### Northshore Hamilton PDA

Water Supply and Sewer Preliminary Analysis

**DSDMIP-EDQ-1502-19** 

Prepared for Economic Development Queensland

4 November 2020

PLANS AND DOCUMENTS referred to in the PDA DEVELOPMENT APPROVAL

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### **Table of Contents**

1	Introduc	tion	1
2	Assump	tions	2
	2.1	PDA Population	2
	2.2	Standards of Service	3
	2.3	Staging of Infrastructure	3
	2.4	Costing Parameters	3
3	Water S	upply Network Planning	4
	3.1	Water Supply Network Demands	4
	3.2	Urban Utilities Existing Infrastructure	4
	3.3	Urban Utilities Future Infrastructure	4
	3.4	Proposed PDA Water Supply Network	5
	3.5	Water Supply Modelling	5
	3.6	Water Supply Modelling Results	6
4	Sewerag	ge Network Planning	11
	4.1	Sewerage Network Loads	11
	4.2	Urban Utilities Existing Network	11
	4.3	Urban Utilities Future Network	11
	4.4	Proposed PDA Sewerage Infrastructure	11
	4.5	Sewerage Modelling	11
	4.6	Sewerage Modelling Results	12
5	Cost Est	timate	17
	5.2	Water Supply	18
	5.3	Sewerage	18
6	Conclus	ion	19
	6.1	Water	19
	6.2	Sewerage	19

### **Appendices**

APPENDIX A Population Figure and Table

APPENDIX B Proposed Road Infrastructure and Development Staging Plan

APPENDIX C SEQ Design Code Tables

APPENDIX D Water Infrastructure Plans

APPENDIX E Sewerage Infrastructure Plans

APPENDIX F Cost Estimate – Water and Sewerage



### **Tables**

Table 2-1	Water Supply and Sewerage Population Conversion Rates	2
Table 2-2	PDA Water Supply and Sewerage Population Summary	2
Table 3-1	Estimated Total Water Supply Demand	4
Table 3-2	Proposed PDA Water Supply Network	5
Table 4-1	Estimated Total Sewage Load	11
Table 5-1	Water Supply Infrastructure Unit Rates	17
Table 5-2	Sewerage Infrastructure Unit Rates	17
Table 5-3	Water Supply Infrastructure Capital Cost Estimate	18
Table 5-4	Northshore Hamilton PDA Proposed Sewerage Cost	18

### **Figures**

Figure 1-1 I	Location Plan of Northshore Hamilton PDA	1
Figure 3-1 I	Peak-Hour pressure results – Ultimate Scenario – Modelling completed by Cardno	7
Figure 3-2 I	Fire-flow residual pressure results – Ultimate Scenario – Modelling completed by Cardno	8
Figure 3-3 I	Peak-Hour pressure results – Ultimate Scenario – Model provided by Urban Utilities	9
Figure 3-4 I	Fire-flow residual pressure results – Ultimate Scenario – Model provided by Urban Utilities	10
Figure 4-1 I	Modelling Results within PDA – Ultimate Scenario – Modelling Completed by Cardno	13
Figure 4-2 I	Modelling Results for the Wider Network – Ultimate Scenario – Modelling Completed by Cardno	14
•	Longitudinal Profile – Existing Constrained Sewer – Remora Road (MH150847 to MH150845) – Ultimate Scenario	15
Figure 4-4 I	Longitudinal Profiles – Proposed Sewer Main Within PDA – Ultimate Scenario	16



### 1 Introduction

Cardno were engaged to review the water supply and wastewater augmentation strategy proposed for the Northshore Hamilton Priority Development Area (PDA). Figure 1-1 below illustrates the PDA.

This report adopts the servicing strategy presented in the Sewer and Water Investigation and Masterplan for the Northshore Hamilton Redevelopment (Bornhorst and Ward, November 2018) report as the basis of the assessment. Cardno's report will, where necessary, revise any strategies and infrastructure accordingly.

All water supply and sewerage network models were provided by Urban Utilities for this assessment.



Figure 1-1 Location Plan of Northshore Hamilton PDA

**LEGEND** 



PDA Boundary



### 2 Assumptions

### 2.1 PDA Population

The PDA includes a mix of residential, commercial/industrial and green space land uses. Urban Utilities use an Equivalent Person (EP) for the basis of water supply and sewerage network planning. The current yield for the PDA, and Urban Utilities EP conversion rates were used to develop the water supply and sewerage EP for the PDA, refer Table 2-1. Table 2-2 details the water supply and sewerage EP projected for the PDA.

Appendix A, Figure 201 illustrates the land use distribution within PDA and Appendix A Figure 305 shows the population and yield details. Development staging is outlined in Appendix B Figure 306.

Table 2-1 Water Supply and Sewerage Population Conversion Rates

Planning Scheme Use Type	Value	Units	Use	Document	Reference
Attached Dwelling	1.79	EP/ET	Residential	SEQCODE	Table A6 (Pg. 43)
Detached Dwelling	2.65	EP/ET	Residential	SEQCODE	Table A6 (Pg. 43)
Multi-Purpose Centers - Suburban Centre M3	65	EP/Ha	Retail/Commercial	Urban Utilities advice 05/05/14 <sup>1</sup>	(Bornhorst and Ward, November 2018)
General Industry	65	EP/Ha	Community	Urban Utilities advice 05/05/14 <sup>1</sup>	(Bornhorst and Ward, November 2018)
Community Facilities	65	EP/Ha	Industrial	Urban Utilities advice 05/05/14 <sup>1</sup>	(Bornhorst and Ward, November 2018)

Note: 1 - Adopting Urban Utilities advice from 05/05/2014 for *Multi-Purpose Centres* - Suburban Centre M3, General Industry and Community Facilities imposes a relatively minor 8% increase in total population.

Table 2-2 PDA Water Supply and Sewerage Population Summary

Land Use	EP
Residential	24,820
Retail	454
Commercial	2,689
Community	103
Industrial	2,159
TOTAL	30,224

### 2.1.2 Comparison with Past Planning

The population developed for this assessment are consistent with the population presented in Bornhorst and Ward, 2018 report. No modification or change is proposed or required.



### 2.1.3 Northshore Hamilton PDA Growth

The 2018 report by Bornhorst and Ward projected a population of 8,269 EP, 11,217 EP and 30,214 EP for the existing, 2031 and Ultimate scenarios respectively. The newly derived existing and ultimate EP is 5,000 EP and 30,225 EP respectively. The Ultimate EP within PDA is almost equal to the projections in the 2018 Bornhorst and Ward report.

### 2.2 Standards of Service

The South East Queensland Water Supply and Sewerage Design and Construction Code (SEQ WS&S D&C Code) has been adopted for assessment. This is included in Appendix C Figure 307.

The following additions and exceptions have been adopted:

- Gravity Sewers (NuSewer):
  - Depth of Flow, PWWF: Existing gravity sewers must maintain PWWF depth no greater than
     1.2m from ground level
  - Minimum Shear stress: Proposed sewers shall achieve self-cleansing shear stress of 1.6Pa at PDWF. This is in lieu of minimum velocity requirements outlined in SEQ Code, but consistent with WSA02-2014.

### 2.3 Staging of Infrastructure

Water supply and sewerage infrastructure has been assumed to be delivered following the sequence of development, i.e. Stage 2 (2022-2026), Stage 3 (2026-2031), and Stage 4 (post 2031), refer Appendix B Figure 306.

However, where necessary the staging of water and sewer infrastructure has been brought forward to coincide with planned roadworks to optimise delivery.

### 2.4 Costing Parameters

Cardno have adopted standard unit rates which have been previously developed by Cardno via benchmarking and recent construction costs. These rates have been used to determine capital works costs for the augmentations identified within this report. The adopted rates are nominal and represent an indicative cost as at 2016. However, the costs developed for this report would require updating with up to date data for each new budget year.

The indicative total costs include:

- > Project management and design costs (13%)
- Construction Contingency (25%)



### 3 Water Supply Network Planning

This section identifies the inputs and results of the water supply network modelling and planning for the Northshore Hamilton PDA.

### 3.1 Water Supply Network Demands

The projected demand within the Northshore Hamilton PDA was compared to that in the Urban Utilities network model. The Urban Utilities model projects an ultimate population of 22,173 EP within the PDA compared to the projected 30,224 EP for this report, representing a 36% increase. This increase will be assessed to determine the need for additional network augmentation.

Based on the adopted design criteria, Table 3-1 below shows a summary of the projected water supply demand within the PDA.

Table 3-1	Estimated T	⁻otal Water	Supply	Demand
-----------	-------------	-------------	--------	--------

Zoning	Water Demand (EP)	Average Day (L/s)	Maximum Day (L/s)	Maximum Hour (L/s)
Residential	24,820	74.7	140.8	272.9
Retail	454	1.37	2.57	3.54
Commercial	2,689	8.09	15.25	20.98
Community	103	0.31	0.58	0.80
Industrial	2,159	6.50	12.24	16.84
TOTAL	30,224	91	171.4	315.1

### 3.2 Urban Utilities Existing Infrastructure

The Northshore Hamilton PDA is located within the Bartley's Hill Reservoir Water Supply Zone (WSZ) which is supplied by Bartley's Hill Reservoir with a capacity of 19 ML. The existing trunk network including the DN300/315 main along Kingsford Smith Drive will supply the site.

### 3.3 Urban Utilities Future Infrastructure

The model provided by Urban Utilities included an extract of the Barley's Hill WSZ. The provided model included future population scenarios but only existing infrastructure. No augmentations have been identified outside of the PDA.

Network planning for the wider zone will be undertaken by Urban Utilities. The model is considered appropriate for assessing the network performance internal to the PDA. However, no assessment has been made of the impact of the PDA upon the future external network as this is not viable without UU's planned network augmentations.



### 3.4 Proposed PDA Water Supply Network

The proposed network includes a connection to the existing network along Kingsford Smith Drive, Theodore Street, Fison Avenue, Links Avenue, and MacArthur Avenue.

It should be noted that the proposed network, Appendix D, Figure 202 and Figure 203 is representative at this time. Further detailed assessment during the next stages of planning and design should confirm:

- > the alignment of mains with consideration to other services,
- > the location of valves, with consideration to maintaining service during planned and un-planned shutdowns, and
- > the location of service connections and other fittings (hydrants etc) not considered at this stage

Further, it is recommended that detailed geotechnical assessment is undertaken to ensure all mains are appropriately designed and installed with due consideration to the known poor-quality ground conditions within the PDA.

The proposed infrastructure and staging within the PDA are illustrated in Appendix D Figures 202 and Figure 203 and detailed in Table 3-2.

Table 3-2 Proposed PDA Water Supply Network

Diameter (DN -mm)	Length (mm)
180	2,470
250	991
315	1,151
355	326
450	304

### 3.5 Water Supply Modelling

Water Supply modelling was undertaken to confirm the water supply infrastructure required to service the Northshore Hamilton PDA. WaterGEMS simulations were undertaken for base and Ultimate scenarios. Only a steady state simulation of the maximum hour design flow was undertaken for the PDA network.

### 3.5.1 Water Model

Urban Utilities provided the following Bentley's WaterGEMS water supply model for assessment:

- BRH2.wtg received on 28 Aug 2019.

### 3.5.2 Model Set-up

The following updates are undertaken in the planning model provided by Urban Utilities:

- Proposed water supply pipes within the PDA have been added to the model (Appendix D Figures 202 and Figure 203)
- Water supply pipes proposed to be decommissioned within the PDA have been removed from the model (Appendix D Figures 202 and Figure 203 show the decommissioned mains)
- Previous load allocations within the PDA have been removed from the model
- Fire-flow demand has been allocated within the PDA based upon proposed land use zones. Although
  the PDA technically 'Brownfield', Greenfield fire-flow demands have been applied where network
  augmentations are proposed.
  - Low Density Urban = 25 L/s (Greenfield)
  - Medium Density Urban = 45 L/s (Greenfield)
  - High Density Urban = 60 L/s
  - Commercial/Industrial 45 L/s (Greenfield) and 30 L/s (Brownfield)
- Residual pressure has been set as 12m minimum in the main as per design criteria.



### 3.6 Water Supply Modelling Results

Results from modelling completed by Cardno, for the ultimate planning horizon have been outlined below with results from the model provided by Urban Utilities for comparison.

### 3.6.1 Peak Hour Results

Modelling has shown that the proposed network for the PDA will maintain minimum pressures within the PDA during peak hour, refer Figure 3-1.

Deficiencies were observed within the wider water supply zone during peak hour in the model provided by Urban Utilities and the modelling completed by Cardno, refer Figure 3-3 and Figure 3-1 respectively. Peak Hour performance of the proposed network within the PDA will not be adversely impacted by Urban Utilities augmenting the water supply zone capacity to resolve network deficiencies external to the PDA.

### 3.6.2 Fire-flow Results

Modelling has shown that the proposed network for the PDA maintain minimum pressures within the PDA during fire flow, Figure 3-2.

The model provided by Urban Utilities does not define the fire flow requirements outside of the PDA. Allocating appropriate fire flow loading to the wider water supply zone is beyond the scope of this assessment and has not been completed.

Fire flow performance of the proposed network within the PDA will not be adversely impacted by Urban Utilities augmenting the water supply zone capacity to resolve network deficiencies external to the PDA.

