SP321692 and LOT 50 SP305312

FIRST AVENUE MAROOCHYDORE CITY CENTRE

Walker Corporation

September 2024

Rev C

Projex Partners Pty Ltd Level 3 135 Horton Parade Maroochydore Qld 4558

Our ref: 571-002





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CERTIFICATION

| Report Title | Stormwater Management Plan LOT 600 SP321692, LOT 50 SP305312 FIRST AVENUE / SOUTH SEA ISLANDER WAY MAROOCHYDORE CITY CENTRE | | |
|------------------------|---|---|--|
| Affected Properties | LOT 600 SP321692, LOT 50 SP305312 | | |
| Street Address | First Avenue, Maroochydore QLD 4558 | | |
| RP Description | LOT 600 SP321692, LOT 50 SP305312 | | |
| Prepared For | Walker Corporation | | |
| Date | 17/09/2024 | | |
| Revision No. | С | | |
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| Signature | 1 herry | | |



1 INTRODUCTION

1.1 Background Information

Projex Partners have been engaged to develop a Stormwater Management Plan (SMP) for submission to Economic Development Queensland (EDQ) as part of a Material Change of Use (MCU) application for the proposed multi-use development to be located on Lot 600 and Lot 50 First Avenue, Maroochydore (Lot 600 SP321692 and Lot 50 SP305312).

The proposed development will involve the construction of two multi-storey towers, supported on a common podium recreation area over three parking levels, ground floor retail and carparking.

1.2 Scope of SMP

The objective of this SMP is to address how the proposed development will satisfy SCC Planning Scheme policies for stormwater quality. The SMP will document how the proposed development will satisfy the State Planning Policy (SPP) stormwater quality objectives. The SMP will document the pre and post development peak flow rates and document the proposed treatment trains to ensure compliance with SPP water quality targets.

1.3 Referenced Documentation

- Queensland Urban Drainage Manual (QUDM) 2017
- State Planning Policy 2017 (SPP)
- Sunshine Coast Council Flooding and Stormwater Management Guidelines, September 2020
- Sunshine Coast Council Planning Scheme Policy Development Works.



2 PRE-DEVELOPMENT CONDITIONS

2.1 Location of Site

The development site is located at lot 600 SP321692 and lot 50 SP305312 on First Avenue and South Sea Islander Way, Maroochydore. The site location is shown below in Figure 2-1.



Figure 2-1: Site Locality (QLD Globe, 2024)

2.2 Existing Site Characteristics

The proposed development site is bordered by a sewerage easement and the A1 Maroochydore office development on the northern boundary, First Avenue and South Sea Islander Way on the western boundary, Future Way on the southern boundary, and Gaba Lane on the eastern boundary.

The current site is undeveloped and primarily composed of pervious surfaces. Most of the area is covered with gravel providing private parking for workers, surrounded by grassed slopes leading to the parking lot. Two concrete driveways provide access to the site, with the southern entrance connecting to approximately 85m² of sealed pavement.

The northern section of the property is currently used for construction materials and machinery storage, as shown in Figure 2-2. This storage area is currently fenced.





Figure 2-2: Northern Extent Conditions (Projex Partners Site Inspection, 2024)

2.3 Existing Drainage Infrastructure

The feature and services survey conducted by Project Urban on 28 June 2021 (*Appendix A*) identified five field inlets located on the grassed slope next to the concrete footpath along the western boundary of the property. These inlets are connected to the road network by 375mm or 450mm reinforced concrete pipes (RCP).

Lot 50 is drained via a field inlet within the site that discharges to the South Sea Islander Way network.

2.4 Lawful Point of Discharge

2.4.1 Existing Discharge Regime

The existing site catchments have been identified and illustrated in Figure 2-3, enabling the assessment of the current discharge regimes.

The details are as follows:

- Sheet flow in Catchment A and B runs as overland flow into the surrounding road drainage network for First Avenue and South Sea Islander Way.
- Stormwater runoff from Catchment C is collected through a field inlet and discharged via a 450mm RCP into the South Sea Islander Way drainage network.





Figure 2-3: Existing Catchment Area Delineation

The existing discharge regime is shown in Figure 2-4 below.



Figure 2-4: Existing Discharge Regime



2.4.2 Proposed Lawful Point of Discharge

The proposed lawful points of discharge (LPD) for the development site are as detailed below in Figure 2-5. These points connect to the existing First Ave/South Sea Islander Way underground stormwater network. Site runoff flows up to the 1% AEP event will be captured in the proposed site drainage system and discharge to the existing Lawful Points of Discharge.

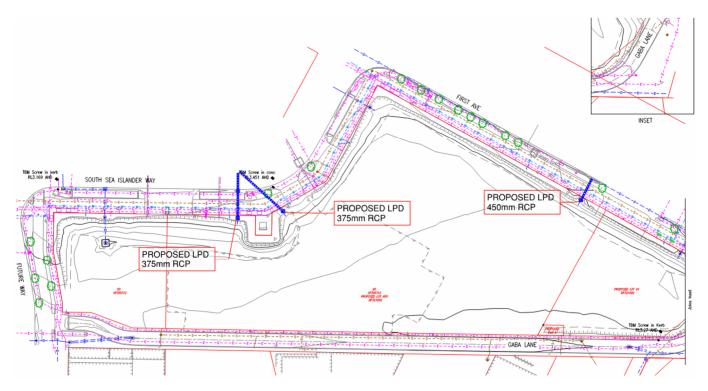


Figure 2-5: Proposed Lawful Point of Discharge

2.5 Flooding Assessment

Council's MyMaps (Flood Mapping and Information, 2023) indicates that the site is not subject to current and future (Year 2100) flooding up to a 1% AEP flood event. An extract of flood hazards (ARR) from Council mapping for the site is provided below in Figure 2-6.





Figure 2-6: SCC MyMaps Flooding Hazards ARR (Sunshine Coast Council)

Further assessment shows that the site is within the flood hazard buffer zone as detailed in the flood hazard area buffer on Council's MyMaps. An extract of flood hazard area for land use planning from Council mapping for the site is provided below in Figure 2-7.



Figure 2-7: SCC MyMaps Flooding Hazards ARR (Sunshine Coast Council)

It is noted that the Maroochydore City Centre master drainage plan and Cornmeal Creek Flood Study (*Cardno*, 06/11/2013) intends for these lots to be fully developed and has established finished floor levels for the site.



3 DEVELOPED CONDITIONS

3.1 Description of Proposed Development

The proposed development will involve the construction of two multi-storey towers, supported on a common podium recreation area over three parking levels, ground floor retails and a basement carpark. The proposed layout is attached in *Appendix B*.

3.2 Stormwater Drainage Infrastructure

The stormwater drainage infrastructure was designed to satisfy the requirements of the SCC Planning Scheme Policy – Development Works and QUDM.

The drainage network was sized to capture peak flow rates up to the 1% AEP storm event. The underground network was sized to cater for larger storm events than what is required by the SCC Planning Scheme Policy – Development Works to avoid on site detention storage.

To comply with the State Planning Policy's stormwater quality reduction targets, a proprietary treatment train is proposed to treat stormwater prior to discharging from the site. Further information on the treatment train proposed to satisfy the SPP reduction targets is discussed further in Section 6.



4 STORMWATER QUANTITY MANAGEMENT

4.1 Stormwater Quantity Analysis

Stormwater quantity analysis to determine pre and post development peak flow rates was undertaken using the Rational Method, as described in Section 4.3 of the Queensland Urban Drainage Manual (QUDM).

All catchments' areas have been maintained to match the previous masterplanning catchments as defined in Section 2.4. The internal building hydraulics has been designed to maintain the catchment areas.

Rainfall intensities for each storm event were obtained using the Rainfall Intensity-Frequency-Duration (IFD) information provided by the Bureau of Meteorology (BoM). Predevelopment catchment areas were calculated using Project Urban survey plans. Post development catchment areas were developed using architectural site layouts. Time of concentration for pre and post development conditions were calculated per Section 4.6 of QUDM. Predevelopment time of concentrations were calculated using Friends equation. Post development time of concentrations were calculated using standard inlet times.

To comply with SCC *Flooding and Stormwater Management Guidelines (September 2020)*, an allowance of 20% was added to peak flow rates to account for future climate change rainfall intensities.

Rational Method calculations are included in *Appendix D*. A summary of peak flow rates for the minor and major storm events (10% and 1% AEP) in both pre and post development conditions is provided in Table 4-1.

Table 4-1: Pre vs Post Development Peak Flow Rates Summary

| Storm Event (AEP) | Pre-Development % Impervious | Post Development % Impervious | Pre-Development Peak Flow Rate (m³/s) | Post Development Peak Flow Rate (m³/s) |
|-------------------|---------------------------------|----------------------------------|---|--|
| 10% | 20 | 90 | 0.298 | 0.463 |
| 1% | 20 | 90 | 0.517 | 0.831 |

4.2 Minor Drainage System

As the site is located within the "Principal Centre Zone" under the SCC Planning Scheme, the underground drainage network has been designed to convey peak flows up to the 10% AEP storm event. Captured stormwater will discharge to the proposed lawful point of discharge documented in Section 2.4.2.

4.3 Major Drainage System

Peak flow rates above the 10% AEP and up to the 1% AEP event will discharge to the underground stormwater network within the site and to the proposed Lawful Points of Discharge.

4.4 Detention Modelling

As the site characteristics will change from pervious to impervious surfaces, increases in peak flow rates in post development conditions are anticipated. Stormwater from the site is proposed to discharge via the existing 375mm and 450mm RCPs as detailed in Figure 2-5.

The drainage network downstream of the Lawful Points of Discharge flows to a major detention water body prior to discharge from the Maroochydore City Centre development. This water body has been designed to ameliorate flow volumes from the fully developed upstream catchments, including this development.

As there is no change to the developed use previously anticipated for these lots in the site-wide development planning and previous site-wide flood detention modelling, no on-site flow amelioration or detention is proposed.



5 FINISHED FLOOR LEVELS

5.1 Master Planning Phase Finished Floor Levels

Finished floor levels for development on the site were identified during the initial site master planning phase for each sub-catchment within Lots 600 and 50.

The Finished Floor Levels previously adopted align with sub-catchments and the existing drainage discharges from the site and the previous property boundaries assumed during the site master planning and are shown in Council's Flood Information Search (*Appendix C*) and in Figure 5-1.



Figure 5-1: Finished Floor Level Sub-Catchments

Minimum finished floor levels established during the site master-planning as listed on Sunshine Coast Council's Flood Information Search Cer24 08605 are as follows:

Table 5-1: Minimum Finished Floor Levels (extracted from SCC Flood Information Search Cer24 08605)

| Lot / Catchment Identifier | Pit Identifier | Minimum Floor Level (mAHD) |
|----------------------------|----------------|----------------------------|
| A2 | 1-60 | 3.89 |
| A3 | 1-26 | 3.74 |
| A4 | 1-25 | 3.70 |
| A5 | 1-24 | 3.70 |
| A6 | 1-22 | 3.66 |

We note that these Finished Floor Levels were developed prior to the Lot 600 lot amalgamation and assume independent development within each catchment area.

It is proposed to undertake flow diversion and amendment of these Finished Floor Levels as outlined in Section 5.

5.2 Proposed Amendments to Finished Floor Levels

The approach previously adopted for Finished Floor Levels assumed independent development on each of the previously planned lots and assumes a "worst case" for each lot.



The lot amalgamation create Lot 600 has significantly changed the development to create an integrated development footprint.

On the First Avenue Frontage, the floor level control (RL3.89m AHD) is via the inlet pit on the northern-most side of Lot 600 (*Pit 1-60 on Cardno Drawing 249402-CI-1302 in Appendix C*) that accommodates overflow from this pit and ingress into the development. This pit is also nominated as a Lawful Point of Discharge for the development and will collect all flows from the Gaba Lane frontage to First Avenue (*Catchment A2 on Cardno Drawing 249402-CI-1302 in Appendix C*).

It is noted that the previous master planning catchments do not anticipate that flows within the Gaba Lane frontage are a control on the Finished Floor Level due to the significantly lower levels of Gaba Lane compared to the First Avenue/ South Sea Islander Way and Future Way frontages. Review of the local catchment flows on Gaba Lane indicates local runoff from the Maud Street properties and the minor areas on the Maroochydore City Centre side of Gaba Lane are contained within the Gaba Lane formation (refer **Appendix J** for Gaba Lane capacity calculations).

To provide a consistent form of development within the site and reflect the current lot amalgamation it is proposed that the extents of the Finished Floor Levels be adjusted to reflect the potential overflow from the First Avenue onstreet drainage as follows:

- Maintain the overland flows external to the site within the road frontages in accordance with previous master planning, including no changes to runoff catchments or Points of Discharge as outlined above.
- Finished Floor Level of the proposed terrace housing frontage on First Avenue to be above RL3.89m AHD.
 This will provide flow diversion of any flows in excess of the underground drainage network capacity south within the First Avenue reserve along the frontage of the townhouses. This provides compliance with the minimum floor levels proposed in Council's Flood Search and the intent of the drainage regime.
- Amend the proposed Finished Floor Levels within the balance of Catchment A2 to reflect the Finished Floor Level defined by the diverted flows on Catchment A3 (minimum RL3.74m AHD). This provides compliance with Council's Flood Search as the only point of overland flow ingress into the balance of Lot 600 on the First Avenue frontage is through Catchment A3 (FFL = 3.74m AHD).
- Maintain the balance of the lots at or above the Finished Floor Levels defined in Council's Flood Search

The proposed overland drainage regime and Finished Floor Levels are shown in Appendix I.



6 STORMWATER QUALITY MANAGEMENT

6.1 Construction Phase Water Quality Issues

Water quality management is required to be implemented during the construction and operational phases of the development. Potential pollutants associated with the construction phase cannot be modelled due to the site-specific nature of the pollutant sources. The major pollutant of concern is suspended solids due to erosion associated with earthworks operations on site. Other pollutants of concern include hydrocarbons resulting from fuel and oil spills from construction equipment and vehicles and toxic materials from construction works. Potential pollutant export is largely dependent on site management practices and varies throughout the construction phase depending on the construction activities being undertaken.

6.2 Erosion and Sediment Control

The construction contractor is required to prepare a construction phase Erosion and Sediment Control Plan (ESCP), to document the proposed ESC devices that will be utilised on site to minimise impacts associated with stormwater discharging from the site during construction and meet SCC water quality objectives.

6.3 Water Quality Objectives

Table 6-1 below documents the water quality objectives applied to developments within the Sunshine Coast Council area. These objectives were extracted from the State Planning Policy 2017.

Table 6-1: State Planning Policy Water Quality Targets

| Pollutant | Reduction Requirement |
|------------------------------|----------------------------|
| Total Suspended Solids (TSS) | 80% of average annual load |
| Total Phosphorus | 60% of average annual load |
| Total Nitrogen | 45% of average annual load |
| Gross Pollutants (GP) | 90% of average annual load |

6.4 Proposed Water Quality Treatment Train

A SQIDEP approved proprietary stormwater treatment device, AtlanFilter, will be implemented on the site to treat stormwater runoff prior to discharge.

The SQIDEP approval certificate for the AtlanFilter system is included in Appendix E.

The proposed AtlanFilter installation location can be noted on the indicative drainage layout in *Appendix F* and treats all site runoff prior to discharge.

6.5 MUSIC Modelling

Model for Urban Stormwater Improvement Conceptualisation (MUSIC) Version 6.3 was utilised to determine the requirements for the water quality treatment trains.

6.5.1 Rainfall Data

Six-minute rainfall data, obtained from eWater for station 40282 – Nambour DPI was used to develop the model. This station was recommended for use when modelling site in this area of the Sunshine Coast. The data for the station is documented below in Table 6-2.



Table 6-2: MUSIC Rainfall Data

| Rainfall Station | Modelling Period | Annual Rainfall (mm) | Recording Interval (mins) |
|---------------------|-----------------------|----------------------|---------------------------|
| 40282 – Nambour DPI | 1/1/1989 – 31/12/1998 | 1527 | 6 |

6.5.2 Pollutant Export Parameters

The catchments were modelled using the Split Urban Residential catchment parameters. The pollutant export parameters for this node are documented below in Table 6-3. These values were obtained from Table 3.8 of the MUSIC Modelling Guidelines.

Table 6-3: Split Urban Residential Pollutant Export Parameters

| Land Use | Flow Type TSS log | TSS log^{10} value | | TP log^{10} value | | TN log^{10} value | |
|---|-------------------------|----------------------|------|---------------------|------|---------------------|------|
| Land Use | | Std Dev | Mean | Std Dev | Mean | Std Dev | |
| Split Urban Residential – Roof | Baseflow Parameters | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | Stormflow Parameters | 1.30 | 0.34 | -0.89 | 0.31 | 0.26 | 0.23 |
| Split Urban Residential – Roads | Baseflow Parameters | 1.00 | 0.34 | -0.97 | 0.31 | 0.20 | 0.20 |
| | Stormflow Parameters | 2.43 | 0.39 | -0.30 | 0.31 | 0.26 | 0.23 |
| Split Urban Residential – Ground Level | Baseflow Parameters | 1.00 | 0.34 | -0.97 | 0.31 | 0.20 | 0.20 |
| | Stormflow Parameters | 2.18 | 0.39 | -0.47 | 0.31 | 0.26 | 0.23 |

6.5.3 Rainfall-Runoff Parameters

The MUSIC Rainfall-Runoff parameters for Urban Residential Sites are documented below in Table 6-4. These parameters were obtained from Table A1.2 of the MUSIC modelling guidelines.

Table 6-4: Rainfall Runoff Parameters

| Parameter | Value |
|-------------------------------------|-------|
| Rainfall Threshold (mm) | 1 |
| Soil Storage Capacity (mm) | 500 |
| Initial Storage Capacity (%) | 10 |
| Field Capacity (mm) | 200 |
| Infiltration Capacity Coefficient A | 211 |
| Infiltration Capacity Coefficient B | 5.0 |
| Initial Depth (mm) | 50 |
| Daily Recharge Rate (%) | 28 |
| Daily Baseflow Rate (%) | 27 |
| Daily Deep Seepage Rate (%) | 0 |



6.5.4 Treatment Train

The node parameters that were entered into the MUSIC model are documented as part of the SQIDEP approval certificate (*Appendix E*) and were applied to this project.

The treatment train used in the MUSIC model is shown below in Figure 6-1. The stormwater catchment areas used to generate the MUSIC nodes shown below are documented in *Appendix G* and are sourced from the Cardno Stormwater Drainage Plan for Maroochydore City Centre.

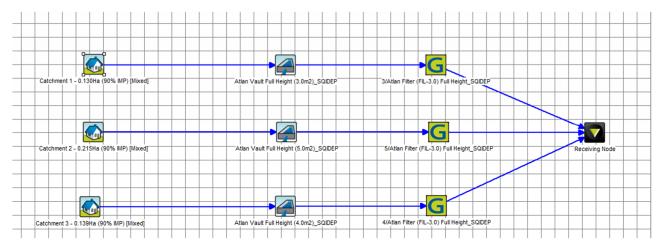


Figure 6-1: MUSIC Modelling Treatment Train (Atlan Stormwater)

The MUSIC modelling results shown in Figure 6-2 demonstrate that the nominated AtlanFilters within the Atlan CircaVault satisfy the SPP water quality targets.

| | Sources | Residual Load | % Reduction |
|--------------------------------|---------|---------------|-------------|
| Flow (ML/yr) | 6.3 | 6.3 | 0 |
| Total Suspended Solids (kg/yr) | 2520 | 491 | 80.5 |
| Total Phosphorus (kg/yr) | 4.04 | 1.2 | 70.3 |
| Total Nitrogen (kg/yr) | 13.1 | 5.79 | 55.9 |
| Gross Pollutants (kg/yr) | 146 | 0 | 100 |

Figure 6-2: MUSIC Modelling Results

6.5.5 AtlanFilter FIL-3.0 Maintenance and Whole of Life Information

The following information was provided by Atlan Stormwater regarding the lifecycle and maintenance frequencies of the AtlanFilter:

- Filters to be replaced at scheduled maintenance intervals. Atlan estimates the life of the AtlanFilter to be between 6-8 years. As a minimum requirement, each AtlanFilter cartridge should be replaced within 10 years.
- The site will require 12x AtlanFilter FIL-3.0, 2x CircaVault SV.350D-1615, and 1x CircaVault SV.250D-1610.

