# **Plans**

# APPROVED



|   | 2000 1000,  | GENERAL KEY:  |  |
|---|---|---|--|
|   |   | YELLOW PAINTED DIRECTIO   | NAL ARROW  |
| ensland<br>ernment                          | Ċ.  | WHITE "SYMBOL OF ACCESS<br>SQUARE 1200mm SQ. TO CO<br>AS1428.1  | S" 900mm ON BLUE<br>MPLY WITH                                  |
|   |   | PROPRIETARY WHEEL STOP  | PS   |
|   |   | BLACK CONCRETE TO DRIVI<br>THRU ORDER STATION, ALL<br>5% BLACK OXIDE, BORAL MI                                      | E-THRU LANE, DRIVE<br>KERBS AND CHANNELS.<br>NOX B100 OR EQUAL |
|   |   | BOUNDARY LINE   |  |
| BOVE  | В   | BIN WITH CONCRETE BASE  |  |
| ZING  | KR  | KERB RAMP   |  |
|   | C   | SAFETY BOLLARDS, REFER<br>EXTERNAL FINISHES SCHED   | TO<br>JULE   |
|   |   | ILLUMINATED RED LIGHTBO   | x  |
|   |   | 1.2m HIGH PERFORATED SC<br>THRU, REFER TO EXTERNAL  | REEN ALONG DRIVE<br>. FINISHES SCHEDULE                        |
|   |   | 2m HIGH XF12 SLATTED SCI<br>EXTERNAL FINISHES SCHED   | REENS, REFER TO<br>JULE  |
|   |   | LANDSCAPE - REFER TO LAI  | NDSCAPE DRAWINGS   |
| [   | AREA SCHEDULE   |   |  |
|   | LOT SIZE:<br>GFA  | 1   | 925m <sup>2</sup><br>244 m <sup>2</sup>                        |
|   | BIN ROOM  | -   | 18 m²  |
|   | PLANT   | Ş   | ∂ m²   |
|   | ACCESSIBLE PAR  | RKING: 1  | I SPACES   |
|   | DELIVERY PARKI  | NG: 2   | 2 SPACES   |
|   | STAFF SPACES P  | ROVIDED:  | B SPACES   |
|   | TOTAL CAR PARKIN  | G 1   | 3 SPACES   |
|   | MOTORBIKE/EV SCO<br>BICYCLE PARKING   | DOTER PARKING 4   | SPACES<br>SPACES   |
|   | GFA (GROSS FLOOF<br>FROM THE OUTSIDE  | R AREA FOR QLD) - MEASURED<br>E OF EXTERNAL WALLS.  | )  |
| ſ   |   |   |  |
|   | PAVEMENT LEVEL AT DRI<br>FFL FOR EASE OF OPERA  | VE-THRU SERVICE WINDOWS<br>TIONS  | TO MATCH INTERNAL  |
|   | NOTE: SITE PLAN IS DRAV<br>THIS IS ONLY CONCEPT D<br>PRIOR TO COMMENCEME<br>OF SOLAR PANELS ON RC | VIN BASED ON CAD FROM OTH<br>ESIGN. CHECK SURVEY DRAW<br>NT OF ANY SITE WORKS. EXTE<br>DOF TBC<br>NOT FOR CONSTRUCT | ERS.<br>/INGS<br>ENT <b>N</b>                                  |
|   |   |   |  |
| ROJECT LUNC                                 | RV LACK'S   | 5.511110  |  |
| ROJECT HUNG                                 | BRY JACK'S  | PROPOSED SITE   | & SIGNAGE  |
| ROJECT HUNG<br>ALBION<br>254-270 AE<br>ROAD | BRY JACK'S<br>BBOTSFORD   | PROPOSED SITE<br>LOCATION PLAN<br>PROJECT NO. 211106  | & SIGNAGE  |





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Nominated Architect: Ken Sonjes Registered No. 7902 NSW | 2907 WA | 19823 VIC

ARCHITECTS

254-270 ABBOTSFORD ROAD **BOWEN HILLS QLD 4006** 

PROJECT NO. 211106

SCALE

1:100@A3

DRAWING NO. DA20 REV. 1





-FEATURE CLADDING TO PORTAL WITH ILLUMINATED

> PLANS AND DOCUMENTS referred to in the PDA DEVELOPMENT APPROVAI



Approval no.: DEV2023/1392 Date: 1 September 2023

LIGHTWEIGHT AWNING ABOVE DRIVE THRU LANE

#### NOT FOR CONSTRUCTION

| ROJECT HUNGR | Y JACK'S |
|--------------|----------|
|--------------|----------|

#### ALBION

254-270 ABBOTSFORD ROAD **BOWEN HILLS QLD 4006**  **PROPOSED ELEVATIONS 2 OF** 2

PROJECT NO. 211106

DRAWING

SCALE 1 : 100@A3 DRAWING NO. DA21 REV. 1





254-270 ABBOTSFORD ROAD **BOWEN HILLS QLD 4006** 

#### ALBION

PROJECT HUNGRY JACK'S

#### DRAWING ORDER STATION CANOPY

DRAWING NO.

DA40

REV.

1

#### NOT FOR CONSTRUCTION

DETAILS

SCALE

PROJECT NO. 211106

As indicated@A3







3M HIGH BLADE WALL WITH FEATURE CLADDING & ILLUMINATED 2m BUN LOGO & JACK'S CAFE SIGN

#### ILLUM. BUN LOGO & JACKS CAFE SIGN 1 1:50

| S01  | ILLUMINATED BUN LOGO & JACK'S CAFE     |
|------|--|
| S02  | ILLUMINATED HEIGHT BAR GANTRY          |
| S03  | DRIVE THRU PREVIEW MENUBOARD           |
| S04  | DRIVE THRU MENUBOARD AND SPEAKERS      |
| S05  | ILLUMINATED RED BAND FASCIA            |
| S06A | 2.4m ILLUMINATED SQUARE BUN LOGO       |
| S07  | EXTERNAL RECESSED PRINTED GRAPHIC      |
| S08  | DRIVE THRU PRINTED GRAPHIC             |
| S09A | DT WINDOW BOOTH 'PAY HERE' SIGN        |
| S09B | DT WINDOW BOOTH 'PICK-UP' SIGN         |
| S10A | 2.3m HIGH ILLUMINATED DIRECTIONAL SIGN |
| S10B | 2.3m HIGH ILLUMINATED DIRECTIONAL SIGN |
| S11  | WAITING BAY SIGN AND LINEMARKING       |
| S12  | DELIVERY LINEMARKING                   |
| S13a | PEDESTRIAN SIGN                        |
| S14  | DIAGONAL BUN LOGO FILM GRAPHIC         |
| S15  | ILLUMINATED HUNGRY JACK'S LETTERSET    |



#### ILLUMINATED DRIVE THRU MENUBOARDS. BUILDER TO INSTALL CONC. PLINTH AND **MENUBOARD & SPEAKER** SKETCH VERIFIALD DIVERSIONS AND EVERSION OF THE COMMENCEMENT OF WORK. DISCREPANCIES PRIOR TO THE COMMENCEMENT OF WORK. DRAWINGS ARE TO BE READ IN CONJUCTION WITH ALL CONTRACT DOCUMENTS. USE FIGURED DIMENSIONS ONLY. DO NOT SCALE FROM Hurstville NSW 2220 ABN 48 602 616 928 L6 - 100 WILLIAM STREET PLANNING PERMIT JAC WOOLLOOMOOLOO NSW 2011 O AMENDED DA PH: 02 9579 6292 DRAWINGS. THE COMPLETION OF THE ISSUE DETAILS CHECKED AND ◯ BA/CC AUTHORISED SECTION IS CONFIRMATION OF THE STATUS OF THE COPYRIGHT HUNGRY JACK'S PTY LTD COPYING, REPRODUCTION OR USE OF THIS DESIGN OR DRAWING IN WHOLE OR PART IS PROHIBITED WITHOUT THE WRITTEN CONSENT DRAWING. THE DRAWING SHALL NOT BE USED FOR CONSTRUCTION UNLESS ENDORSED 'FOR CONSTRUCTION' AND AUTHORISED FOR ISSUE Nominated Architect: Ken Sonj ARCHITECTS 7902 NSW | 2907 WA | 19823 VIC OF HUNGRY JACK'S PTY LTD





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7902 NSW | 2907 WA | 19823 VIC

**BOWEN HILLS QLD 4006** 

#### **SIGNAGE DETAILS 2 OF 3**

N.T.S

DRAWING NO. DA42 REV. 1

50

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DRW LW

ARCHITECTS



🔘 ѕкетсн PLANNING PERMIT ◯ AMENDED DA ◯ BA/CC 

1. ALL HJS SIGNAGE BY HJ SIGNAGE SUPPLIER.

AUTHORITY BY BUILDER

CLIENT

JACK

6. ALL LINE MARKING BY BUILDER

2. STEEL CAGE AND BOLTS FOR HJS BRANDING SIGNAGE SUPPLIED BY HJs SIGNAGE CONTRACTOR

3. ALL CONCRETE FOOTING D&C BY BUILDER - BLACK OXIDE 4. ALL POWER, DATA, CONDUIT FOR SIGNAGE BY BUILDER 5. ALL TRAFFIC SIGNS TO COMPLY WITH LOCAL TRAFFIC

| NOTES: |  |  |  |
|--------|--|--|--|

| 502  | ILLUMINATED HEIGHT BAR GANTRY          |
|------|--|
| S03  | DRIVE THRU PREVIEW MENUBOARD           |
| S04  | DRIVE THRU MENUBOARD AND SPEAKERS      |
| S05  | ILLUMINATED RED BAND FASCIA            |
| S06A | 2.4m ILLUMINATED SQUARE BUN LOGO       |
| S07  | EXTERNAL RECESSED PRINTED GRAPHIC      |
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| S11  | WAITING BAY SIGN AND LINEMARKING       |
| S12  | DELIVERY LINEMARKING                   |
| S13a | PEDESTRIAN SIGN                        |
| S14  | DIAGONAL BUN LOGO FILM GRAPHIC         |
| S15  | ILLUMINATED HUNGRY JACK'S LETTERSET    |









DIAGONAL BUN LOGO, OPAQUE VINYL FILM TO SHOPFRONT GLAZING, BY SIGNAGE SUPPLIER

REFER TO ELEVATIONS FOR SETOUT

DIAGONAL BUN LOGO FILM (S14) 1:50

> PLANS AND DOCUMENTS referred to in the

PDA DEVELOPMENT APPROVAL

Approval no.: **DEV2023/1392** Date: 1 September 2023





(S15) ILLUI

ILLUMINATED HUNGRY JACK'S LETTERSET

254-270 ABBOTSFORD ROAD BOWEN HILLS QLD 4006 SIGNAGE DETAILS 3 OF 3

NOT FOR CONSTRUCTION

PROJECT NO. 211106

REV.

PROJECT HUNGRY JACK'S

#### ALBION

DRAWING

1

SCALE

As indicated@A3

DA43

DRAWING NO.