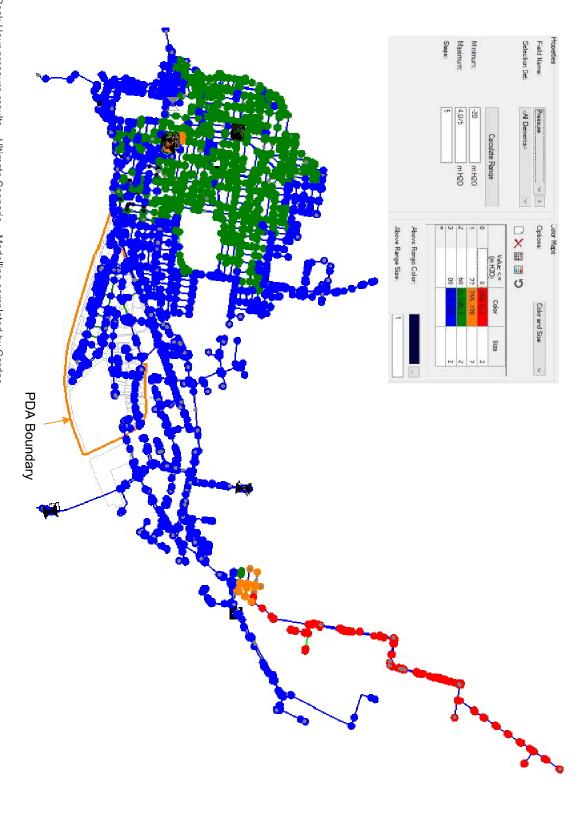
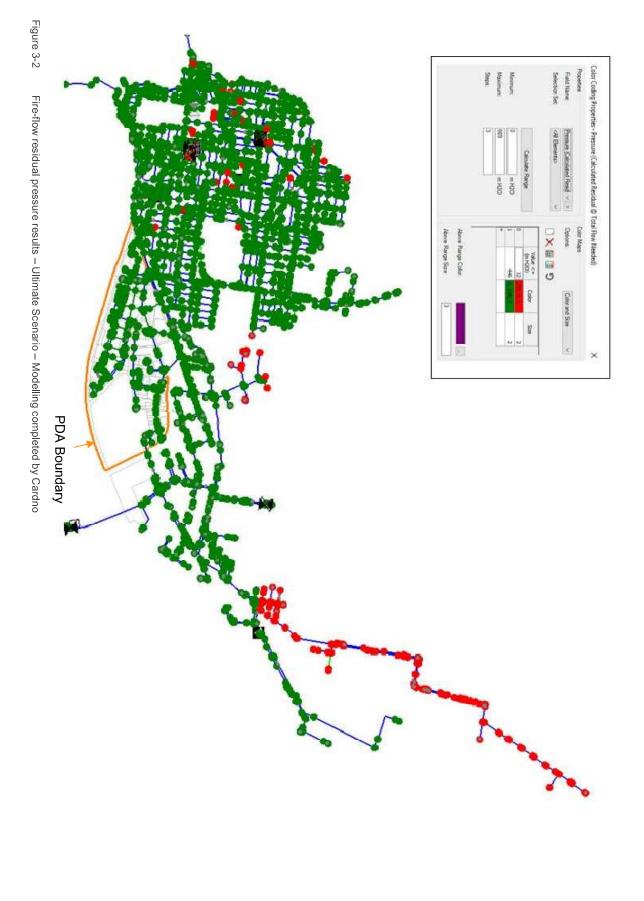
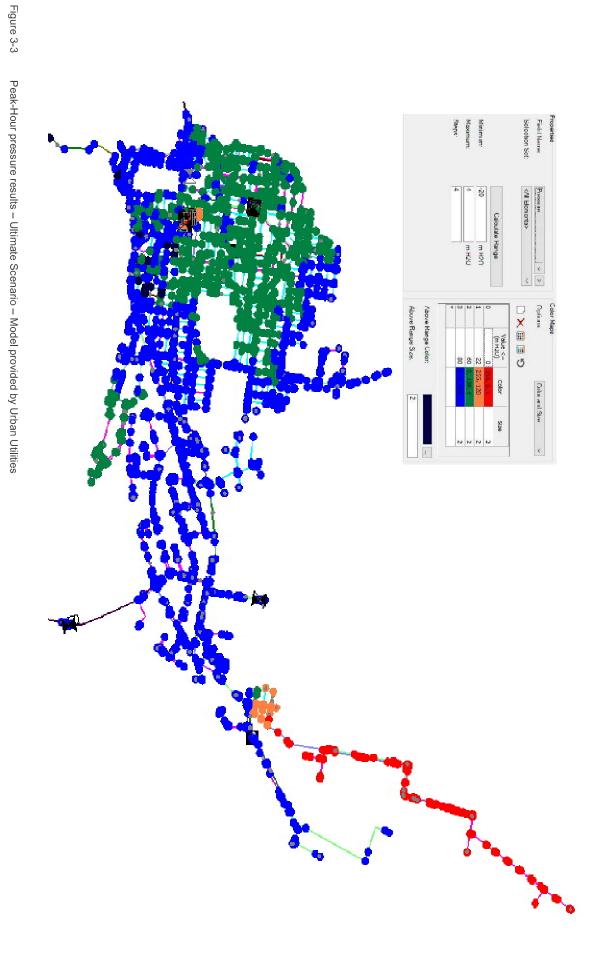


Figure 3-1 Peak-Hour pressure results – Ultimate Scenario – Modelling completed by Cardno

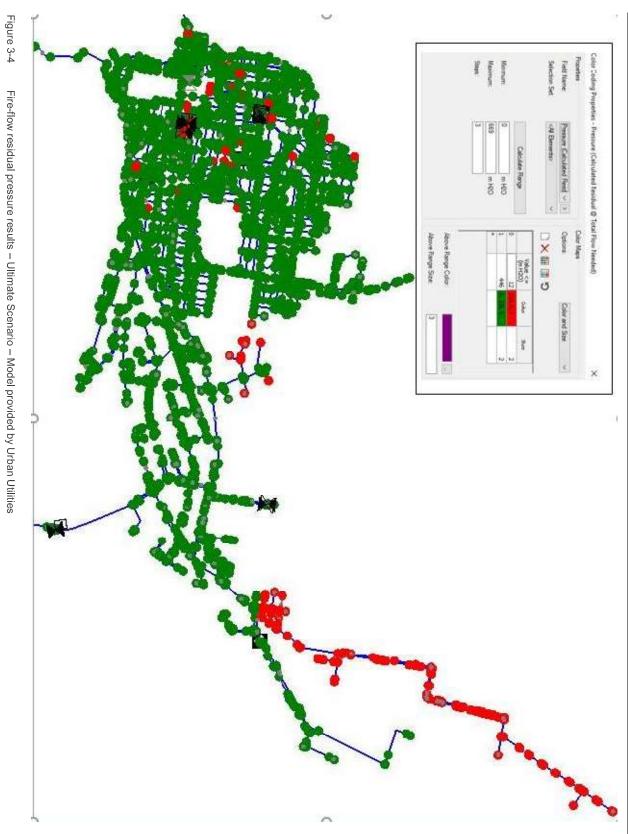




DSDMIP-EDQ-1502-19 | 4 November 2020 | Commercial in Confidence



DSDMIP-EDQ-1502-19 | 4 November 2020 | Commercial in Confidence



DSDMIP-EDQ-1502-19 | 4 November 2020 | Commercial in Confidence



### 4 Sewerage Network Planning

### 4.1 Sewerage Network Loads

The projected demand within the Northshore Hamilton PDA was compared to that in the Urban Utilities network model. The Urban Utilities model projects an ultimate population of 22,184 EP within the PDA compared to new projected 30,225 EP within the same area, representing a 36% increase.

Based on the adopted design criteria, the Table 4-1 below shows a summary of the projected sewage load within the PDA.

Table 4-1 Estimated Total Sewage Load

Sewage Load (EP)	Average Dry Weather	Peak Dry Weather	Peak Wet Weather Flow,
	Flow, ADWF (L/s)	Flow, PDWF (L/s)	PWWF (L/s)
30,225	73.5	113.7	239.6

### 4.2 Urban Utilities Existing Network

The Northshore Hamilton PDA is located within the Luggage Point Wastewater Treatment Plant (WWTP) catchment. Urban Utilities administers the wastewater conveyance and treatment.

Presently, the PDA is serviced by a number of gravity connections to the external network and existing pump station SP164.

All loads from the PDA are conveyed to the S1 trunk sewers DN1400 along Kingsford Smith Drive and onwards to the Luggage Point WWTP.

### 4.3 Urban Utilities Future Network

The provided model included future population scenarios but only existing infrastructure. No augmentations have been identified outside of the PDA. Network planning for the wider catchment will be undertaken by Urban Utilities.

### 4.4 Proposed PDA Sewerage Infrastructure

All sewers within the PDA have been planned as Nusewers. The proposed infrastructure and staging within the PDA are illustrated in Appendix E Figures 301 and Figure 302. Grades for proposed sewers are outlined in Figure 4-4.

It should be noted that the proposed network is representative at this time. It is recommended that detailed geotechnical assessment is undertaken to ensure all mains are appropriately designed and installed with due consideration to the known poor-quality soil conditions within the PDA.

### 4.5 Sewerage Modelling

### 4.5.1 Sewerage Model

Urban Utilities provided the following InfoWorks ICM sewer model for assessment:

 S1 Luggage Pt and S2 Fairfield WW Models.icmt received on 28 Aug 2019. This model has been adopted for assessment.

### The model:

- > Has been adopted and modified by Cardno for this assessment
- > Includes various load scenarios with the existing sewer network
- > Does not include the planned augmentations (as confirmed by Urban Utilities)
- > Does not include InfoWorks ICM Wastewater or previous Runs



### 4.5.2 Model Set-up

In the above model, the following updates are done:

- Proposed sewers within the PDA have been added to the model (Appendix E Figures 301 and Figure 302)
- Sewers proposed to be decommissioned within the PDA have been removed from the model (Appendix E Figures 301 and Figure 302 show the decommissioned sewer mains)
- Proposed loads within the PDA have been added to the model
- Previous load allocations within the PDA have been removed from the model
- A wastewater group was created with a PWWF unit flow of 750L/EP/d. This results in a PWWF from the total PDA area consistent with the method outlined in SEQ Code, refer Section 2.1.

### 4.6 Sewerage Modelling Results

Results from modelling completed by Cardno for the Ultimate planning horizon have been outlined below.

Modelling completed by Cardno shows, the Ultimate PWWF water depth with in the PDA sewer network maintains design service standards, refer Figure 4-1. The key outcomes are:

- Proposed sewers within the PDA maintain PWWF within <75% pipe full</li>
- Existing sewers within the PDA maintain PWWF flood depth no greater than 1.2m from ground level in accordance with Standards of service. More specifically, only one sewer exceeds pipe capacity but this is only marginal, refer Figure 4-3.

Figure 4-4 shows the longitudinal profiles of the proposed sewer mains within the PDA.

Outside the PDA, some surcharges occur in the network, refer Figure 4-2. These sewer sections are shown in RED and represent locations where the sewage depth is greater than 1m below ground. These are expected as the model provided by Urban Utilities does not include augmentations to cater for future growth.

There are no network performance non-compliances within close proximity to the PDA.

The impact of the PDA on the S1 trunk sewer and greater external network is not able to be determined with the model provided by Urban Utilities as it does not include future planned augmentations to the upstream network. Notwithstanding, it is Cardno's opinion that the loads from the PDA should not have a material impact to the S1 trunk system given the relatively large scale of the S1 system compared with the relatively small loads from the PDA.

Liaison with Urban Utilities should be undertaken to ensure any augmentations in the vicinity of the PDA are compatible with the proposed network for the PDA.

There may be opportunity to decommission pump station SP164 in future when land parcels 44 and 50 develop post 2038 (as per zoning plan), refer Figure 4-1. These lands would be serviced by proposed gravity sewers located in the vicinity.



## Proposed Sewer - Curtin Ave West (NHMH11 to MH511828)

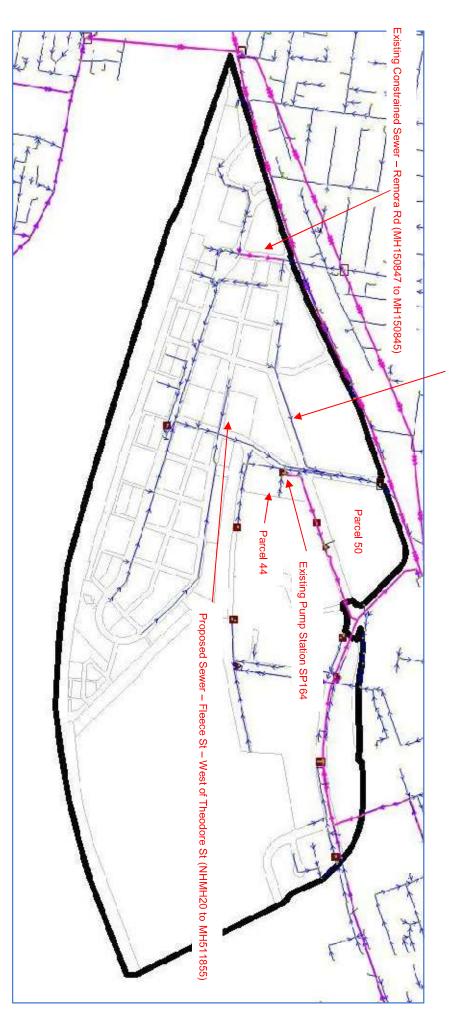


Figure 4-1 Modelling Results within PDA – Ultimate Scenario – Modelling Completed by Cardno

LEGENDS

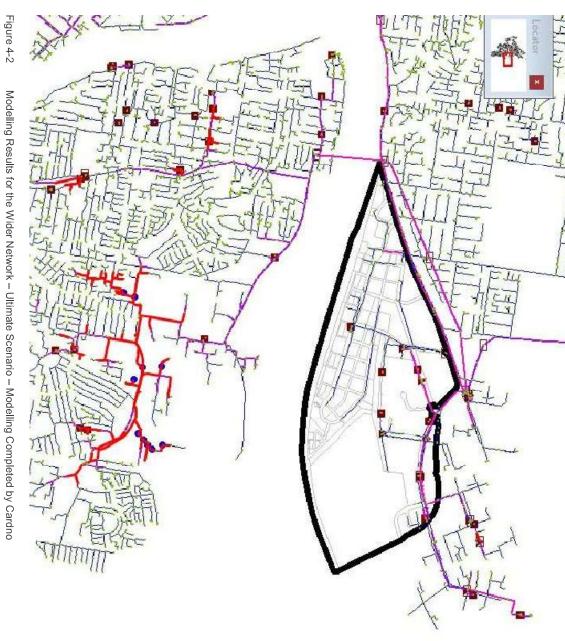
Sewer – No surcharge

Backwatered Sewer (downstream constraint)

Sewer capacity exceeded

Sewers surcharging >1m from GL

Overflows from Manhole



Modelling Results for the Wider Network - Ultimate Scenario - Modelling Completed by Cardno

() Cardno

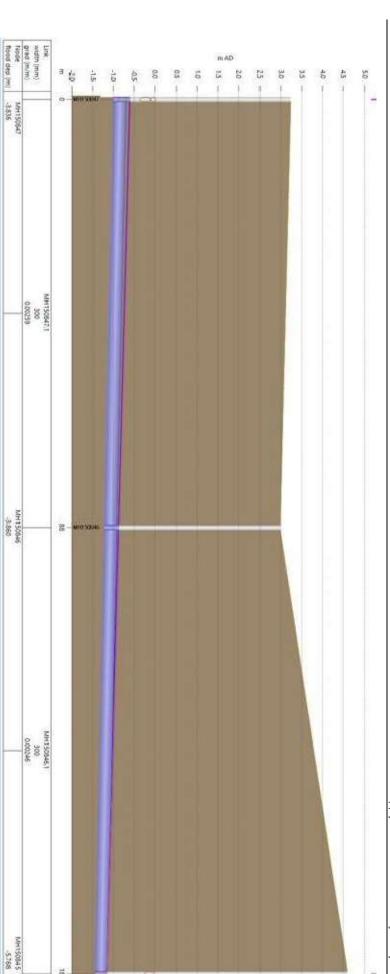
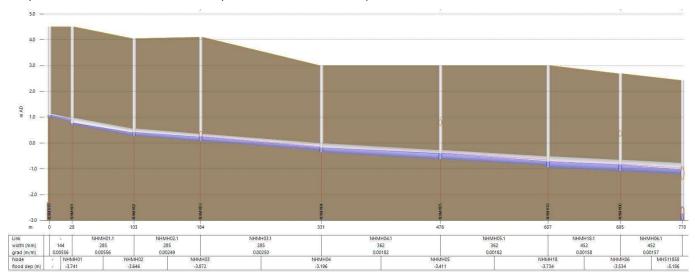


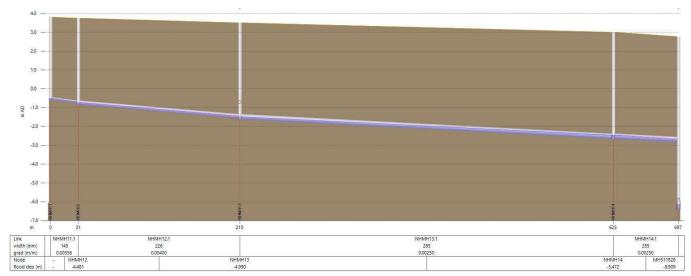
Figure 4-3 Longitudinal Profile – Existing Constrained Sewer – Remora Road (MH150847 to MH150845) – Ultimate Scenario



### Proposed Sewer on Macarthur Ave (NHMH 19 to MH511858)



### Proposed Sewer on Curtin Ave West (NHMH 11 to MH511828)



### Proposed Sewer - Fleece St – West of Theodore St (NHMH 20 to MH511855)

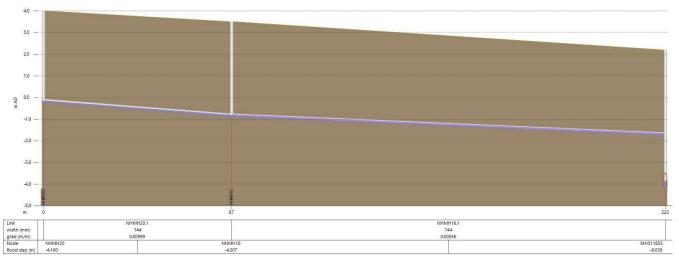


Figure 4-4 Longitudinal Profiles – Proposed Sewer Main Within PDA – Ultimate Scenario



### 5 Cost Estimate

Capital cost estimates have been prepared for the proposed water and sewer mains identified within this report. Costs have been developed from Cardno's cost model developed by Cardno from benchmarking recent construction projects. This method is considered fit for purpose for the Northshore Hamilton PDA.