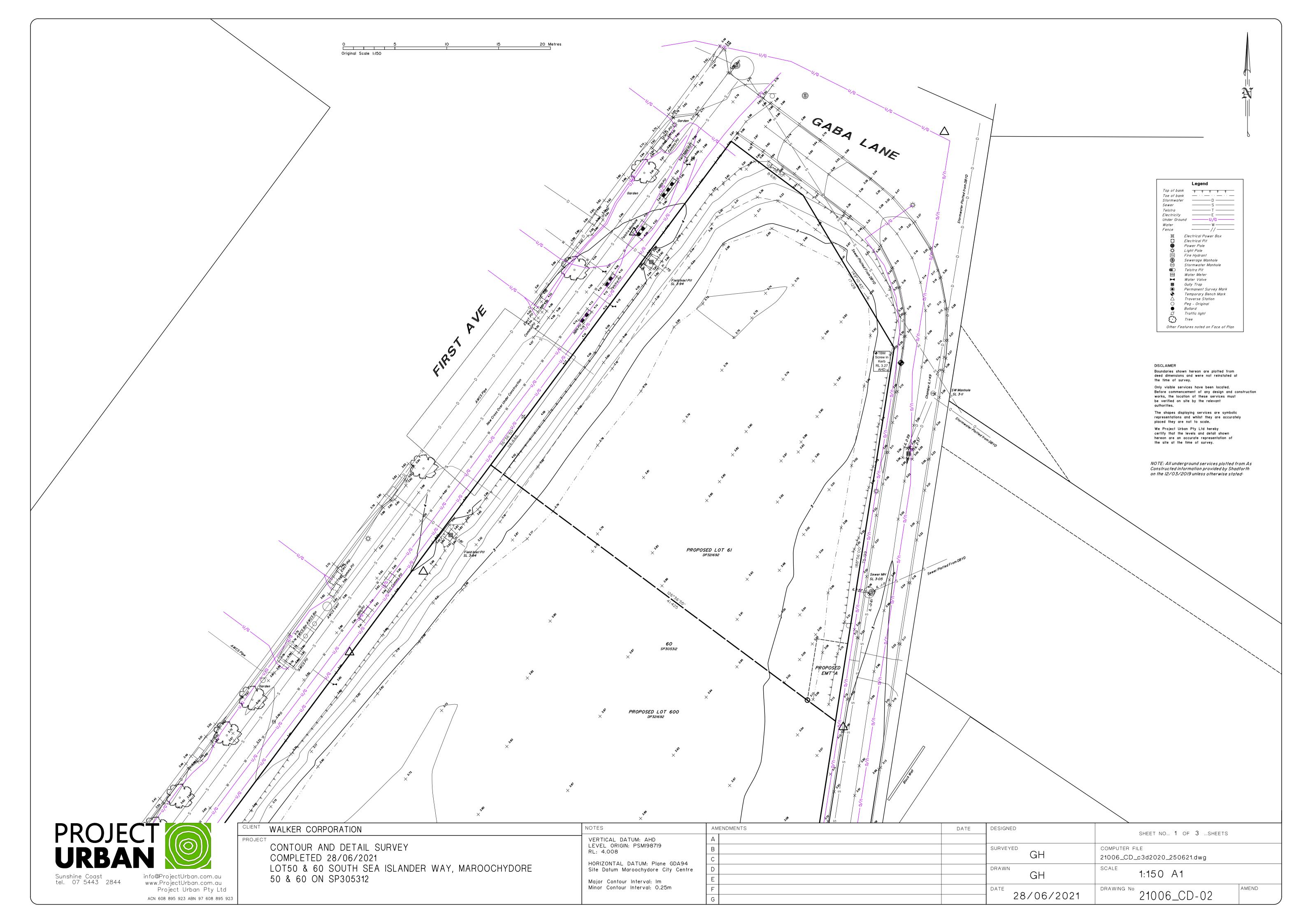
The AtlanFilter Operations and Maintenance Manual is attached in *Appendix H* for detailed information on the operation of the AtlanFilter and maintenance requirements.

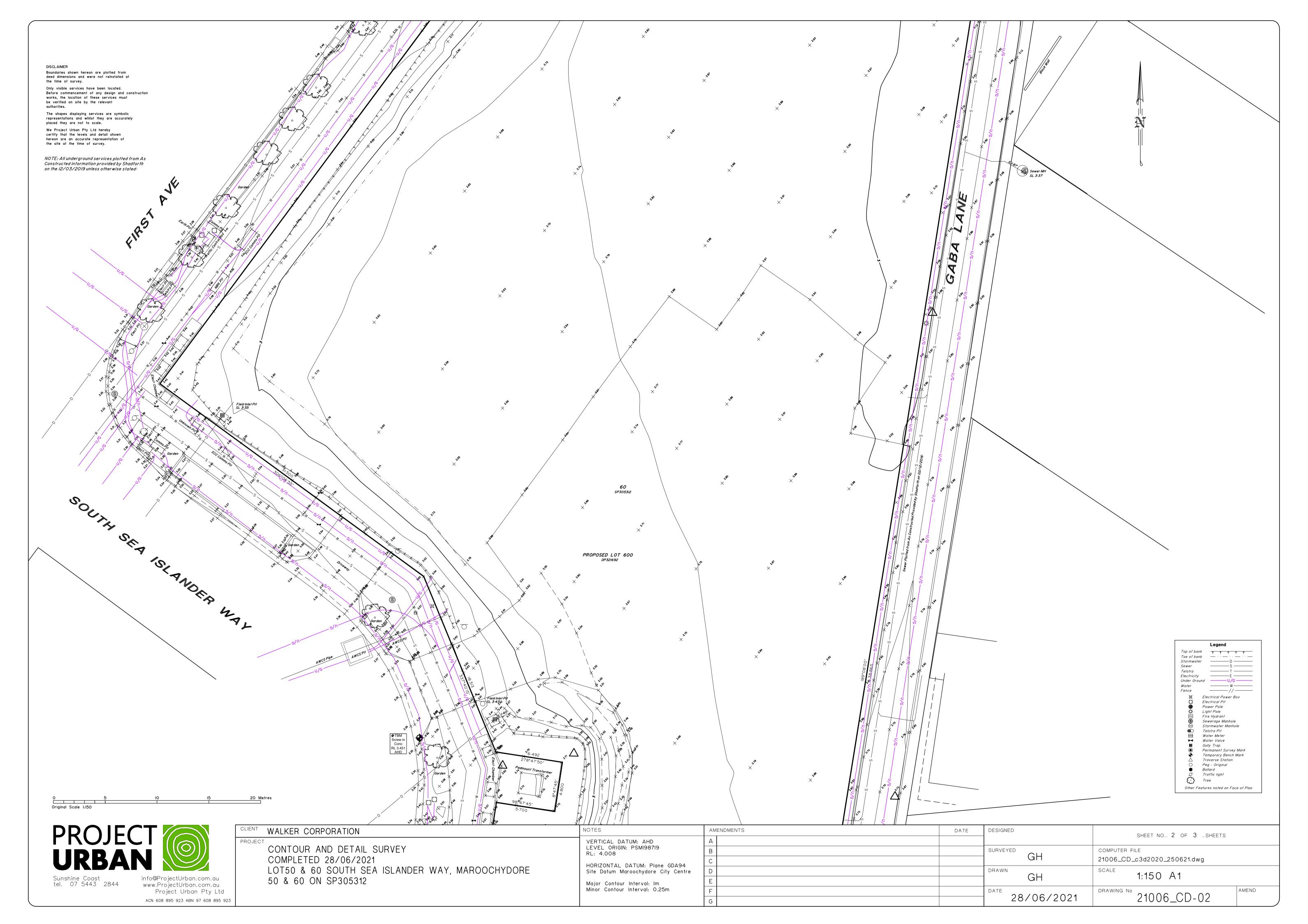


APPENDIX A

Survey









APPENDIX B

Proposed Site Layout



DA100 FLOOR PLAN - GROUND LEVEL



ISSUE I

Date of Issue | 24.07.31



APPENDIX C

SCC Flood Information Search



| Request 7 | Γνρε |
|-----------|------|
|-----------|------|

| Self-Assessable Dwelling |
|--------------------------|
| |

All Other

Flood Information Search



Applicant's Name Brooke Ferguson Issue Date 19 July 2024
Applicant's Address 16 Stephenson Ct Land Number 1536513

BEERWAH
QLD 4519

Land Number
1536513

Property Description
Address

First Ave

MAROOCHYDORE
QLD 4558

Our Reference

Email Address brookeferguson@projexpartners.com.au Issuing Officer jdm
Your Reference Not Applicable

REGISTERED OWNER(S) NAME:

ENQUIRY DATE:

Sunshine Coast Regional Council

15/07/2024

Cer24/08605

Flood Hazard Area for Building Regulation Purposes - Minimum Finished Floor Level

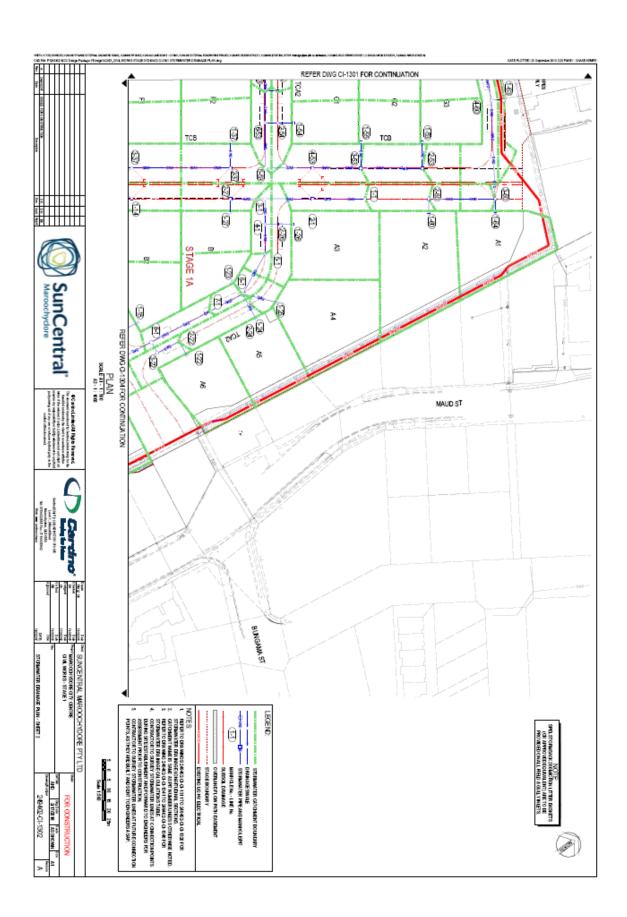
For the purposes of the QDC MP 3.5 (2012) and The Building Regulations S8.1 (2021) the levels provided in this table for new buildings are a declaration of the Finished Floor Level requirements for Class 1 buildings built in all or part of the Flood Hazard Area

| Defined Flood Event (DFE) level – 1% AEP (at 2100) | As per table | | | |
|--|---|--|--|--|
| Source of information (DFE): | Technical Memorandum – Maroochydore City Centre Stage 1 Local Flooding (Cardno, 29 October 2015) | | | |
| Maximum flow velocity: | Not Available | | | |
| Backwater or inactive flow area | Velocity Not provided | | | |
| Freeboard | Not Available | | | |
| Minimum Finished Floor Level: | As per table | | | |

| Lot Identifier | Pit Identifier | 1% AEP (at 2100) (m <i>A</i> | Minimum Floor Level | |
|----------------|-----------------|---------------------------------|---------------------|--------|
| Lot Identifier | i it identifies | Local Drainage | Regional | (mAHD) |
| A2 | 1-60 | 3.59 | 2.92 | 3.89 |
| A3 | 1-26 | 3.44 | 2.92 | 3.74 |
| A4 | 1-25 | 3.40 | 2.92 | 3.70 |
| A5 | 1-24 | 3.40 | 2.92 | 3.70 |



Figure 1. Property Boundary Relative to Council Flood Mapping



NOTES SPECIFIC TO THE FLOOD LEVELS QUOTED ON THIS SEARCH.

None Applicable

CLIMATE ASSUMPTIONS

The advice provided in this search is based upon standards relating to current and year 2100 climatic conditions and historically recorded flood events only. Year 2100 estimates include allowances for future climate conditions which specifically include increased rainfall intensity (20%) and higher mean sea level (0.8m).

Are you flood ready? Prepare with Council's award-winning Disaster Hub, now including Council's network of rainfall & water level gauges.

- Review Flood Mapping that shows how flood hazard changes as events get larger.
- Prepare your emergency plan and kit.
- Keep current with water levels, emergency warnings and road closure information.



INTERPRETATION NOTES FOR THIS SEARCH

- 1. Minimum finished floor levels are provided for residential land uses only in accordance with the criteria for self-assessable development in the Sunshine Coast Planning Scheme, 2014, Flood Overlay Code. For other types of development the flood overlay code of the planning scheme may assign a different event probability to the Defined Flood Event and specify different freeboard requirements. Refer to Table 8.2.7.3.3 of the Flood Overlay Code. In such instances a development application should already be lodged and the Development Services staff assisting with this application will provide guidance on the determination of minimum finished floor levels.
- 2. This search has not been prepared with knowledge of the date of construction or approval for development. It is incumbent upon the applicant, or the agent representing the applicant, in a purchasing situation to determine the date of approval for development in order to ascertain which of the minimum floor levels provided on this search are appropriate.
- 3. The absence of Highest Historical Flood Level information does not imply that the property is not subject to flooding, simply that Council has no record of this property flooding. Applicants are encouraged to make their own local enquiries.
- 4. The absence of local flood mapping does not imply that the above property is not subject to localised stormwater flooding. Please be aware of the natural topography in your area and the location of drainage infrastructure. Water runoff which exceeds the capacity of the drainage system (if present) and/or concentrates in surface depressions and gullies can cause localised stormwater flooding which may not be identified in this search.
- 5. Where a storm tide flood level is greater than the riverine flood level at the probability of the Defined Flood Event, then the Defined Flood Event is the Defined Storm Tide Event as reported on this search.
- 6. The MINIMUM FINISHED FLOOR LEVEL as required by the Flood Overlay Code of the Sunshine Coast Council Planning Scheme, 2014, is calculated as whichever is greater of either:
- (a) 500mm freeboard added to the Defined Flood Event Level (Regional, Riverine or Storm Tide) for the site; or
- (b) 300mm freeboard added to the Defined Flood Event Level (Drainage/Overland Flow) for the site as per the Queensland Urban Drainage Manual.
- 7. Surface water should be managed according to the requirements of the National Construction Code (Volume 2 and the ABCB Housing Provisions). In order to meet these requirements, the FINISHED FLOOR LEVEL may need to be higher than specified in this search.
- 8. Construction of all internal stormwater drainage must comply with the relevant sections of Australian Standard AS/NZS 3500.3 Plumbing and Drainage.
- 9. Building certifiers should be aware that their certification requires them to ensure no unacceptable off-site or on-site impacts associated with the drainage of buildings or land.
- 10. If the property is located within a declared Drainage Deficient Area the MINIMUM FINISHED FLOOR LEVEL may be returned as 'DDA Survey Required'. If so, refer Drainage Deficient Area requirements attachment for details.
- 11. For properties located adjacent to Lake Weyba or within 200m of the Pumicestone Passage, when calculating MINIMUM FINISHED FLOOR LEVEL an additional 300mm allowance for wave setup is added to the 500mm freeboard for properties. This results in a total freeboard of 800mm above the Defined Flood Level.
- 12. All buildings shall conform to the relevant Planning Scheme Code in the Sunshine Coast Regional Council, 2014.
- 13. Flood modelling is based on periodic aerial laser survey of the ground surface which filters out buildings and fences. Flow diversions caused by solid obstructions may not be identified in this search. Changes to surface levels and drainage may have altered the overland flow and flood behaviour within this property.
- 14. Council advises that if there are openings to basements these openings require a minimum level at least equal to the minimum finished floor level.
- 15. The levels and velocities provided on this search are derived from information relating to the flood hazard that is deemed most current and reliable at the time of search provision. This information may supersede flood information contained on the Sunshine Coast Regional Council Planning Scheme Flood Overlay (2014) which requires planning scheme amendment to maintain currency.
- 16. Section 8 of Building Regulations defines an inactive flow or backwater area to mean all or part of a flood hazard area where the maximum flow velocity of water is not likely to be greater than 1.5m/s. Council advises that velocity in some waterways, floodways and overland flow paths is less than 1.5m/s and would therefore meet this definition. Obstructing such flow paths is inherently problematic and likely to cause adverse impact. The declaration of a backwater area or inactive flow path should not be interpreted as acceptable to obstruct.
- 17. Additional information on the frequency and extent of flooding within this property can be found on Council's online mapping at: https://www.sunshinecoast.qld.gov.au/Development/Development-Tools-and-Guidelines/Sunshine-Coast-Mapping-MyMaps

DISCLAIMERS

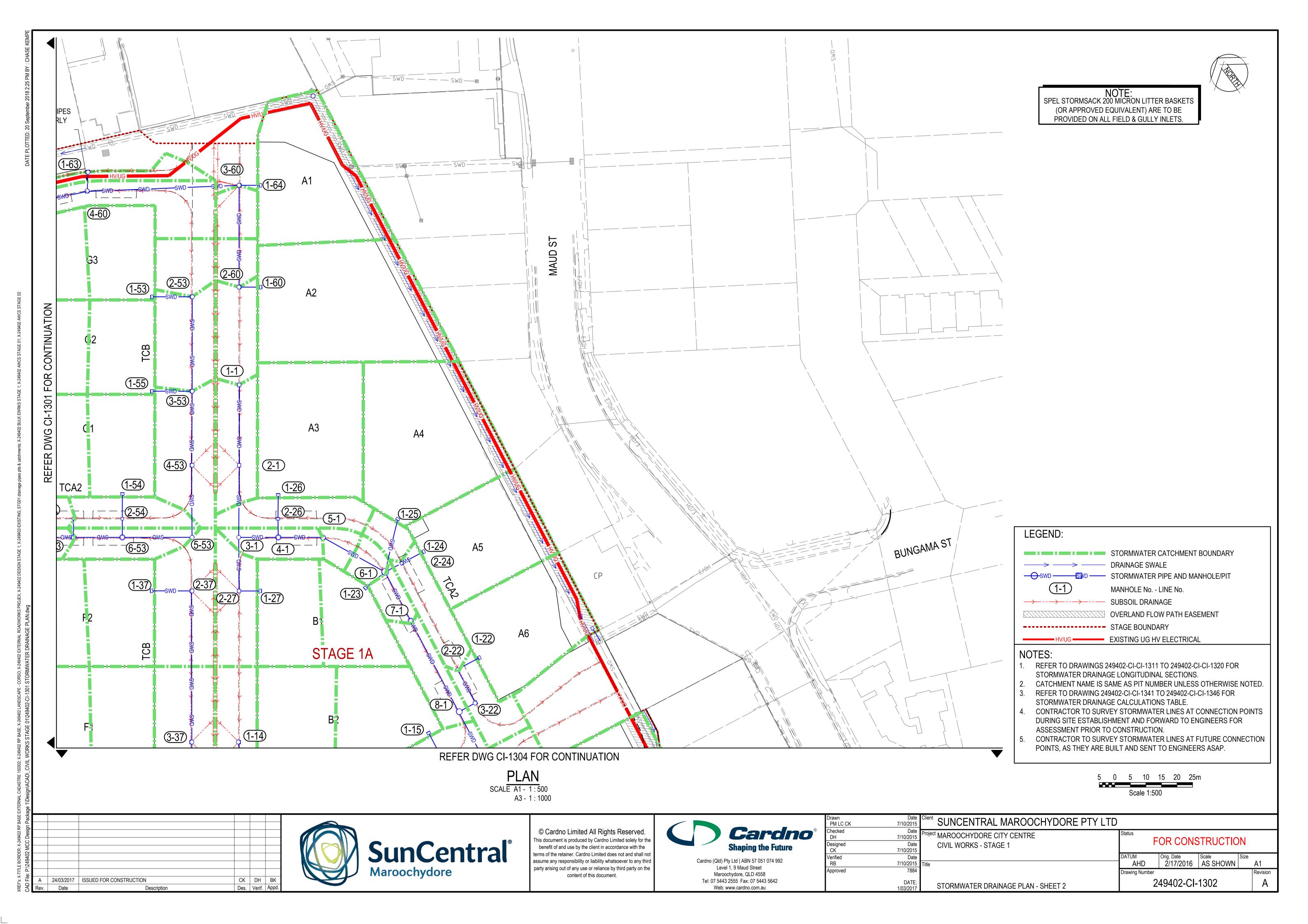
Flood information provided by Council represents the best information available to Council. It should only be used as a guide to the extent of flooding on the property. This information may be inaccurate or incomplete and it is recommended that purchasers make their own local enquiries with regard to the flooding and drainage history of the site.