## EXTERNAL FINISHES SCHEDULE

| 0005  |  |   |   |  |
|-------|--|---|---|--|
| XF1A  | PAINT FC PANEL                               | COLOUR: BEIGE<br>FINISH: SATIN<br>APPLY CLEAR ANTI GRAFFITI COATING     | EXTERNAL WALLS, SEE ELEVATIONS<br>FOR LOCATION                          |  |
| XF1B  | PAINT FC PANEL                               | COLOUR: BROWN<br>FINISH: SATIN<br>APPLY CLEAR ANTI GRAFFITI COATING     | EXTERNAL WALLS, SEE ELEVATIONS<br>FOR LOCATION                          |  |
| XF1C> | PAINT FC PANEL                               | COLOUR: DARK GREY<br>FINISH: SATIN<br>APPLY CLEAR ANTI GRAFFITI COATING | EXTERNAL WALLS, SEE ELEVATIONS<br>FOR LOCATION                          |  |
| XF2   | PAINT FINISH                                 | COLOUR: DARK GREY<br>FINISH: SATIN                                      | POSTS AND METAL WORKS,<br>DT WINDOW 3 AWNING                            |  |
| XF3   | POWDERCOAT FINISH                            | COLOUR: CHARCOAL<br>FINISH: SATIN                                       | DOOR & WINDOW FRAMES,<br>LOUVERS SUN SHADING                            |  |
| XF4   | FEATURE CLADDING WALL                        | TIMBERLOOK CLADDING (WOODGRAIN)   | EXTERNAL WALLS,<br>PORTAL WALLS WHERE NOTED,<br>DRIVE-THRU WINDOW WALLS |  |
| XF6   | PAINT<br>COMPRESSED FIBRE<br>CEMENT CLADDING | COLOUR: OFF WHITE<br>FINISH: SATIN                                      | EXTERIOR SOFFITS,<br>ENTRY AND DELIVERY SOFFIT                          |  |
| XF7   | ILLUMINATED LIGHT BOX                        | INTERNALLY ILLUMINATED RED LIGHT<br>BOX                                 | BUILDING FASCIA,<br>REFER TO ELEVATION                                  |  |
| XF8   | PRE-FINISHED METAL                           | COLOURBOND<br>COLOUR: DARK GREY TO MATCH XF2                            | GUTTERS/ FASCIA   |  |
| XF12  | SLATTED COMPOSITE<br>CLADDING - TIMBERLOOK   | COLOUR: DARK BROWN  | DELIVERY AREA SCREENS   |  |

| CODE  | DESCRIPTION                  | FINISH SPECIFICATION  | LOCATION  | SAMPLE PICTURE FOR REFERENCE ONLY |
|-------|------------------------------|---|---|-----------------------------------|
| XF14  | METAL LOUVRE                 | BRAND: HOLOAKE OHL<br>COLOUR: DARK GREY POWDERCOAT  | CO <sup>2</sup> ENCLOSURE, PLANT<br>ENCLOSURE                       |                                   |
| XF15  | ALUMINIUM<br>COMPOSITE PANEL | COLOUR: DARK GREY   | FRONT ENTRY AWNING  |                                   |
| XF16  | PERFORATED SCREENS           | COLOUR: DARK GREY   | ALONG DRIVE THRU  |                                   |
| XF17> | SLATTED ALUM. SCREENS        | COLOUR: LIGHT GREY<br>SLATTED ALUMINIUM SCREENS   | ON ROOF MECHANICAL PLATFORM<br>AND WHERE NOTED TO CONCEAL<br>PLANTS |                                   |
| WS    | WHEEL STOP                   | PRODUCT: REPLAS WHEELSTOPS<br>DIMENSION: 100mm X 135mm<br>LENGHT: 1650<br>COLOR: YELLOW - MOD 3# BLACK WITH 4<br>DIAMOND REFLECTORS ON FRONT, 2<br>ROUND REFLECTORS ON BACK<br>CONTACT: KIMBERLEY WILLIAMS<br>0459 269 692<br>kimberley.williams@replas.com.au  | SEE SITE PLAN FOR LOCATION  |                                   |
| B1    | VEHICLE BOLLARD              | BRAND: SAFETY EXPRESS OR EQUAL<br>PRODUCT: BELOW GROUND 90mm Ø<br>GALVANISED BOLLARD<br>COLOUR: SILVER WITH CLASS 1 RED<br>REFLECTIVE TAPE<br>HEIGHT: 1300mm (1000mm ABOVE<br>GROUND AND 300mm BELOW GROUND)<br>FIXING: ANCHOR ROD INCLUDED AT BASE<br>WHICH CAN BE REMOVED WHEN CORE<br>DRILLING INTO EXISTING CONCRETE OR<br>INSERTED WHEN SETTING IN NEW<br>CONCRETE | SEE SITE PLAN FOR LOCATION  |                                   |
|       | PLANS AND DO                 |   |   | l                                 |

PLANS AND DOCUMENTS referred to in the PDA DEVELOPMENT APPROVAL Approval no.: **DEV2023/1392** Date: **1 September 2023** 



| CLIENT   | REV | DATE     | AMENDMENT    | DRW |  |                               |   |                 |
|--|-----|----------|--------------|-----|--|-------------------------------|---|-----------------|
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#### ALBION

254-270 ABBOTSFORD ROAD BOWEN HILLS QLD 4006 EXTERNAL FINISHES SCHEDULE

PROJECT NO. 211106

SCALE

N.T.S

DRAWING NO.

REV. 1

# APPROVED

# Landscape concept plans

# **BRISBANE CITY COUNCIL** 254 & 270 ABBOTSFORD ROAD, BOWEN HILLS PLANS AND DOCUMENTS LOT 10 ON SP335757

referred to in the PDA DEVELOPMENT APPROVAL Approval no.: **DEV2023/1392** Date: 1 September 2023



SITE LOCATION

| DRAWING INDEX  |  |          |  |  |  |
|----------------|--|----------|--|--|--|
| DRAWING No.    | DRAWING TITLE                          | REVISION |  |  |  |
| 2208-015-SK001 | COVER SHEET & DRAWING INDEX            | E        |  |  |  |
| 2208-015-SK002 | PLANTING PLAN                          | E        |  |  |  |
| 2208-015-SK004 | PLANT SPECIES SCHEDULE, IMAGES & NOTES | E        |  |  |  |

### PRELIMINARY

| Е   | REVISED ISSUE | SX    | 14.07.23 |
|-----|---------------|-------|----------|
| D   | REVISED ISSUE | SX    | 12.07.23 |
| rev | description   | drawn | date     |

HICKEY OATLEY

254 & 270 ABBOTSFORD ROAD, BOWEN HILLS LANDSCAPE CONCEPT PLAN **COVER SHEET & DRAWING INDEX** 



only be used by LALID ink's client (and any oth

job no. | 2208-015 for A1 JULY 2023 rev no. F SK001

approved E. NICHOLAOU\*

Landscaping to be updated in response to any changes required by Condition 19 - Stormwater Management (Quality)



### ANNOTATION NOTES

- DRIVEWAY ENTRY / EXIT
- 2 PEDESTRIAN ENTRY / EXIT
- 3 FEATURE PALM TREES WOD bif TO DEFINE SITE ENTRANCE
- 4 SHADE TREE CUP ana TO BE KEPT WITH 1.8m CLEAR TRUNK. TREE TO BE UNDERPLANTED WITH LOW PLANTINGS, INCLUDING SHRUBS AGA att, CAL LJ, WES GB AND GROUNDCOVERS CAR gla, LIR JR, LOM SHA
- 5 SHADE TREES CUP ana TO PROVIDE AMENITY TO PARKING AREA, UNDERPLANTED WITH SHRUBS AGA att, COR RS AND GROUNDCOVERS AGA afr (B), AGA afr (W), LIR JR, LOM SHA
- 6 GARDEN BED AT FRONTAGE TO BE PLANTED WITH LOW FEATURE SHRUBS AGA att, COR sen, WES GB AND GROUNDCOVERS DIA ara, LOM sha AND PEN nat
- PROPOSED GARDENBED TO BE FULLY PLANTED WITH FEATRE SHRUBS CAL LJ, COR RS, STR reg, WES GB AND GROUND COVER AGA afr (B), AGA afr (W), CAR gla, LIR JR
- PROPOSED LOW MAINTENANCE SHRUBS AGA att, CAL LJ, WES GB TO REAR OF THE SITE, UNDERPLANTED WITH GROUNDCOVERS LIR JL, LOM SHAAND PEN NAF
- 9 PODIUM PLANTERS TO INCLUDE FEATURE SHRUBS AGA att, COR RS, STR reg AND GROUNDCOVERS AGA afr (B), AGA afr (W), LIR JR TO PROVIDE VISUAL AMENITY TO OUTDOOR SEATING AREA
- 10 PROPOSED TRUNCATION REFER TO TRAFFIC ENGINEERS DRGS FOR DETAILS
- LOW BUFFERING SHRUBS MUR MM TO BE USED ALONG PROPERTY BOUNDARY, SHRUBS TO BE UNDERPLANTED WITH GROUNDCOVERS LOM SHA AND LIR JR
- 12 PROPOSED 1.2m WIDE FOOTPATH TO BE INSTALLED IN ACCORDANCE WITH BBC STREETSCAPE HIERARCHY INDUSTRIAL STREET REQUIREMENT
- 13 PROPOSED 1.8m WIDE FOOTPATH TO BE INSTALLED IN ACCORDANCE WITH BBC STREETSCAPE HIERARCHY SUBTROPICAL BOULEVARD OUT OF CENTRE VERGE WIDTH 3.75m/4.25m (SBO3) REQUIREMENT
- 14 EXISTING STREET TREES TO BE RETAINED, MAKE GOOD IF DAMAGED DURING CONSTRUCTION
- 15 PROPOSED 1.2m HIGH PERFORATED SCREEN ALONG DT REFER ARCHITECTS DRGS FOR DETAILS

PLAN SCALE 1:200

AMENDED IN RED By: Matthew Buchanan Date: 23 August 2023







PROPOSED FEATURE TREES

PROPOSED SHADE TREES

PROPOSED SHRUB AND LOW LEVEL PLANTING

PROPOSED GROUNDCOVER PLANTING

PROPOSED BUFFER PLANTING

TURF

HARDSTAND SURFACE FINISH TO PEDESTRIAN PRIORITY PATHWAY

CONCRETE AREA - REFER CIVIL ENGINEERS DRGS FOR DETAILS

OBSTRUCTION CLEAR ZONE FOR PEDESTRIAN SAFETY SIGHT LINE

**PYLON SIGNS** 

ROOF LINE OVER

PROPERTY BOUNDARY

**EXISTING LIGHTPOLES** 

#### NOTES

(LP)

1. REFER TO DRG 2208-015-SK010 FOR PLANT SPECIES SCHEDULE, IMAGES AND GENERAL NOTES 2. REFER ARCHITECTS DRGS FOR ALL FENCE DETAILS 3. REFER CIVIL ENGINEERS DRGS FOR ALL DRIVEWAY CROSSOVER AND RETAINIG WALL DETAILS

| 0 | 2      | 4       | 6     | 8      | 10m |
|---|--------|---------|-------|--------|-----|
|   |        |         |       |        | -   |
| S | CALE 1 | :200 AT | ORIGI | NAL SI | ZE  |

#### PRELIMINARY

| rev | description   | drawn | date     |
|-----|---------------|-------|----------|
| D   | REVISED ISSUE | SX    | 12.07.23 |
| Е   | REVISED ISSUE | SX    | 14.07.23 |

HICKEY OATLEY

254 & 270 ABBOTSFORD ROAD, BOWEN HILLS LANDSCAPE CONCEPT PLAN PLANTING PLAN



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scale | 1:200 for A1 job no. | 2208-015 date JULY 2023 rev no. E SK002

approved E. NICHOLAOU\*

**PROPOSED PLANT SPECIES IMAGES** 



CUPANIOPSIS anacardioides





TRISTANIOPSIS laurina 'Luscious' WATERHOUSEA floribunda

WODYETIA bifurcata







AGAVE attenuata CALLISTEMON viminalis 'Little John'



'Red Sensation'





MURRAYA paniculata STRELITZIA reginae Min-a-Min

SYZYGIUM australe

'Straight and Narrow'



WESTRINGIA fruticosa 'Grey Box'





CARPOBROTUS glaucescens 'Aussie Rambler'

A AREA IN APPEND



AGAPANTHUS africanus

LOMANDRA fluviatilis 'Shara' PENNISETUM alopecuroides 'Nafray'



LIRIOPE muscari 'Just Right'