The adopted rates are nominal and represent costs as at 2019.

Table 5-1 below shows the base unit cost adopted for water supply infrastructure and Table 5-2 details the base unit rates for sewerage infrastructure.

Table 5-1 Water Supply Infrastructure Unit Rates

Diameter (DN- mm)	Unit Rate (\$/m)
160	264
200	312
250	374
400	719
450	990

Table 5-2 Sewerage Infrastructure Unit Rates

Diameter (DN- mm)	Unit Rate (\$/m) per depth 1.5-3.0m	Unit Rate (\$/m) per depth 3.0- 4.5m	Unit Rate (\$/m) per depth >4.5m
160		671	
250	574	778	1,139
315		785	1,114
400		1090	
450			
500		1436	

The indicative total costs include:

- > Construction Contingency (25% as requested by EDQ)
- Project Owners Cost (Project management and designing depends 13% to align with transport).
- > Unit Cost adjustment factors:
  - Scaling Factor: Pipe length of 200m-500m is considered.
  - Construction Constraints: High Constraints: High concentration of office, retail, commercial or industrial containing high-to-heavy traffic density and heavily congested services. Large amounts of high-quality footpaths and road pavement.
  - Soil Types: Acid Sulphate Soils (ASS): Areas where the presence of acid sulphate is detected, and is characterised by a marine mud / clay type soil with high organics and pungent odour.



### 5.2 Water Supply

Table 5-3 outlines the capital cost estimate for the proposed water supply infrastructure within the PDA. A detailed breakdown has been provided in Appendix Figure 308.

Table 5-3 Water Supply Infrastructure Capital Cost Estimate

Planning Horizon	Capital Cost
2022-2026 (Stage 2)	\$3,413,822
2027-2031 (Stage 3)	\$713,623
Post 2031 (Stage 4)	\$2,931,248
TOTAL	\$7,058,693

### 5.3 Sewerage

Table 5-4 shows the breakdown of the sewerage cost. The detailed cost estimate is shown in Appendix Figure 309.

Table 5-4 Northshore Hamilton PDA Proposed Sewerage Cost

Planning Horizon	Capital Cost	Items
2022-2026 (Stage 2)	\$3,178,337	MacArthur Ave (East) / Theodore St
2027-2031 (Stage 3)	-	
Post 2031 (Stage 4)	\$3,444,678	Curtin Ave (West) / Fleece St
TOTAL	\$6,623,015	



### 6 Conclusion

The study considers the latest population projection within Northshore Hamilton PDA and the impact of this population on the proposed water and sewerage network within the PDA. Urban Utilities' water and sewerage model was updated with this proposed population to assess the impact on the water and sewerage network.

The following summarises the findings of this assessment and the further work required:

### 6.1 Water

- > Proposed growth within the PDA represents increase in load to 30,225EP from Urban Utilities' previous forecast of 22,173EP, representing a 36% increase.
- > The proposed network within the PDA is adequate to supply peak hour and fire flow requirements within the PDA.
- Deficiencies are observed outside of the PDA in Urban Utilities' planning model under both Peak Hour and fire-flow scenarios. It is not expected that external network augmentations will affect the network performance within the PDA.
- > Subsequent network planning and design stages shall consider the location of valves to optimise network conditions during planned or unplanned events to minimise disruption.
- > Detailed geotechnical investigations shall be undertaken to minimise construction risks.

### 6.2 Sewerage

- > Proposed growth within the PDA represents increase in load to 30,225EP from Urban Utilities' previous forecast of 22,174EP, representing a 36% increase.
- > The proposed network within the PDA is adequate to support development within the PDA. The key findings are:
  - Proposed sewers within the PDA maintain PWWF within <75% pipe full</li>
  - Existing sewers within the PDA maintain PWWF flood depth no greater than 1.2m from ground level
  - No deficiencies are observed in the external network adjacent the PDA, including the network between the PDA and the S1 trunk sewers (DN1400) which services the PDA.
- Loads from the PDA should not have a material impact to the S1 trunk system given the relatively large scale of the S1 system compared with the relatively small loads from the PDA.
- > Detailed geotechnical investigations shall be undertaken as part of future sewer detailed design to minimise sewer design & construction risks.

Water Supply and Sewer Preliminary Analysis

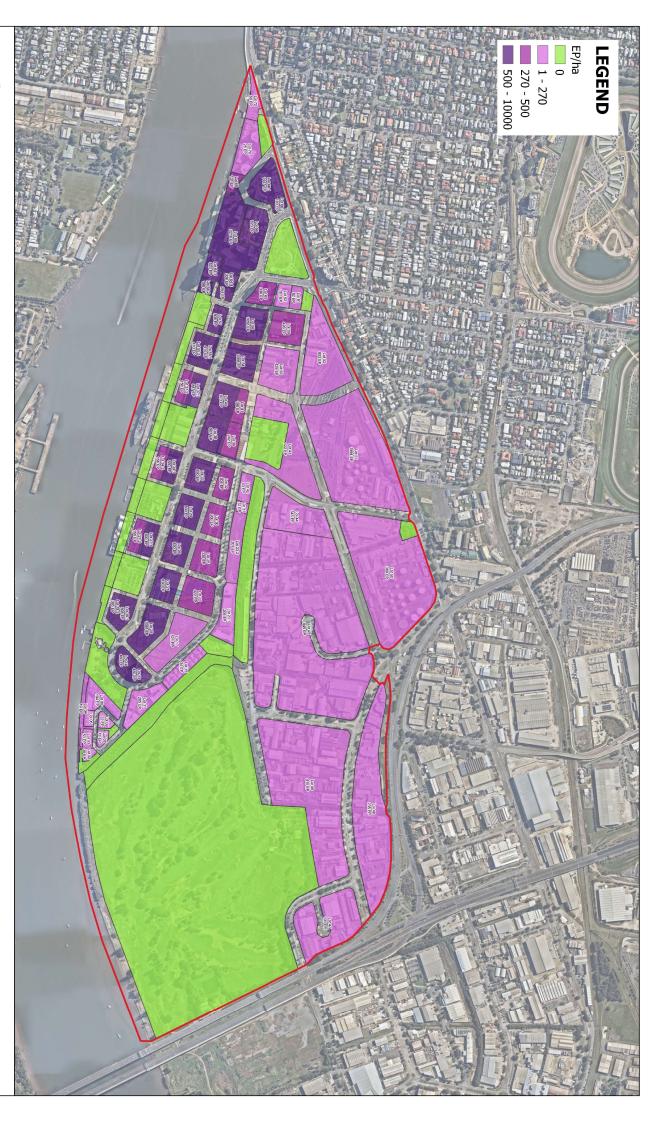
### **APPENDIX**



### POPULATION FIGURE AND TABLE

- FIGURE 201
- FIGURE 305







## **Northshore Hamilton PDA**

Figure 201 - Northshore Population



Map Produced by APAC lotth (Traffic & Transport)
Date 1790/2019 for Stransport)
Coordinate System GDA 1984 - MGA Zone 55
Map CTT 19059 Northshore Hamiton LGP Map 20150808 ags RevA

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0 0	418	0	0	885	221	234	36 Med MU	ω
0 0 0	170	0	0	930	1,006	95	35 Med MU	ω
0 0	430	0	0	0	0	240	22 Med MU	2
O	285	0	0	0	0	159	21 Med MU	2
	18	0	0	0	0	10	19 Med MU	1
0	21	0	0	0	0	12	18 Med MU	1
0	360	0	0	0	0	201	17 Med MU	1
ω	153	0	0	324	81	86	132 Med MU	13
ω	153	0	0	324	81	86	Med MU	112
ω	153	0	0	324	81	86	902 Med MU	90
0	206	0	0	0	0	115	Med MU	
14	816	0	0	1,728	432	456	131 Max MU	13
14	816	0		1,728	432	456	111 Max MU	
. <u>ω</u>	816	0		1,728	3,000	456	901 Max MU	1 9
2//		10,011		42,152	52/	0	54 Industry Business	3 .
21 0	0					0 0	54 I I do Susilless	1
		0 0					52 Industry Business	Л
ا د	0 (	0			0		Industry Business	л ,
0	0	0	0	0	0	0	Industry Business	51
429	0	15,494	0	65,239	815	0	49 Industry Business	4
0	0	20,167	0	0	20	0	63 Industrial	6
0	0	3,890	0	0	4	0	Industrial	6
0	0	32,197	0	0	32	0	Industrial	61
0	0	63,769	0	0	64	0	60 Industrial	6
1	0	129,930	0	0	130	0	59 Industrial	5
0	0	56,771	0	0	57	0	58 Industrial	5
30	1,253	0	0	2,652	2,007	700	402 High MU	40
112	2,927	0	0	759	16,417	1,635	401 High MU	40
28	308	0	0	3,736	535	172	34 High MU	lω
18	1,038			2,197	549	580	33 High MU	ا ،
16	1,000			7,200	740	500	22 111811 MIO	ار
19	1 080	0		2 286	571	603	High MU	ارر
50	822	0	0	1,741	6,000	459	31 High MU	ω
51	856	0	0	1,813	6,000	478	30 High MU	ω
14	816	0	0	1,728	432	456	29 High MU	2
14	816	0	0	1,728	432	456	28 High MU	2
14	816	0	0	1,728	432	456	27 High MU	2
14	816	0	0	1,728	432	456	26 High MU	2
10	573	0		1,214	303	320	25 High MU	2
8	477	0		1,009	252	266	24 High MU	2
000	452	0		95/	239	253	23 High MU	
28	865	0	0	1,831	2,500	483	High MU	15
22	1,304	0		2,762	690	729	8 High MU	
74	1,330	0		0,111	3,226	200	o mgii ivio	
74	1 556	0 0		0 111	3 778	960	3 District Certific	
1 171	423			170,120	10,239	726	57 District Centre	٦ ر
E00	201			81 013	10 220	114	District Contro	
20	0	0		2,820	188		551 Community	55
mercial EP Community	EP Residential   EP Retail/Commercial	Industrial (GFA) EP	Community (GFA)	Commercial (GFA)	Retail (GFA)	Residential Units	Zone	Block
Resulting EP			timates	Ultimate Yield Estimates	Oltin			
					-			

2,159	103	3,142	24,820	332,230	15,792	413,633	69,791	13,866		TOTAL
0	0		0		0	0	0	0	64 Open Space	62
0	0	0	0			0	0	0	552 Open Space	552
0	0	0	0	0	0	0	0	0	50 Open Space	50
0	0	0	0	0	0	0	0	0	48 Open Space	48
0	0	0	0	0	0	0	0	0	47 Open Space	47
0	0	0	0	0	0	0	0	0	20 Open Space	20
0	0	0	0	0	0	0	0	0	16 Open Space	16
0	0	0	0	0	0	0	0	0	14 Open Space	1/
0	0	0	0	0	0	0	0	0	12 Open Space	12
0	0	0	0	0	0	0	0	0	10 Open Space	10
0	0	0	0	0	0	0	0	0	7 Open Space	
0	0	0	0	0	0	0	0	0	6 Open Space	6
0	0	0	0	0	0	0	0	0	5 Open Space	
0	0	0	0	0	0	0	0	0	2 Open Space	,
0	0	0	34	0	0	0	0	19	46 Med MU	46
0	0	4	206	0	0	436	109	115	45 Med MU	45
0	0	5	306	0	0	649	162	171	44 Med MU	44
0	0	7	414	0	0	877	219	231	43 Med MU	43
0	0	6	334	0	0	706	177	186	42 Med MU	42
0	0	4	255	0	0		135	143	41 Med MU	41
0	0	3	200	0	0	424	106	112	40 Med MU	40
0	0	4	238	0	0	503	126	133	39 Med MU	35
EP Industrial	nunity	EP Retail/Commercial	EP Residential	Industrial (GFA)	Community (GFA)	Commercial (GFA)	Retail (GFA)	Residential Units	Zone	Block
	g EP	Resulting EP			timates	Ultimate Yield Estimates	Ultir			

Water Supply and Sewer Preliminary Analysis

### **APPENDIX**

### B

PROPOSED ROAD INFRASTRUCTURE AND DEVELOPMENT STAGING PLAN

- FIGURE 101
- FIGURE 306





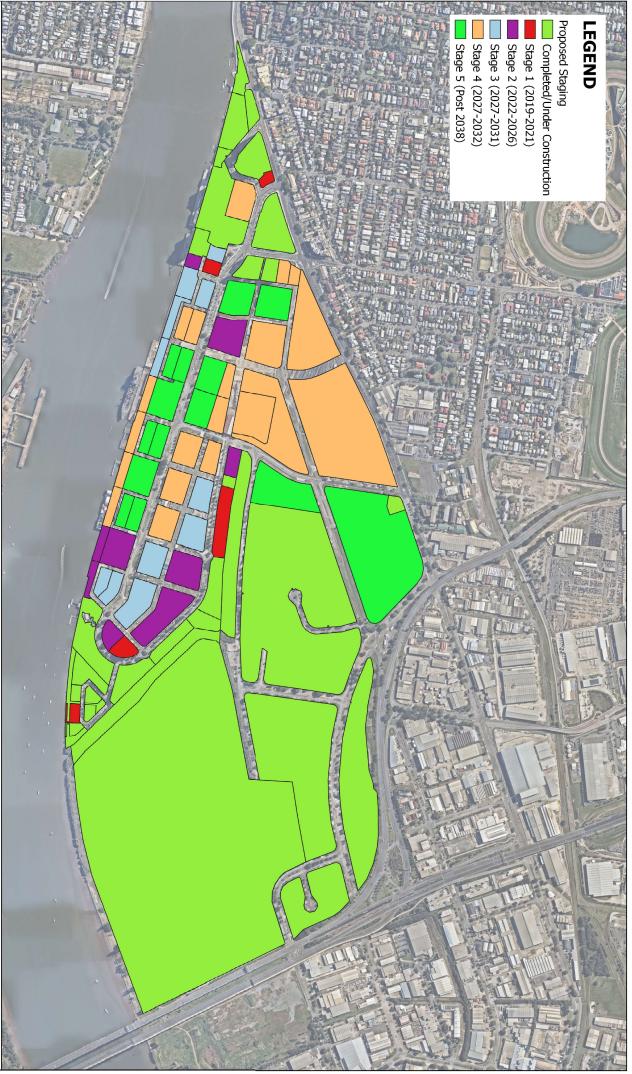


## **Northshore Hamilton PDA**

Figure 101 - Proposed Road Infrastructure



Map Produced by APAC both (Traffic & Transport)
Date: 1/20/2019 is 27
Coordinate System GDA: 1964 - MGA Zone 55
Nap:OTT19059 Northshore Hamiton LOBP Map 20190808 ags RevA