The flood level information supplied does not represent the highest possible flood level that could occur on this property. Statistics indicate that a flood of equivalent or greater magnitude than the defined flood event is possible and has a 1% chance of occurring in any given year and similarly a 50% chance of occurring within 70 years.

The absence of flood information does not imply that the property is not subject to flooding, simply that Council has no information for this property flooding. If the property has a history of flooding or drainage problems, Council recommends you seek professional advice on this matter.

GLOSSARY OF TERMS

| Term | Definition | | | | |
|---------------------------------------|--|--|--|--|--|
| Applicant | The individual(s) requesting a flood search to be completed for a specified property. | | | | |
| Registered Owners | The individual(s) that are registered by Council as owning the property for which a flood search is requested. | | | | |
| AHD | The Australian Height Datum (AHD) is the reference level for defining reduced levels adopted by the National Mapping Council of Australia. The level of 0.0 m AHD is approximately mean sea level. | | | | |
| Defined Flood Event Level | A water level derived through mathematical modelling of the Defined Flood Event. | | | | |
| Defined Flood Event | Terminology consistent with Single State Planning Policy (SPP, 2013) which states "Defined Flood Event is the flood event adopted by a local government for the management of development in a particular area". This may also be the defined storm tide event where the flood level of the storm tide exceeds the flood level of the freshwater flood event (at the AEP of the defined flood event). | | | | |
| Source of Information | Is a reference to the document summarising the results of the anticipated flooding relevant to this location. | | | | |
| Highest Recorded Flood Level | The highest relevant flood water level from all historic events for which Council has records. | | | | |
| Location of Highest Recorded Event | A description of the site where the Highest Historical Flood Level was recorded. | | | | |
| Date of Highest Recorded Event | The date on which the Highest Historical Flood Level occurred. | | | | |
| Minimum Finished Floor Level | The minimum finished floor level calculated in accordance with the planning scheme flood overlay through the addition of the relevant freeboard to the Defined Flood Event Level or the Highest Recorded Historical Flood Level. The minimum finished floor level on this search relates to a flooding requirement. In some instances town planning notation may also specify a minimum finished floor level. The applicant should ensure that a town planning notation search is also undertaken. The minimum finished floor level is the higher of the level provided on this search and a minimum finished floor level from a town planning notation. | | | | |
| AEP | Annual Exceedance Probability. The 1% AEP has a 1% chance of exceedance in any year. | | | | |
| Rainfall Intensity | The amount of rainfall occurring in a unit of time, usually expressed in millimetres/hour. | | | | |
| Mean Sea Level | A tidal datum; the arithmetic mean of hourly heights of the sea at the tidal station observed over a period of time (preferably 19 years). Source: BOM This is approximately 0.0 m AHD | | | | |
| Storm Tide | The elevation of water generated by a severe weather event such as an east coast low pressure system or tropical cyclone above the normal astronomical tide. | | | | |
| Tropical Cyclone | A tropical cyclone is a low-pressure system which is sufficiently intense to produce sustained winds of at least 63 km/h or greater and gusts in excess of 90 km/h near the centre. | | | | |
| Freeboard | A factor of safety usually expressed as a height above the adopted Defined Flood Level. A freeboard tends to compensate for factors such as wave action and historical and modelling uncertainties. | | | | |
| Flood Hazard Area | An area, whether or not mapped, designated by a local government as a natural hazard area (flood) in the Building Regulation 2021, section 8. | | | | |
| Drainage Flood | This flood type has a flood level derived from a stormwater drainage study with rainfall as the source of flooding. This is normally a local area study that incorporates elements of the stormwater network in the assessment. These studies can provide flood levels associated with overland flow beyond the flood extent shown derived from a Riverine\Creek flood study | | | | |
| Regional/Riverine | This flood type has a flood level derived from a Regional (Riverine or Creek) flood study with rainfall as the source of flooding. As these studies are for larger areas they only consider surface flows and not the sub surface drainage network. Often flows will be input into the flood model at 'source points' and thus overland flows are not represented for the whole catchment area. | | | | |
| Storm Tide Flood | This flood type has a flood level derived from a Storm Tide flood study with the ocean condition as the source of flooding. | | | | |





Technical Memorandum

Title Maroochydore City Centre

Stage 1 Local Flooding

Client Suncentral Maroochydore Project No 249402

Date 29 October 2015 Status Preliminary

Author Nadia Guterres Discipline Civil Engineering

Reviewer Darryl Hone Office Sunshine Coast

1. Summary

Given the flat nature of the Stage 1 works and the locations of raised intersections which would block overland flow paths, detailed two-dimensional flood analysis was conducted to ensure that the proposed road and internal drainage design would be sufficient to convey stormwater flows during major flood events. The purpose of this analysis was to:

- > Determine the 100 year ARI local flood levels throughout Stage 1 and the corresponding floor levels for each lot.
- > Determine the impact of complete blockage of stormwater gully and field inlets to ensure that the freeboard provided to minimum floor levels was sufficient.
- > Determine whether the peak depths within the road reserve during major flood events complied with the requirements of QUDM.
- > Determine if any areas required additional drainage infrastructure.

The proposed stormwater drainage has been designed to have 5% Annual Exceedance Probability (AEP) capacity using 12d. This drainage design was then transferred into TUFLOW for analysis of the major 1% AEP storm event.

2. Methodology

The TUFLOW model was set up using the following methodology:

- > The 1% AEP rainfall was increased by 20% to account for the potential impact of climate change.
- > The Duration Independent Storm (DIS) was used, with a time step of 5 minutes. The DIS method converts peak rainfall intensities from various storm duration into the one temporal pattern.
- > A 0.5m grid size was adopted so that the road reserve was captured in sufficient detail.
- > The road reserve areas were modelled using rainfall on grid. No rainfall losses were assumed
- > The runoff from the surrounding lots was directed towards the underground drainage network. As the roof drainage is likely to have 5% AEP capacity, flows in excess of this capacity were directed as inflows onto the road surface. No rainfall losses were assumed.
- > The tailwater level in the canal was assumed to be 2.35m AHD. This is the 1% AEP storm tide level with potential climate change included. Storm tide levels are to be used in preference to

storm surge levels as wave runup is not included as it is not a factor in protected waterways such as Maud Canal.

- > The tailwater level for the existing northern drainage system was assumed to be equal to the obvert of the existing pipe.
- > The road reserve was modelled with a Manning's roughness of 0.02.
- > For the design scenario the blockage factors for field and gully inlets as specified by QUDM were assumed.
- > For the blockage scenario all inlets were blocked by 100%. Roof water drainage (to 5% AEP capacity) was still assumed to be able to enter the drainage network.
- > The manhole losses were automatically calculated by TUFLOW using the Engelhund Method.

3. Results

The preliminary results of the analysis identified areas where additional inlets would be required. Once these modifications were made to the design the results showed that:

- > The depth of flooding in the 1% AEP climate change design event was less than 250mm in all areas of the proposed development.
- > Once complete blockage of inlets was included the increase in peak water levels was less than 300mm in all areas of the site. As freeboard of 300mm above the 1% AEP local flood level is required for minimum floor levels based on the requirements of QUDM, this confirmed that all lots would have sufficient flood immunity for the major local flood event. For the majority of the site the increase was less than 100mm, with 95% of impacts being less than 200mm.
- > The peak depth-velocity (dV) product for the 1% AEP design flood event was extremely low in all areas, with a maximum of around 0.05m²/s. This indicates that flood hazards to motorists and pedestrians will be minimal.

The preliminary proposal for drainage design within Stage 1 nominated that areas where overland flow paths were blocked would have a duplicate drainage network with 1% AEP capacity. The results of this analysis have shown that even if all inlets are completely blocked that the peak water levels will not be increased by more than the specified minimum freeboard of 300mm. This is because there are some alternate flow paths available for areas around the raised intersections. It has therefore been deemed not necessary to provide a dual drainage network for these areas.

The results of the TUFLOW modelling are shown in the attached figures.

The minimum floor level for each lot, as specified by the manhole number relating to the roof drainage inlet point, is summarised in Table 1. A freeboard of 300mm above the 1% AEP flood level with climate change has been specified to comply with QUDM. The minimum floor levels required are all higher than those obtained using the 1% AEP climate change storm surge level, i.e. 3.32m AHD. The minimum floor levels in Table 1 were obtained by adding 300mm to the maximum design flood level along the street frontage of each lot.

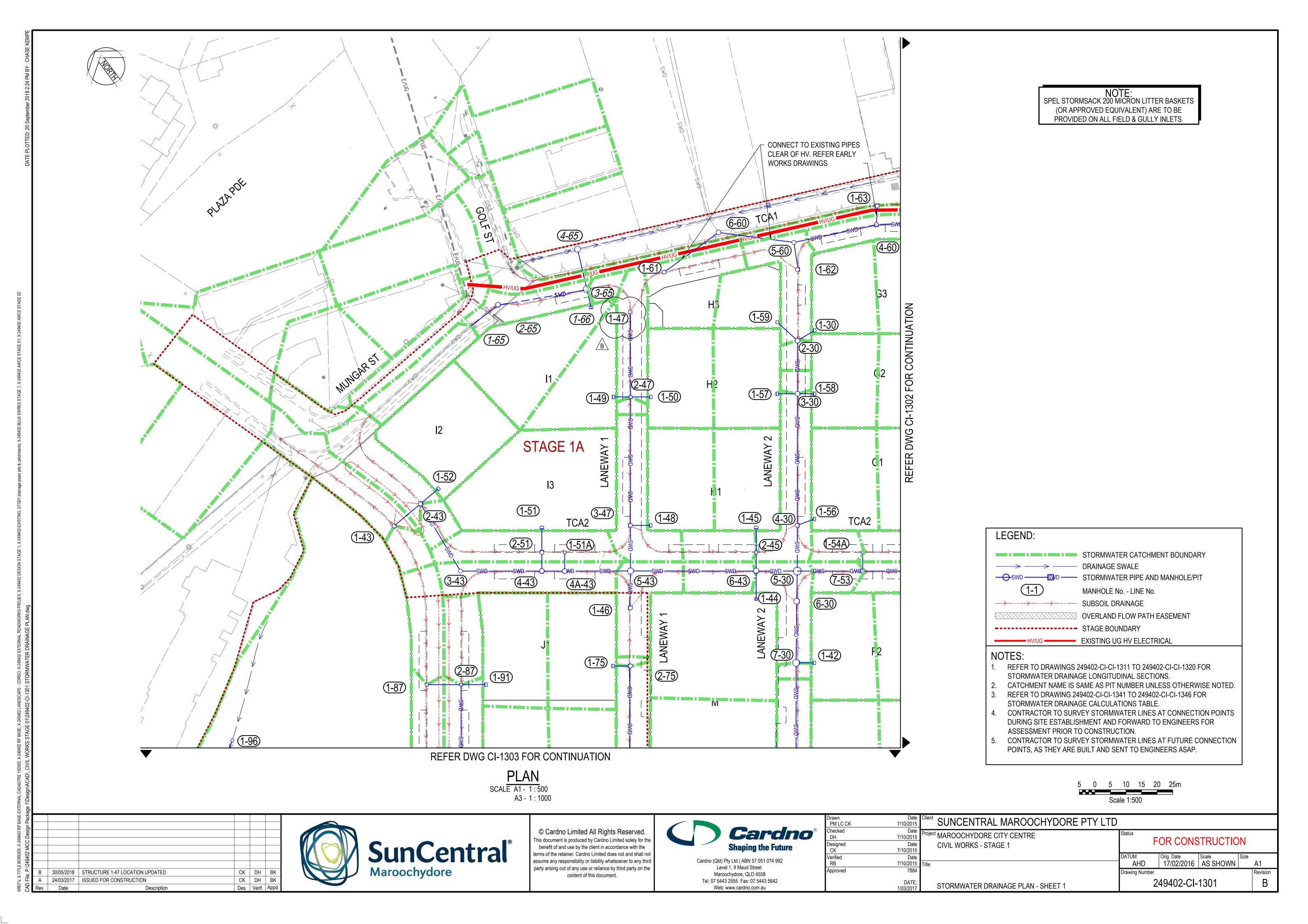


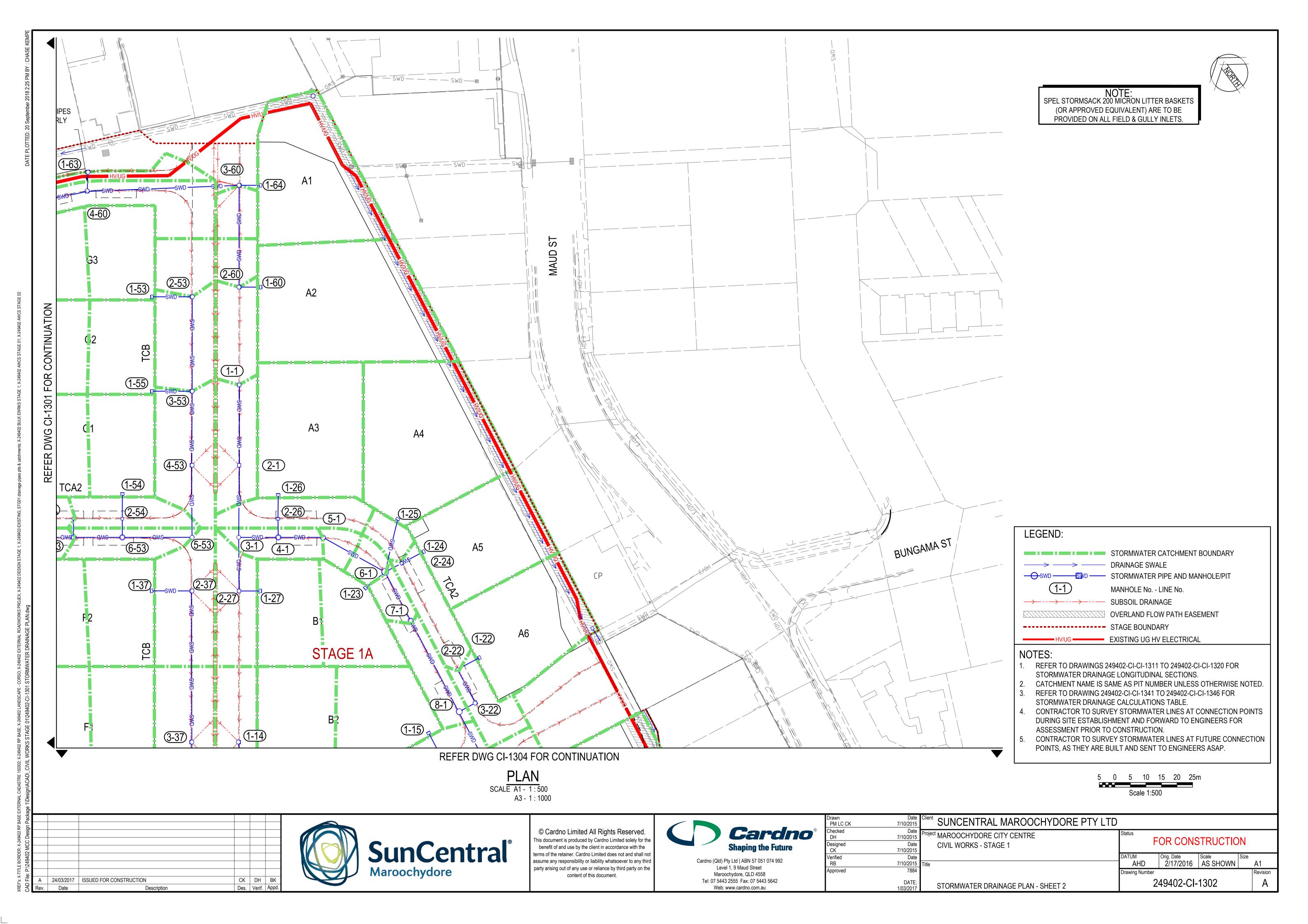
Addendum to Table 1 in Maroochydore City Centre Stage 1 Local Flooding Technical Memo 2015