#### PROPOSED PLANT SPECIES SCHEDULE

| CODE        | PLANT SPECIES                                      | COMMON NAME               | CENTRES<br>(mm) | POT SIZE<br>(AT INSTALL) | MATURE SIZE<br>(HEIGHT x WIDTH) |
|-------------|--|---------------------------|-----------------|--------------------------|---------------------------------|
| TREE SPEC   |  |                           |                 |                          |                                 |
| CUP ana     | CUPANIOPSIS anacardioides                          | Tuckeroo                  | AS SHOWN        | 25L                      | 10 x 4 (HxW)                    |
| ELA eum     | ELAEOCARPUS eumundii                               | Eumundii Quandong         | AS SHOWN        | 25L                      | 8-10 X 3-5 (HxW)                |
| TRI LUS     | TRISTANIOPSIS laurina 'Luscious'                   | Luscious                  | AS SHOWN        | 25L                      | 7-12 x 5 (HxW)                  |
| WAT flo     | WATERHOUSEA floribunda                             | Weeping Lilly Pilly       | AS SHOWN        | 25L                      | 10x8 (HxW)                      |
| WOD bif     | WODYETIA bifurcata                                 | Foxtail Palm              | AS SHOWN        | 25L                      | 15 x 3 (HxW)                    |
| SHRUB SPE   | ECIES  |                           |                 |                          |                                 |
| AGA att     | AGAVE attenuata                                    | Century Plant             | 500mm           | 200mm                    |                                 |
| CAL LJ      | CALLISTEMON viminalis `Little John`                | Dwarf Weeping bottlebrush | 1500mm          | 200mm                    |                                 |
| COR RS      | CORDYLINE australis 'Red Sensation'                | Red Sensation Cordyline   | 700mm           | 200mm                    |                                 |
| MUR MM      | MURRAYA paniculata 'Min-a-Min'                     | Dwarf Murraya             | 500mm           | 200mm                    |                                 |
| STR reg     | STRELITZIA reginae                                 | Bird of Paradise          | 750mm           | 200mm                    |                                 |
| SYZ SN      | SYZYGIUM australe 'Straight & Narrow' -' SAN01'    | Straight and Narrow       | 1000mm          | 25L                      |                                 |
| WES GB      | WESTRINGIA fruticosa 'Grey Box' - 'WES04'          | Grey Box Costal Rosemary  | 400mm           | 200mm                    |                                 |
| GROUNDCO    | OVER SPECIES                                       |                           |                 |                          |                                 |
| AGA afr (B) | AGAPANTHUS africanus                               | Blue African Lily         | 500mm           | 140mm                    |                                 |
| AGA afr (W) | AGAPANTHUS africanus                               | White African Lily        | 500mm           | 140mm                    |                                 |
| CAR gla     | CARPOBROTUS glaucescens 'Aussie Rambler' - 'CAR10' | Pigface                   | 350mm           | 140mm                    |                                 |
| LIR JR      | LIRIOPE muscari 'Just Right' - 'LIRJ'              | Just Right                | 500mm           | 140mm                    |                                 |
| LOM SHA     | LOMANDRA fluviatilis 'Shara' - 'ABU7'              | Shara Lomandra            | 300mm           | 140mm                    |                                 |
| PEN NAF     | PENNISETUM alopecuroides 'Nafray' - 'PA300'        | Fountin Grass             | 750mm           | 140mm                    |                                 |
| TURF        |  |                           |                 |                          |                                 |
| CYN LEG     | CYNODON dactylon 'Legend'                          | Green Couch               |                 |                          |                                 |





1. REFER TO LANDSCAPE CONCEPT PLAN 2208-015-SK002 FOR PROPOSED PLANTING DESIGN 2. REFER TO CIVIL ENGINEERS DRAWINGS FOR DRIVEWAY AND CROSSOVER DETAILS 3. REFER TO ARCHITECTS DRAWINGS FOR ALL FENCE DETAILS

4. LANDSCAPE DETAILED DESIGN IS TO BE COORDINATED WITH HYDRAULIC AND ENGINEERING DESIGN TO CONFIRM LOCATIONS OF UNDERGROUND SERVICES PRIOR TO CONSTRUCTION 5.LANDSCAPE GENERAL STANDARDS.

5.1 CULTIVATION MINIMUM DEPTH 150mm FOR TURFED AREAS AND PLANTING AREAS 5.2 IMPORTED TOPSOIL TO AS 4419. MINIMUM DEPTHS, GRASSED AREAS (TURF) 100mm, PLANTING AREAS 300mm.

5.3 MULCH TO AS 4454 PROVIDE MULCH WHICH IS FREE OF DELETERIOUS AND EXTRANEOUS MATTER SUCH AS SOIL, WEEDS AND STICKS.

5.4 STAKE SIZES FOR PLANTS 1-2.5m HEIGHT TWO 50 x 50 x 1800mm STAKES PER PLANT PROVIDE TIES FIXED SECURELY

TO THE STAKES, ONE TIE AT HALF THE HEIGHT OF THE MAIN STEM, OTHERS AS NECESSARY TO STABLILISE PLANT. FOR PLANTS <2.5m HIGH 50mm HESSIAN WEBBING STAPLED TO THE STAKES. 6. FOR ALL STREETSCAPE WORKS REFER TO THE FOLLOWING BRISBANE CITY COUNCIL STANDARD DRAWINGS

FOR LANDSCAPE CONSTRUCTION DETAILS: 6.1 SOFTWORKS:

- 6.1.1 BSD-9051 PLANTING GENERAL NOTES SHEET 1
- 6.1.2 BSD-9051 PLANTING GENERAL NOTES SHEET 2
- 6.1.3 BSD-9052 PLANTING MEDIA PROFILES (TURF AND GARDEN)
- 6.1.4 BSD-9053 PLANTING TYPICAL TREE, SHRUB & TUBE STOCK

6.1.5 BSD-9082 ROOT DEFLECTOR INSTALLATION ADJACENT TO EXISTING ROAD AND STRUCTURES

7. ALL BCC STANDARD DRAWINGS ARE TO BE READ IN CONJUNCTION WITH THE FOLLOWING BRISBANE CITY

COUNCIL TECHNICAL REFERENCE SPECIFICATIONS:

7.1 S190 LANDSCAPING

### PRELIMINARY

| rev | description   | drawn | date     |
|-----|---------------|-------|----------|
| D   | REVISED ISSUE | SX    | 12.07.23 |
| Е   | REVISED ISSUE | SX    | 14.07.23 |

HICKEY OATLEY

254 & 270 ABBOTSFORD ROAD, BOWEN HILLS LANDSCAPE CONCEPT PLAN PLANT SPECIES SCHEDULE, IMAGES & NOTES



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scale | NTS for A1 job no. | 2208-015 date JULY 2023 rev no. E SK010

approved E. NICHOLAOU\*

# APPROVED

# **Civil engineering assessment report**

PLANS AND DOCUMENTS referred to in the PDA DEVELOPMENT APPROVAI

HCE Engine Sate 1 September 2023



Ref. (22224)

PROPOSED COMMERICAL DEVELOPMENT 254 & 270 ABBOTSFORD ROAD, BOWEN HILLS

### CIVIL ENGINEERING ASSESSMENT REPORT REVISION 3



Prepared For HICKEY OATLEY PLANNING & DEVELOPMENT



PO Box 7214, Redland Bay Qld 4165 55-57 Jardine Dr, Redland Bay QLD Tel: (07) **3829 1399** Email: mail@hce-engineers.com.au Web: www.hce-engineers.com.au



### **REPORT CONTROL SHEET**

| HCE Ref. No.: | 22224                                  |
|---------------|--|
| Site:         | 254 & 270 Abbotsford Road, Bowen Hills |
| Report Title: | Civil Engineering Assessment Report    |

| Rev No. | Date     | Written By | Reviewed By | Authorised<br>By | Signed |
|---------|----------|------------|-------------|------------------|--------|
| 3       | 20/07/23 | MB         | GH          | GH               |        |
|         |          |            |             |                  |        |
|         |          |            |             |                  |        |
|         |          |            |             |                  |        |

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| HCE - File                           | -        | $\boxtimes$ | $\boxtimes$ | $\boxtimes$ | $\boxtimes$ | $\boxtimes$ |    |   |   |   |
| Hickey Oatley Planning & Development | 17/01/23 | $\boxtimes$ |             |             |             |             |    |   |   |   |
| Hickey Oatley Planning & Development | 09/02/23 |             | $\boxtimes$ |             |             |             |    |   |   |   |
| Hickey Oatley Planning & Development | 13/07/23 |             |             | $\boxtimes$ |             |             |    |   |   |   |
| Hickey Oatley Planning & Development | 14/07/23 |             |             |             | $\boxtimes$ |             |    |   |   |   |
| Hickey Oatley Planning & Development | 20/07/23 |             |             |             |             | $\boxtimes$ |    |   |   |   |
|                                      |          |             |             |             |             |             |    |   |   |   |
|                                      |          |             |             |             |             |             |    |   |   |   |
|                                      |          |             |             |             |             |             |    |   |   |   |



### **INDEX**

- 1. Introduction
- 2. Verge Works
- 3. Stormwater Drainage
- 4. Sewerage
- 5. Water Reticulation
- 6. Earthworks
- 7. Conclusions



#### 1. INTRODUCTION

This report has been prepared to support the development application for material change of use at 254 & 270 Abbotsford Road, Bowen Hills.

A general description of proposed works and items of particular note are contained within the body of this report.

Information presented in this report should not be applied to properties or developments other than the subject development. No responsibility is accepted for use of any part of this report in any other context or for any other purposes or by any third party.

Revision 3 of this report has been created to reflect the updated site layout. Refer to drawing 22224-SK01.

#### 2. VERGE WORKS

An existing 1.20m wide concrete footpath exists along the Abbotsford Road frontage of the existing site. It is proposed to construct new footpaths to Brisbane City Council requirements along the Taylor Street and Hadwen Lane frontages. New footpaths are proposed to connect to the existing footpath on Abbotsford Road as shown on concept design drawings.

No changes are proposed to existing verge gradients in Taylor Street or Abbotsford Road, with the exception of footpath construction. Widening of Hadwen Lane is proposed, and land dedicated as road reserve will be cleared from existing improvements, and finished at a gradient of 2.0% to the existing kerb and channel to Brisbane City Council requirements.

#### 3. STORMWATER DRAINAGE

Existing discharge from the site currently discharges to Abbotsford Road, Hadwen Lane and Taylor Street as surface flow. Existing surface contours indicate that surface flows are ultimately conveyed to the existing sag gully in Taylor Street.

It is proposed to capture and convey on site stormwater to the existing stormwater gully in Taylor Street as shown on concept design drawings in accordance with Brisbane City Councils Infrastructure Design Planning Scheme Policy.

As the development will reduce peak flows, and discharge to existing stormwater drainage under control of the local authority, the discharge to the existing stormwater infrastructure in Taylor Street is considered lawful per Section 3.9.1 of the Queensland Urban Drainage Manual.

Water quality treatment on site is to be undertaken by implementation of best management practices. It is proposed to install gross pollutant traps on all inlets within carparking areas to capture pollutants prior to discharge. Refer to concept design drawings for additional information.

Refer to the Stormwater Management Plan prepared by HCE Engineers for further information.



#### 4. <u>SEWERAGE</u>

The site is currently serviced by a twin property connection from the existing manhole within the Abbotsford Road verge. It is proposed to review the condition of the existing property connection and retain for the proposed use. The existing property connection will be modified to seal one of the existing branches of the twin connection in accordance with Urban Utilities requirements.

Refer to concept design drawings for additional information.

A Service Advice Notice has been requested to confirm the existing sewerage network has adequate capacity for the proposed development.

#### 5. WATER RETICULATION

The existing site currently has two metered service connections from the existing 100mm reticulation main in Abbotsford Road. The existing water service connections are to be removed and plugged at the main, and a new water meter and service provided for the development as required. Concept design drawing show the indicative location of the future service and meter.

Refer to concept design drawings for additional information.

A Service Advice Notice has been requested to confirm the existing water supply network has adequate capacity for the proposed development.

#### 6. EARTHWORKS

Existing site levels range from approximately 3.60m AHD to 2.40m AHD. It is proposed to undertake minor earthworks to suit the proposed building and carparking in coordination with the architectural design.

Changes in surface level up to 0.5m are expected on site to accommodate the architectural design. Battering within landscaped areas are proposed such that new retaining walls are not required.

#### 7. <u>CONCLUSIONS</u>

The proposed commercial development at 254 & 270 Abbotsford Road, Bowen Hills can be adequately serviced with regards to sewerage, water reticulation and stormwater drainage.

Reasonable and relevant conditions can be applied to the development approval to achieve compliant and adequate servicing of the development.