**Hamilton Northshore PDA** 

Figure 1 - Proposed Staging

Map Produced by APAC buth (Tireff 3 Transport)
Date: 10052012 is
Coordinate System COA: 1564. NGA Zone 55
Project: CIT 1905.9
MapCGTT: 9059 Northshore Harriton LSIP Map 20150505. qps RevA

(Cardno

Water Supply and Sewer Preliminary Analysis

### **APPENDIX**

C

SEQ DESIGN CODE TABLES

- FIGURE 307





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# Table 4.1 - Water Network Design Criteria – Single Supply (Drinking Water Only) Network

									}	A5					4			А3	A2	<u>A</u>	A. Drinking W Supply Zone)
Background Demand							Urban	(Political of the Political of the Polit	Rural and Small Communities (Definitions as per Glossary)	Fire Fighting	Emergency fire operating conditions (Minimum Residual Mains Pressures)	Maximum SERVICE Pressure	In areas defined by the SP, properties requiring domestic private boosters	Normal operating conditions	Pressure  Minimum SERVICE pressure (at PH on PD with Reservoirs at MOL) with no flow through service, Urban and Rural	PH/PD PH/AD	MDMM/AD	Peaking Factors	Estimated Non-Revenue Water (NRW)	Average Day Demand (AD) per EP, excluding NRW (Note: EP/ET conversion rate provided in separate tables from Water Service Provider)	No Parameter A. Drinking Water – Conventional (Single Supply Zone)
Res: 2/3 PH (not less than AD) and +ve residual pressure at PH Non Res: PH for localised Commercial/industrial or 2/3 PH for water supply zone. Worst case scenario should be used based on reservoir at MOL, based on single residential or single commercial/industrial fire within water supply zone										the	12m min at the main at the hydrant 9m minimum for infrastructure in small isolated or high elevated areas within	Targ. N		22 m in the m		2.84 2.05 6.03 2.97		Residential Multi-			•
Res: 2/3 PH (not less than AD) and +ve residual pressure at PH or localised Commercial/industrial or 2/3 PH for water supply zor lid be used based on reservoir at MOL, based on single residen commercial/industrial fire within water supply zone							Residential: 15 L/s for 2 hours Commercial/Industrial: 30 L/s for 4 hours	, care	Rural	he existing water supply zone	2m min at the main at the hydrant structure in small isolated or high e	Target maximum pressure 55 m Maximum pressure 80 m		22 m in the main adjoining the Property boundary.		2.07 2.32	1.06	Commercial	20 L/EP/d	220 L/EP/d	Gold Coast
d +ve residual pi or 2/3 PH for wa //OL,based on s //thin water sup							s for 2 hours 30 L/s for 4 hou	Committee Control	Rural Commercial: 151 /s for 2 hours	supply zone 	ydrant · high elevated a	55 m უ		erty boundary.		1.12 2.51 1.38 2.40 1.54 6.03		Indus.   Tourist			
ressure at PH ter supply zone ingle resident ply zone							I'S	11	.5L/5 101 z 110u1	5l /s for 2 hour	reas within		-			1.75 2.40	1.15	-			
e. Worst case ii <b>al or single</b>									Ū	3			12 m at					Low and Me			Logan
Res(Detached/ Multi storey): Highest of 2/3 PH or AD Commercial/Industrial: PH demand (between 10am and 4pm) (single fire event only)			Risk Hazard Buildings – assessed on needs basis	buildings: 30 L/s for 4 hours w background Demand	Demand Commercial/Industrial	Multi storey Res (> 3 storeys): 30 L/s for 4 hours w background	Detached Res (<= 3 storeys): 15 Ls for 2hrs w background Demand				12 6 m else		12 m at the property boundary			4 2 2	1.5	Low and Med Density Res			Redland
peak h sidentia nands.	Commercial/Industrial: Greenfield 45 L/s for 4 hrs Brownfield 30 L/s for 4 hrs	City CBD/Inner City High Rise: Case by case but in the order of 300 L/s for 4 hrs	High Density Urban (>6 storeys): 60 L/s for 4 hrs	Medium Density Urban (4-6 storeys): Greenfield 45 L/s for 4 hrs Brownfield 30 L/s for 4 hrs	Greenfield 25 L/s for 2 hrs Brownfield 15 L/s for 2 hrs	/Timber: 25 L/s for 2 hours  Low Density Urban (1-3 storeys) Brick/Tile:	Semi-Rural (1,000 to 5,000 m² lots): 15 L/s for 2 hours		Noted (20,000 tilz lots). 7.3E/s lot z flodis	Positive pressure throughout  Rural (>5 000m2 lots): 7 5l /s for 2 hours	12 m min in the main at the flowing hydrant 6 m elsewhere in mains that have customer connections	55 m		22 m at the property boundary		1.75 3.5	າ.5	High Density Res	30 L/EP/d	230 L/EP/d	Queensland Urban Utilities
Res (Detached/ Multi storey): Highest of 2/3 PH or AD Commercial/ Industrial: PH demand (between 10am and 4pm) (single fire event only)				Demand  Risk Hazard Buildings – assessed on needs basis	Commercial/Industrial buildings: 30 L/s for 4 hours w background	Multi story Res (> 3 storeys): 30 L's for 4 hours w background Demand	Detached Res (<= 3 storeys): 15 L/s for 2hrs w background Demand	Rural Commercial/Industrial: 15L/s for 2 hours	hours	Rural Residential only: 7.51 /s for 2	ns					1.4 2.8	2.5	Commercial/Industrial			Unitywater

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		A9	A8		_		Α7		A6	Sup Sup	
Maximum allowable velocity	Maximum Allowable Headloss (PH) (m/km)	Pipe Friction Losses Hazen Williams Friction Factors Based on the preferred material types outlined in the SEQ Water Supply Code (as amended), Any variation from these material types needs to be subject to further investigation.	Pipeline Capacity Requirements	Standby pump capacity	Elevated reservoir – Duty Pump	Ground level reservoir – Duty Pump	Reservoir Pump Servicing Requirements		Reservoir storage—perational capacity (Min Operating Storage – four consecutive hours of demand)	No Parameter A. Drinking Water – Conventional (Single Supply Zone)	CHICITIONS .
			Trunk gravity system: MDMM in 24hours; Reticulation Mains: Maintain pressure for PH and fire flow performance Pump system: MDMM in 20 hours					ELEVATED RESERV  6 x (PH - 1/12 MDMM)+1500: In supply zones where 8xPH is less than or equal to (2xPH)+150kL fire st  Note: PH is in kL/h, MDMM is in kL/d and reservoir s	GROUND LEVEL RESERVOIR: 3 x (PD – MDMM) + Emergency Storage  (Emergency Storage - Greater of 4 hrs at MDMM or 0.5 ML. For less than 1000 EP, 150 kL)	Gold Coast	LOGAN Utilities
	5m, 3m,	>15.		Match larges	Capacity	ME		$6 \times (PH - 1/12)$ $6 \times (PH - 1/12)$ $ere 8xPH is less that (2xPH $	rage or less than 1000 E	Logan	lities
2.5m/s	5m/km for DN<=150 3m/km for DN>=200	<=150, C=100 >150 -300mm, C=110	Reticulation mains;	Match largest single pump unit capacity	Capacity (L/s) = Peak Hour (L/s)	MDMM over 20 hrs		ELEVATED RESERVOIR:  6 x (PH - 1/1/2 MIDMM)H+150kL fire storage 6 x (PH - 1/1/2 MIDMM)H+150kL fire storage In supply zones where 8xPH is less than or equal to MIDMM the following equation is used (2xPH)+150kL fire storage Note: PH is in kL/n, MDMM is in kL/d and reservoir storage is in kL in the above formulae.	EP, 150 kL)	Rediand	
			Transport MDMM in 20 hrs Reticulation mains; Maintain pressure for Peak Hour and fire flow performance					<u>(OJR.)</u> (I fire storage MDMM the following equation is used orage to in kL in the above formulae.	GROUND LEVEL RESERVOIR:  3 v (PD – MDMM) + greater of 4 hrs  3 v (PD – MDMM) + greater of 4 hrs  MDMM and Firefighting Storage, subject to a minimum reservoir size of 150 kL (Firefighting Storage based on flow and duration requirements stated under item A5 for development types serviced by the reservoir)	Queensland Urban Utilities	Redland WATER
			performance						GROUND LEVEL RESERVOIR:  3 x (PD – MDMM) + Emergency Storage (Emergency Storage - Greater of 4 hrs at MDMM or 0.5 ML. For less than 1000 EP, 150 kL)	Unitywater	Unitywater

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## Table 10 - Sewerage Network Design Criteria