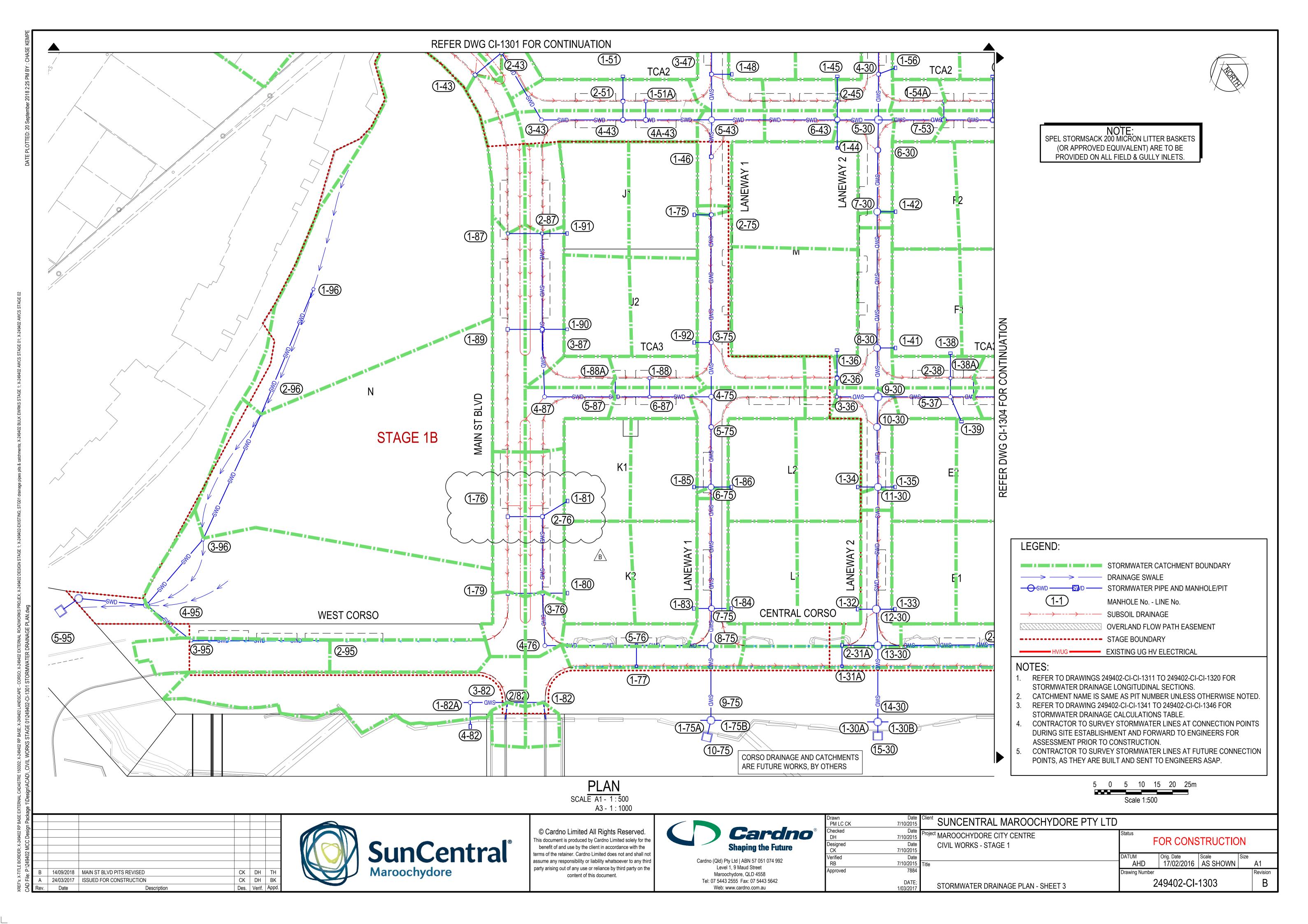
Table 1 Minimum Floor Levels for each lot

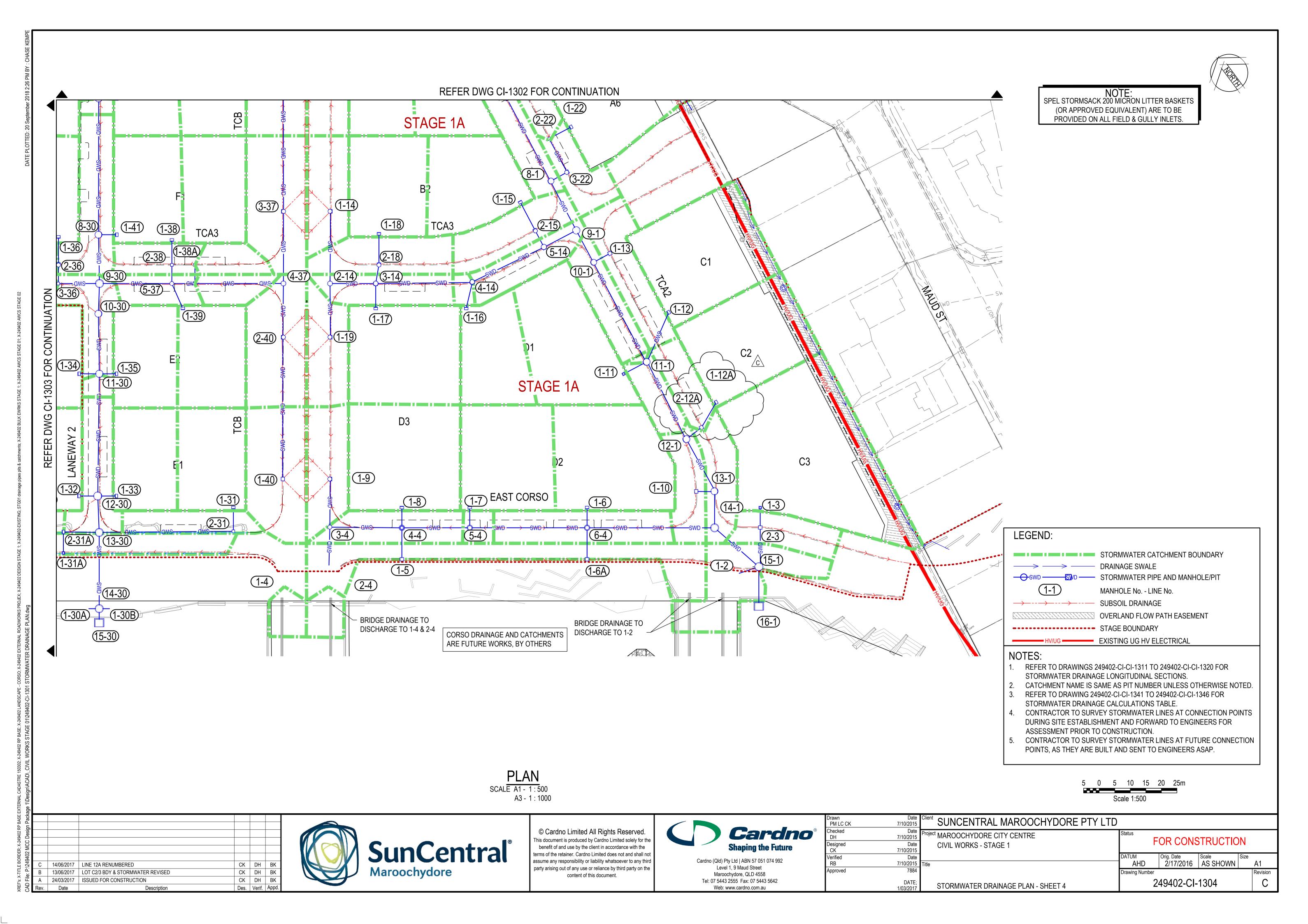
| LOT No. | PIT No. | MINIMUM FLOOR LEVEL (mAHD) | FREEBOARD WITH COMPLETE BLOCKAGE (mm) | LOT No. | PIT No. | MINIMUM FLOOR LEVEL (mAHD) | FREEBOARD WITH COMPLETE BLOCKAGE (mm) |
|------------|---------|-------------------------------------|---|------------|---------|-------------------------------------|---|
| A1 | 1-64 | 3.89 | 299 | G2 | 1-55 | 3.86 | 292 |
| A2 | 1-60 | 3.89 | 299 | G2 | 1-58 | 3.87 | 300 |
| А3 | 1-26 | 3.74 | 248 | G3 | 1-30 | 3.85 | 397 |
| A4 | 1-25 | 3.70 | 222 | G3 | 1-53 | 3.90 | 300 |
| A5 | 1-24 | 3.70 | 244 | H1 | 1-45 | 3.86 | 290 |
| A6 | 1-22 | 3.66 | 248 | H1 | 1-48 | 3.89 | 285 |
| B1 | 1-23 | 3.69 | 206 | H2 | 1-50 | 3.88 | 294 |
| B1 | 1-27 | 3.69 | 203 | H2 | 1-57 | 3.87 | 300 |
| B2 | 1-15 | 3.60 | 179 | Н3 | 1-59 | 3.92 | 300 |
| B2 | 1-18 | 3.68 | 213 | Н3 | 1-61 | 3.87 | 284 |
| C1 | 1-12 | 3.67 | 258 | I1 | 1-49 | 3.88 | 296 |
| C2 | 1-12A | 3.56 | 159 | I1 | 1-65 | 3.32* | 590 |
| С3 | 1-3 | 3.71 | 300 | I1 | 1-66 | 3.79 | 294 |
| D1 | 1-11 | 3.60 | 187 | 12 | 1-52 | 3.74 | 300 |
| D1 | 1-16 | 3.59 | 175 | 13 | 1-51 | 3.97 | 300 |
| D2 | 1-6 | 3.58 | 237 | J1 | 1-75 | 3.80 | 215 |
| D2 | 1-7 | 3.52 | 263 | J1 | 1-91 | 3.97 | 300 |
| D3 | 1-17 | 3.66 | 238 | J2 | 1-90 | 3.78 | 267 |
| D3 | 1-8 | 3.67 | 257 | J2 | 1-92 | 3.70 | 186 |
| E1 | 1-31 | 3.66 | 215 | K1 | 1-81 | 3.77 | 245 |
| E1 | 1-33 | 3.60 | 184 | K1 | 1-85 | 3.63 | 118 |
| E2 | 1-35 | 3.63 | 162 | К2 | 1-80 | 3.70 | 175 |
| E2 | 1-39 | 3.70 | 227 | К2 | 1-83 | 3.63 | 180 |
| F1 | 1-38 | 3.69 | 210 | L1 | 1-32 | 3.60 | 182 |
| F1 | 1-41 | 3.70 | 226 | L1 | 1-84 | 3.63 | 180 |
| F2 | 1-37 | 3.70 | 199 | L2 | 1-34 | 3.74 | 254 |
| F2 | 1-42 | 3.72 | 217 | L2 | 1-86 | 3.72 | 209 |
| G1 | 1-54 | 3.74 | 245 | N | 1-76 | 3.77 | 247 |
| G1 | 1-56 | 3.82 | 297 | N | 1-79 | 3.67 | 147 |

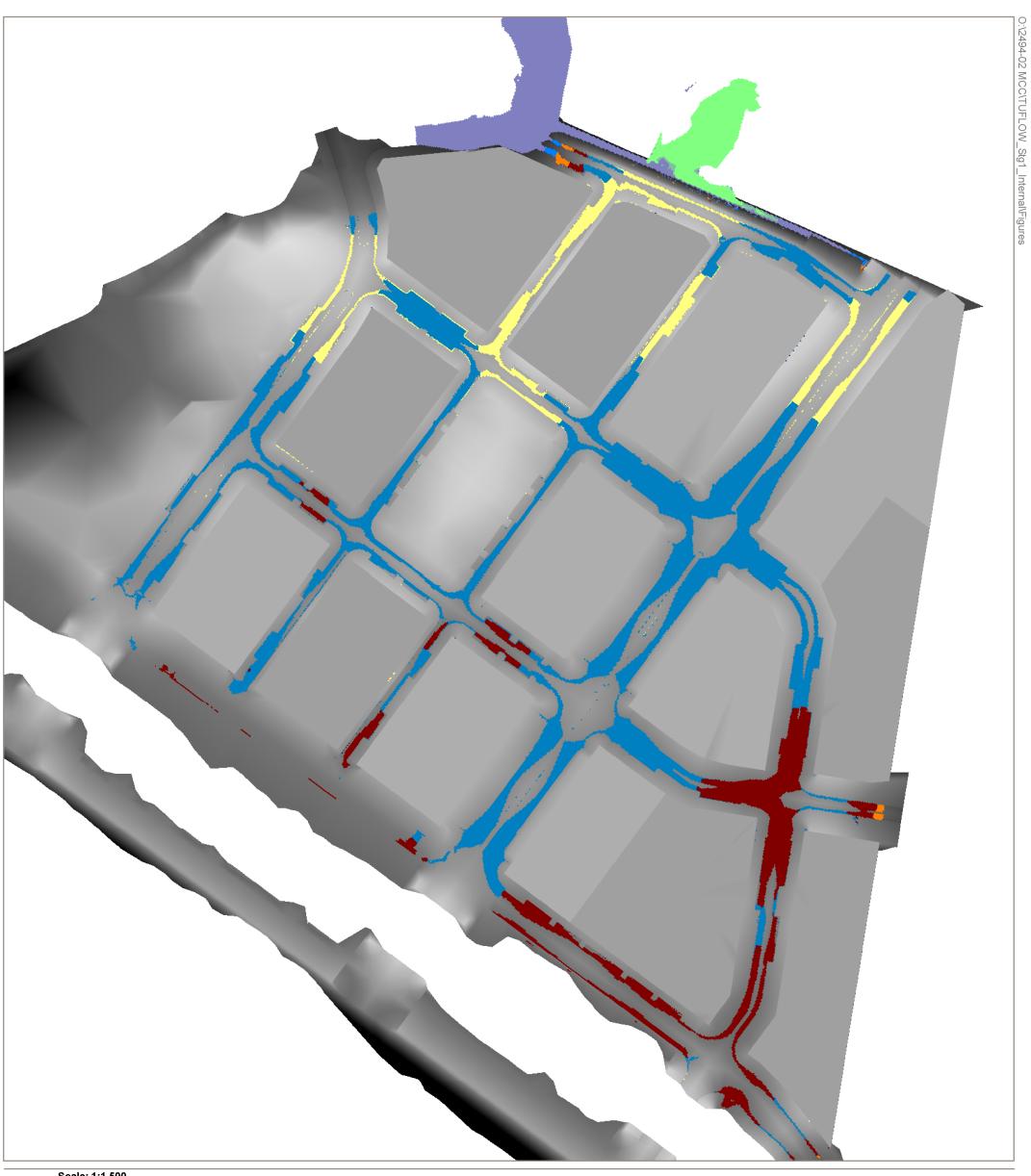
^{*} Based on 1% AEP Strom Surge Level











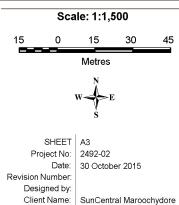


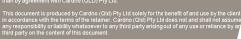


Figure 1 1% AEP Design Peak Flood Level with Climate Change

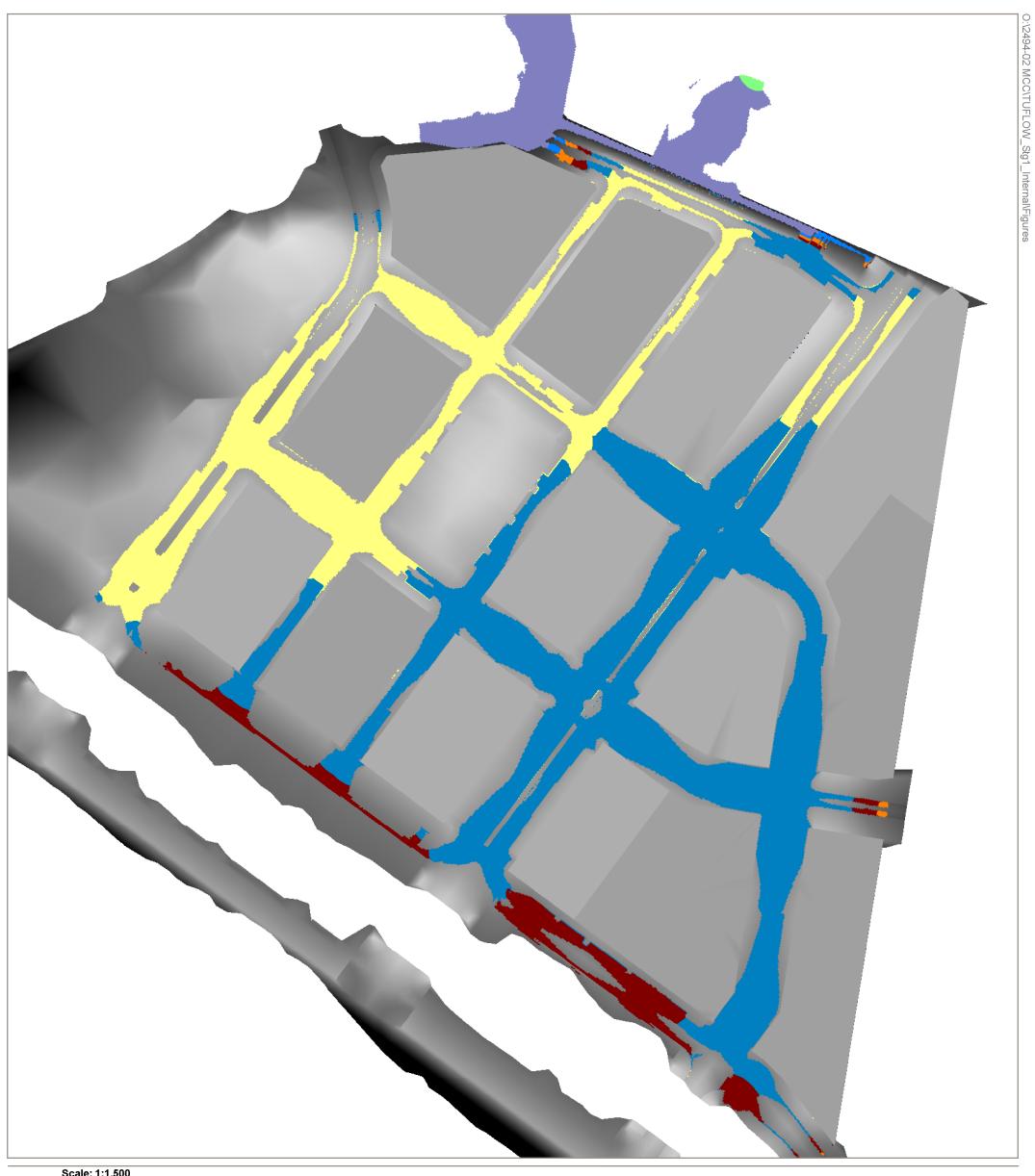
Stage 1 Internal Drainage

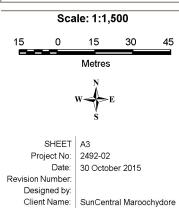


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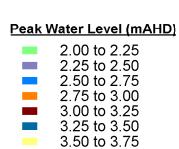