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|                | 13/07/23  | Approval No.                  |             |                   | Scale  |             |
|                | 14/07/23  |                               | -           |                   | AS SH  | OWN         |
| LEVELS AMENDED | 20/07/23  | Drawing No.                   |             |                   |        | Rev.        |
|                |           |                               | 222         | 224-SK01          |        | I E I       |

# **Traffic Impact Assessment**

# SUPPORTING DOCUMENT





## 254-270 ABBOTSFORD ROAD, BOWEN HILLS

## TRAFFIC IMPACT ASSESSMENT

24 JULY 2023

PREPARED FOR HICKEY OATLEY







#### **DOCUMENT CONTROL RECORD**

| DOCUMENT |           |  |        |          |                    |        |  |  |  |  |
|----------|-----------|--|--------|----------|--------------------|--------|--|--|--|--|
| Report   | t Title:  | 254-270 Abbotsford Road, Bowen Hills – Traffic Impact Assessment |        |          |                    |        |  |  |  |  |
| Client   | •         | Hickey Oatley on behalf of Hungry Jack's Pty Ltd                 |        |          |                    |        |  |  |  |  |
| Projec   | t Number: | umber: 23-114  |        |          |                    |        |  |  |  |  |
| RE∨      | PURPOSE   | DATE   | AUTHOR | REVIEWER | APPROVED           | SIGNED |  |  |  |  |
| A        | DRAFT     | NOV-22   | CJ/CB  | AAP      | AAP<br>(RPEQ 5286) |        |  |  |  |  |
| В        | FINAL     | NOV-22   | CJ/CB  | AAP      | AAP<br>(RPEQ 5286) |        |  |  |  |  |
| С        | FINAL     | MAY-23   | CJ/CB  | AAP      | AAP<br>(RPEQ 5286) |        |  |  |  |  |
| D        | FINAL     | JUL-12   | CJ/CB  | AAP      | AAP<br>(RPEQ 5286) |        |  |  |  |  |

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#### **CONTENTS**

| 1.0 | INT | RODUCTION                   | 1  |
|-----|-----|-----------------------------|----|
|     | 1.1 | Background                  | 1  |
|     | 1.2 | Aim                         | 1  |
|     | 1.3 | Scope of Report             | 1  |
| 2.0 | EXI | STING CONDITIONS            | 2  |
|     | 2.1 | Subject Site                | 2  |
|     | 2.2 | Access                      | 3  |
|     | 2.3 | Road Network                | 3  |
|     | 2.4 | Traffic Volumes             | 4  |
|     | 2.5 | Road Upgrades               | 4  |
|     | 2.6 | Intersection Operations     | 5  |
|     | 2.7 | Active and Public Transport | 8  |
| 3.0 | PRO | DPOSED DEVELOPMENT          | 9  |
|     | 3.1 | Site Layout                 | 9  |
|     | 3.2 | Access                      | 10 |
|     | 3.3 | Parking                     | 11 |
|     | 3.4 | Queuing                     | 13 |
|     | 3.5 | Servicing                   | 13 |
|     | 3.6 | Active Transport            | 15 |
| 4.0 | TRA | FFIC OPERATIONS             | 17 |
|     | 4.1 | Development Staging         | 17 |
|     | 4.2 | Traffic Generation          | 17 |
|     | 4.3 | Directional Distribution    | 18 |
|     | 4.4 | Intersection Operations     | 19 |
| 5.0 | COI | NCLUSIONS                   | 22 |

| APPENDIX A  | TRAFFIC COUNT DATA         |
|-------------|----------------------------|
| APPENDIX B  | INTERSECTION ANALYSES      |
| APPENDIX C  | PLANS OF DEVELOPMENT       |
| APPENDIX D  | SWEPT PATH ANALYSES        |
| APPENDIX E: | TURNING MOVEMENT FORECASTS |
|             |                            |



#### **1.0 INTRODUCTION**

#### 1.1 BACKGROUND

In November 2022, PTT was commissioned by Hickey Oatley, on behalf of Hungry Jack's Pty Ltd, to undertake a traffic impact assessment for a proposed food and drink outlet, located at 254-270 Abbotsford Road, Bowen Hills. The location of the subject site is shown in Figure 1.1.

This version of the TIA has been amended in response to a revised development layout, with modifications to the on-site car parking and servicing arrangements.





#### 1.2 AIM

The aim of this assessment is to evaluate the proposed development in terms of its access, parking and servicing arrangements, pedestrian / cyclist facilities, likely peak hour traffic generation and impact on the surrounding road network.

#### 1.3 SCOPE OF REPORT

This report begins by summarising the characteristics of the existing road network (Chapter 2), followed by a description of the scope and scale of the proposed development, including the access, parking and servicing arrangements (Chapter 3). The predicted peak hour traffic generation of the development is estimated along with a consideration of its likely traffic impact on the surrounding road network (Chapter 4). The report concludes with a summary of key findings and recommendations (Chapter 5).



#### 2.0 EXISTING CONDITIONS

#### 2.1 SUBJECT SITE

The subject site is located at 254-270 Abbotsford Road, Bowen Hills and is formally identified as Lot 10 on SP335757. The site is currently vacant but previously accommodated commercial and low impact industry uses. Under the Brisbane City Council (Council) City Plan (2014), the site is zoned as Industry Investigation and is located within the City Frame. The site is also part of the Bowen Hills Priority Development Area (PDA) within which it is included in the Industrial zone.

The site is bounded to the north by Taylor Street, to the east by Abbotsford Road, to the south by Hadwen Lane and to the west by low impact industry uses. An aerial view of the site is shown in Figure 2.1.

#### Figure 2.1: SUBJECT SITE





#### 2.2 ACCESS

Vehicular access to the site is currently provided via six driveway crossovers, as indicated in Figure 2.1 and outlined as follows:

- two crossovers on Taylor Street
- three crossovers on Abbotsford Road,
- one crossover on Hadwen Lane

#### 2.3 ROAD NETWORK

Key attributes of the surrounding road network are summarised in Table 2.1.

#### Table 2.1: INTERSECTION ATTRIBUTES

| ATTRIBUTE               | ABBOTSFORD<br>ROAD  | TAYLOR STREET      | HADWEN LANE      |
|-------------------------|---|--------------------|------------------|
| Road Hierarchy          | Arterial  | Neighbourhood      | Neighbourhood    |
| Cross-section           | Five-lane undivided<br>(two lanes<br>northbound, three<br>lanes southbound) | Two-lane undivided | Two-lane divided |
| Speed Limit             | 60 km/h   | 50 km/h            | 50 km/h          |
| Jurisdiction            | Council   | Council            | Council          |
| Predominant Land<br>Use | Commercial  | Industrial         | Industrial       |
| Dedicated Parking       | No  | Both sides         | No               |
| Footpaths               | Both Sides  | Both Sides         | No               |
| Bicycle Lanes           | No  | No                 | No               |
| Bus Route               | No  | No                 | No               |

At the north-east corner of the subject site, Taylor Street meets Abbotsford Road at a prioritycontrolled T-intersection where it forms the minor approach. This intersection accommodates all turn movements but has no auxiliary turn treatments on the major road.

Approximately 20m south of the Taylor Street intersection, Abbottsford Road meets Gebbie Street at a signal-controlled T-intersection. This intersection accommodates all turn movements. There is a pedestrian crossing on the southern Abbottsford Road approach to the intersection at the eastern frontage of the subject site.

The Abbottsford Road / Hadwen Lane T-intersection is located immediately south of the signalcontrolled intersection of Abbottsford Road and Gebbie Street. The Abbottsford Road / Hadwen Lane intersection is priority-controlled and is limited to left-in / left-out operations by the double barrier centre-line on Abbotsford Road.



#### 2.4 TRAFFIC VOLUMES

Turning movement surveys were conducted at the following intersections, on Tuesday 22 November 2022 from 7:00 to 9:00am and from 3:00pm to 5:00pm:

- Abbotsford Road / Gebbie Street signalised intersection
- Abbotsford Road / Taylor Street priority-controlled intersection
- Burrows Street / Taylor Street priority-controlled intersection

The peak periods and key operational attributes of the intersection are shown in Table 2.2, with raw survey data attached in Appendix A.

| Table 2.2: | INTERSECTION ATTRIBUTES |
|------------|-------------------------|
|------------|-------------------------|

| ATTRIBUTE                       | WEEKDAY MORNING | WEEKDAY EVENING |  |  |  |
|---------------------------------|-----------------|-----------------|--|--|--|
| Abbotsford Road / Gebbie Street |                 |                 |  |  |  |
| Peak Hour                       | 7:00 – 8:00am   | 4:30 – 5:30pm   |  |  |  |
| Volume (vph)                    | 2,805 vehicles  | 2,840 vehicles  |  |  |  |
| % Heavy Vehicles                | 2.5%            | 1.0%            |  |  |  |
| Peak Flow Factor                | 95.6%           | 98.3%           |  |  |  |
| Abbotsford Road / Taylor        | Street          |                 |  |  |  |
| Peak Hour                       | 7:00 – 8:00am   | 4:30 – 5:30pm   |  |  |  |
| Volume (vph)                    | 2,820 vehicles  | 2,835 vehicles  |  |  |  |
| % Heavy Vehicles                | 2.6%            | 0.9%            |  |  |  |
| Peak Flow Factor                | 95.6%           | 98.3%           |  |  |  |
| Burrows Street / Taylor Street  |                 |                 |  |  |  |
| Peak Hour                       | 7:15 – 8:15am   | 4:45 – 5:45pm   |  |  |  |
| Volume (vph)                    | 1,750 vehicles  | 2,040 vehicles  |  |  |  |
| % Heavy Vehicles                | 2.0%            | 0.7%            |  |  |  |
| Peak Flow Factor                | 97.6%           | 98.5%           |  |  |  |

#### 2.5 ROAD UPGRADES

A review of Council's Local Government Infrastructure Plan (LGIP) has not identified any proposed upgrades to the surrounding road network in the vicinity of the subject site. However, in pre-lodgement advice, Council has advised there will be a widening requirement along the Hadwen Lane site frontage and a 6.0m by three chord truncation at the Abbotsford Road / Hadwen Lane intersection.



#### 2.6 INTERSECTION OPERATIONS

#### 2.6.1 Intersection Assessment Parameters

A series of SIDRA analyses were conducted to quantify the existing traffic operations on the adjacent external road network. The analyses were based on the traffic count data presented in Appendix A, with:

- peak flow factors (PFF) as detailed in Table 2.2
- the observed proportion of heavy vehicles (%HV) for each movement
- signal phasing data and cycle times sourced from Council
- level of reduction with opposing flow rate factor set to "medium"
- SIDRA default values for other parameters

The level of reduction with opposing flow rate factor is used to reflect the tendency of drivers to accept smaller gaps in circumstances where the opposing traffic volume is high. The application of a "medium" value is consistent with guidance published in the SIDRA User Manual (based on the surveyed through traffic volumes on Abbotsford Road and Burrows Street) and is expected to accurately reflect the intersection operations of these roads with Taylor Street under existing, pre and post development scenarios.

The results are presented in terms of the degree of saturation (DOS), 95<sup>th</sup> percentile vehicle queues and critical movement. The degree of saturation for a movement is defined as the ratio of traffic demand to the capacity of the movement. The critical movement relates to the approach or movement with the highest degree of saturation. Table 2.3 is an extract from the SIDRA manual and defines the operational rating and level of service for all intersection types.

| LEVEL OF | E                    | Ν                    |                      |
|----------|----------------------|----------------------|----------------------|
| SERVICE  | SIGNALS              | ROUNDABOUT           | PRIORITY             |
| LOS A    | x ≤ 60%              | x ≤ 60%              | x ≤ 60%              |
| LOS B    | $60\% < x \le 70\%$  | $60\% < x \le 70\%$  | $60\% < x \le 70\%$  |
| LOS C    | $70\% < x \le 90\%$  | $70\% < x \le 85\%$  | $70\% < x \le 80\%$  |
| LOS D    | $90\% < x \le 95\%$  | $85\% < x \le 95\%$  | $80\% < x \le 90\%$  |
| LOS E    | $95\% < x \le 100\%$ | $95\% < x \le 100\%$ | $90\% < x \le 100\%$ |
| LOS F    | 100% < x             | 100% < x             | 100% < x             |

#### Table 2.3: SIDRA INTERSECTION RATINGS

#### 2.6.2 Abbotsford Road / Gebbie Street

Given their close proximity, the Abbotsford Road / Gebbie Street and Abbotsford Road / Taylor Street intersections have been modelled as a network, using the SIDRA representation shown in Figure 2.2. There is sufficient width on Taylor Street for a left-turning vehicle to pass a rightturning vehicle stopped at the give-way line. Therefore, the intersection has been modelled with a short left-turn lane on the western approach.