As shown in the Sewer Pump Station Code (As are Sassist) = C1 x ADWF  Duty/assist  Bassist) = C1 x ADWF  Whichever is the greater) Overflows should not occur at the work of Clause 5.2.4 of Sewer Sewer Land VEP/d  Refer Clause 5.2.4 of Sewer Pump Station Code (As an office of Clause 5.2.4 of Sewer Pump Station Code (As 900 L/EP/d  Refer Clause 5.2.4 of Sewer Pump Station Code (As 900 L/EP/d  1.0—1.5 m/s	ADWF where C2 = 4.7 X (EP) <sup>4.165</sup> WIF = 5 x ADWF  Coomera Pimpama in Gold Coast Area <sup>41</sup> ; PWWF=4 x ADWF  Vacuum Sewer/Low Pressure Sewer PWWF = (4 x ADWF)  1.9 x Q / N  As shown in the Sewer Pump Station Code (As ama 6hrs at ADWF)  Duty/assist  As shown in the Sewer Pump Station Code (As ama 6hrs at ADWF)  Duty/assist  Duty/assist  As wifer Clause 5.2.4 of Sewer Pump Station Code (As ama 6hrs at ADWF; Whichever is the greater) Overflows should not occur at thow 4 x ADWF; Whichever is the larger).  Refer Clause 5.2.4 of Sewer Pump Station Code (As a ma 6hrs at ADWF; Whichever is the larger).  Refer Clause 5.2.4 of Sewer Pump Station Code (As a ma 6hrs at ADWF; Whichever is the larger).  Refer Clause 5.2.4 of Sewer Pump Station Code (As a ma 6hrs at ADWF; Whichever is the larger).  Refer Clause 5.2.4 of Sewer Pump Station Code (As a ma 6hrs at ADWF; Whichever is the larger).  Refer Clause 5.2.4 of Sewer Pump Station Code (As a ma 6hrs at ADWF; Whichever is the larger).  Refer Clause 5.2.4 of Sewer Pump Station Code (As a ma 6hrs at ADWF; Whichever is the larger).	Salled Actionly	T
Smart Sewer Option	ADWF where C2 = 4.7 × (EP) <sup>-0.105</sup> ADWF where C2 = 4.7 × (EP) <sup>-0.105</sup> WF = 5 × ADWF  Coomera Pimpama in Gold Coast Area <sup>-1</sup> : PWWF=-4 × ADWF  Coomera Pimpama in Gold Coast Area <sup>-1</sup> : PWWF=-4 × ADWF  Vacuum Sewer/Low Pressure Sewer PWWF = (4 × ADWF)  PWWF = (4 × ADWF)  PWWF = (4 × ADWF)  As shown in the Sewer Pump Station Code (As an 6hrs at ADWF)  As shown in the Sewer Pump Station Code (As an 6hrs at ADWF)  Duty/assist  Sx (EP) <sup>-0.1387</sup> Duty/assist  As shown in the Sewer Pump Station Code (As an 6hrs at ADWF)  PWWF = (5 × ADWF min or C1 × ADWF)  PWWF = (6 × 5 × ADWF min or C1 × ADWF)  Whichever is the greater) Overflows should not occur at flow < 5 × ADWF or C1 × ADWF.  Refer Clause 5.2.4 of Sewer Pump Station Code (As 900 L/EP/d)	forred Velocity	اه
Smart Sewer Option   Average Dry Weather Flow (ADWF)   Average Dry Weather Flow (ADWF)   For RIGS 200 LEPId	ADWF where C2 = 4.7 X (EP) -0.105  ADWF where C2 = 4.7 X (EP) -0.105  WF = 5 x ADWF  Coomera Pimpama in Gold Coast Area <sup>11</sup> : PWWF=4 x ADWF  Vacuum SewerLow Pressure Sewer PWWF = (4 x ADWF)  10.9 x Q / N  (L/s) of duty pump or Total Pump Capacity (L/s) if multiple duty pumps.  10.9 x Q / N  As shown in the Sewer Pump Station Code (As are sold)	sing Main Requirements	
Smart Sewer Option   Average   Dry Weather Flow (ADWF)   POWF = C2 x ADWF where C2 = 4,7 x (EP) and   For 'tosseline' calculations for existing Conventional Sever   Pow   P	ADWF where C2 = 4.7 × (EP) -0.105  WF = 5 × ADWF  Coomera Pimpama in Gold Coast Area <sup>11</sup> : PWWF=4 × ADWF  Vacuum Sewer/Low Pressure Sewer PWWF = (4 × ADWF)  1. Sy x Q / N  Vacuum Sewer/Low Pressure Sewer PWWF = (4 × ADWF)  Vacuum Sewer/Low Pressure Sewer PWWF = (4 × ADWF)  Sy x Q / N  As shown in the Sewer Pump Station Code (As area of the foreign of the follows)  Duty/assist  Be within the range 3.5 - 5  Value of C1 to be minimum of 3.5  PWWF  Whichever is the greater) Overflows should not occur at flow of 5 x ADWF;  Whichever is the larger).  Refer Clause 5.2.4 of Sewer Pump Station Code (As ADWF; ABWF)  Refer Clause 5.2.4 of Sewer Pump Station Code (As ABWF)  Refer Clause 5.2.4 of Sewer Pump Station Code (As ABWF)  Refer Clause 5.2.4 of Sewer Pump Station Code (As ABWF)  Refer Clause 5.2.4 of Sewer Pump Station Code (As ABWF)	w Pressure Sewer Flow	
Smart Sewer Option   Average Dry Weather Flow (ADWF)   PDWF = C2 X ADWF where C2 = 4.7 X (EP) -0.105.   Power read Country and in Gold Coast Area**. PWWF=4 x ADWF	ADWF where C2 = 4.7 × (EP) -0.105  WF = 5 × ADWF  Coomera Pimpama in Gold Coast Area <sup>11</sup> : PWWF=4 × ADWF  Vacuum Sewer/Low Pressure Sewer PWWF = (4 × ADWF)  (L/s) of duty pump or Total Pump Capacity (L/s) if multiple duty pumps. 10.9 × Q / N  As shown in the Sewer Pump Station Code (As are 6hrs at ADWF)  Sokw  >200kw  As shown in the Sewer Pump Station Code (As are 6hrs at ADWF)  Minimum 4 hours (up to 6hours)  5 × (EP) -0.1387  Duty/ass/st  Socur at flow < 5 × ADWF min or C1 × ADWF; Whichever is the greate) Overflows should not (whichever is the larger).  PWWF (whichever is the larger).	e of Pump Station Lot (and buffer)	╀
Smart Sewer Option  Average Dry Weather Flow (ADWF)  Average Dry Weather Flow (ADWF)  Peak Dry Weather Flow (PDWF)  Peak Dry Weather Flow (PDWF)  Peak Dry Weather Flow (PDWF)  Power and Coonera Pimpama in Gold Coast Area*1: PWWF=4 x ADWF  NuSewer and Coonera Pimpama in Gold Coast Area*1: PWWF=4 x ADWF  NuSewer and Coonera Pimpama in Gold Coast Area*1: PWWF=4 x ADWF  Pump Station Servicing Requirements  Operating storage (m3)  Pump Station Servicing Requirements  Operating storage (m3)  Pimp Debeation Mode*2  Minimum Wet Well diameter  Emergency storage (existing)  Minimum Wet Well diameter  Area (Lis) of duty pump or Total Pump Capacity (Lis) if multiple duty pumps.  As shown in the Sewer Pump Station Code (As an DWF)  As shown in the Sewer Pump Station Code (As an DWF)  Where C1 = 15 x (EP) -0.1035  Value of C1 to be minimum of 3.5  Fellows (i.e. upstream pump Stations Surned off)  Where C1 = 15 x (EP) -0.1035  Value of C1 to be minimum of 3.5  Fellows (i.e. upstream pump Stations Surned off)  Where C1 = 15 x (EP) -0.1035  Value of C1 to be minimum of 3.5  Fellows (i.e. upstream pump Station Code (As an DWF)  Where C1 = 15 x (EP) -0.1035  Value of C1 to be minimum of 3.5	ADWF where C2 = 4.7 × (EP) -0.105  WF = 5 × ADWF  Coomera Pimpama in Gold Coast Area <sup>11</sup> : PWWF=4 × ADWF  Vacuum Sewer/Low Pressure Sewer PWWF = (4 × ADWF)  1.0.9 × Q / N  2.0.9 × Q / N  2.0.9 × Q / N  As shown in the Sewer Pump Station Code (As are short of starts per hr are: 1.0.9 × Q / N  As shown in the Sewer Pump Station Code (As are short of Section Polity)  As shown in the Sewer Pump Station Code (As are short of Section Polity)  As shown in the Sewer Pump Station Code (As are short of Section Polity)  As shown in the Sewer Pump Station Code (As are short of Section Polity)  As shown in the Sewer Pump Station Code (As are short of Section Polity)  As shown in the Sewer Pump Station Code (As are short of Section Polity)  As shown in the Sewer Pump Station Code (As are short of Section Polity)  As shown in the Sewer Pump Station Code (As are short of Section Polity)  As shown in the Sewer Pump Station Code (As are short of Section Polity)  As shown in the Sewer Pump Station Code (As are short of Section Polity)  As shown in the Sewer Pump Station Code (As are short of Section Polity)  As shown in the Sewer Pump Station Code (As are short of Section Polity)  As shown in the Sewer Pump Station Code (As are short of Section Polity)  As shown in the Sewer Pump Station Code (As are short of Section Polity)  As shown in the Sewer Pump Station Code (As are short of Section Polity)  As shown in the Sewer Pump Station Code (As are short of Section Polity)  As shown in the Sewer Pump Station Code (As are short of Section Polity)  As shown in the Sewer Pump Station Code (As are short of Section Polity)  As shown in the Sewer Pump Station Code (As are short of Section Polity)  As shown in the Sewer Pump Station Code (As are short of Section Polity)  As shown in the Sewer Pump Station Code (As are short of Section Polity)	tal pump station capacity	
Smart Sewer Option Average Dry Weather Flow (ADWF) Average Dry Weather Flow (ADWF)  Peak Dry Weather Flow (PDWF)  Peak Dry Weather Flow (PDWF)  Peak Wet Weather Flow (PDWF)  Por RIGS PMVF = C2 X ADWF where C2 = 4.7 X (EP) -0.135  NUSewer and Coomera Pimpama in Gold Coast Area <sup>11</sup> : PWVF=4 x ADWF  NuSewer and Coomera Pimpama in Gold Coast Area <sup>11</sup> : PWWF=4 x ADWF  Vacuum Seweri Conventional Sever PWWF = (4 x ADWF)  Pump Station Servicing Requirements  Ops Storage = 0.9 x Q / N  Operating storage (m3)  Pump Capacity (L/s) if multiple duty pumps.  As shown in the Sewer Pump Station Code (As area)  Minimum Wet Wet Wet I diameter  Emergency storage (existing)  Minimum A hours (up to 6 hours)  Value of C1 = 15 x (EP) -0.1387  Where C1 = 15 x (EP) -0.1387  Minimum A hours (up to 6 hours)  Where C1 = 15 x (EP) -0.1387	ADWF where C2 = 4.7 X (EP) -0.105  WE = 5 x ADWF  Coomera Pimpama in Gold Coast Area <sup>11</sup> : PWWF=4 x ADWF  Vacuum Sewer/Low Pressure Sewer PWWF = (4 x ADWF)  1.0.9 x Q / N  (L/s) of duty pump or Total Pump Capacity (L/s) if multiple duty pumps.  1.0.9 x Q / N  (L/s) of duty pump or Total Pump Capacity (L/s) if multiple duty pumps.  1.0.9 x Q / N  (L/s) of duty pump or Total Pump Capacity (L/s) if multiple duty pumps.  1.0.9 x Q / N  (L/s) of duty pump Startion Code (As are Shown in the Sewer Pump Station Code (As are Shown)  2.0.9 x Q / N  (L/s) of duty pump or Total Pump Capacity (L/s) if multiple duty pumps.  1.0.9 x Q / N  (L/s) of duty pumps.  1.0.9 x Q / N  As shown in the Sewer Pump Station Code (As are Shown)  2.0.0 x Q / N  As shown in the Sewer Pump Station Code (As are Shown)  2.0.0 x Q / N  As shown in the Sewer Pump Station Code (As are Shown)  2.0.0 x Q / N  As shown in the Sewer Pump Station Code (As are Shown)  2.0.0 x Q / N  As shown in the Sewer Pump Station Code (As are Shown)  2.0.0 x Q / N  As shown in the Sewer Pump Station Code (As are Shown)  3.0 x Q / N  4.0 x Q / N  As shown in the Sewer Pump Station Code (As are Shown)  4.0 x Q / N  As shown in the Sewer Pump Station Code (As are Shown)  4.0 x Q / N  As shown in the Sewer Pump Station Code (As are Shown)  4.0 x Q / N  5.0 x Q / N  5.0 x Q / N  5.0 x Q / N  6.0 x Q / N  7.0 x Q / N  8.0 x	Value of C1	
Smart Sewer Option Average Dry Weather Flow (ADWF) Average Dry Weather Flow (ADWF)  For RIGS 200 L/EP/d Fo	ADWF where C2 = 4.7 X (EP) 4.105  ADWF where C2 = 4.7 X (EP) 4.105  Where: SF = Sanitar GWI = 5 x ADWF  Coomera Pimpama in Gold Coast Area 1: PWWF=4 x ADWF  Coomera Pimpama in Gold Coast Area 1: PWWF=4 x ADWF  Vacuum Sewer/Low Pressure Sewer PWWF = (4 x ADWF)  Vacuum Sewer/Low Pressure Sewer PWWF = 16 x ADWF  1.30  Vacuum Sewer/Low Pressure Sewer PWWF = 4 x ADWF  1.30  As shown in the Sewer Pump Station Code (As amended) Ohkw 200kw  As shown in the Sewer Pump Station Code (As amended) Ohrs at ADWF  Duty/assist		· ·
Smart Sewer Option  Average Dry Weather Flow (ADWF)  Average Dry Weather Flow (ADWF)  Peak Dry Weather Flow (PDWF)  Peak Dry Weather Flow (PDWF)  Peak Dry Weather Flow (PDWF)  Power C2 X ADWF where C2 = 4.7 X (EP) -0.105  Power C3 X ADWF where C2 = 4.7 X (EP) -0.105  For "baseline" calculations for existing Conventional Sewer 190 LEP/d  For "baseline" calculations for existing Conventional Sewer 210 LEP/d  For RIGS 200 LEP/d  For Nussewer 180 LEP/d  For Nussewer 180 LEP/d  For Nussewer 210 LEP/d  For Nuse	ADWF where C2 = 4.7 x (EP) 4.105  ADWF where C2 = 4.7 x (EP) 4.105  Where:  SF = Sanitar  GWI = 5 x ADWF  Coomera Pimpama in Gold Coast Area <sup>11</sup> : PWWF=4 x ADWF  Coomera Pimpama in Gold Coast Area <sup>11</sup> : PWWF=4 x ADWF  Vacuum Sewer/Low Pressure Sewer  PWWF = 9D  PWWF = 4 x ADWF  Vacuum Sewer/Low Pressure Sewer  PWWF = 44 x ADWF)  PWWF = 480LV  As shown in the Sewer Pump Station Code (As amended)  As shown in the Sewer Pump Station Code (As amended)  Minimum 4 hours (up to 6hours)	3 4	ه ا
Smart Sewer Option  Average Dry Weather Flow (ADWF)  Average Dry Weather Flow (ADWF)  Peak Dry Weather Flow (PDWF)  Peak Dry Weather Flow (PDWF)  Peak Wet Weather Flow (PDWF)  Peak Wet Weather Flow (PDWF)  Power and Coomera Pimpama in Gold Coast Area 11: PWWF=4 x ADWF  NuSewer and Coomera Pimpama in Gold Coast Area 11: PWWF=4 x ADWF  Pump Station Servicing Requirements  Operating storage (ma)  Operating storage (ma)  All 2 for motors-100w  Na Bor (100-200w)  Na Bor	ADWF where C2 = 4.7 X (EP) 4.105  ADWF where C2 = 4.7 X (EP) 4.105  Where:  SF = Sanitar  GWI = Grour  FD = 30  Where:  SF = Sanitar  GWI = Grour  FD = 30  Where:  SF = Sanitar  GWI = Grour  FD = 30  Where:  SF = Sanitar  GWI = Grour  FD = 30  Where:  SF = Sanitar  GWI = Grour  FD = 30  Where:  SF = Sanitar  GWI = Grour  FD = 30  Where:  SF = Sanitar  GWI = Grour  FD = 30  Where:  SF = Sanitar  GWI = Grour  FD = 30  Where:  SF = Sanitar  GWI = Grour  FD = 30  Where:  SF = Sanitar  GWI = Grour  FD = 30  Where:  SF = Sanitar  GWI = Grour  FD = 30  Where:  SF = Sanitar  GWI = Grour  FD = 30  Where:  SF = Sanitar  GWI = Grour  FD = 30  Where:  SF = Sanitar  GWI = Grour  FD = 30  Where:  SF = Sanitar  GWI = Grour  FD = 30  Where:  SF = Sanitar  GWI = Grour  FD = 30  Where:  SF = Sanitar  GWI = Grour  FD = 30  As shown in the Sewer Pump Station Code (As amended)  Ghrs at ADWF	ergency storage (existing)	ılmı
Smart Sewer Option  Average Dry Weather Flow (ADWF)  Average Dry Weather Flow (ADWF)  Peak Dry Weather Flow (PDWF)  Peak Dry Weather Flow (PDWF)  Peak Dry Weather Flow (PDWF)  Por RIGS PWWF = 5 x ADWF where C2 = 4,7 x (EP) 4.105  Peak Wet Weather Flow (PWWF)  Pump Station Servicing Requirements  Ops Storage = 0.9 x Q / N  Ops Storage = 0.9 x Q / N  However, Muniber of starts per fir are:  N=5 of motors > 200kw  N=5 of motors > 200kw  As shown in the Sewer Pump Station Code (As amended)	ADWF where C2 = 4.7 X (EP) <sup>0.105</sup> NuSewer - d Where: SF = Sanitar GWI = 5x ADWF  Coomera Pimpama in Gold Coast Area <sup>11</sup> ; PWWF=4 x ADWF  Vacuum Sewer/Low Pressure Sewer PWWF = (4 x ADWF)  10.9 x Q / N  (L/s) of duty pump or Total Pump Capacity (L/s) if multiple duty pumps.  ber of starts per hr are: 1x	∯	⇒ zim
Smart Sewer Option  Average Dry Weather Flow (ADWF)  Average Dry Weather Flow (ADWF)  Peak Dry Weather Flow (PDWF)  Peak Dry Weather Flow (PDWF)  Peak Wet Weather Flow (PDWF)  Por RIGS 200 L/EP/d For NuSewer 180 L/EP/d For NuSewer 180 L/EP/d For NuSewer 180 L/EP/d For NuSewer 180 L/EP/d For NuSewer 210L/E  Where: SF = Sanitan G/W = C2 × ADWF  NuSewer and Coomera Pimpama in Gold Coast Area <sup>11</sup> ; PWWF=4 × ADWF  Pump Station Servicing Requirements Operating storage (m3)  Ops Storage = 0.9 × Q / N  N=12 for motors > 200kw  N=5 of motors > 200kw  N=5 of motors > 200kw  Ops Storage = 0.9 × Q / N  N=5 of motors > 200kw  N=5 of motors > 200kw	For "baseline" calculations for existing Conventional Sewer 210L/E  NuSewer - d  Where: SF = Sanitar  GWI = Grour  EP 30  d" 7.8  PWWF = 960L/  PWWF = 4 x ADWF  Vacuum Sewer/Low Pressure Sewer  PWWF = (4 x ADWF)  otal Pump Capacity (L/s) if multiple duty pumps.	er	2
Smart Sawer Option Average Dry Weather Flow (ADWF)  Peak Dry Weather Flow (PDWF)  Peak Dry Weather Flow (PDWF)  Peak Wet Weather Flow (PWWF)  For RIGS PWWF = 5 x ADWF  NuSewer and Coomera Pimpama in Gold Coast Area 11. PWWF=4 x ADWF  PWWF = PDWF + Re PWWF = ADWF  PWWF = ADWF   PW	For "baseline" calculations for existing Conventional Sewer 210L/EP/d  NuSewer - d x SF + GWI Where: SF = Sanitary Flow of 150L/EP/d GWI = Groundwater Infiltration of 30L/EP/d FP 30 30 30 600 1.2k 3k 12k  GW   7.8   4.2   3.7   3.2   2.7   2.2  PWWF = PDWF + Rainfall Dependent Inflow(RD RDF = 360L/EP/d  Vacuum Sewer/Low Pressure Sewer  Vacuum Sewer/Low Pressure Sewer		
Smart Sewer Option Average Dry Weather Flow (ADWF)  Peak Dry Weather Flow (PDWF)  Peak Wet Weather Flow (PWWF)  Por RIGS PWWF = 5 x ADWF  NuSewer and Coomera Pimpama in Gold Coast Area **: PWWF=4 x ADWF  Vacuum Sewer/Low Pressure Sewer  Vacuum Sewer/Low Pressure Sewer  Vacuum Sewer/Low Pressure Sewer  Vacuum Sewer/Low Pressure Sewer	For "baseline" calculations for existing Conventional Sewer 210L/EP/d    NuSewer - d x SF + GW    Where:   SF = Sanitary Flow of 150L/EP/d   GW  = Groundwater Infiltration of 30L/EP/d   EP   30   300   600   1.2k   3k   12k     GW  = Groundwater Infiltration of 30L/EP/d   EP   30   300   600   1.2k   3k   12k     GW  = Sewer   1.2k   3.7   3.2   2.7   2.2     PWWF = PDWF + Rainfall Dependent Inflow(RD   RDF = 360L/EP/d   PWWF = 360L/EP/d   PWWF = 360L/EP/d	_	4
Smart Sewer Option	NuSewer 210L/EP/d   NuSewer - d x SF + GWI   Where:   SF = Sanitary Flow of 150L/EP/d   GWI = Groundwater Infiltration of 30L/EP/d   EP   30   300   600   1.2k   3k   12k       GWI = Groundwater Infiltration of 30L/EP/d   EP   30   300   600   1.2k   3k   12k       GWI = Groundwater Infiltration of 30L/EP/d   EP   30   300   600   1.2k   3k   12k       GWI = Sanitary Flow of 150L/EP/d   GWI = Sanitary Flow of 150L/EP/d   EP   30   300   600   1.2k   3k   12k       GWI = Sanitary Flow of 150L/EP/d   GWI = Sanitary Flow of 150L/EP/d   GWI = Sanitary Flow of 150L/EP/d   EP   30   300   600   1.2k   3k   12k       GWI = Sanitary Flow of 150L/EP/d   GWI = Sanitary Flow of 150L/EP/d   GWI = Sanitary Flow of 150L/EP/d   EP   30   300   600   1.2k   3k   12k       GWI = Sanitary Flow of 150L/EP/d   GWI = Sanitary Flow of 150L/EP/d   GWI = Sanitary Flow of 150L/EP/d   EP   30   300   600   1.2k   3k   12k       GWI = Sanitary Flow of 150L/EP/d   GWI = Sa		
Smart Sewer Option  Average Dry Weather Flow (ADWF)  Average Dry Weather Flow (ADWF)  Peak Dry Weather Flow (PDWF)  Peak Dry Weather Flow (PDWF)  Power = C2 x ADWF where C2 = 4.7 x (EP) -0.105  Power = C2 x ADWF where C2 = 4.7 x (EP) -0.105  NuSewer - d x SF + C Where C2 = 4.7 x (EP) -0.105  SF = Sanitary Flow of GWI = Groundwater I (EP) -0.106 (GWI = GWI	NuSewer 210L/EP/d   NuSewer - d x SF + GW    Where - Sanitary Flow of 150L/EP/d   SF = Sanitary Flow of 150L/EP/d   GW  = Groundwater Infiltration of 30L/EP/d   EP   30   300   600   1.2k   3k   12k   d"   7.8   4.2   3.7   3.2   2.7   2.2   2.2		
Smart Sewer Option RIGS Nusewer or RIGS  Average Dry Weather Flow (ADWF)  For RIGS 200 L/EP/d  For Nusewer 180 L/EP/d  For "baseline" calculations for existing Conventional Sewer 210L/EP/d	For "baseline" calculations for existing Conventional Sewer 210L/EP/d		
Smart Sewer Option RIGS NuSewer or RIGS NuSewer or RIGS	For RIGS 200 L/EP/d For NuSewer 180 L/EP/d		
Const Course Defen Course BICC	NUSEWEI OF NIGS	erage Dry Weather Flow (ADWF)	+
	RIGS Nispens or RIGS		4