Figure 2

1% AEP Peak Flood Level with Climate Change and Complete Inlet Blockage

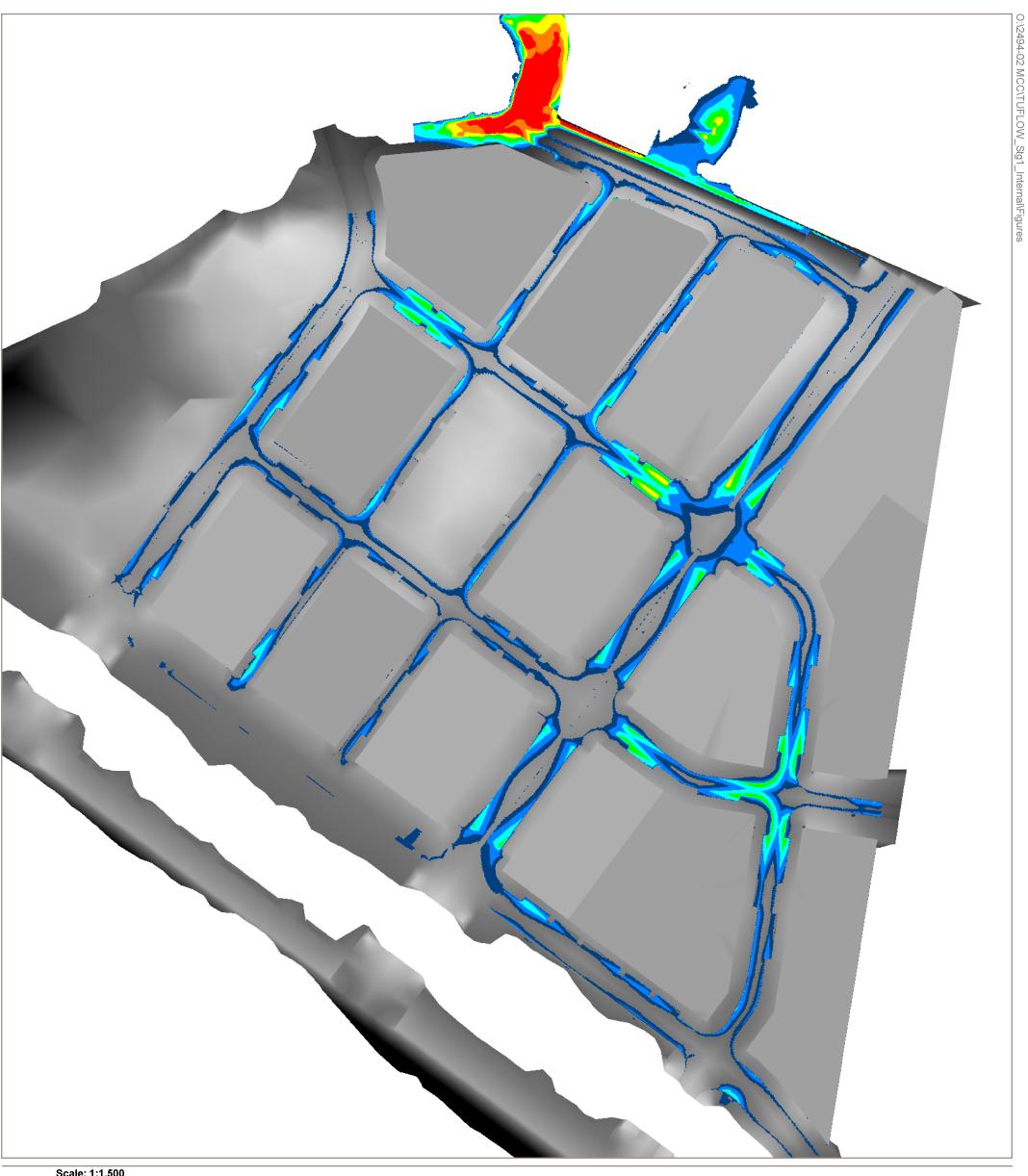
Stage 1 Internal Drainage

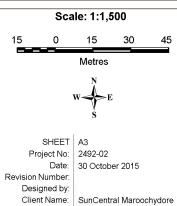


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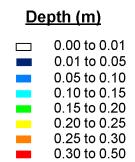


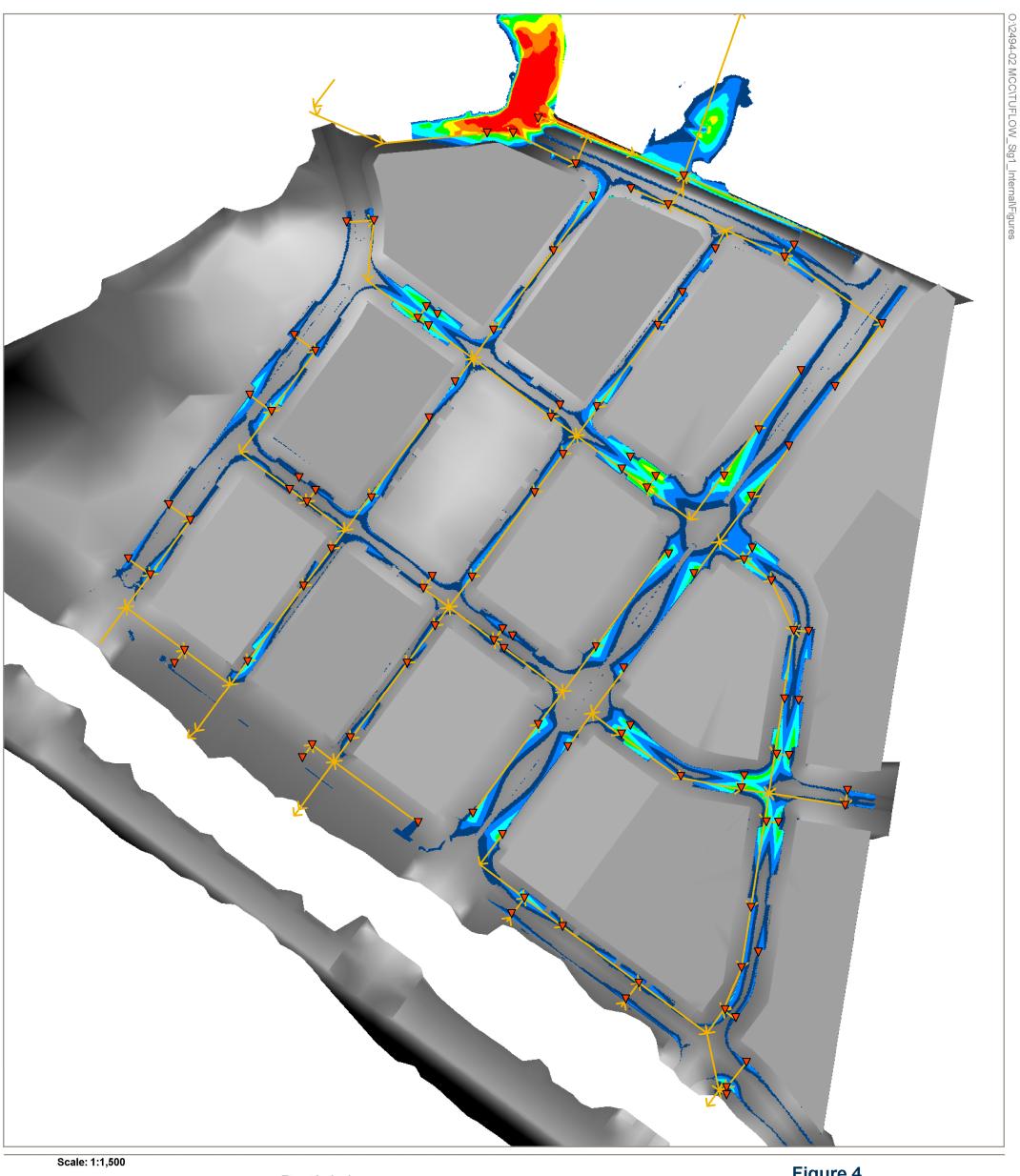
Figure 3

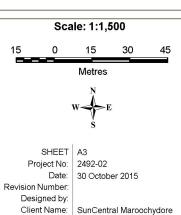
1% AEP Design Peak Depth with Climate Change

Stage 1 Internal Drainage









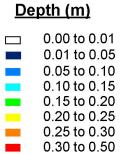




Figure 4

1% AEP Design Peak Depth with Climate Change

Stage 1 Internal Drainage



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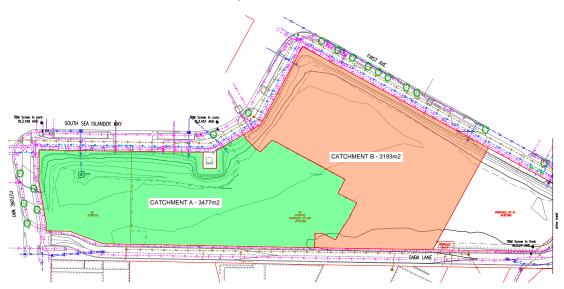
APPENDIX D

Rational Calculations

| ROJECT NO: | 571-002 | | 03/07/2024 |
|------------|---------|----------|------------|
| | | REVISION | |

CATCHMENT DEFINITION

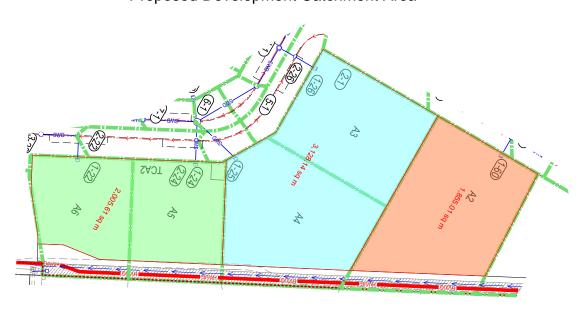
Pre-Development Catchment Areas



Catchment EA (20% impervious) = 3,477m2 = 0.3477haCatchment EB (20% impervious) = 3,193m2 = 0.3193ha

Total = 0.6670ha

Proposed Development Catchment Area



Catchment PA (90% impervious) = 1,855 = 0.1855ha Catchment PB (90% impervious) = 3,128 = 0.3128ha Catchment PC (90% impervious) = 2,005 = 0.2005ha

| ROJECT NO: | | | 03/07/2024 |
|------------|----|----------|------------|
| | WB | REVISION | |

TIME OF CONCENTRATION FOR PREDEVLOPMENT CONDITIONS

Friend's equation:

 $t = (107n L^{0.333})/S^{0.2}$ (4.5)

where:

t = overland sheet flow travel time (min)
 L = overland sheet flow path length (m)
 n = Horton's surface roughness factor

S = slope of surface (%)

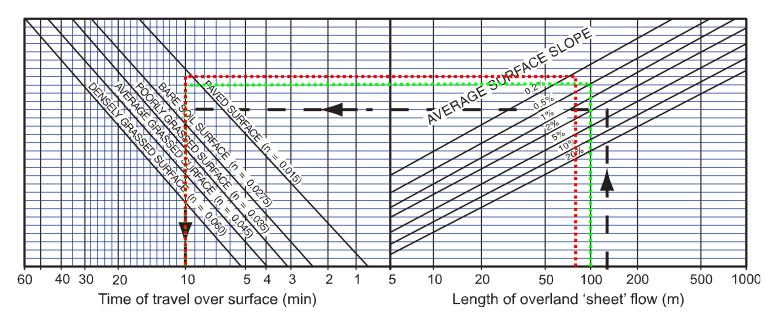


Figure 4.4 – Overland sheet flow times (shallow sheet flow only) (source: ARR, 1977)

Adopted Times

CATCHMENT A time of concentration - 10mins CATCHMENT B time of concentration - 10mins

Standard time of concentration 5mins used for Proposed Catchments



| PROJECT NO: | 571-002 | | 03/07/2024 |
|-------------|---------|----------|------------|
| | | REVISION | |

Issued: 03 July 2024

IFD RAINFALL DATA

7/3/24, 11:50 AM

Rainfall IFD Data System: Water Information: Bureau of Meteorology



Location

Label: Not provided

Latitude: -26.6584 [Nearest grid cell: 26.6625 (S)] **Longitude:**153.0927 [Nearest grid cell: 153.0875 (E)]

IFD Design Rainfall Intensity (mm/h)

Rainfall intensity for Durations, Exceedance per Year (EY), and Annual Exceedance Probabilities (AEP).

<u>FAQ for New ARR probability terminology</u>

Unit: mm/h ✓

| | | Offic: [IIIII/II] | | | | | | | | | | | |
|---------------|-------|-------------------------------------|------|------|------|------|------|--|--|--|--|--|--|
| | | Annual Exceedance Probability (AEP) | | | | | | | | | | | |
| Duration | 63.2% | 50%# | 20%* | 10% | 5% | 2% | 1% | | | | | | |
| 1 min | 176 | 197 | 264 | 309 | 353 | 410 | 453 | | | | | | |
| 2 min | 149 | 168 | 228 | 271 | 315 | 376 | 425 | | | | | | |
| 3 <u>min</u> | 140 | 157 | 214 | 253 | 293 | 347 | 391 | | | | | | |
| 4 min | 133 | 150 | 203 | 239 | 275 | 324 | 362 | | | | | | |
| 5 <u>min</u> | 127 | 143 | 193 | 226 | 260 | 304 | 338 | | | | | | |
| 10 <u>min</u> | 104 | 117 | 156 | 181 | 206 | 238 | 262 | | | | | | |
| 15 <u>min</u> | 88.2 | 98.8 | 132 | 153 | 174 | 201 | 221 | | | | | | |
| 20 <u>min</u> | 77.0 | 86.3 | 115 | 134 | 152 | 176 | 194 | | | | | | |
| 25 <u>min</u> | 68.6 | 76.9 | 103 | 120 | 136 | 158 | 174 | | | | | | |
| 30 <u>min</u> | 62.1 | 69.6 | 93.1 | 109 | 124 | 144 | 160 | | | | | | |
| 45 <u>min</u> | 49.0 | 55.1 | 74.2 | 87.3 | 100 | 117 | 131 | | | | | | |
| 1 hour | 41.1 | 46.3 | 62.8 | 74.2 | 85.5 | 101 | 113 | | | | | | |
| 1.5 hour | 31.8 | 36.0 | 49.4 | 58.8 | 68.3 | 81.2 | 91.4 | | | | | | |
| 2 hour | 26.4 | 30.0 | 41.7 | 49.9 | 58.1 | 69.5 | 78.6 | | | | | | |
| 3 hour | 20.4 | 23.3 | 32.8 | 39.6 | 46.4 | 55.9 | 63.4 | | | | | | |
| 4.5 hour | 15.8 | 18.2 | 26.0 | 31.5 | 37.2 | 44.9 | 51.1 | | | | | | |
| 6 hour | 13.3 | 15.3 | 22.1 | 26.9 | 31.8 | 38.5 | 43.9 | | | | | | |
| 9 hour | 10.4 | 12.1 | 17.6 | 21.5 | 25.5 | 31.0 | 35.3 | | | | | | |
| 12 hour | 8.75 | 10.2 | 15.0 | 18.3 | 21.8 | 26.5 | 30.2 | | | | | | |
| 18 hour | 6.86 | 8.03 | 11.9 | 14.6 | 17.4 | 21.2 | 24.2 | | | | | | |
| 24 hour | 5.76 | 6.75 | 10.0 | 12.3 | 14.7 | 18.0 | 20.7 | | | | | | |
| 30 hour | 5.01 | 5.88 | 8.73 | 10.8 | 12.9 | 15.8 | 18.2 | | | | | | |
| 36 hour | 4.46 | 5.23 | 7.78 | 9.61 | 11.5 | 14.2 | 16.3 | | | | | | |
| 48 hour | 3.69 | 4.33 | 6.43 | 7.96 | 9.53 | 11.8 | 13.7 | | | | | | |
| 72 hour | 2.78 | 3.25 | 4.83 | 5.98 | 7.18 | 9.01 | 10.5 | | | | | | |
| 96 hour | 2.24 | 2.62 | 3.88 | 4.82 | 5.79 | 7.30 | 8.56 | | | | | | |
| 120 hour | 1.88 | 2.20 | 3.26 | 4.04 | 4.85 | 6.13 | 7.21 | | | | | | |



| PROJECT NO: | | | 03/07/2024 |
|-------------|----------|----------|------------|
| | : WB | DEVISION | |

 $Q_y = (C_y \cdot {}^t I_y \cdot A)/360$

(4.2)

where:

 Q_y = peak flow rate (m³/s) for annual exceedence probability (AEP) of 1 in 'y' years

 C_y = coefficient of discharge (dimensionless) for AEP of 1 in 'y' years

A = area of catchment (ha)

 $^tI_y = ext{average rainfall intensity (mm/h) for a design duration of 't' hours and an AEP of 1 in 'y' years$

t = the nominal design storm duration as defined by the time of concentration (t_c)

Table 4.5.2 - Table of frequency factors

| AEP (%) | ARI (years) | Frequency factor (F _y) |
|---------|-------------|------------------------------------|
| 63% | 1 | 0.80 |
| 39% | 2 | 0.85 |
| 18% | 5 | 0.95 |
| 10% | 10 | 1.00 |
| 5% | 20 | 1.05 |
| 2% | 50 | 1.15 |
| 1% | 100 | 1.20 |

| Table 4.5.3 – Table of C_{10} values |
|--|
|--|

| Intensity | | Fraction impervious f _i | | | | | | | | | | | |
|---|----------|------------------------------------|------|------|------|------|------|--|--|--|--|--|--|
| (mm/hr) ¹ I ₁₀ | 0.00 | 0.20 | 0.40 | 0.60 | 0.80 | 0.90 | 1.00 | | | | | | |
| 39-44 | | 0.44 | 0.55 | 0.67 | 0.78 | 0.84 | 0.90 | | | | | | |
| 45-49 | le 4.5.4 | 0.49 | 0.60 | 0.70 | 0.80 | 0.85 | 0.90 | | | | | | |
| 50-54 | | 0.55 | 0.64 | 0.72 | 0.81 | 0.86 | 0.90 | | | | | | |
| 55-59 | Table | 0.60 | 0.68 | 0.75 | 0.83 | 0.86 | 0.90 | | | | | | |
| 60-64 | Refer to | 0.65 | 0.72 | 0.78 | 0.84 | 0.87 | 0.90 | | | | | | |
| 65-69 | Refe | 0.71 | 0.76 | 0.80 | 0.85 | 0.88 | 0.90 | | | | | | |
| 70-90 | | 0.74 | 0.78 | 0.82 | 0.86 | 0.88 | 0.90 | | | | | | |

| | CATCHMENT EA (EXISTING) | | | | | | | | | | |
|-------|-------------------------|------------------------|--------------------------|------|-------------------------------|------------------|-----------|----------|-------------------------|--------|--|
| AEP % | Frequency Factor (Fy) | I (mm/h) for 1hr 1in10 | Fraction Impervious (Fi) | C10 | Coefficient of discharge (Cy) | I (mm/h (10mins) | Area (ha) | Q (m3/s) | CC Factor (+20%) (m3/s) | L/s | |
| 63 | 0.80 | | | | 0.59 | 104 | | 0.0595 | 0.0714 | 71.36 | |
| 39 | 0.85 | | | | 0.63 | 117 | | 0.0711 | 0.0853 | 85.29 | |
| 18 | 0.95 | | | | 0.70 | 156 | | 0.1059 | 0.1271 | 127.11 | |
| 10 | 1.00 | 74.2 | 0.2 | 0.74 | 0.74 | 181 | 0.3477 | 0.1294 | 0.1552 | 155.24 | |
| 5 | 1.05 | | | | 0.78 | 206 | | 0.1546 | 0.1855 | 185.51 | |
| 2 | 1.15 | | | Γ | 0.85 | 238 | | 0.1956 | 0.2347 | 234.74 | |
| 1 | 1.20 | | | | 0.89 | 262 | | 0.2247 | 0.2696 | 269.65 | |

| | CATCHMENT EB (EXISTING) | | | | | | | | | | |
|-------|-------------------------|------------------------|--------------------------|------|-------------------------------|------------------|-----------|----------|-------------------------|----------|--|
| AEP % | Frequency Factor (Fy) | I (mm/h) for 1hr 1in10 | Fraction Impervious (Fi) | C10 | Coefficient of discharge (Cy) | I (mm/h (10mins) | Area (ha) | Q (m3/s) | CC Factor (+20%) (m3/s) | L/s | |
| 63 | 0.80 | | | | 0.59 | 104 | | 0.0546 | 0.0655 | 65.5289 | |
| 39 | 0.85 | | | | 0.63 | 117 | | 0.0653 | 0.0783 | 78.3275 | |
| 18 | 0.95 | | | | 0.70 | 156 | | 0.0973 | 0.1167 | 116.7233 | |
| 10 | 1.00 | 74.2 | 0.2 | 0.74 | 0.74 | 181 | 0.3193 | 0.1188 | 0.1426 | 142.5568 | |
| 5 | 1.05 | | | | 0.78 | 206 | | 0.1420 | 0.1704 | 170.3593 | |
| 2 | 1.15 | | | | 0.85 | 238 | | 0.1796 | 0.2156 | 215.5679 | |
| 1 | 1.20 | | | | 0.89 | 262 | | 0.2064 | 0.2476 | 247.6235 | |