#### Figure 2.2: INTERSECTION LAYOUTS AND EQUIVALENT REPRESENTATION



The results of the analysis of the Abbotsford Road / Gebbie Street signalised intersection are summarised in Table 2.4 and included in Appendix B. The results indicate that the intersection currently experiences LOS A operations during the weekday morning and evening peak hours.

#### Table 2.4: ABBOTSFORD ROAD / GEBBIE STREET OPERATIONS

| PEAK HOUR       | DOS | CYCLE<br>TIME | 95%<br>QUEUE  | CRITICAL MOVEMENT         |
|-----------------|-----|---------------|---------------|---------------------------|
| Weekday Morning | 46% | 120s          | 5.5 vehicles  | Northern Approach Through |
| Weekday Evening | 48% | 120s          | 11.3 vehicles | Southern Approach Through |

#### 2.6.3 Abbotsford Road / Taylor Street

The results of the analysis of the Abbotsford Road / Taylor Street priority-controlled intersection are summarised in Table 2.5 and included in Appendix B. The results indicate that the intersection



currently experiences LOS A operations during the weekday morning hour and LOS C operations during the evening peak hour.

The analyses indicate that the average delay for the right-turn movement from Taylor Street is very high (ie more than five minutes) in both peak hours. The LOS A operation in the morning peak hour is achieved because only one vehicle was surveyed undertaking this right-turn. In practice, it is expected that the delay for this movement would be less than modelled (but still high), as some southbound through vehicles queued on approach to the Gebbie Street signalised intersection would leave a gap for vehicles to turn out of Taylor Street.

| PEAK HOUR       | DOS | AVG<br>DELAY | 95%<br>QUEUE | CRITICAL MOVEMENT           |
|-----------------|-----|--------------|--------------|-----------------------------|
| Weekday Morning | 37% | 0.5s         | 9.7 vehicles | Northern Approach Through   |
| Weekday Evening | 73% | 1.4s         | 3.3 vehicles | Western Approach Right Turn |

#### Table 2.5: ABBOTSFORD ROAD / TAYLOR STREET OPERATIONS

#### 2.6.4 Burrows Street / Taylor Street

The existing Burrows Street / Taylor Street priority-controlled intersection layout and equivalent SIDRA representation is shown in Figure 2.3. The results of the intersection analysis are summarised in Table 2.6 and included in Appendix B. The results indicate that the intersection currently experiences LOS A operations during the weekday morning and evening peak hours.







| PEAK HOUR       | DOS | AVG<br>DELAY | 95%<br>QUEUE | CRITICAL MOVEMENT         |  |
|-----------------|-----|--------------|--------------|---------------------------|--|
| Weekday Morning | 28% | 0.8s         | 0.5 vehicles | Northern Approach Through |  |
| Weekday Evening | 35% | 0.6s         | 0.6 vehicles | Southern Approach Through |  |

#### Table 2.5: BURROWS STREET / TAYLOR STREET OPERATIONS

#### 2.7 ACTIVE AND PUBLIC TRANSPORT

#### 2.7.1 Active Transport

There are pedestrian footpaths on both sides of Abbotsford Road and Burrows Street in the vicinity of the subject site. A pedestrian footpath is also provided on the northern side of Taylor Street and on the southern side to the west of the site (but not along the site frontage). There are currently no pedestrian footpaths on either side of Hadwen Lane. There are signalised pedestrian crossings on the eastern and southern legs of the Abbotsford Road / Gebbie Street intersection along the site's eastern frontage.

There are no formal cycle facilities currently provided in the vicinity of the site, although Abbotsford Road is designated as a secondary cycle route.

#### 2.7.2 Public Transport

There are public bus stops on both sides of Abbotsford Road around 130m south of the subject site. The stops are serviced by Translink routes 301 and 320, which operate approximately five times an hour in each direction between 6:00am and 8:00pm on weekdays. Accordingly, the site is well served by public transport.



#### 3.0 PROPOSED DEVELOPMENT

#### 3.1 SITE LAYOUT

The development proposal comprises a 244m<sup>2</sup> GFA food and drink outlet, with a drive-through facility. The proposed site layout is Figure 3.1, with plans of development attached in Appendix C.



#### Figure 3.1: PROPOSED DEVELOPMENT LAYOUT

Consistent with Council's pre-lodgement advice, the development layout provides the following:

- 1.25m road verge widening along the Hadwen Lane site frontage to achieve a minimum verge width of 2.5m
- a 6.0m by three chord truncation on the south-east corner of the site boundary at the Abbotsford Road / Hadwen Lane intersection



#### 3.2 ACCESS

#### 3.2.1 Location

As indicated in Figure 3.1, access to the site is proposed via a single crossover on Taylor Street along the site's northern boundary. All existing crossovers are to be removed. Therefore, the development would result in a significant rationalisation of access points along the site frontage, with the six existing crossovers (including three on the Abbotsford Road frontage) consolidated to a single access driveway.

Council's Transport, Access, Parking and Serving (TAPS) Policy requires that access driveways on minor roads (ie Taylor Street) be located a minimum of 20m from the property boundary of an intersecting major road (ie Abbotsford Road). Council's TAPS policy also requires that access driveways on minor roads be located a minimum 3m from adjacent driveways. The proposed driveway achieves 40m separation from the Abbotsford Road / Taylor Street intersection and approximately 5m separation from the adjacent driveway to the west. Therefore, the proposed access location complies with Council's TAPS Policy requirements.

#### 3.2.2 Design

The design vehicle for the proposed development is a refuse collection vehicle (RCV) and a medium rigid vehicle (MRV), as outlined in Section 3.5. Based on the design vehicle, Council's TAPS Policy requires a 7.0m wide Type B2 crossover, designed in accordance with Standard Drawing BSD-2021.

However, it is proposed to provide a 7.0m wide Type B1 driveway. This crossover type is expected to operate safely and efficiently because:

- it is sufficiently wide to facilitate simultaneous operations for passenger vehicles (ie a vehicle would be able to enter the site with a vehicle exiting at the same time)
- it is sufficient to facilitate design vehicle (ie RCV and MRV) access utilising the entire width of the driveway
- it minimises the driveway crossing distance for pedestrians

#### 3.2.3 Sight Distance

Based on the posted speed limit of 50km/h on Taylor Street, Council's TAPS Policy specifies a desirable sight distance of 90m and minimum sight distance of 70m. On-site observations indicate the proposed access location achieves approximately 55m sight distance to the east (ie to / from the Taylor Street/ Abbotsford Road intersection) and 80m sight distance to the west (ie to / from the Taylor Street / Burrows Street intersection). However, vehicles entering Taylor Street from both Abbotsford Road and Burrows Street will need slow to around 20 – 30km/h in order to negotiate the tight turn radii. Accordingly, the available sight distance at the proposed access driveway location is sufficient.



#### 3.3 PARKING

#### 3.3.1 Requirement

Based on the location of the subject site within the City Frame, a maximum car parking rate of one space per 100m<sup>2</sup> GFA (for non-residential use) would be relevant as per Table 13 of Council's TAPS Policy. As shown in Table 3.1, the application of this rate would result in the proposed development being supported by a maximum of three on-site parking spaces.

#### Table 3.1: MAXIMUM CAR PARKING REQUIREMENT

| USE                   | SCALE     | PARKING RATE                      | REQUIRED |
|-----------------------|-----------|-----------------------------------|----------|
| Food and drink outlet | 244m² GFA | 1 space per 100m <sup>2</sup> GFA | 3 spaces |

#### 3.3.2 Provision

The proposed development layout provides a total of 17 on-site parking spaces including:

- eight standard car parking bays (including three spaces allocated for staff parking only)
- one person with disability (PWD) bay
- two dedicated delivery bays
- two drive-through customer waiting spaces
- four motorcycle bays

The proposed on-site parking provision equates to a rate of seven spaces per 100m<sup>2</sup> GFA. While the parking provision is above the maximum requirement from Council's TAPS Policy, it is:

- comparable with similar food and drink outlets in inner Brisbane
- appropriate for the location of the subject site which is right on edge of the City Frame
- reflective of current trends in parking at food and drink outlets in terms of:
  - high drive-through patronage and lower demand for a traditional dine-in experience
  - a much shorter duration of stay (typically less than five minutes) as customers (or their delivery representative) enter the store to pick-up orders only
  - a much higher proportion of motorcycle use with the majority of drivers of meal delivery services operating a scooter, motorbike or e-bike rather than a car
- expected to cater for the peak parking demand generated by the food and drink use

#### 3.3.3 Persons with Disabilities (PWD) Parking

Council's TAPS Policy requires that PWD parking be provided at a rate of one space per 50 ordinary car parking spaces, with a minimum provision of one PWD space. Based on the on-site parking provision, one PWD space is required. Accordingly, the proposed development layout makes provision for a single PWD parking space and complies with the Council's TAPS Policy requirements.


### 3.3.4 Design

The proposed car parking layout has been designed in accordance with the requirements of Council's TAPS Policy in terms of parking bay dimensions, aisle widths, vehicle circulation and manoeuvring. The design of the parking layout is typified by:

- staff and customers spaces are dimensioned 2.6m wide by 5.4m long.
- a PWD space dimensioned 2.4m x 5.4m bay plus an adjacent 2.4m by 5.4m shared area in accordance with AS2890.6<sup>1</sup>
- motorcycle bays dimensioned 1.2m wide by 2.5m long
- car parking aisles dimensioned a minimum of 6.1m wide
- an additional 0.3m clearance provided between parking spaces and adjacent walls
- end of aisle treatments
- no grade changes across the car parking area

Vehicles would be able to use the area behind loading bay to turn around and exit the site in a forward gear should al customer car parking spaces be occupied on arrival, as demonstrated in Figure 3.2.



## Figure 3.2: VEHICLE TURNAROUND

<sup>1</sup> Standards Australia AS/NZS 2890.6:2009 "Parking Facilities – Part 6: Off-Street Parking for People with Disabilities"



### 3.4 QUEUING

### 3.4.1 Drive Through Facility

Council's TAPS Policy requires that drive-through facilities provide queuing space for a minimum 10 vehicles. The proposed drive-through provides queuing space for at least 10 vehicles, measured between the drive-through entry (ie parallel to the southern edge of the loading bay) and the pick-up window, and complies with the Council's TAPS policy requirements for queuing.

### 3.4.2 Site Access

Based on a total parking provision of 17 spaces, Council's TAPS Policy requires that queuing space for one vehicle (ie 6m) be provided. The effective available queuing space at the Taylor Street site access is approximately 7m, measured from the site entrance to the first car parking space within the site. Therefore, the queuing provision is expected to adequality cater for the proposed development in accordance with Council's TAPS Policy requirements.

### 3.5 SERVICING

### 3.5.1 Requirement

The design service vehicles specified in Council's TAPS Policy for the proposed food and drink outlet are outlined in Table 3.2. As shown, the largest vehicles required to service the development are a Refuse Collection Vehicle (RCV) and Medium Rigid Vehicle (MRV).

### Table 3.2:SERVICE VEHICLE REQUIREMENTS

| USE                   | SCALE                 | REGULAR VEHICLE | OCCASIONAL VEHICLE |
|-----------------------|-----------------------|-----------------|--------------------|
| Food and drink outlet | 244m <sup>2</sup> GFA | MRV             | RCV                |

### 3.5.2 Provision

One RCV / MRV loading bay is proposed to cater for the servicing demands of the development. Servicing by the MRV and RCV is proposed to be accommodated in the dedicated loading bay, which is dimensioned 6.0m wide by 9.1m long and complies with Bowen Hills PDA Development scheme and Council's TAPS Policy requirements.