Version 1.0 - 1 July 2013 SEQ WS&S D&C Code - Design Criteria

28 of (

<sup>11</sup> Based on licence requirements
12 For "Duty/standby" arrangement, in a 2 pump sewerage pump station, EACH pump delivers PWWF and only 1 pump runs at a time. Under a "Duty/Assist" operating philosophy each pump delivers C1 x ADWF and 2 pumps together deliver PWWF
12 For "Duty/standby" arrangement, in a 2 pump sewerage pump station, EACH pump delivers PWWF and only 1 pump runs at a time. Under a "Duty/Assist" operating philosophy each pump delivers C1 x ADWF and 2 pumps together deliver PWWF
12 For "Duty/standby" arrangement, in a 2 pump sewerage pump station, EACH pump delivers PWWF and only 1 pump runs at a time. Under a "Duty/Assist" operating philosophy each pump delivers C1 x ADWF and 2 pumps together deliver PWWF
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14 For "Duty/standby" arrangement, in a 2 pump sewerage pump station, EACH pump delivers PWWF and only 1 pump runs at a time. Under a "Duty/Assist" operating philosophy each pump delivers C1 x ADWF and 2 pumps together deliver PWWF
15 For "Duty/standby" arrangement, in a 2 pump sewerage pump station, EACH pump delivers PWWF and only 1 pump runs at a time. Under a "Duty/Assist" operating philosophy each pump delivers C1 x ADWF and 2 pumps together deliver PWWF
16 For "Duty/standby" arrangement, in a 2 pump sewerage pump station, EACH pump delivers PWWF and only 1 pump runs at a time. Under a "Duty/Assist" operating philosophy each pump delivers C1 x ADWF and 2 pumps together deliver PWWF
18 For "Duty/standby" arrangement, in a 2 pump sewerage pump station, EACH pump delivers PWWF and only 2 pump sewerage pump



LOGAN









D9						_																					D8					8
Average Dry Weather Flow (ADWF) for Treatment Plants	Minimum Velocity	Maximum depth of flow																					below)	(subject to minimum velocity stated	Minimum nino aradon	- Roughness Equation	Gravity Sewer Requirements (Conventional)	Odour Management Requirements	Roughness	Maximum velocity		Parameter
263L/EP/d																												Odour management rec			Gold Coast	
																												uirements (including dete			Logan Redland	
	Maxin																375	300	225	150		100	RIGS (PVC) (mm)			A		ntion times) to be de	As per (		nd	
	านm: 3.0m/s (re	-							1200	1000		800		630		500	400	315	250		160	110	(PE) (mm)		Mis	Smart Sewers		termined as par	Clause 10.3.3 of	٠	Unitywater	
As per	0.7m/s at PDWI fer Cl 4.5.9.1 of	75% d (at PWWF)	Note 1 – where may be laid at 1 agreed reduction main line sewer	1800	1650	1500	1350	1200	1050	900	825	750	675	600	525	450	375	300	225	150		100	Nominal Bore (mm)	Millimini Sewer Grades	0	(Nu Sewer and	Manning's	t of the odour in	WSA 04 Sewag	3m/s	vater	
As per network flows	0.7m's at PDWF Maximum: $3.0m$ 's (refer Cl $4.5.9.1$ of the 2002 Sewer Code)	VF)	Note 1 — where approved by the Water Agency, DN 150 main line sewers may be laid at 1:200 in Canal Developments together with a Water Agency agreed reduction in the minimum PDWF Velocity Criteria for the DN 150 main line sewer	1:4200	1:3700	1:3250	1:2800	1:2400	1:2000	1:1600	1:1380	1:1200	1:1050	1:900	1:750	1:700	1:550	1:400	1:300		House connection Branch and/or sewers for first 10 allotments: 1:100	House Connection Branch, one allotment only at 1:60	slope	sidues	70000	All Smart Sewers (Nu Sewer and RIGS) - n = 0.0128		Odour management requirements (including detention times) to be determined as part of the odour impact study for the site (refer Sewerage Pump Station Code (as amended) Clause 2.5)	As per Clause 10.3.3 of WSA 04 Sewage Pumping Station Code		Queensland Urban Utilities	

SEQ WS&S D&C Code - Design Criteria

Version 1.0 - 1 July 2013

Water Supply and Sewer Preliminary Analysis

### **APPENDIX**

WATER INFRASTRUCTURE PLANS

- FIGURE 202
- FIGURE 203
- FIGURE 204
- FIGURE 205







Figure 202 - Proposed Water Infrastructure (Western Area)

**Northshore Hamilton PDA** 



Map Produced by JAPAC North (Traffic & Transport)
Date: 3/11/2020
Coordinate System (DDA 1894 - MGA Zone 56
Project 790523 Northshore Hamton (LaP Map 20190822 ags Rev A
Map: 790523 Northshore Hamton (LaP Map 20190822 ags

1:5,000 Scale at A3





## **Northshore Hamilton PDA**

( ) Cardno

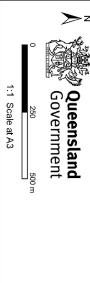
Map Produced by APAC North (Traffic & Transport)
Date: 3/11/2020
Coordinate System GDA 1994 - MGA Zone 56
Polect 70022 - MGA Zone 56
Map:790523 Northshore Hamiton LGIP Map 20190822 ags RevA

1:5,000 Scale at A3

\_\_\_\_500 m

Figure 203 - Proposed Water Infrastructure (Eastern Area)





# Northshore Hamilton PDA

Figure 204 - Existing and to be Decommissioned Water Infrastructure (Western Area)



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 All Right Repenved.
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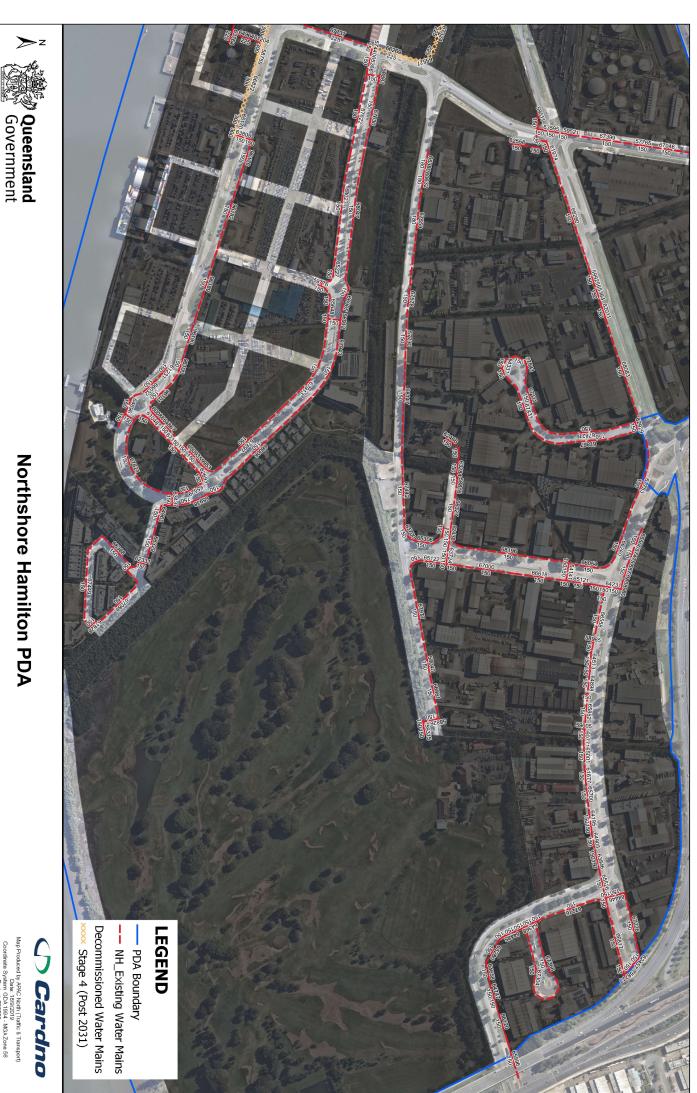




Figure 205 - Existing and to be Decommissioned Water Infrastructure (Eastern Area)

1:1 Scale at A3

Map Produced by APAC Moth (Trains a Trainsport)
Date: 1892/2019
Coordinate System GDA 1994- M3A Zone 56
Polystar 705/233 M3A 20190822 ags RevA
Map:790523 Northshore Haritton LGIP Map 20190822 ags RevA

Water Supply and Sewer Preliminary Analysis

### **APPENDIX**

SEWERAGE INFRSTRUCTURE PLANS

- FIGURE 301
- FIGURE 302
- FIGURE 303
- FIGURE 304







1:1 Scale at A3

**Northshore Hamilton PDA** 

Figure 301 - Proposed Sewer (Western Area)



Map Produced by APAC North (Triaffic & Transport)
Date: 2/11/2007
Coordinate System GDA 1984 - MGA Zone 56
Map: 790523 Northshore Hamiton LGIP Map 20190822 ags RevA
All Systems (Map 20190822 ags RevA
All Systems (Map 20190822 ags RevA





1:1 Scale at A3

## **Northshore Hamilton PDA**

Figure 302 - Proposed Sewer (Eastern Area)



Map Produced by APAC North (Traffic & Transport)
Date: 2/11/2020
Coordinate System GDA 1994 - MGA Zone 56
Doject 700223 MGA Zone 56
Map:790523 Northshore Hamiton LGIP Map 20190822 ags RevA





Northshore Hamilton PDA

Figure 303 - Existing and to be Decommissioned Sewer (Western Area)



Map Produced by APAC North (Traffic & Transport)
Dobe 189/2019
Coordinate System GDA 1894-1 MGA Zone 56
Poljett GDA 189/2019
Map 790523 Northshore Hamiton IGRO 2023
Northshore Hamiton IGRO 2





**Queensland** Government

1:1 Scale at A3

Figure 304 - Existing and to be Decommissioned Sewer(Easern Area)



Map Produced by APAC North (Traffic & Transport)
Date: 1892/0119
Coordinate System GD, 1892-1 MBA Zone 56
Polyett - 1905/23 1905/23 Aps Rev/
Map 790523 Northshore Hamiton (GD/S)

Souther Hamiton (GD/S)

Souther Hamiton (GD/S)

The coolered is analysis of June Limited (Sept. of the Map 2011) of the three of our Map 1 of the Map 2011 of the Map 2011