| | CATCHMENT PA (PROPOSED) | | | | | | | | | | |
|-------|-------------------------|------------------------|--------------------------|------|-------------------------------|------------------|-----------|----------|-------------------------|----------|--|
| AEP % | Frequency Factor (Fy) | I (mm/h) for 1hr 1in10 | Fraction Impervious (Fi) | C10 | Coefficient of discharge (Cy) | I (mm/h (10mins) | Area (ha) | Q (m3/s) | CC Factor (+20%) (m3/s) | L/s | |
| 63 | 0.80 | | | | 0.70 | 127 | | 0.0461 | 0.0553 | 55.2839 | |
| 39 | 0.85 | | | | 0.75 | 143 | | 0.0551 | 0.0661 | 66.1394 | |
| 18 | 0.95 | | | | 0.84 | 193 | | 0.0831 | 0.0998 | 99.7668 | |
| 10 | 1.00 | 74.2 | 0.9 | 0.88 | 0.88 | 226 | 0.1855 | 0.1025 | 0.1230 | 122.9741 | |
| 5 | 1.05 | | | | 0.92 | 260 | | 0.1238 | 0.1485 | 148.5484 | |
| 2 | 1.15 | | | | 1.01 | 304 | | 0.1585 | 0.1902 | 190.2290 | |
| 1 | 1.20 | | | | 1.06 | 338 | | 0.1839 | 0.2207 | 220.7005 | |

| | CATCHMENT PB (PROPOSED) | | | | | | | | | | |
|-------|-------------------------|------------------------|--------------------------|------|-------------------------------|------------------|-----------|----------|-------------------------|----------|--|
| AEP % | Frequency Factor (Fy) | I (mm/h) for 1hr 1in10 | Fraction Impervious (Fi) | C10 | Coefficient of discharge (Cy) | I (mm/h (10mins) | Area (ha) | Q (m3/s) | CC Factor (+20%) (m3/s) | L/s | |
| 63 | 0.80 | | | | 0.70 | 127 | | 0.0777 | 0.0932 | 93.2227 | |
| 39 | 0.85 | | | | 0.75 | 143 | | 0.0929 | 0.1115 | 111.5278 | |
| 18 | 0.95 | | | | 0.84 | 193 | | 0.1402 | 0.1682 | 168.2322 | |
| 10 | 1.00 | 74.2 | 0.9 | 0.88 | 0.88 | 226 | 0.3128 | 0.1728 | 0.2074 | 207.3655 | |
| 5 | 1.05 | | | | 0.92 | 260 | | 0.2087 | 0.2505 | 250.4902 | |
| 2 | 1.15 | | | | 1.01 | 304 | | 0.2673 | 0.3208 | 320.7743 | |
| 1 | 1.20 | | | | 1.06 | 338 | | 0.3101 | 0.3722 | 372.1569 | |

| | CATCHMENT PC (PROPOSED) | | | | | | | | | |
|-------|-------------------------|------------------------|--------------------------|------|-------------------------------|------------------|-----------|----------|-------------------------|----------|
| AEP % | Frequency Factor (Fy) | I (mm/h) for 1hr 1in10 | Fraction Impervious (Fi) | C10 | Coefficient of discharge (Cy) | I (mm/h (10mins) | Area (ha) | Q (m3/s) | CC Factor (+20%) (m3/s) | L/s |
| 63 | 0.80 | | | | 0.70 | 127 | | 0.0498 | 0.0598 | 59.7543 |
| 39 | 0.85 | | | | 0.75 | 143 | | 0.0596 | 0.0715 | 71.4876 |
| 18 | 0.95 | | | | 0.84 | 193 | | 0.0899 | 0.1078 | 107.8342 |
| 10 | 1.00 | 74.2 | 0.9 | 0.88 | 0.88 | 226 | 0.2005 | 0.1108 | 0.1329 | 132.9181 |
| 5 | 1.05 | | | | 0.92 | 260 | | 0.1338 | 0.1606 | 160.5604 |
| 2 | 1.15 | | | | 1.01 | 304 | | 0.1713 | 0.2056 | 205.6114 |
| 1 | 1.20 | | | | 1.06 | 338 | | 0.1988 | 0.2385 | 238.5469 |

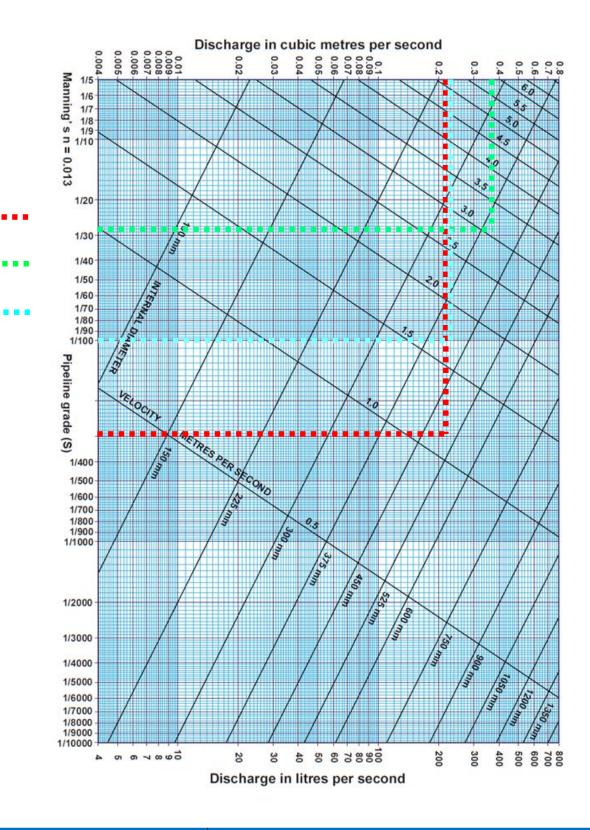
PΑ

PB

PC

| PROJECT NO: | | | 03/07/2024 |
|-------------|----|----------|------------|
| 3Y: | WB | REVISION | |

PROPOSED LAWFUL POINT OF DISCHARGE - CATCHMENT NOMOGRAPH VERIFICATION



| Catchment | Q (m3/s) | | Nompgraph Validation | | | | |
|------------|----------|--------|----------------------|-----------------------------|---------|------------|---------------------|
| Gatchinent | 10% | 1% | LPD | Existing Pipe Diameter (mm) | Grade % | S (1 in X) | Aligns with ex. LPD |
| EA | 0.1552 | 0.2696 | | | | | |
| EB | 0.1426 | 0.2476 | | | | | |
| PA | 0.1230 | 0.2207 | 1 | 450 | 0.78 | 1 in 129 | YES |
| PB | 0.2074 | 0.3722 | 2 | 375 | 3.50 | 1 in 28 | YES |
| PC | 0.1329 | 0.2385 | 3 | 375 | 0.98 | 1 in 100 | YES |



APPENDIX E

SQIDEP Certification for AtlanFilter



Stormwater Quality Improvement Device Evaluation Protocol (SQIDEP)

VERIFICATION CERTIFICATE

Applicant Information

| Applicant Name | SPEL Stormwater Pty Ltd |
|-------------------|--------------------------------------|
| Applicant Address | 130 Sandstone Pl, Parkinson QLD 4115 |
| Phone Number | +61 1300 773 500 |
| Email | sales@spel.com.au |
| Website | www.spel.com.au |

| Verified Technology | SPELFilter |
|---------------------|--|
| Issue Date | 23 December 2022 |
| Reviewed Documents | SPEL Body of Evidence application submission (Prepared by Drapper Environmental Consultants) Statutory Declaration by Drapper Environmental Consultants Hydrographs of compliant and partially compliant events at the Hilton Foods site showing inflow, outflow, rainfall and samples collected (42 items) Sample collection and/or reset emails/site records at the Hilton Foods site (50 items) Laboratory Chain of Custody forms, Quality Control reports, QC Compliance Reviews & Certificates of Analysis Subsequent hydrograph plots for Hilton Foods site that included monitored outflow rates (and summary table of results) – (37 items), 17 October 2022. |

Technology Information

| \ F | Applicant's /erified Performance Claims | Treatable flow rate = 3 L/s per f Total Suspended Solids (TSS) Total Phosphorus (TP) Total Nitrogen (TN) Total Petroleum Hydrocarbons | ilter cartridge 85 % 74 % 59 % 0 % |
|--------|--|---|--|
| | | Gross Pollutants | 0 % |



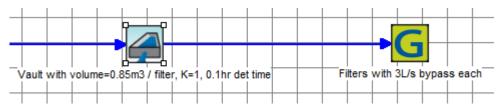
| Maintenance |
|-------------|
| performed |
| during |
| monitoring |

None over 13 months

Verified method to model in MUSIC

Modelling a SPELFilter in MUSIC is as follows:

- 1. Use a detention basin node to represent the vault (with modified 'K' values and nominal detention time set to the treatment flow rate of the cartridges)
- 2. Use a generic node with the monitored pollutant reduction values and have a high flow bypass of 3 L/s per cartridge.



- The input criteria for the node is;
- 1. Use a detention basin node to represent the vault
 - with modified 'K' values with K=1
 - use size of 1m² per cartridge and 0.85m extended detention depth
 - adopt a nominal detention time of 0.1 hours (plus or minus 10%).
- 2. Use a generic node with:
 - a high flow bypass of 3 L/s per cartridge
 - pollutant reductions of 85% for TSS
 - pollutant reductions of 74% for TP
 - pollutant reductions of 59% for TN.

When entering the data into MUSIC the detention basin surface area and high flow bypass rate of the generic node is factored up depending on the number of filter cartridges proposed. All other values listed above remain the same (note: the *Notional Detention Time* is adjusted by changing the *Low Flow Pipe Diameter*).

Conditions

The limitations of the acceptance of these claims include:

- Pit insert "Stormsacks" (for coarse material capture) are used for inlets upstream of the SPELFilter installation to ensure longevity of the filters
- Regular inspection & maintenance should be performed in accordance with the Manufacturer's Maintenance Plans.

| Independent |
|-------------|
| Reviewers |

Dr Robin Allison

Dr Ricky Kwan

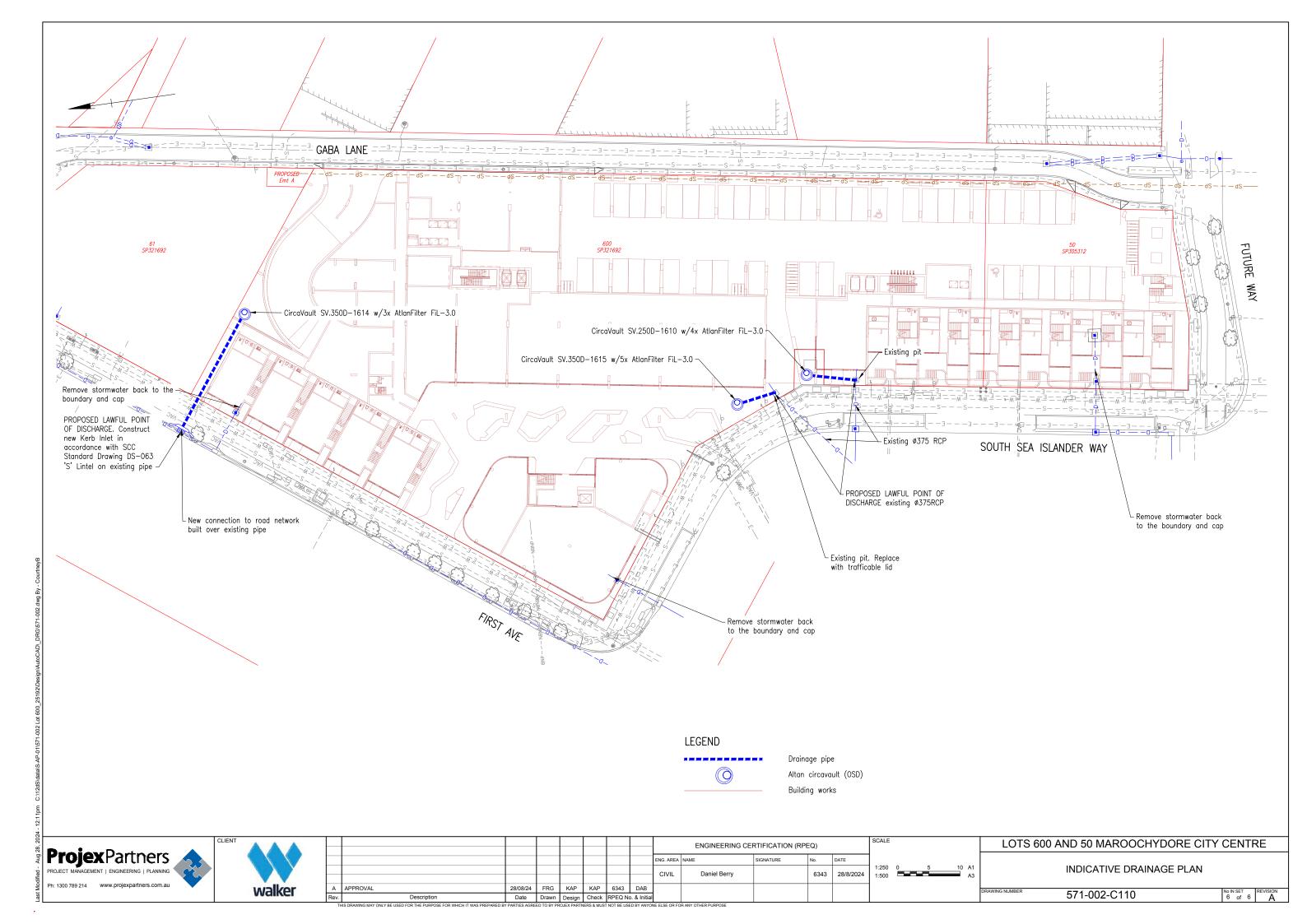


| Accepted by Governance Panel | 22 December 2022 |
|--|------------------|
| Accepted by Stormwater Australia Board | 23 December 2022 |



APPENDIX F

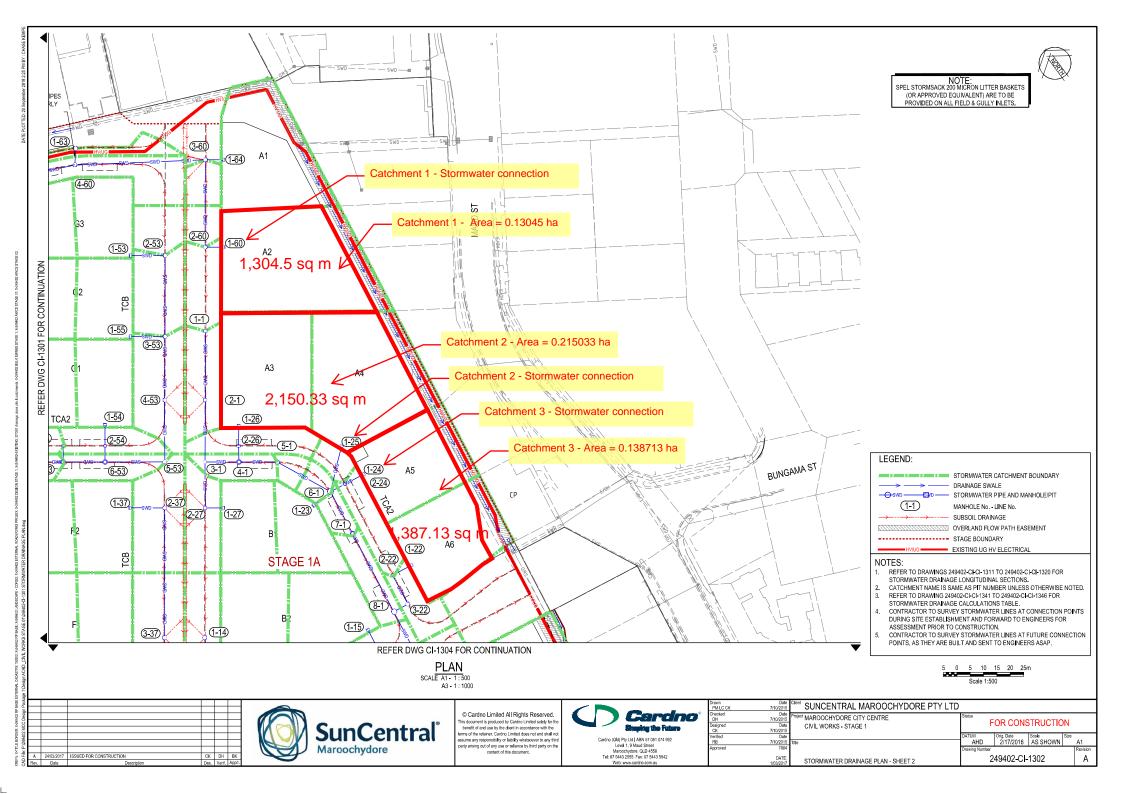
Indicative Drainage Layout





APPENDIX G

MUSIC modelling catchments (proposed development)





APPENDIX H

AltanFilter Manual

OPERATION & MAINTENANCE MANUAL

AtlanFilter

(Formerly SPELFilter)





CONTENTS

| Introduction | 3 |
|-------------------------------------|----|
| Features | 4 |
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| System Configuration | 7 |
| Health and Safety | 8 |
| Maintenance frequency | 10 |
| Maintenance Procedure | 11 |
| General Cleaning | 12 |
| Cartridge Recycling and Replacement | 13 |
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| Site Evit and Clean Lin | 16 |





INTRODUCTION

Understanding how to correctly and safely maintain the AtlanFilter (formerly SPELFilter) is essential for the preservation of the filter's condition and its operational effectiveness. The AtlanFilter is a highly engineered stormwater filtration device designed to remove sediments, heavy metals, nitrogen and phosphorus from stormwater runoff.

The filters can be housed in either a concrete or fibreglass structure that evenly distributes the flow between cartridges.

Flow through the filter cartridges is gravity driven and self-regulating, which makes the AtlanFilter system a low maintenance, high performance stormwater treatment device.

This guide will provide the necessary steps that are to be taken to correctly and efficiently ensure the life of the AtlanFilter product.





Figure 1 - AtlanFilters in a concrete chamber / vault

FEATURES

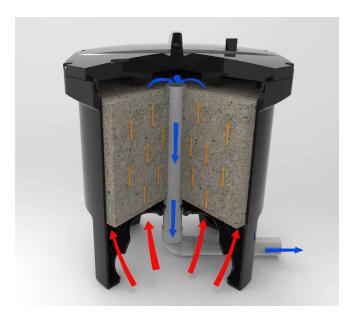


Figure 2 - Diagram of water flow through AtlanFilter

The AtlanFilter has a patented design that facilitates influent flow over the entire surface area of the media, providing consistent pollutant removal within a small footprint.

The AtlanFilter provides highly effective media filtration using gravity flow conditions, without the need for moving parts or floating valves. This eliminates the risk of mechanical failure, such as stuck valves and seizing components during its service life. This provides highly robust treatment performance.

Hydraulic head provided by a suitably sized weir in the filter vault forces stormwater through the filter media via the inlet ports underneath the filter cartridge.

Refer to the table below for minimum head required for the AtlanFilter cartridges to assist in sizing the weir.

The water to be treated enters the AtlanFilter cartridge via an upwards direction as the water level builds up around the AtlanFilter. This 'up flow' reduces the amount of sediment that could enter the media cartridge, as the sediment is allowed to drop to the vault floor under gravity. Any remaining sediment in the water is introduced through the filter media under hydraulic pressure and is filtered.