Vehicle swept paths showing a 10.24m long rear-lift RCV and an 8.8m long MRV entering the site, accessing the loading area and then exiting the site are shown in Figures 3.3 and 3.4 (and attached in PTT Drawings 23-114-001 and 23-114-002 at Appendix D) respectively. As shown, the design vehicles would be able to:

- enter and exit the site in a forward gear
- enter and exit the loading area with one reverse manoeuvre





### Figure 3.3: RCV MANOEUVRING

### Figure 3.4: MRV MANOEUVRING





### 3.6 ACTIVE TRANSPORT

### 3.6.1 Pedestrians

Pedestrian access to the site from the external network is proposed at three separate locations; one at the on the northern frontage from Taylor Street, one on the eastern frontage from Abbotsford Road and the other on the north-east corner of the site from Abbotsford Road, as shown in Figure 3.5. A series of new pedestrian pathways and crossings are proposed within the site, which are expected to facilitate safe and convenient pedestrian movement between the proposed building and parking spaces.

As shown in Figure 3.5, 2.0m wide by 2.5m long pedestrian sight splays are provided on both side of the driveway to ensure adequate inter-visibility between vehicles egressing the development and pedestrians on the Taylor Street footpath. This is consistent with the requirements of AS2890.1<sup>2</sup>. No permanent obstructions to sight distance should be constructed or installed within the identified sight splay area.



#### Figure 3.5: PROPOSED PEDESTRIAN / CYCLIST FACILITIES

<sup>2</sup> Standards Australia AS/NZS 2890.11:2004 "Parking Facilities Part 1: Off-street Car Parking"



# 3.6.2 Cyclists

Councils TAPS Policy does not specify a minimum bicycle parking provision for food and drink outlets. Nevertheless, given that the development is likely to generate some demand for bicycle parking, particularly in relation to meal delivery services, the development layout incorporates a total of four bicycle parking spaces for visitors and staff, adjacent to the building entrance, as shown in Figure 3.5. Bicycle rails / racks at this location would:

- be well-lit
- be conveniently located (ie close to building entry points)
- have a high level of casual surveillance



# 4.0 TRAFFIC OPERATIONS

### 4.1 DEVELOPMENT STAGING

### 4.1.1 Timing

It is standard practice to adopt a ten-year design horizon from the year of full occupation when analysing future year traffic operations on Council's road network. Therefore, the following development staging has been adopted:

| _ | Traffic Data:               | 2022 |
|---|-----------------------------|------|
| _ | Development Application:    | 2023 |
| _ | Construction and Operation: | 2025 |
| _ | Design Horizon:             | 2035 |

### 4.1.2 Assessment Scenarios

The following assessment scenarios have been considered:

- Opening year (2025) pre-development
- Opening year (2025) post-development
- Future year (2035) pre-development
- Future year (2035) post-development

### 4.1.3 Background Traffic Growth

The scenarios modelled reflect the development staging with detailed analysis undertaken on the existing conditions, opening year (2025) and a ten-year design horizon (2025-2035). According to QLD Government Statisticians Office the population of the Bowen Hills and the surrounding area is expected to grow at a rate of 1.1% per annum. While population growth is not equal to traffic growth, it is a useful proxy in the absence of site-specific historical traffic growth data or modelling. We have therefore conservatively adopted a background traffic growth rate of 1.1% per annum. The application of this rate equates to a 15.3% increase in background traffic volumes over the next 13 years (2022-2035).

### 4.2 TRAFFIC GENERATION

### 4.2.1 Trip Generation

The likely peak hour traffic generation associated with the proposed development has been determined based on the maximum trip rate for a lower-intensity food and drink outlet (eg KFC or similar) with a drive-through from the NSW RTA Guide to Traffic Generating Developments (2002). An in:out split of 50:50 has been adopted during the peak hours. As shown in Table 4.1, the proposed development is expected to generate an additional 120 trips (60 arrivals and 60 departures) during the weekday morning and evening peak hours.



| land use              | SCALE                 | TRIP GENERATION RATE                       | TRIPS<br>(VPH) | IN : OUT<br>SPLIT |
|-----------------------|-----------------------|--|----------------|-------------------|
| Food and drink outlet | 244m <sup>2</sup> GFA | 120 vehicle trips per hour<br>per facility | 120            | 60 : 60           |

### Table 4.1: PREDICTED DEVELOPMENT PEAK HOUR TRAFFIC GENERATION

### 4.2.2 New vs Undiverted Trips

It is standard practice to take into account undiverted (linked) trips for food and drink outlets (ie accounting for the proportion of passing trade that is already on the network. Consistent with accepted practice, we have assumed 30% of trips associated with the food and drink use would be undiverted drop-in trips. This is consistent with the recommendations of the NSW RTA Guide to Traffic Generation Developments. The segmentation of the traffic associated with the proposed development is summarised in Table 4.2.

### Table 4.2: SEGMETNATION OF DEVELOPMENT TRAFFIC

| land use              | TRIPS (VPH) | NEW OR UNDIVERTED<br>DROP-IN TRIPS | DIVERTED DROP IN<br>TRIPS |
|-----------------------|-------------|------------------------------------|---------------------------|
| Food and drink outlet | 120 (60:60) | 84 (42:42)                         | 36 (18:18)                |

### 4.3 DIRECTIONAL DISTRIBUTION

The distribution of development traffic on the surrounding road network has been estimated based on the directional splits inherent in the traffic count surveys. The resulting distribution is shown in Figure 4.1 and Figure 4.2 for the weekday morning and evening peak hours and the diverted traffic for the weekday morning and evening peak hours, respectively.

### Figure 4.1: DEVELOPMENT TRAFFIC DISTRIBUTION: NEW TRIPS







### Figure 4.2: DEVELOPMENT TRAFFIC DISTRIBUTION: DIVERTED TRIPS

### 4.4 INTERSECTION OPERATIONS

The likely impact of the proposed development on the peak hour operation of the surrounding road network has been assessed using SIDRA. These analyses are based on the peak hour turning movement forecasts presented in Appendix E.

### 4.4.1 Abbotsford Road / Taylor Street

The analysis of the Abbotsford Road / Taylor Street priority-controlled intersection was undertaken using the SIDRA representation shown in Figure 2.2. The results of the analyses are summarised in Table 4.3 and attached in Appendix E. The results indicate that the intersection is expected to experience LOS A operations during the weekday morning peak hour and LOS F operations during the weekday evening peak hour, under 2025 and 2035 pre and post development conditions.

The high degree of saturation in the evening peak hour is due to the right turn movement from Taylor Street to Abbotsford Road. The right turn out of Taylor Street is a very difficult manoeuvre at peak times due to the high traffic flows on Abbotsford Road and the lack of any central median that would allow drivers to undertake a right turn in two distinct movements. The number of right turn vehicles currently making the turn is low, with no right turns recorded in the morning peak hour and eight movements in the evening peak hour. This suggests that the few drivers who perform the right turn movement from Taylor Street will be more aggressive and prepared to accept a much smaller gap than the typical gap acceptance parameters assumed by the SIDRA software. It is also possible that many of the vehicles turning right out of Taylor Street rely on the courtesy of drivers in Abbottsford Road to perform a "forced merge" in highly congested conditions where there is queuing in both directions.

The operation of the proposed development would not materially increase the demand for right turns out of Taylor Street because:

- the difficulty of performing this manoeuvre would deter most drivers and it would be largely self-enforcing
- an acceptable alternative route exists to enable motorists to avoid this difficult turn (eg via Burrows Street and the traffic signals at the Abbotsford Road / Burrows Street intersection)



| PEAK HOUR &<br>SCENARIO | DOS  | AVG<br>DELAY | 95%<br>QUEUE  | CRITICAL MOVEMENT           |
|-------------------------|------|--------------|---------------|-----------------------------|
| Weekday Morning         |      |              | '             |                             |
| 2025 Pre Development    | 38%  | 0.6s         | 10.4 Vehicles | Northern Approach Through   |
| 2025 Post Development   | 39%  | 0.9s         | 10.4 Vehicles | Northern Approach Through   |
| 2035 Pre Development    | 43%  | 0.8s         | 13.3 Vehicles | Northern Approach Through   |
| 2035 Post Development   | 44%  | 1.2s         | 13.2 Vehicles | Northern Approach Through   |
| Weekday Evening         |      |              |               |                             |
| 2025 Pre Development    | 86%  | 1.7s         | 3.7 Vehicles  | Western Approach Right Turn |
| 2025 Post Development   | 87%  | 2.1s         | 3.7 Vehicles  | Western Approach Right Turn |
| 2035 Pre Development    | 163% | 3.7s         | 4.9 Vehicles  | Western Approach Right Turn |
| 2035 Post Development   | 163% | 4.1s         | 4.9 Vehicles  | Western Approach Right Turn |

### TABLE 4.3: INTERSECTION OPERATIONS - ABBOTSFORD ROAD/ TAYLOR STREET

### 4.4.2 Abbotsford Road / Gibbie Street

The analysis of the Abbotsford Road / Gibbie Street signalised intersection was undertaken using the SIDRA representation shown in Figure 2.2. The results of the analyses are summarised in Table 4.4 and attached in Appendix E. The results indicate that the intersection is expected to experience LOS C operations during the weekday morning peak hour and LOS B operations during the weekday evening peak hour, under 2025 and 2035 pre and post development conditions. The addition of development generated traffic is not expected to have a significant adverse impact on the intersection operations.

| PEAK HOUR &<br>SCENARIO | DOS | CYCLE<br>TIME | AVG<br>DELAY | 95%<br>QUEUE  | CRITICAL MOVEMENT         |
|-------------------------|-----|---------------|--------------|---------------|---------------------------|
| Weekday Morning         | ,   |               |              |               |                           |
| 2025 Pre Development    | 48% | 120s          | 5.4s         | 5.7 Vehicles  | Northern Approach Through |
| 2025 Post Development   | 48% | 120s          | 5.4s         | 5.9 Vehicles  | Northern Approach Through |
| 2035 Pre Development    | 53% | 120s          | 5.7s         | 6.7 Vehicles  | Northern Approach Through |
| 2035 Post Development   | 53% | 120s          | 5.7s         | 6.8 Vehicles  | Northern Approach Through |
| Weekday Evening         |     |               |              |               |                           |
| 2025 Pre Development    | 49% | 120s          | 4.6s         | 11.9 Vehicles | Southern Approach Through |
| 2025 Post Development   | 50% | 120s          | 4.6s         | 12.1 Vehicles | Southern Approach Through |
| 2035 Pre Development    | 55% | 120s          | 4.9s         | 14.5 Vehicles | Southern Approach Through |
| 2035 Post Development   | 56% | 120s          | 4.9s         | 14.8 vehicles | Southern Approach Through |

### Table 4.4: INTERSECTION OPERATIONS - ABBOTSFORD ROAD / GIBBIE STREET



### 4.4.3 Taylor Street / Burrows Street

The analysis of the Taylor Street / Burrows Street priority-controlled intersection was undertaken using the SIDRA representation shown in Figure 2.3. The results of the analyses are summarised in Table 4.5 and attached in Appendix E. The results indicate that the intersection is expected to experience LOS B (or better) operations during the weekday morning peak hour and LOS C operations during the weekday evening peak hour, under 2025 and 2035 pre and post development conditions. The addition of development generated traffic is not expected to have a significant adverse impact on the intersection operations.

| PEAK HOUR &           | DOS | AVG<br>DELAV | 95%          | CRITICAL MOVEMENT           |
|-----------------------|-----|--------------|--------------|-----------------------------|
|                       |     | DLLAI        | QULUL        |                             |
| weekaay Morning       |     |              |              |                             |
| 2025 Pre Development  | 29% | 0.9s         | 0.6 vehicles | Northern Approach Through   |
| 2025 Post Development | 32% | 1.4s         | 1.2 vehicles | Eastern Approach Right Turn |
| 2035 Pre Development  | 33% | 1.1s         | 0.9 vehicles | Northern Approach Through   |
| 2035 Post Development | 35% | 1.4s         | 1.3 vehicles | Eastern Approach Right Turn |
| Weekday Evening       |     |              |              |                             |
| 2025 Pre Development  | 36% | 0.6s         | 0.6 vehicles | Southern Approach Through   |
| 2025 Post Development | 36% | 1.0s         | 1.1 vehicles | Southern Approach Through   |
| 2035 Pre Development  | 40% | 0.8s         | 0.8 vehicles | Southern Approach Through   |
| 2035 Post Development | 46% | 1.4s         | 1.8 vehicles | Eastern Approach Right Turn |