Water Supply and Sewer Preliminary Analysis

### **APPENDIX**

F

### COST ESTIMATE – WATER AND SEWERAGE

- FIGURE 308
- FIGURE 309



### FIGURE - 308

																		-	_			-
P-16(2)	P-16(1)	P-35	P-34	P-31	P-30	P-29	P-25	P-20(2)	P-20(1)	P-24	P-23	P-22	P-21	P-19	P-18	P-17	P-15	WATER SUPPLY MAINS	WATER	ASSET ID		
NON-TRUNK	NON-TRUNK	TRUNK	TRUNK	TRUNK	TRUNK	TRUNK	TRUNK	NON-TRUNK	NON-TRUNK	NON-TRUNK	TRUNK	TRUNK	TRUNK	NON-TRUNK	NON-TRUNK	NON-TRUNK	NON-TRUNK			TRUNK / NON-TRUNK		
2	3	2	2	2	2	2	4	4	4	4	4	4	4	4	4	2	ω			STAGING		
WATERMAIN	WATERMAIN	WATERMAIN	WATERMAIN	WATERMAIN	WATERMAIN	WATERMAIN	WATERMAIN	WATERMAIN	WATERMAIN	WATERMAIN	WATERMAIN	WATERMAIN	WATERMAIN	WATERMAIN	WATERMAIN	WATERMAIN	WATERMAIN			ASSET DESCRIPTION		
PE	PE	PE	PE	PE	PE	PE	PE	PE	PE	PE	PE	PE	PE	PE	PE	PE	PE			MATERIAL		
180	180	315	315	315	315	315	355	180	180	180	450	450	450	180	180	180	180			DIA (mm)	NORTHSH	
37	79	105	157	52	14	25	142	202	241	41	56	55	194	137	127	125	108			LENGTH (m)	ORE HAMI	000
\$ 312	\$ 312	\$ 448	\$ 448	\$ 448	\$ 448	\$ 448	\$ 719	\$ 312	\$ 312	\$ 312	\$ 990	\$ 990	\$ 990	\$ 312	\$ 312	\$ 312	\$ 312			UNIT COST EX ADJ. FACTOR (\$2019/UNIT)	LTON PDA	
ASS areas	ASS areas	ASS areas	ASS areas	ASS areas	ASS areas	ASS areas	ASS areas	ASS areas	ASS areas	ASS areas	ASS areas	ASS areas	ASS areas	ASS areas	ASS areas	ASS areas	ASS areas			SOIL TYPE	NORTHSHORE HAMILTON PDA - FUTURE ASSETS	
HIGH	нібн	нібн	нібн	нібн	HIGH	HIGH	нібн	нісн	HIGH	HIGH	HIGH	HIGH	нібн	нібн	нібн	HIGH	HGH			CONSTRUCTION CONSTRAINTS	ASSETS	
2.28	2.28	2.28	2.28	2.28	2.28	2.28	2.28	2.28	2.28	2.28	2.28	2.28	2.28	2.28	2.28	2.28	2.28			UNIT COST ADJ. FACTOR		
\$ 711	\$ 711	\$ 1,020	\$ 1,020	\$ 1,020	\$ 1,020	\$ 1,020	\$ 1,638	\$ 711	\$ 711	\$ 711	\$ 2,256	\$ 2,256	\$ 2,256	\$ 711	\$ 711	\$ 711	\$ 711			UNIT COST INC. ADJ. FACTOR		
\$ 26,220	\$ 55,890	\$ 107,490	\$ 160,210	\$ 52,930	\$ 14,720	\$ 24,990	\$ 232,920	\$ 143,870	\$ 171,190	\$ 29,260	\$ 125,470	\$ 123,600	\$ 437,640	\$ 97,680	\$ 90,430	\$ 88,740	\$ 76,590			BASE COST		
\$ 3,409	\$ 7,266	\$ 13,974	\$ 20,827	\$ 6,881	\$ 1,914	\$ 3,249	\$ 30,280	\$ 18,703	\$ 22,255	\$ 3,804	\$ 16,311	\$ 16,068	\$ 56,893	\$ 12,698	\$ 11,756	\$ 11,536	\$ 9,957		13%	PROJECT MANAGEMENT & DESIGN COSTS		
\$ 7,407	\$ 15,789	\$ 30,366	\$ 45,259	\$ 14,953	\$ 4,158	\$ 7,060	\$ 65,800	\$ 40,643	\$ 48,361	\$ 8,266	\$ 35,445	\$ 34,917	\$ 123,633	\$ 27,595	\$ 25,546	\$ 25,069	\$ 21,637		25%	CONTINGENCY COST		
\$ 37,036	\$ 78,945	\$ 151,830	\$ 226,297	\$ 74,764	\$ 20,792	\$ 35,298	\$ 329,000	\$ 203,216	\$ 241,806	\$ 41,330	\$ 177,226	\$ 174,585	\$ 618,167	\$ 137,973	\$ 127,732	\$ 125,345	\$ 108,183			TOTAL CAPITAL COST		

180   258   5 312   ASS areas   HIGH   2.28   5 711   5 183,140   5 2,126   5 4,619		202	\$ 4,557,5UD												
180   258   \$ 312   ASS areas   HIGH   228   \$ 711   \$ 183,140   \$ 2,380   \$ 5,1737   \$ 2,500   \$ 2,300   \$ 5,1737   \$ 2,500   \$ 2,300   \$ 2,300   \$ 5,1737   \$ 2,500   \$ 2,30															
180   258   5 312   ASS reas   HIGH   2.28   5 711   5 18,340   5 23,808   5 11,167   5	\$ 24,563	-			.28	HIGH	+			315	PE	WATERMAIN	2	TRUNK	P-33(2)(2)
180   258   \$ 312   ASS areas   HIGH   2.28   \$ 711   \$ 183.40   \$ 23,808   \$ 21,757   \$ 2,750	\$ 21,710				28	HIGH				315	PE	WATERMAIN	2	TRUNK	P-33(2)(1)
180   258   5   312   ASS areas   HIGH   2.28   5   711   5   183,140   5   23,808   5   11,167   5	\$ 17,837				.28	HIGH				355	PE	WATERMAIN	4	TRUNK	P-26(2)
180   258   S   312   ASS areas   HIGH   2.28   S   711   S   18.31.40   S   23.808   S   51.737   S	\$ 67,356	-	1 1		.28	HIGH	1. 1		Ш	355	PE	WATERMAIN	4	TRUNK	P-26(1)
180   258   \$ 312   ASS areas   HIGH   2.28   \$ 711   \$ 183,140   \$ 2,286   \$ 51,737   \$	\$ 6,359				.28	HIGH				180	PE	WATERMAIN	2	NON-TRUNK	P-51(2)
180   258   5 312   ASS areas   HIGH   2.28   5 711   5 18.3.140   5 23.808   5 51.737   5 25.037	\$ 19,518					HIGH				180	PE	WATERMAIN	2	NON-TRUNK	P-51(1)
180   258   \$ 312   ASS areas   HIGH   2.28   \$ 711   \$ 183,140   \$ 23,808   \$ 23,208   \$ 51,737   \$	\$ 6,591				28	HIGH	ASS			180	PE	WATERMAIN	2	NON-TRUNK	P-49(2)
180   258   \$ 312   ASS areas   HIGH   2.28   \$ 711   \$ 183,140   \$ 23,808   \$ 51,737   \$	\$ 40,536				.28	HIGH				180	PE	WATERMAIN	2	NON-TRUNK	P-49(1)
180   258   5   312   ASS areas   HIGH   2.28   5   711   5   18,340   5   2,126   5   4,619   5   4	\$ 6,664			711	.28	HIGH	ASS			180	PE	WATERMAIN	2	NON-TRUNK	P-48(2)
180   258   \$ 312   ASS areas   HIGH   2.28   \$ 711   \$ 183,140   \$ 23,808   \$ 51,737   \$	\$ 39,420			711	.28	HIGH	$\vdash$		Ш	180	PE	WATERMAIN	з	NON-TRUNK	P-48(1)
180 258 \$ 312 ASS areas HIGH 2.28 \$ 711 \$ 183,140 \$ 23,808 \$ 51,737 \$ 250 250 46 \$ 374 ASS areas HIGH 2.28 \$ 711 \$ 183,140 \$ 23,808 \$ 51,737 \$ 250 250 46 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 39,530 \$ 5,139 \$ 11,167 \$ 250 250 62 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 53,140 \$ 6,908 \$ 15,012 \$ 250 359 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 36,1250 \$ 7,963 \$ 11,167 \$ 250 250 359 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 306,155 \$ 39,800 \$ 11,000 \$ 86,489 \$ 250 120 \$ 312 ASS areas HIGH 2.28 \$ 711 \$ 72,470 \$ 9,421 \$ 20,473 \$ 180 102 \$ 312 ASS areas HIGH 2.28 \$ 711 \$ 72,470 \$ 9,421 \$ 20,473 \$ 180 102 \$ 374 ASS areas HIGH 2.28 \$ 711 \$ 72,470 \$ 9,421 \$ 20,473 \$ 180 102 \$ 374 ASS areas HIGH 2.28 \$ 711 \$ 72,470 \$ 9,421 \$ 20,473 \$ 180 102 \$ 374 ASS areas HIGH 2.28 \$ 711 \$ 72,470 \$ 9,421 \$ 20,473 \$ 180 102 \$ 374 ASS areas HIGH 2.28 \$ 711 \$ 72,470 \$ 9,421 \$ 20,473 \$ 16,390 \$ 13,831 \$ 30,055 \$ 16,390 \$ 13,831 \$ 30,055 \$ 16,390 \$ 13,831 \$ 30,055 \$ 16,390 \$ 13,831 \$ 30,055 \$ 16,390 \$ 13,831 \$ 30,055 \$ 16,390 \$ 13,831 \$ 30,055 \$ 16,390 \$ 13,831 \$ 30,055 \$ 16,390 \$ 13,831 \$ 30,055 \$ 16,390 \$ 13,831 \$ 30,055 \$ 16,390 \$ 13,831 \$ 30,055 \$ 16,390 \$ 13,831 \$ 30,055 \$ 16,390 \$ 13,831 \$ 30,055 \$ 10,050 \$ 10,0	\$ 24,747 \$			853	.28	HIGH	$\rightarrow$			250	PE	WATERMAIN	2	NON-TRUNK	P-38(2)
180 258 \$ 312 ASS areas HIGH 2.28 \$ 711 \$ 183,140 \$ 23,808 \$ 51,737 \$ 24,619 \$ 250 46 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 39,530 \$ 2,126 \$ 4,619 \$ 250 46 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 39,530 \$ 5,139 \$ 11,167 \$ 250 46 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 39,530 \$ 5,139 \$ 11,167 \$ 250 A5	\$ 37,154 \$			853	.28	HIGH	_			250	PE ?	WATERMAIN	2	NON-TRUNK	P-38(1)
180 258 \$ 312 ASS areas HIGH 2.28 \$ 711 \$ 183,140 \$ 23,808 \$ 51,737 \$ 250,000 \$ 250 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 39,530 \$ 5,139 \$ 11,167 \$ 250 46 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 39,530 \$ 5,139 \$ 11,167 \$ 250 359 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 39,530 \$ 5,139 \$ 11,167 \$ 250 359 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 30,155 \$ 2,063 \$ 11,071 \$ 250 359 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 30,155 \$ 3,000 \$ 120 \$ 312 ASS areas HIGH 2.28 \$ 853 \$ 30,155 \$ 39,200 \$ 1,303 \$ 2,0473 \$ 180 102 \$ 312 ASS areas HIGH 2.28 \$ 853 \$ 30,155 \$ 39,200 \$ 5,139 \$ 11,67 \$ 2,281 \$ 2,29 \$	\$ 7,193 \$			711	28	HIGH	+			180	ם ה	WATERNAIN	4 u	NON-TRUNK	P-47(1)
180   258   \$ 312   ASS areas   HIGH   2.28   \$ 711   \$ 183,140   \$ 23,808   \$ 51,737   \$	\$ 36,465 \$			1,020	.28	HIGH	+			315	PE PE	WATERMAIN	2	TRUNK	P-32(1)(1)(2)
180   258   312   ASS areas   HIGH   2.28   5 711   5 183,140   5 23,808   5 51,737   5 180,140   180   258   312   ASS areas   HIGH   2.28   5 711   5 183,140   5 23,808   5 51,737   5 183,140   180   238   5 312   ASS areas   HIGH   2.28   5 711   5 16,350   5 2,126   5 4,619   5 1,737   5 183,140   5 23,808   5 1,737	\$ 15,735 \$			1,020	.28	HIGH	-			315	PE	WATERMAIN	2	TRUNK	P-32(1)(1)(1)
180 258 \$ 312 ASS areas HIGH 2.28 \$ 711 \$ 183,140 \$ 23,808 \$ 51,737 \$ 180 250 46 \$ 374 ASS areas HIGH 2.28 \$ 711 \$ 183,140 \$ 23,808 \$ 51,737 \$ 180 250 46 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 39,530 \$ 5,139 \$ 11,167 \$ 15,000 \$ 125 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 306,155 \$ 39,800 \$ 11,303 \$ 12	\$ 30,586 \$			711	.28	HIGH	$\vdash$			180	PE	WATERMAIN	3	NON-TRUNK	P-50
180 258 \$ 312 ASS areas HIGH 2.28 \$ 711 \$ 183,140 \$ 23,808 \$ 51,737 \$ 180 250 46 \$ 374 ASS areas HIGH 2.28 \$ 711 \$ 183,140 \$ 23,808 \$ 51,737 \$ 180 250 46 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 39,530 \$ 5,139 \$ 11,167 \$ 180 250 72 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 61,250 \$ 7,963 \$ 11,303 \$ 180 102 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 306,155 \$ 39,800 \$ 13 \$ 312 ASS areas HIGH 2.28 \$ 853 \$ 306,155 \$ 39,800 \$ 86,849 \$ 5 180 250 70 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 59,960 \$ 11,65 \$ 2,531 \$ 180 102 \$ 312 ASS areas HIGH 2.28 \$ 711 \$ 72,470 \$ 9,421 \$ 20,473 \$ 180 250 70 \$ 374 ASS areas HIGH 2.28 \$ 711 \$ 72,470 \$ 9,421 \$ 20,473 \$ 180 250 70 \$ 374 ASS areas HIGH 2.28 \$ 711 \$ 72,470 \$ 9,421 \$ 20,473 \$ 16,939 \$ 180 21 \$ 312 ASS areas HIGH 2.28 \$ 711 \$ 8,960 \$ 1,165 \$ 2,531 \$ 16,939 \$ 180 21 \$ 312 ASS areas HIGH 2.28 \$ 853 \$ 106,390 \$ 13,831 \$ 30,055 \$ 16,939 \$ 13,831 \$ 30,055 \$ 13,831 \$ 30,055 \$ 14,944 \$ 15,000 \$ 13,831 \$ 20,055 \$ 14,944 \$ 15,000 \$ 13,831 \$ 20,055 \$ 14,944 \$ 15,000 \$ 13,831 \$ 20,055 \$ 14,944 \$ 15,000 \$ 13,831 \$ 20,055 \$ 14,944 \$ 15,000 \$ 13,831 \$ 20,055 \$ 14,944 \$ 15,000 \$ 13,831 \$ 20,055 \$ 14,944 \$ 15,000 \$ 13,831 \$ 20,055 \$ 14,944 \$ 15,000 \$ 13,831 \$ 20,055 \$ 14,944 \$ 15,000 \$ 13,831 \$ 20,055 \$ 14,944 \$ 15,000 \$ 13,831 \$ 20,055 \$ 14,944 \$ 15,000 \$ 13,831 \$ 20,055 \$ 14,944 \$ 15,000 \$ 14,944 \$ 15,000 \$ 14,944 \$ 15,000 \$ 12,955 \$ 14,944 \$ 14,9	\$ 45,160	_		1,020	.28	HIGH	-		4	315	PE 7	WATERMAIN	2	TRUNK	P-32(1)(2)
180 258 \$ 312 ASS areas HIGH 2.28 \$ 711 \$ 183,140 \$ 23,808 \$ 51,737 \$ 180 250 46 \$ 374 ASS areas HIGH 2.28 \$ 711 \$ 183,140 \$ 23,808 \$ 51,737 \$ 180 250 46 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 39,530 \$ 5,139 \$ 11,167 \$ 15,000 \$ 125 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 61,250 \$ 7,963 \$ 17,303 \$ 180 102 \$ 312 ASS areas HIGH 2.28 \$ 853 \$ 361,250 \$ 7,963 \$ 17,303 \$ 180 102 \$ 312 ASS areas HIGH 2.28 \$ 853 \$ 306,155 \$ 39,800 \$ 86,489 \$ 180 102 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 306,155 \$ 39,800 \$ 86,489 \$ 5 15,012 \$ 180 102 \$ 312 ASS areas HIGH 2.28 \$ 711 \$ 72,470 \$ 9,421 \$ 20,473 \$ 180 125 \$ 374 ASS areas HIGH 2.28 \$ 711 \$ 8,960 \$ 1,165 \$ 2,531 \$ 16,939 \$ 1	\$ 29,555	_		1,020	28   20	HER	+		1	315	ק ק	WATERMAIN	2	TRUNK	P-33(1)
180 258 \$ 312 ASS areas HIGH 2.28 \$ 711 \$ 183,140 \$ 23,808 \$ 51,737 \$ 180 250 46 \$ 374 ASS areas HIGH 2.28 \$ 711 \$ 183,140 \$ 23,808 \$ 51,737 \$ 180 250 46 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 39,530 \$ 5,139 \$ 11,167 \$ 180 250 70 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 306,155 \$ 39,800 \$ 11,267 \$ 2,531 \$ 180 102 \$ 312 ASS areas HIGH 2.28 \$ 853 \$ 59,960 \$ 1,795 \$ 16,939 \$ 250 70 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 59,960 \$ 1,795 \$ 16,939 \$ 3,705 \$ 3,74 ASS areas HIGH 2.28 \$ 853 \$ 59,960 \$ 1,383 \$ 30,055 \$ 5 16,939 \$ 1,383 \$ 30,055 \$ 5 16,939 \$ 1,383 \$ 10,055 \$ 5 16,939 \$ 1,383 \$ 10,055 \$ 1,383 \$ 10,055 \$ 1,383 \$ 10,055 \$ 1,383 \$ 10,055 \$ 1,383 \$ 10,055 \$ 1,383 \$ 10,055 \$ 1,383 \$ 1,38	\$ 4,294	_	1	711	.28	HIGH	-			180	7 PE	WATERMAIN	4	NON-TRUNK	P-46
180 258 \$ 312 ASS areas HIGH 2.28 \$ 711 \$ 183,140 \$ 23,808 \$ 51,737 \$ 180 250 46 \$ 374 ASS areas HIGH 2.28 \$ 711 \$ 18,040 \$ 23,808 \$ 51,737 \$ 180 250 46 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 39,530 \$ 5,139 \$ 11,167 \$ 180 102 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 39,530 \$ 5,139 \$ 11,167 \$ 180 102 \$ 312 ASS areas HIGH 2.28 \$ 853 \$ 306,155 \$ 39,800 \$ 13 \$ 312 ASS areas HIGH 2.28 \$ 711 \$ 72,470 \$ 9,421 \$ 20,473 \$ 250 70 \$ 374 ASS areas HIGH 2.28 \$ 711 \$ 8,960 \$ 1,165 \$ 2,531 \$	\$ 30,055	_	ı	853	⊢	HIGH	-			250	PE	WATERMAIN	2	NON-TRUNK	P-41(2)
180 258 \$ 312 ASS areas HIGH 2.28 \$ 711 \$ 183,140 \$ 23,808 \$ 51,737 \$ 180 250 46 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 39,530 \$ 5,139 \$ 11,167 \$ 180 250 359 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 39,530 \$ 5,139 \$ 15,012 \$ 180 102 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 306,155 \$ 39,800 \$ 13,000 \$ 86,489 \$ 180 13 \$ 312 ASS areas HIGH 2.28 \$ 711 \$ 72,470 \$ 9,421 \$ 20,473 \$ 180 13 \$ 312 ASS areas HIGH 2.28 \$ 711 \$ 8,960 \$ 1,165 \$ 2,531 \$	\$ 16,939	_	Ш	853	.28	HIGH	Н			250	PE	WATERMAIN	2	NON-TRUNK	P-41(1)
180 258 \$ 312 ASSareas HIGH 2.28 \$ 711 \$ 183,140 \$ 23,808 \$ 51,737 \$  180 258 \$ 312 ASSareas HIGH 2.28 \$ 711 \$ 183,140 \$ 23,808 \$ 51,737 \$  180 23 \$ 312 ASSareas HIGH 2.28 \$ 711 \$ 16,350 \$ 2,126 \$ 4,619 \$  250 46 \$ 374 ASSareas HIGH 2.28 \$ 853 \$ 39,530 \$ 5,139 \$ 11,167 \$  250 62 \$ 374 ASSareas HIGH 2.28 \$ 853 \$ 53,140 \$ 6,908 \$ 15,012 \$  250 72 \$ 374 ASSareas HIGH 2.28 \$ 853 \$ 306,155 \$ 9,800 \$ 17,303 \$  180 102 \$ 312 ASSareas HIGH 2.28 \$ 853 \$ 306,155 \$ 9,800 \$ 86,489 \$	\$ 2,531	$\overline{}$			_	HIGH	$\dashv$			180	PE	WATERMAIN	4	NON-TRUNK	P-45
180 258 \$ 312 ASSareas HIGH 2.28 \$ 711 \$ 183,140 \$ 23,808 \$ 51,737 \$ 180 250 46 \$ 374 ASSareas HIGH 2.28 \$ 853 \$ 53,140 \$ 5,130 \$ 11,167 \$ 1250 720 \$ 374 ASSareas HIGH 2.28 \$ 853 \$ 51,250 \$ 12,000 \$ 12	\$ 20.473	_			-	HIGH	$\dashv$			180	PE -	WATERMAIN	4	NON-TRUNK	P-44
180 258 \$ 312 ASS areas HIGH 2.28 \$ 711 \$ 183,140 \$ 23,808 \$ 51,737 \$ 2  180 258 \$ 312 ASS areas HIGH 2.28 \$ 711 \$ 183,140 \$ 23,808 \$ 51,737 \$ 2  180 23 \$ 312 ASS areas HIGH 2.28 \$ 711 \$ 16,350 \$ 2,126 \$ 4,619 \$ 2  250 46 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 39,530 \$ 5,139 \$ 11,167 \$ 2  250 62 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 53,140 \$ 6,908 \$ 15,012 \$ 2  250 77 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 53,140 \$ 6,908 \$ 15,012 \$ 2	\$ 86,489	_			86	HGH	٦.			250	<u> </u>	WATERMAIN	2	NON-TRUNK	P-43
180 258 \$ 312 ASS areas HIGH 2.28 \$ 711 \$ 183,140 \$ 23,808 \$ 51,737 \$ 2  180 258 \$ 312 ASS areas HIGH 2.28 \$ 711 \$ 183,140 \$ 23,808 \$ 51,737 \$ 2  250 46 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 39,530 \$ 5,139 \$ 11,167 \$	\$ 17 303	_			28	HIGH	$\pm$		1	250	PF	WATERMAIN	2	NON-TRIINK	P-47
180 258 \$ 312 ASS areas HIGH 2.28 \$ 711 \$ 183,140 \$ 23,808 \$ 51,737 \$ 2  180 250 46 \$ 374 ASS areas HIGH 2.28 \$ 853 \$ 39,530 \$ 5,139 \$ 11,167 \$	\$ 15,012	_			28	HIGH				250	PE	WATERMAIN	2	NON-TRUNK	P-40
180 258 \$ 312 ASS areas HIGH 2.28 \$ 711 \$ 183,140 \$ 23,808 \$ 51,737 \$ 2	\$ 11,167					HIGH	ASS			250	PE	WATERMAIN	2	NON-TRUNK	P-39
180 258 \$ 312 ASS areas HIGH 2.28 \$ 711 \$ 183,140 \$ 23,808 \$ 51,737 \$ 258	\$ 4,619				28	HIGH				180	PE	WATERMAIN	4	NON-TRUNK	P-37(2)
313 3 446 A33 dieds midm 2.26 \$ 1,020 \$ 136,130 \$ 17,303 \$ 35,039 \$ 135	\$ 51,737					HIGH				180	PE	WATERMAIN	4	NON-TRUNK	P-37(1)
11E 11E 6 140 MCC 1101 110 0 1101 0 1 1 1101 0 1 1 1101 0 1 1 1101 0 1 1 1101 0 1	17,965 \$ 39,039 \$	190 \$	\$ 138,1	\$ 1,020	2.28	HIGH	ASS areas	\$ 448	135	315	PE	WATERMAIN	2	TRUNK	P-36
															WATER SUPPLY MAINS
13% 25%															WATER
MATERIAL  DIA (mm)  LENGTH (m)  UNIT COST EX ADJ. FACTOR (\$2019/UNIT)  SOIL TYPE  CONSTRUCTION CONSTRAINTS  UNIT COST ADJ. FACTOR  UNIT COST INC. ADJ. FACTOR  BASE COST  PROJECT MANAGEMENT & DESIGN COSTS  CONTINGENCY COST	DESIGN COSTS  CONTINGENCY COST	PROJECT MANAGEMENT 9	BASE COST		UNIT COST ADJ. FACTOR		SOIL TYPE		LENGTH (m)	DIA (mm)	MATERIAL	ASSET DESCRIPTION	STAGING	TRUNK / NON-TRUNK	ASSET ID
NORTHSHORE HAMILTON PDA - FUTURE ASSETS						ASSETS	- FUTURE	ON PDA	ORE HAMILI	NORTHSH					