Water is filtered through the media, where dissolved and particulate Total Nitrogen and Total Phosphorus are removed via reaction with the media, in addition to the removal of Total Suspended Solids / sediment.

AtlanFilter Media Self-Backwash feature

A one-way air release valve located at the top of the filter cartridge allows air to escape as the cartridge fills up with water. This creates a siphonic flow condition as the air is completely evacuated from inside the AtlanFilter cartridge. Siphonic flow conditions are maintained until such time the water level outside of the cartridge falls beneath the inlet ports underneath the filter. At this moment, the water level inside the AtlanFilter cartridge is higher than the surrounding water level.

The water inside the AtlanFilter cartridge is then expelled upon the break of the siphon, and the water flows down and out of the inlet ports under gravity, onto the vault floor.

This is a highly effective backwash of the media and allows the expulsion of a high proportion of sediment out from the AtlanFilter media. The expelled sediment can be removed either manually or with a vacuum from the vault floor.

This backwash effect allows the media to remain highly conductive and is the key to the industry leading longevity of the AtlanFilter cartridge system, which does not need replacement for at least 5 years, and typically will achieve up to 6-8years of service, subject to the AtlanFilter being regularly maintained in accordance with this guideline and in accordance with the specific needs of the catchment.



Figure 3 - Typical Outlet Weir Wall

FEATURES

Self Supporting Feet

Each AtlanFilter cartridge stands on 4 feet, which negates the need for the construction of a false floor in the vault. The feet are bolted to the vault floor with the supplied stainless steel angles and M10 bolts. The feet allow a clear height from the vault floor up to the inlet ports of 240mm. The absence of a false floor allows plenty of room for backwashed sediment to evacuate from underneath the cartridges and thereby avoid blocking the inlet ports to the AtlanFilter from sediment buildup. It is for this reason that Atlan recommended the sediment buildup not exceed 150mm above the vault floor, so as to avoid blocking the inlet ports of the AtlanFilter. Blockage of the inlet ports due to sediment accumulation in the vault floor will cause the AtlanFilter to go into bypass and be ineffective. Hence it is important to keep up to date with monitoring and maintaining the AtlanFilter vault.



Figure 4 - Bolting the feet.



Figure 5 - Underside of the AtlanFilter showing the screened inlet ports and the connection for the outlet pipe in the middle.



Figure 6 - the top of the AtlanFilter showing the location of the one way air valve.

SIZES

Atlan Stormwater manufactures two height cartridges for varying site constraints as shown below. Each cartridge is designed to treat stormwater at a flow rate of 1.5 litres per second and 3.0 litres per second for the half height cartridge (model no. FIL-1.5) and full-height cartridge (model no. FIL-3.0) respectively.

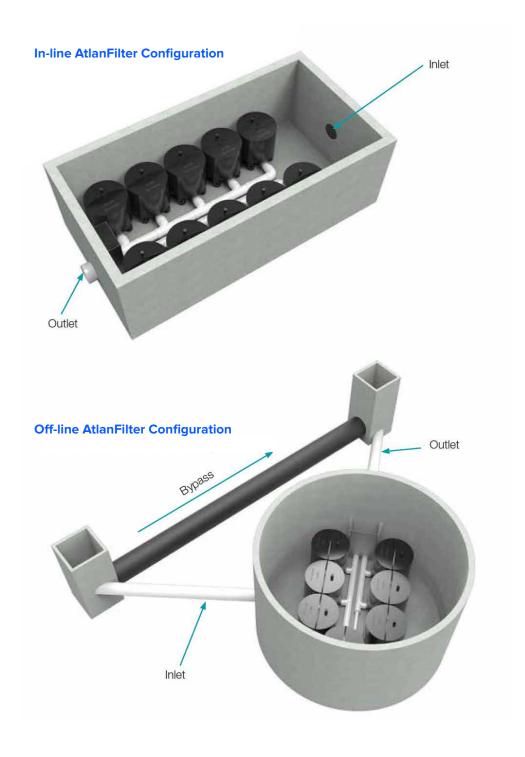
| | Full Height FIL-3.0 | Half Height FIL-1.5 |
|---|---------------------|---------------------|
| AtlanFilter total height | 860mm | 660mm |
| AtlanFilter Diameter | 740mm | 740mm |
| Minimum Head required | 850mm | 550mm |
| Treatment flow rate | 3.0 L/s | 1.5 L/s |
| Height of inlet ports above vault floor | 250mm | 250mm |
| Filtered water collection pipe diameter | 50mm | 50mm |

AtlanFilter Full Height - FIL-3.0



SYSTEM CONFIGURATION

AtlanFilter cartridges are installed in concrete or fibreglass tanks commonly referred to as 'vaults'. The vault selection and configuration are based on site characteristics and/or constraints; computational stormwater quality modelling; and selected AtlanFilter models. Typical AtlanFilter system configurations are shown below.



HEALTH AND SAFETY

A. Personal health & safety

When carrying out the necessary installation operations of the AtlanFilter all contractors and staff personnel must comply with all current workplace health and safety legislation.

The below measures should be adhered to as practically as possible.

- Comply with all applicable laws, regulations and standards.
- All those involved are informed and understand their obligations in respect of the workplace health and safety legislation.
- Ensure responsibility is accepted by all employees to practice and promote a safe and healthy work environment.

B. Personal protective equipment/safety equipment

When carrying out the necessary installation operations of the AtlanFilter, wearing the appropriate personal protective equipment and utilising the adequate safety equipment is vital to reducing potential hazards.

Personal protective equipment / safety equipment in this application includes:

- Eye protection
- Safety apron
- · Fluorescent safety vest
- Form of skin protection
- · Puncture resistant gloves
- Steel capped safety boots
- · Ear muffs
- Hard hat/s
- Sunscreen

C. Confined space

In the event access is required into the vault, confined space permits will be required which is not covered in this Guide. Typical equipment required for confined space entry include:

- Harness
- · Gas detector
- Tripod
- Spotter

D. Traffic Control

It is not uncommon for Atlan Filter cartridges to be installed underneath trafficable areas. Minimum traffic control measures will need to be put in place in accordance with traffic control plans set out by respective local and state road authorities.



Vaults are to be treated as confined space.

Entry by permit only.



Monitor weather conditions prior to operation maintenance. Do not enter a vault during an episode of heavy rain as this can create a risk of drowning.

















MAINTENANCE FREQUENCY

The AtlanFilter's design allows for a greater life span when frequently maintenance. Maintenance is broken up into three categories which include:

- · Standard inspection
- General cleaning
- · Cartridge replacement.

Standard Inspection

Standard inspections are conducted at regular four month intervals. At this time, an approved trained maintenance officer or Atlan representative shall undertake all measures outlined in Maintenance Procedure, Standard Inspection.

General Cleaning

At the end of each standard inspection, trigger measures will identify if general cleaning is required.

General cleaning will need to be executed immediate during standard inspections if the follow triggers are satisfied:

- Build-up of debris/pollutants within the vault greater than 150mm;
- Accumulation of debris/pollutants on the outlet chamber of the AtlanFilter vault;
- After large storm events, tidal or flooding impacts at the request of the owner;

Cartridge Replacement

Stormwater treatment is dependent on the effectiveness of the AtlanFilter cartridge system. As the AtlanFilter ages, pollutants will inundate the cartridge and ultimately reduce the treatment flow rate. At this point, a AtlanFilter flow test apparatus will be utilities to determine if replacement cartridges are required.

Based on the [site] concept modelling (MUSIC) and previous industry experience, we estimate the life of the AtlanFilter to be between 6 - 8 years. As a minimum requirement, each AtlanFilter cartridge should be replaced within 10 years.

The life cycle of the AtlanFilter can be impacted if standard inspections and general maintenance is not undertaken in accordance with this operation and maintenance Guide.

Other factors that will affect the above life cycle of the AtlanFilter include:

- Installation of cartridge system during construction phase and impacted by construction sediment loads;
- Neglecting to install pre-treatment using an industry approved GPT or a surface inlet pit trash bag such as the Atlan StormSack.
- Unforeseen environmental hazards affecting the AtlanFilter functionality.

9

MAINTENANCE PROCEDURES

Stormwater pollutants captured and retained by the AtlanFilter system need to be periodically removed to ensure environmental values are upheld. All associated maintenance works is heavily dependent on the site's operational activities and generated stormwater pollutants. To ensure the longevity of the installed AtlanFilter treatment system, it is imperative that the procedures detailed in this Guide are followed and all appropriate measures are actioned immediately.

Standard inspection

The standard inspection requires personal experience of Atlan products to visual inspection the vault and filter conditions.

Confined space requirements may not be required if a full inspection and assessment of each AtlanFilter can be achieved at surface level without being deemed a confined space entry.

The standard inspection requires personal experience of Atlan products to visual inspection the vault and filter conditions.

Confined space requirements may not be required if a full inspection and assessment of each AtlanFilter can be achieved at surface level without being deemed a confined space entry.

Site Inspection Procedures

1. Implement pre-start safety measures

Ensure that the area in which operational works are to be carried out is cordoned off, to prevent unauthorised access. Adequate safety barriers must be erected.

Area in which work is to be carried out must be clean, safe and hazard free. (Refer to figure 4.)

2. Set-up gantry tripod above manhole

Assemble and position the gantry above the manhole safely and as practically as possible. Attach the winch or chain block to the gantry for lifting the Atlan Filters.

Perform safety procedures ie. Attach harnesses etc. (if confined space).

3. Open manhole lid

Once you have set up the Gantry and ensured that the area is safe to operate in, you can proceed to open the manhole lid, using lid lifters.

4. Conduct gas tests

(If tank is classed confined space)

Once the lids have been removed to a safe distance to prevent tripping, you must then proceed to conduct gas tests. Perform necessary gas tests according to the confined space regulations.

5. Once confined space has been deemed safe to operate in, enter tank safely

Once you have carried out the required gas test and the work area is deemed safe, you may then enter the pit via a ladder or winch system to assess the work area you will be operating in. Ensure all confined space

6. AtlanFilter system assessment

Perform a review of the AtlanFilter system using the AtlanFilter assessment report/checklist. Sign off and forward a copy of the report to property manager and Atlan representative.

7. Reinstate AtlanFilter system and disposal

At the completion of the site inspection, ensure the site is reinstated back to its initial state and all pollutants are removed from the site in line with pollutant disposal procedures.

8. Sign off and forward a copy of the report to property manager and Atlan representative

GENERAL CLEANING

Vacuum out of Filter tank, removal, and disposal of pollutants at the completion of a standard inspection, general cleaning may be deemed necessary immediately or scheduled for a future date. Steps undertaken for general cleaning should be in general accordance with the procedure outlined below but not limited.

1. Implement pre-start safety measures

Ensure that the area in which operational works are to be carried out is cordoned off, to prevent unauthorised access. Adequate safety barriers must be erected.

Area in which work is to be carried out must be clean, safe and hazard free. (Refer to figure 4.)

2. Set-up gantry tripod above manhole

Assemble and position the gantry above the manhole safely and as practically as possible. Attach the winch or chain block to the gantry for lifting the AtlanFilters.

Perform safety procedures ie. attach harnesses etc. (if confined space).

3. Open manhole lid

Once you have sent up the Gantry and ensured that the area is safe to operate in, you can proceed to open the manhole lid, using lid lifters.

4. Conduct gas tests

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Once the lids have been removed to a safe distance to prevent tripping, you must then proceed to conduct gas tests. Perform necessary gas tests according to the confined space regulations.

5. Once confined space has been deemed safe to operate in, enter tank safely

Once you have carried out the required gas test and the work area is deemed safe, you may then enter the pit via a ladder or winch system to assess the work area you will be operating in. Ensure all confined space

6. AtlanFilter system assessment

Perform a review of the AtlanFilter system using the AtlanFilter assessment report/checklist.

7. Pollutant removal from tank

Perform clean-up using a licenced vacuum truck contractor or wet/dry vacuum, depending on level of sediment built up and/or tank size.

8. Reinstate AtlanFilter system and disposal

At the completion of the site inspection, ensure the site is reinstated back to its initial state and all pollutants are removed from the site in line with pollutant disposal procedures.

9. Sign off and forward a copy of the report to property manager and Atlan representative

CARTRIDGE RECYCLING AND REPLACEMENT

AtlanFilter cartridges can be swapped out for new cartridges. The spent AtlanFilter cartridges can be collected from site and sent to Atlan Stormwater's facilities, where the spent media will be removed from the cartridge in factory conditions and disposed of in accordance with environmental regulations.

The AtlanFilter cartridge will be recharged with new media, thereby recycling and repurposing the cartridge.

AtlanFilter replacement procedures may vary depending on the configuration of the AtlanFilters, the type of vault and engineers' specs. Replacement instructions for manhole AtlanFilter systems and precast vault AtlanFilter systems are contained in this section.

At the completion of a standard inspection, AtlanFilter replacement may be deemed necessary immediately or scheduled for a future date. Steps undertaken for cartridge replacement should be in general accordance with the procedure outlined below but not limited.

1. Implement pre-start safety measures

Ensure that the area in which operational works are to be carried out is cordoned off, to prevent unauthorised access. Adequate safety barriers must be erected.

Area in which work is to be carried out must be clean, safe and hazard free.

2. Set-up gantry tripod above manhole

Assemble and position the gantry above the manhole safely and as practically as possible. Attach the winch or chain block to the gantry for lifting the AtlanFilters.

Perform safety procedures ie. attach harnesses etc. (if confined space).

3. Open manhole lid

Once you have sent up the gantry and ensured that the area is safe to operate in, you can proceed to open the manhole lid, using lid lifters.

4. Conduct gas tests

(If tank is classed confined space)

Once the lids have been removed to a safe distance to prevent tripping, you must then proceed to conduct gas tests. Perform necessary gas tests according to the confined space regulations.

5. Once confined space has been deemed safe to operate in, enter tank safely

Once you have carried out the required gas test and the work area is deemed safe, you may then enter the pit via a ladder or winch system to assess the work area you will be operating in. Ensure all confined space procedures are followed.

6. Remove exhausted cartridges

Disconnect all internal pipe work from inside the vault. Unbolt anti-floatation measures and remove cartridges from the vault using Gantry Tripod method.

7. Pollutant removal

Using a wet/dry vacuum or sucker truck, suck out all the residual pollutant from the vault.

8. Install pipework and AtlanFilters

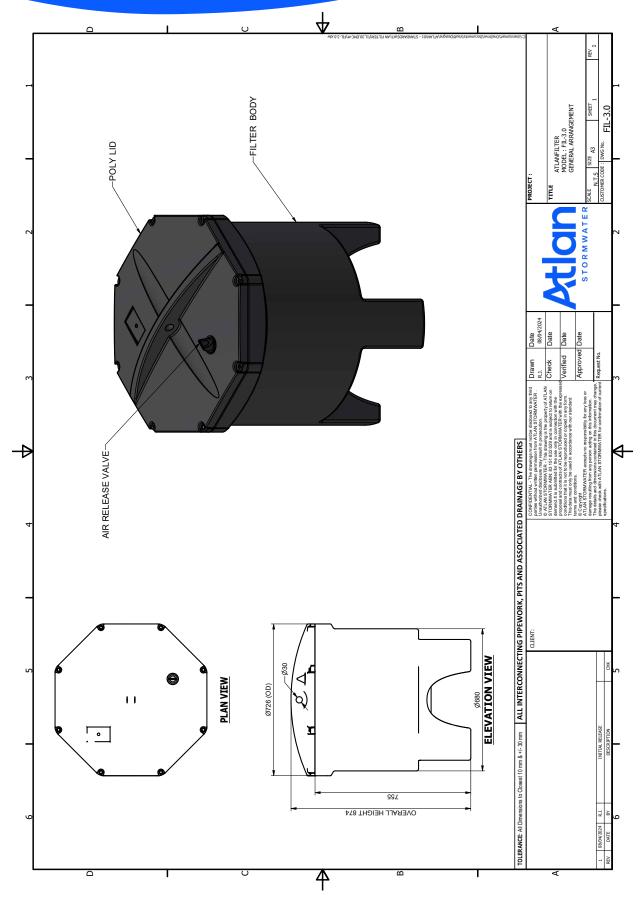
Please refer to the below standard install diagrams for the AtlanFilters. Then refer to your site specific drawings, as site requirements may require something different to the standard layout. Lower filters into tank, position into place, connect filter outlet pipework with the supplied fittings.

9. Install anti-floatation system

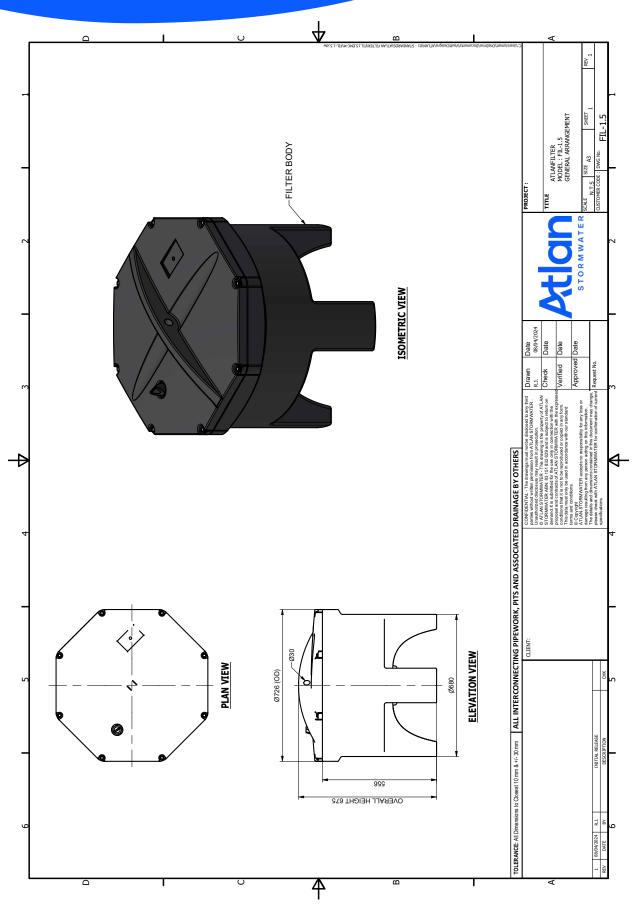
Please refer to the detailed drawings showing how the anti-floatation (anchor) bars are to be installed.

10. Sign off and forward a copy of the report to property manager and Atlan representative

Drawing Full Height



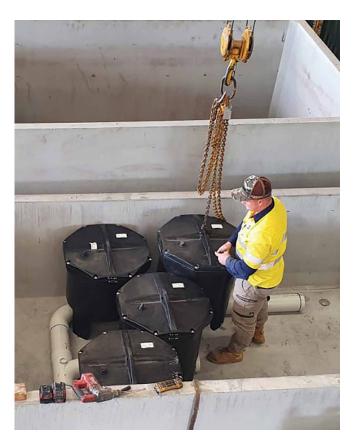
Drawing Half Height



SITE EXIT & CLEAN UP

At the end of the scheduled maintenance, approved contractors or Atlan maintenance crew are required to reinstate the site to pre-existing conditions. Steps included but limited to are:

- Ensure all access covers are securely inserted back into their frames;
- Remove and dispose collected pollutants from the site in accordance with local regulator authorities;
- Retrieve all traffic control measures and maintenance tools; and
- Return all exhausted and/or damaged Atlan products to Atlan Stormwater to begin recycling program.