### Table 4.5: INTERSECTION OPERATIONS - TAYLOR STREET/ BURROWS STREET



### 5.0 CONCLUSIONS

The proposed food and drink outlet at 254-270 Abbotsford Road, Bowen Hills has been evaluated in terms of its site access arrangements, parking provision and design, servicing arrangements, pedestrian / cyclist facilities and likely traffic impact. The main points to note are:

- the proposal involves a 244m<sup>2</sup> GFA food and drink outlet with a drive-through facility
- vehicle access is proposed via a 7.0m wide Type B1 crossover on Taylor Street, located and designed in accordance with Council's TAPS Policy requirements
- the available sight distance and on-site queuing provision at the site access driveway are consistent with the Council's TAPS Policy
- a total of 17 on-site parking spaces are proposed to support the development comprising:
  - eight standard car parking bays (including three allocated staff parking space)
  - one PWD bay
  - two dedicated delivery bays
  - two drive-through customer waiting spaces
  - four motorcycle bays
- the on-site parking provision is above the maximum requirement from Council's TAPS
   Policy but is comparable with similar food and drink outlets in inner Brisbane and expected
   to be adequate to accommodate peak parking demand
- the drive-through facility provides capacity for up to 10 vehicles to queue without adversely impacting car park operations
- the proposed development layout provides an on-site loading bay which is capable of accommodating a RCV and MRV
- the proposed pedestrian facilities are expected to facilitate safe and convenient pedestrian movement to / from the proposed food and drink outlet
- a total of four bicycle parking spaces are proposed for visitors and staff in the form or rails / racks, located adjacent to the building entrance
- the proposed development is expected to generate a net increase of 120 vehicle trips (comprising 42 new / diverted and 18 undiverted trips) during the weekday morning and evening peak hours
- the addition of development generated traffic is not expected to have a significant adverse impact on the operation of the surrounding road network



APPENDIX A TRAFFIC SURVEYS

### AUSTRAFFIC VIDEO INTERSECTION COUNT

Site No.:1Weather: FineLocation:Abbotsford Road/Gebbie Street, Bowen HillsDay/Date:Tuesday, 22 November 2022AM Peak:Hour ending -8:00 AMPM Peak:Hour ending -5:30 PM



|              |                | Move           | ment 1 |          |                | Move           | ment 2 |          |                | Move           | ment 3    |          |                | Move           | ment 4   |          |                | Move           | ment 5   |          |                | Move           | ment 6 |          |                | Move           | ement 7 |          |                | Move           | ment 8  |          |             |          |             |          | P           | edestria | n Move      | ments    |             |          |             |          |
|--------------|----------------|----------------|--------|----------|----------------|----------------|--------|----------|----------------|----------------|-----------|----------|----------------|----------------|----------|----------|----------------|----------------|----------|----------|----------------|----------------|--------|----------|----------------|----------------|---------|----------|----------------|----------------|---------|----------|-------------|----------|-------------|----------|-------------|----------|-------------|----------|-------------|----------|-------------|----------|
| TIME         |                | more           |        |          |                | more           |        |          |                | move           | inicint o |          |                | more           | intent 4 |          |                | more           | intent o |          |                | more           |        |          |                | more           |         |          |                | move           | inent e |          | Α.          | - В      | В           | - A      | B           | 3 - C    |             | С-В      | C - D       | )        | D -         | С        |
| (1/4 hr end) | Light Vehicles | Heavy Vehicles | Total  | Cyclists | Light Vehicles | Heavy Vehicles | Total  | Cyclists | Light Vehicles | Heavy Vehicles | Total     | Cyclists | Light Vehicles | Heavy Vehicles | Total    | Cyclists | Light Vehicles | Heavy Vehicles | Total    | Cyclists | Light Vehicles | Heavy Vehicles | Total  | Cyclists | Light Vehicles | Heavy Vehicles | Total   | Cyclists | Light Vehicles | Heavy Vehicles | Total   | Cyclists | Pedestrians | Cyclists |
| 7:15 AM      | 0              | 0              | 0      | 0        | 390            | 10             | 400    | 0        | 2              | 0              | 2         | 0        | 0              | 0              | 0        | 0        | 0              | 0              | 0        | 0        | 1              | 0              | 1      | 0        | 0              | 0              | 0       | 0        | 209            | 11             | 220     | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 1           | 0        | 2           | 0        |
| 7:30 AM      | 0              | 0              | 0      | 0        | 508            | 15             | 523    | 0        | 4              | 0              | 4         | 0        | 1              | 1              | 2        | 0        | 2              | 0              | 2        | 0        | 0              | 0              | 0      | 0        | 6              | 0              | 6       | 0        | 241            | 3              | 244     | 0        | 0           | 0        | 0           | 0        | 2           | 0        | 0           | 1        | 3           | 0        | 0           | 0        |
| 7:45 AM      | 0              | 0              | 0      | 0        | 450            | 9              | 459    | 1        | 2              | 0              | 2         | 0        | 0              | 0              | 0        | 0        | 4              | 0              | 4        | 0        | 0              | 0              | 0      | 0        | 7              | 0              | 7       | 0        | 205            | 8              | 213     | 1        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        |
| 8:00 AM      | 0              | 0              | 0      | 0        | 472            | 10             | 482    | 0        | 0              | 0              | 0         | 0        | 0              | 0              | 0        | 0        | 4              | 0              | 4        | 0        | 0              | 0              | 0      | 0        | 4              | 0              | 4       | 0        | 220            | 4              | 224     | 0        | 0           | 0        | 0           | 0        | 1           | 0        | 0           | 0        | 1           | 0        | 0           | 0        |
| 8:15 AM      | 0              | 0              | 0      | 0        | 396            | 8              | 404    | 0        | 5              | 0              | 5         | 0        | 0              | 0              | 0        | 0        | 1              | 0              | 1        | 0        | 0              | 0              | 0      | 0        | 5              | 0              | 5       | 0        | 199            | 1              | 200     | 0        | 0           | 0        | 0           | 0        | 1           | 0        | 0           | 0        | 3           | 0        | 1           | 0        |
| 8:30 AM      | 0              | 0              | 0      | 0        | 436            | 14             | 450    | 0        | 5              | 0              | 5         | 0        | 1              | 0              | 1        | 0        | 2              | 0              | 2        | 0        | 0              | 0              | 0      | 0        | 3              | 0              | 3       | 0        | 198            | 7              | 205     | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        |
| 8:45 AM      | 0              | 0              | 0      | 0        | 344            | 11             | 355    | 0        | 4              | 0              | 4         | 0        | 1              | 0              | 1        | 0        | 2              | 0              | 2        | 0        | 1              | 0              | 1      | 0        | 3              | 0              | 3       | 0        | 183            | 8              | 191     | 0        | 0           | 0        | 0           | 0        | 1           | 0        | 0           | 0        | 0           | 0        | 0           | 0        |
| 9:00 AM      | 0              | 0              | 0      | 0        | 404            | 16             | 420    | 0        | 2              | 0              | 2         | 0        | 0              | 0              | 0        | 0        | 3              | 1              | 4        | 0        | 0              | 0              | 0      | 0        | 1              | 0              | 1       | 0        | 182            | 3              | 185     | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        |
| 2 hr Total   | 0              | 0              | 0      | 0        | 3400           | 86             | 3493   | 1        | 24             | 0              | 24        | 0        | £              | 1              | 4        | 0        | 18             | ٢              | 19       | 0        | 2              | 0              | 3      | 0        | 29             | 0              | 29      | 0        | 1637           | 45             | 1682    | L        | 0           | 0        | 0           | 0        | 5           | 0        | 0           | 1        | 8           | 0        | ю           | 0        |
| AM Peak      | 0              | 0              | 0      | 0        | 1820           | 44             | 1864   | 1        | 8              | 0              | 8         | 0        | 1              | -              | 2        | 0        | 10             | 0              | 10       | 0        | +              | 0              | 1      | 0        | 17             | 0              | 17      | 0        | 875            | 26             | 901     | +        | 0           | 0        | 0           | 0        | 3           | 0        | 0           |          | 2           | 0        | 3           | 0        |

|              |                | Moyo           | mont 1 |          |                | Move           | mont 2   |          |                | Mov            | omont 3 |          |                | Move           | mont 4   |          |                | Move           | mont 5 |          |                | Movo           | mont 6  |          |                | Move           | mont 7 |          |                | Movo           | mont 8   |          |             |          |             |          | Pe          | edestria | n Movem     | ents     |             |          | ·           |          |
|--------------|----------------|----------------|--------|----------|----------------|----------------|----------|----------|----------------|----------------|---------|----------|----------------|----------------|----------|----------|----------------|----------------|--------|----------|----------------|----------------|---------|----------|----------------|----------------|--------|----------|----------------|----------------|----------|----------|-------------|----------|-------------|----------|-------------|----------|-------------|----------|-------------|----------|-------------|----------|
| TIME         |                | WOVE           | ment i |          |                | WOVE           | anient 2 |          |                | NION           | ement 5 |          |                | WOVE           | anient 4 |          |                | WOVE           | ment 5 |          |                | WOVE           | lient o |          |                | WOVE           |        |          |                | WOVE           | illent o |          | Α           | - B      | В           | - A      | В           | - C      | C           | с - В    | 0           | ; - D    | D           | - C      |
| (1/4 hr end) |                |                |        |          |                |                |          |          |                |                |         |          |                |                |          |          |                |                |        |          |                |                |         |          |                |                |        |          |                |                |          |          |             |          |             |          |             |          |             |          |             |          |             |          |
|              | Light Vehicles | Heavy Vehicles | Total  | Cyclists | Light Vehicles | Heavy Vehicles | Total    | Cyclists | Light Vehicles | Heavy Vehicles | Total   | Cyclists | Light Vehicles | Heavy Vehicles | Total    | Cyclists | Light Vehicles | Heavy Vehicles | Total  | Cyclists | Light Vehicles | Heavy Vehicles | Total   | Cyclists | Light Vehicles | Heavy Vehicles | Total  | Cyclists | Light Vehicles | Heavy Vehicles | Total    | Cyclists | Pedestrians | Cyclists |
| 3:15 PM      | 0              | 0              | 0      | 0        | 274            | 4              | 278      | 0        | 0              | 0              | 0       | 0        | 0              | 0              | 0        | 0        | 6              | 0              | 6      | 0        | 1              | 0              | 1       | 0        | 5              | 0              | 5      | 0        | 253            | 5              | 258      | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        |
| 3:30 PM      | 0              | 0              | 0      | 0        | 275            | 9              | 284      | 0        | 0              | 0              | 0       | 0        | 0              | 0              | 0        | 0        | 5              | 0              | 5      | 0        | 0              | 0              | 0       | 0        | 3              | 0              | 3      | 0        | 308            | 6              | 314      | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 1        | 0           | 0        | 0           | 0        |
| 3:45 PM      | 0              | 0              | 0      | 0        | 306            | 5              | 311      | 0        | 1              | 0              | 1       | 0        | 1              | 0              | 1        | 0        | 3              | 0              | 3      | 0        | 0              | 0              | 0       | 0        | 3              | 0              | 3      | 0        | 341            | 6              | 347      | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        |
| 4:00 PM      | 0              | 0              | 0      | 0        | 303            | 5              | 308      | 0        | 0              | 0              | 0       | 0        | 4              | 0              | 4        | 0        | 5              | 0              | 5      | 0        | 1              | 0              | 1       | 0        | 2              | 0              | 2      | 0        | 316            | 11             | 327      | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 1           | 0        | 0           | 0        | 0           | 0        |
| 4:15 PM      | 0              | 0              | 0      | 0        | 255            | 6              | 261      | 1        | 0              | 0              | 0       | 0        | 4              | 0              | 4        | 0        | 6              | 0              | 6      | 0        | 0              | 0              | 0       | 0        | 7              | 0              | 7      | 0        | 305            | 5              | 310      | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 1           | 0        |
| 4:30 PM      | 0              | 0              | 0      | 0        | 261            | 7              | 268      | 0        | 2              | 1              | 3       | 0        | 3              | 0              | 3        | 0        | 4              | 0              | 4      | 0        | 0              | 0              | 0       | 0        | 2              | 0              | 2      | 0        | 408            | 6              | 414      | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 1           | 0        | 0           | 0        | 0           | 0        |
| 4:45 PM      | 0              | 0              | 0      | 0        | 308            | 5              | 313      | 0        | 3              | 0              | 3       | 0        | 1              | 0              | 1        | 0        | 3              | 0              | 3      | 0        | 0              | 0              | 0       | 0        | 0              | 2              | 2      | 0        | 364            | 4              | 368      | 0        | 0           | 0        | 0           | 0        | 1           | 0        | 0           | 2        | 0           | 0        | 0           | 0        |
| 5:00 PM      | 0              | 0              | 0      | 0        | 303            | 3              | 306      | 0        | 2              | 0              | 2       | 0        | 1              | 0              | 1        | 0        | 8              | 0              | 8      | 0        | 0              | 0              | 0       | 0        | 6              | 0              | 6      | 0        | 382            | 2              | 384      | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 1           | 0        | 0           | 0        | 0           | 0        |
| 5:15 PM      | 0              | 0              | 0      | 0        | 316            | 2              | 318      | 0        | 2              | 0              | 2       | 0        | 6              | 0              | 6        | 0        | 13             | 0              | 13     | 0        | 0              | 0              | 0       | 0        | 2              | 0              | 2      | 0        | 370            | 3              | 373      | 0        | 0           | 0        | 0           | 0        | 1           | 0        | 1           | 0        | 0           | 0        | 0           | 0        |
| 5:30 PM      | 0              | 0              | 0      | 0        | 322            | 3              | 325      | 0        | 0              | 0              | 0       | 0        | 1              | 0              | 1        | 0        | 5              | 0              | 5      | 0        | 0              | 0              | 0       | 0        | 1              | 0              | 1      | 0        | 395            | 4              | 399      | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 2           | 0        | 1           | 0        |
| 5:45 PM      | 0              | 0              | 0      | 0        | 273            | 2              | 275      | 0        | 0              | 0              | 0       | 0        | 4              | 0              | 4        | 0        | 3              | 0              | 3      | 0        | 0              | 0              | 0       | 0        | 1              | 0              | 1      | 0        | 371            | 4              | 375      | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 2           | 0        | 0           | 0        | 0           | 0        |
| 6:00 PM      | 0              | 0              | 0      | 0        | 251            | 3              | 254      | 0        | 4              | 0              | 4       | 0        | 4              | 0              | 4        | 0        | 6              | 0              | 6      | 0        | 0              | 0              | 0       | 0        | 2              | 0              | 2      | 0        | 371            | 2              | 373      | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        |
| 3 hr Total   | 0              | 0              | 0      | 0        | 3447           | 54             | 3501     | -        | 14             | -              | 15      | 0        | 29             | 0              | 29       | 0        | 67             | 0              | 67     | 0        | N              | 0              | 2       | 0        | 34             | 2              | 36     | 0        | 4184           | 58             | 4242     | 0        | 0           | 0        | 0           | 0        | 2           | 0        | 9           | e.       | 2           | 0        | 3           | 0        |
| PM Peak      | 0              | 0              | 0      | 0        | 1249           | 13             | 1262     | 0        | 7              | 0              | 7       | o        | 6              | 0              | 6        | 0        | 29             | 0              | 29     | 0        | 0              | 0              | 0       | 0        | 6              | 2              | 1      | 0        | 1511           | 13             | 1524     | 0        | 0           | 0        | 0           | 0        | 2           | 0        | 2           | 3        | 2           | 0        | -           | 0        |