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	NHFZO	OCURIN	NHP17	NHP16	NHP15	NHP14	NHP13	NHP12	NHP19	NHP18	NHP11	NHP10	NHP09	NHP08	NHP07	NHP06	NHP05	NHP04	NHP03	NHP02	NHP01	GRAVITY MAINS	SEWER	ASSET ID
	Irunk	Tl.	Trunk	Non-Trunk	Trunk	Trunk	Trunk	Non-Trunk	Non-Trunk	Non-Trunk	Non-Trunk	Non-Trunk	Non-Trunk	Trunk	Non-Trunk	Trunk	Trunk	Trunk	Trunk	Trunk	Trunk	SNI		TRUNK / NON-TRUNK
	4	٠.	4	4	4	4	4	4	2	2	2	2	2	2	2	2	2	2	2	2	2			STAGING
	GIANIY IIIAIII AIDIIB FIBECE ST	Cravity main along Floors St	Gravity main along Fleece St	Gravity main SC along Curtin Ave (West)	Gravity main SC along Curtin Ave (West)	Gravity main SC along Macarthur Ave (East)	Gravity main SC along Theodore St	Gravity main SC along Macarthur Ave (West)	Gravity main SC along Macarthur Ave (East)	Gravity main SC along Macarthur Ave (East)	Gravity main along Macarthur Ave (East)	Gravity main SC along Macarthur Ave (East)	Gravity main along Macarthur Ave (East)			ASSET DESCRIPTION								
	Too	160	160	160	315	315	250	160	160	180	160	250	250	500	250	500	400	400	315	315	315			DIA (mm)
1,896	0,	67	155	32	72	415	179	31	28	26	45	34	34	76	36	88	131	145	147	81	75			LENGTH (m)
	70	, ה	PΕ	Эd	PΕ	PE	PE	PE	PE	PE	PE	PE	PE	PE	PE	PE	PE	PE	PE	PE	PE			MATERIAL
	\$ 6/1				\$ 1,114	\$ 1,114	\$ 1,139	l	\$ 671	\$ 671	\$ 671	\$ 785	\$ 574	\$ 1,436	\$ 574	\$ 1,436	\$ 1,090	\$ 1,090			\$ 778			UNIT COST EX ADJ. FACTOR (\$2019/UNIT)
	ASS dreas	+	_	ASS areas	_	1 ASS areas	) ASS areas	_	L ASS areas	ASS areas	L ASS areas	ASS areas	1 ASS areas	ASS areas	1 ASS areas	ASS areas					3 ASS areas			SOIL TYPE
	4.29	Ì		3.94					3.58	3.51	3.36	3.57	2.51	3.40	2.52	3.56	3.52				3.63			DEPTH (m)
	I 80	Liigh	High	High	High	High	High	High	High	High	High	High	High	High	High	High	High	High	High	High	High			CONSTRUCTION CONSTRAINTS
	06.2	2 50	2.50	2.50	2.63	2.63	2.63	2.50	2.50	2.50	2.50	2.50	2.28	2.50	2.28	2.50	2.50	2.50	2.50	2.50	2.50			UNIT COST ADJ. FACTOR
				\$ 1			\$ 2	1	\$ 1	\$ 1	\$ 1	\$ 1	\$ 1	\$ 3	\$ 1	\$ 3	\$ 2	\$ 2		\$ 1				UNIT COST INC. ADJ.
\$	¢ c/o/T	+	$\overline{}$	1,675   \$	_	2,927 \$	-	-	1,675 \$	1,675 \$	1,675 \$	1,960 \$	1,308 \$	3,585 \$	1,308 \$	3,585 \$	2,722 \$	2,722 \$		1,943 \$	1,943 \$			FACTOR
4,688,860	112,410	112 /10	259.670	53,780	211,070	1,213,440	536,910	51,430	46,070	44,230	75,050	66,650	45,010	271,010	46,450	315,460	356,270	394,370	285,760	157,350	146,470			BASE COST
	\$ 14,613			\$ 6,991	\$ 27,439			\$ 6,686	\$ 5,989	\$ 5,750	\$ 9,757	\$ 8,665	\$ 5,851	\$ 35,231	\$ 6,039	\$ 41,010	\$ 46,315		37,149	20,456			13%	PROJECT MANAGEMENT & DESIGN COST
	\$ 31,/3b			\$ 15,193					\$ 13,015	\$ 12,495	\$ 21,202	\$ 18,829	\$ 12,715	\$ 76,560	\$ 13,122	\$ 89,117	\$ 100,646	\$ 111,410		\$ 44,451	\$ 41,378		25%	CONTINGENCY COST
\$ 6,623,015	\$ 138,779	٠ ٠	S	\$ 75,964	\$	\$ 1		₩.	\$ 65,074	\$ 62,475	\$ 106,008	\$ 94,143	\$ 63,577	\$ 382,802	\$ 65,611	\$ 445,587		\$	\$	\$ 222,257	\$			TOTAL ESTIMATED COST