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Joy in water

'We believe clean waterways are a right not a privilege and we work to ensure a Joy in Water experience for you, with your children and grandchildren.'

Andy Hornbuckle



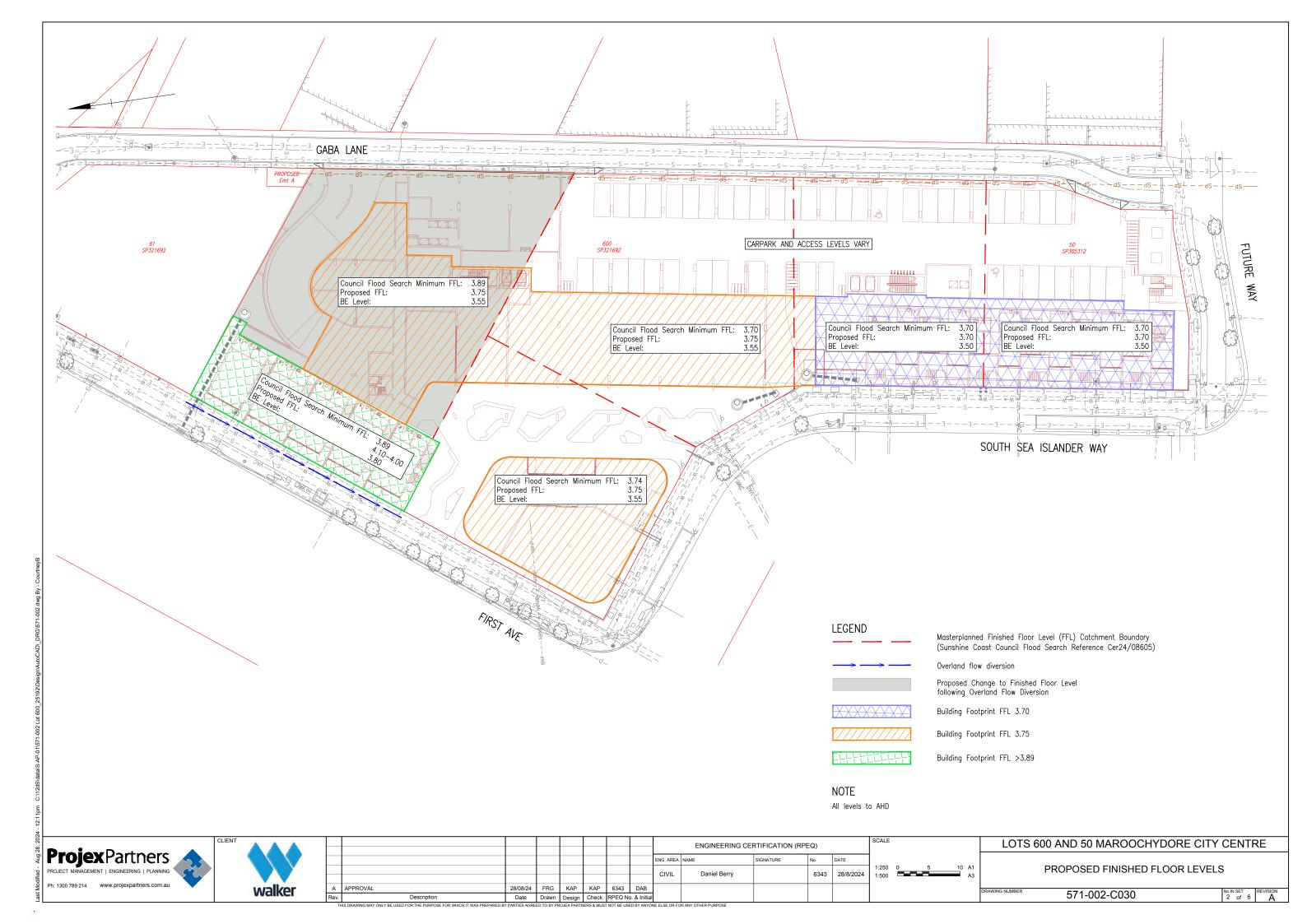


P 02 8705 0255 sales@atlan.com.au 100 Silverwater Rd, Silverwater NSW 2128 atlan.com.au



APPENDIX I

Proposed Finished Floor Levels





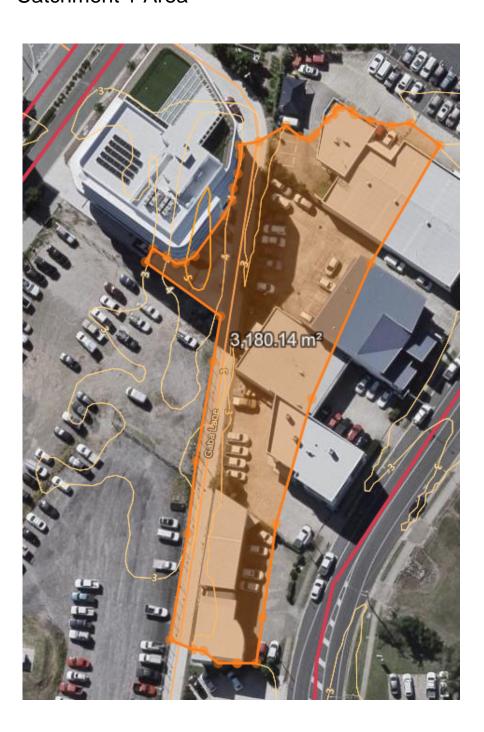
APPENDIX J

Gaba Lane Capacity Calculations

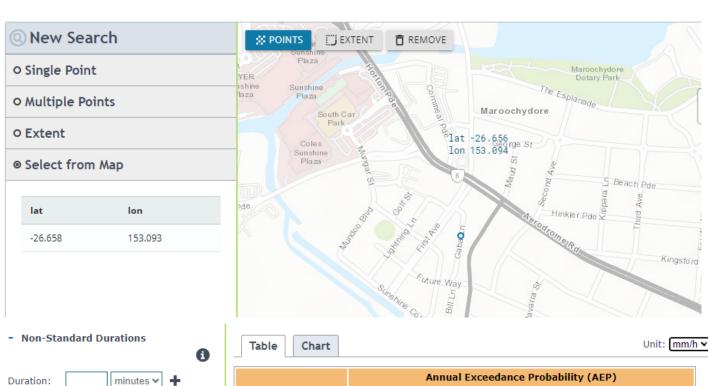


[571-002] Lot 600: Gaba Lane Drainage Calculations

Rational Calculation: Catchment 1 Area



Rational Calculation: IFD Rainfall Data (sourced from BoM)



| | | | • |
|-----------------------------|-------------|-----------|---|
| Duration: | mi | nutes 🗸 🛨 | |
| + Observe | d Rainfalls | | |
| Update | Reset | | |
| Other Optio | ons | | |
| ☐ Coefficier ☐ Seasonali | | | |
| Current Va | lues | | |
| Lahel | Latitude | Longitude | 2 |

-26.658

153.093

| | Annual Exceedance Probability (AEP) | | | | | | | | | |
|---------------|-------------------------------------|------|------|------|------|------|------|--|--|--|
| Duration | 63.2% | 50%# | 20%* | 10% | 5% | 2% | 1% | | | |
| 1 min | 176 | 197 | 264 | 309 | 353 | 410 | 453 | | | |
| 2 <u>min</u> | 149 | 168 | 228 | 271 | 315 | 376 | 425 | | | |
| 3 <u>min</u> | 140 | 157 | 214 | 253 | 293 | 347 | 391 | | | |
| 4 <u>min</u> | 133 | 150 | 203 | 239 | 275 | 324 | 362 | | | |
| 5 <u>min</u> | 127 | 143 | 193 | 226 | 260 | 304 | 338 | | | |
| 10 <u>min</u> | 104 | 117 | 156 | 181 | 206 | 238 | 262 | | | |
| 15 <u>min</u> | 88.2 | 98.8 | 132 | 153 | 174 | 201 | 221 | | | |
| 20 <u>min</u> | 77.0 | 86.3 | 115 | 134 | 152 | 176 | 194 | | | |
| 25 <u>min</u> | 68.6 | 76.9 | 103 | 120 | 136 | 158 | 174 | | | |
| 30 <u>min</u> | 62.1 | 69.6 | 93.1 | 109 | 124 | 144 | 160 | | | |
| 45 <u>min</u> | 49.0 | 55.1 | 74.2 | 87.3 | 100 | 117 | 131 | | | |
| 1 hour | 41.1 | 46.3 | 62.8 | 74.2 | 85.5 | 101 | 113 | | | |
| 1.5 hour | 31.8 | 36.0 | 49.4 | 58.8 | 68.3 | 81.2 | 91.4 | | | |
| 2 hour | 26.4 | 30.0 | 41.7 | 49.9 | 58.1 | 69.5 | 78.6 | | | |
| 3 hour | 20.4 | 23.3 | 32.8 | 39.6 | 46.4 | 55.9 | 63.4 | | | |
| 4.5 hour | 15.8 | 18.2 | 26.0 | 31.5 | 37.2 | 44.9 | 51.1 | | | |
| 6 hour | 13.3 | 15.3 | 22.1 | 26.9 | 31.8 | 38.5 | 43.9 | | | |
| 9 hour | 10.4 | 12.1 | 17.6 | 21.5 | 25.5 | 31.0 | 35.3 | | | |
| 12 hour | 8.75 | 10.2 | 15.0 | 18.3 | 21.8 | 26.5 | 30.2 | | | |
| 18 hour | 6.86 | 8.03 | 11.9 | 14.6 | 17.4 | 21.2 | 24.2 | | | |
| 24 hour | 5.76 | 6.75 | 10.0 | 12.3 | 14.7 | 18.0 | 20.7 | | | |
| 30 hour | 5.01 | 5.88 | 8.73 | 10.8 | 12.9 | 15.8 | 18.2 | | | |
| 36 hour | 4.46 | 5.23 | 7.78 | 9.61 | 11.5 | 14.2 | 16.3 | | | |
| 48 hour | 3.69 | 4.33 | 6.43 | 7.96 | 9.53 | 11.8 | 13.7 | | | |
| 72 hour | 2.78 | 3.25 | 4.83 | 5.98 | 7.18 | 9.01 | 10.5 | | | |
| 96 hour | 2.24 | 2.62 | 3.88 | 4.82 | 5.79 | 7.30 | 8.56 | | | |
| 120 hour | 1.88 | 2.20 | 3.26 | 4.04 | 4.85 | 6.13 | 7.21 | | | |
| 144 hour | 1.62 | 1.89 | 2.81 | 3.48 | 4.18 | 5.28 | 6.20 | | | |
| 168 hour | 1.43 | 1.67 | 2.47 | 3.06 | 3.67 | 4.62 | 5.41 | | | |

Rational Calculation: Fy and C10 value's (sourced from QDUM 2017 4th Edition)

Table 4.5.2 – Table of frequency factors

| AEP (%) | ARI (years) | Frequency factor (F_y) |
|---------|-------------|--------------------------|
| 63% | 1 | 0.80 |
| 39% | 2 | 0.85 |
| 18% | 5 | 0.95 |
| 10% | 10 | 1.00 |
| 5% | 20 | 1.05 |
| 2% | 50 | 1.15 |
| 1% | 100 | 1.20 |

Table 4.5.3 – Table of C_{10} values

| Intensity | | | Frac | tion impervi | ous <i>f_i</i> | | |
|---|-------------|------|------|--------------|--------------------------|------|------|
| (mm/hr) ¹ I ₁₀ | 0.00 | 0.20 | 0.40 | 0.60 | 0.80 | 0.90 | 1.00 |
| 39-44 | | 0.44 | 0.55 | 0.67 | 0.78 | 0.84 | 0.90 |
| 45-49 | .5.4 | 0.49 | 0.60 | 0.70 | 0.80 | 0.85 | 0.90 |
| 50-54 | Table 4.5.4 | 0.55 | 0.64 | 0.72 | 0.81 | 0.86 | 0.90 |
| 55-59 | | 0.60 | 0.68 | 0.75 | 0.83 | 0.86 | 0.90 |
| 60-64 | er to | 0.65 | 0.72 | 0.78 | 0.84 | 0.87 | 0.90 |
| 65-69 | Refer | 0.71 | 0.76 | 0.80 | 0.85 | 0.88 | 0.90 |
| 70-90 | | 0.74 | 0.78 | 0.82 | 0.86 | 0.88 | 0.90 |

Rational Calculation:

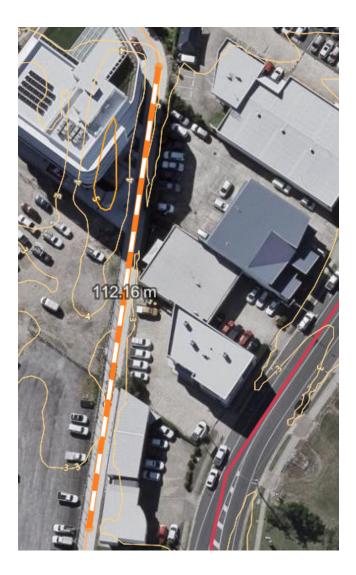
| 571-002 Lot 600 | | Gaba | Lane Drainage Calcul | ations | | | | |
|-----------------|---------------------|------|----------------------|---------------------|----------------------|-----------------|-------------------------------|---|
| | | | Catchment | Area (ha) | Impervious Area (ha) | | Pervious Area (ha) | % Impervious |
| Pre-Deve | eloped Calculations | | Catchment 1 | 0.318 | 0.318 | | 0.318 0.00 | |
| Fy (100) | 1hr, 10yr I (mm/hr) | C10 | C100 | Time of Conc (mins) | | 100yr I (mm/hr) | Q100 Peak Flow Rate (m3/s) | Q100 (20% Increase for Year 2100) m3/s |
| 1.20 | 74.2 | 0.90 | 1.00 | 5.0 | 5.0 338 | | 0.30 | 0.36 |

The 1% AEP of 0.4001 m3/s was adopted to account for climate change.

Extracted from attached excel calculation spreadsheet (571-002 Gaba Lane Rational Calculations).

Manning's Calculation: channel length and width

Length:

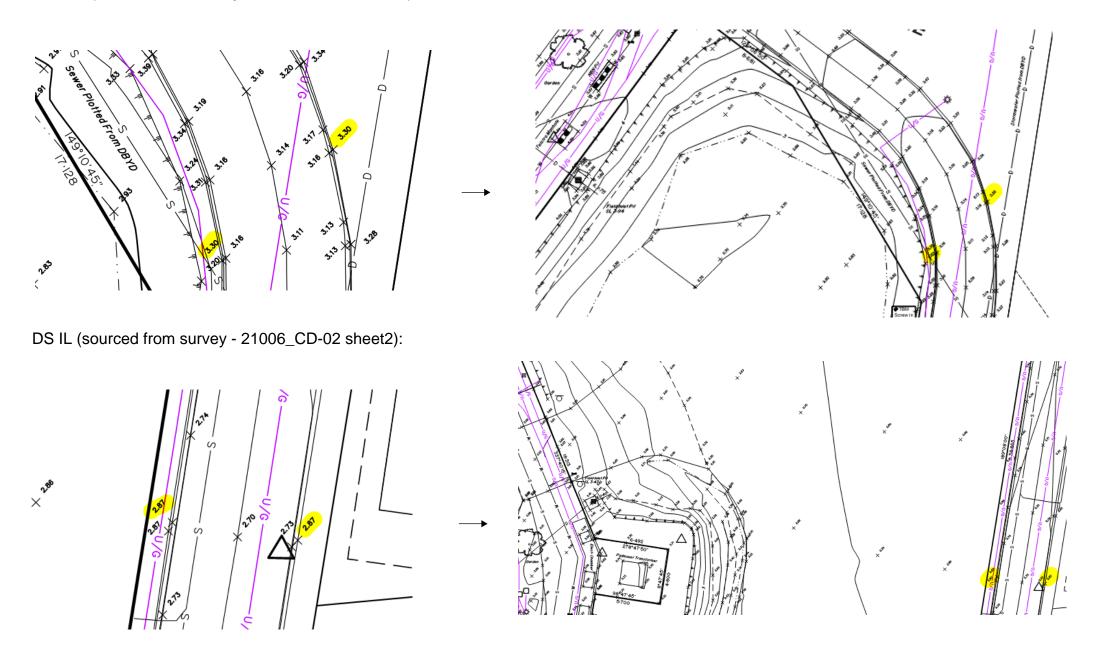


Width:



Manning's Calculation: US and DS IL

US IL (sourced from survey - 21006_CD-02 sheet1):



Manning's Calculation: manning's "n" (sourced from QDUM 2017 4th Edition)

Manning's "n":

Table 7.16.3 – Recommended values for surface roughness (average pipe condition)

| Type of pipe | Manning's <i>n</i> |
|------------------------------------|--------------------|
| Reinforced concrete (RCP and RCBC) | 0.013 |
| Fibre reinforced cement (FRC) | 0.013 |
| UPVC | 0.011 |
| GRP | 0.011 |

Manning's Calculation:

| | SWA | ALE CAPACITY - Rec | tangular Cro | ss Section | 1 | | | | | |
|--|-------|--------------------|--------------|------------|---------|---------|------------|----------|---------|--------|
| DATIONAL FORMULAE | | | | | | | | | | |
| RATIONAL FORMULAE | 0.240 | L _ | | | 400.000 | | | | | |
| Catchment Area | 0.318 | | | | 100.000 | - | 0.00 | ٠ | | |
| Rainfall Intensity | | mm/h | 1 | c= | 5.00 | min | (Kinematic | Wave Equ | uation) | |
| Coefficent of Discharge | 1.00 | | | JS IL | 3.300 | | | | | |
| Flow in Qumecs | 0.30 | | | DS IL | 2.870 | | | | | |
| Pipe Flow | 0.000 | | | _ength | 112.080 | m | | | | |
| Therefore Required Swale Capacity | 0.30 | | | | | | | | | |
| Therefore Required Swale Capacity (including cli | 0.36 | | | Kinematic | Wave E | quation | | | | |
| Rectangular Channel | | | | | | | | | | |
| Total Width | 4.120 | | Length (m) o | f flowpath | | m | US IL | | | |
| | | | Slope of C | atchment | | m/m | DS IL | | | |
| Maximum Flow Depth (m) | 0.15 | Averag | ge Hortons R | oughness | | | | | | |
| Mannings "n" | 0.01 | | Rainfall | Intensity | | | | | | |
| Longitudinal Grade (S, m/m) | 0.00 | | | | | | | | | |
| Effective Channel Flow Area (A, m2) | 0.62 | | | | | | | | | |
| Wetted Perimeter (P, m) | 4.42 | | | | | | | | | |
| Hydraulic Radius (R=A/P, m) | 0.14 | | - | | | 4.12m | | | > | |
| Average Flow Velocity (V, m/s) | 1.3 | Freeboard | 1 | | | | | | 1 | |
| | | = .m | 1 🗼 | | | | | | | Depth |
| Channel Capacity (Q=V.A, m3/s) | 0.81 | | | | | | | | | = .15r |
| Additional Freeboard (m) | 0.00 | Flow Depth | | | | | | | | |
| | | = .15m | | | | | | | - V | |
| Total Channel Depth (inc. Freeboard) (m) | 0.15 | | V | | | | | | | |
| Base Width (m) | 4.12 | | | | | | | | | |
| | | | | | | | | | | |
| | | THIS CHAN | NEL HAS SU | FICENT | ΔΡΔΟΙΤΥ | | | | | |

Extracted from attached excel calculation spreadsheet (571-002 Gaba Lane Manning's Calculations).