### AUSTRAFFIC VIDEO INTERSECTION COUNT

Site No.:2Weather: FineLocation:Abbotsford Road/Taylor Street, Bowen HillsDay/Date:Tuesday, 22 November 2022AM Peak:Hour ending - 8:00 AMPM Peak:Hour ending - 5:30 PM





#### Abbotsford Road (south)

|              |                | Μονο           | mont 1  |          |                | Move           | mont 2  |          |                | Move           | mont 3  |          |                | Μονο           | mont 4 |          |                | Μονο           | mont 5  |          |                | Move           | mont 6 |          |                | Move           | oment 7  |          |                | Move           | mont 8 |          |             |          |             |          | Pe          | destrian | Movem       | ents     |             |          |             |          |
|--------------|----------------|----------------|---------|----------|----------------|----------------|---------|----------|----------------|----------------|---------|----------|----------------|----------------|--------|----------|----------------|----------------|---------|----------|----------------|----------------|--------|----------|----------------|----------------|----------|----------|----------------|----------------|--------|----------|-------------|----------|-------------|----------|-------------|----------|-------------|----------|-------------|----------|-------------|----------|
| TIME         |                | MOVE           | inent i |          |                | move           | inent z |          |                | MOVE           | ament o |          |                | move           | ment 4 |          |                | MOVE           | inent o |          |                | move           |        |          |                | move           | sinent i |          |                | MOVE           | ment o |          | Α-          | в        | В           | - A      | С           | - D      | D           | - C      | D           | - A      | A           | D        |
| (1/4 hr end) | Light Vehicles | Heavy Vehicles | Total   | Cyclists | Light Vehicles | Heavy Vehicles | Total   | Cyclists | Light Vehicles | Heavy Vehicles | Total   | Cyclists | Light Vehicles | Heavy Vehicles | Total  | Cyclists | Light Vehicles | Heavy Vehicles | Total   | Cyclists | Light Vehicles | Heavy Vehicles | Total  | Cyclists | Light Vehicles | Heavy Vehicles | Total    | Cyclists | Light Vehicles | Heavy Vehicles | Total  | Cyclists | Pedestrians | Cyclists |
| 7:15 AM      | 0              | 0              | 0       | 0        | 6              | 0              | 6       | 0        | 392            | 10             | 402     | 0        | 0              | 0              | 0      | 0        | 206            | 11             | 217     | 0        | 3              | 0              | 3      | 0        | 0              | 0              | 0        | 0        | 0              | 0              | 0      | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 1           | 1        |
| 7:30 AM      | 0              | 0              | 0       | 0        | 9              | 1              | 10      | 0        | 512            | 15             | 527     | 0        | 0              | 0              | 0      | 0        | 239            | 3              | 242     | 0        | 3              | 1              | 4      | 0        | 0              | 0              | 0        | 0        | 2              | 0              | 2      | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        |
| 7:45 AM      | 0              | 0              | 0       | 0        | 14             | 0              | 14      | 0        | 452            | 9              | 461     | 1        | 0              | 0              | 0      | 0        | 203            | 8              | 211     | 1        | 2              | 0              | 2      | 0        | 0              | 0              | 0        | 0        | 3              | 0              | 3      | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 1           | 0        |
| 8:00 AM      | 2              | 0              | 2       | 0        | 7              | 1              | 8       | 0        | 472            | 10             | 482     | 0        | 0              | 0              | 0      | 0        | 218            | 4              | 222     | 0        | 2              | 0              | 2      | 0        | 0              | 0              | 0        | 0        | 2              | 0              | 2      | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        |
| 8:15 AM      | 0              | 0              | 0       | 0        | 4              | 0              | 4       | 0        | 399            | 8              | 407     | 0        | 0              | 0              | 0      | 0        | 197            | 1              | 198     | 0        | 2              | 0              | 2      | 0        | 2              | 0              | 2        | 0        | 3              | 0              | 3      | 0        | 0           | 0        | 1           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        |
| 8:30 AM      | 0              | 0              | 0       | 0        | 13             | 1              | 14      | 0        | 440            | 14             | 454     | 0        | 0              | 0              | 0      | 0        | 195            | 7              | 202     | 0        | 4              | 0              | 4      | 0        | 1              | 0              | 1        | 0        | 4              | 0              | 4      | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        |
| 8:45 AM      | 0              | 0              | 0       | 0        | 7              | 1              | 8       | 0        | 344            | 11             | 355     | 0        | 0              | 0              | 0      | 0        | 182            | 8              | 190     | 0        | 2              | 0              | 2      | 0        | 4              | 0              | 4        | 0        | 8              | 0              | 8      | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 1           | 0        |
| 9:00 AM      | 0              | 0              | 0       | 0        | 8              | 0              | 8       | 0        | 406            | 16             | 422     | 0        | 0              | 0              | 0      | 0        | 176            | 3              | 179     | 0        | 6              | 0              | 6      | 0        | 0              | 0              | 0        | 0        | 1              | 0              | 1      | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        |
| 2 hr Total   | 2              | 0              | 3       | 0        | 68             | 4              | 72      | •        | 3417           | 93             | 3510    | -        | •              | •              | 0      | •        | 1616           | 45             | 1661    | -        | 24             | -              | 25     | 0        | 2              | •              | 2        | •        | 23             | •              | 23     | 0        | 0           | 0        | -           | •        | 0           | 0        | 0           | 0        | 0           | 0        | 8           | F        |
| AM Peak      | 2              | 0              | N       | 0        | 36             | 2              | 38      | 0        | 1828           | 44             | 1872    | 1        | ō              | 0              | 0      | 0        | 866            | 26             | 892     | 1        | 10             | -              | 11     | 0        | 0              | 0              | 0        | 0        | 7              | 0              | 7      | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 2           | +        |

|              |       | Marris |         |       |       |      |        |       |       |      |         |       |       | Maria |         |       |       |      |         |       |       |       |         |       |              |      |         |       |       |      |        |       |       |       |       |       | Pe    | edestria | n Moven | nents |       |       |       |       |
|--------------|-------|--------|---------|-------|-------|------|--------|-------|-------|------|---------|-------|-------|-------|---------|-------|-------|------|---------|-------|-------|-------|---------|-------|--------------|------|---------|-------|-------|------|--------|-------|-------|-------|-------|-------|-------|----------|---------|-------|-------|-------|-------|-------|
| ТІМЕ         |       | wove   | ement 1 |       |       | MOVE | ment 2 |       |       | WOVe | ement 3 |       |       | WOVE  | ement 4 |       |       | NOV  | ement 5 |       |       | NIOVE | ement 6 |       |              | NIOV | ement / |       |       | wove | ment 8 |       | A     | - B   | В     | - A   | C     | - D      | 1       | )-C   |       | D - A | Α     | - D   |
| (1/4 hr end) |       |        |         |       |       |      |        |       |       |      |         |       |       |       |         |       |       |      |         |       |       |       |         |       |              |      |         |       |       |      |        |       |       |       |       |       |       |          |         |       |       |       |       |       |
|              | s     | les    |         |       | S     | les  |        |       | s     | les  |         |       | s     | les   |         |       | Ś     | les  |         |       | s     | les   |         |       | s            | les  |         |       | s     | les  |        |       |       |       |       |       |       |          |         |       |       |       |       |       |
|              | hicle | ehic   |         |       | hicle | ehic |        |       | hicle | ehic |         |       | hicle | ehic  |         |       | hicle | ehic |         |       | hicle | ehic  |         |       | hicle        | ehic |         |       | hicle | ehic |        |       | ans   |       | ans   |       | ans   |          | ans     |       | ans   |       | ans   |       |
|              | ıt Ve | 1 11   | 1       | lists | it Ve | 1 1  | 1      | lists | it Ve | 1    | 7       | lists | it Ve | 1 1   | -       | lists | it Ve | 1    | -       | lists | t Ve  | 1 1   | -       | lists | t Ve         | 1    | 7       | lists | it Ve | 1    | -      | lists | estri | lists | estri | lists | estri | lists    | estri   | lists | estri | lists | estri | lists |
|              | Ligh  | Hea    | Tota    | Cyc   | Ligh  | Hea  | Tota   | Cyc   | Ligh  | Hea  | Toti    | Cyc   | Ligh  | Hea   | Toti    | Cyc   | Ligh  | Hea  | Toti    | Cyc   | Ligh  | Hea   | Toti    | Cyc   | Ligh         | Hea  | Toti    | Cyc   | Ligh  | Hea  | Toti   | Cyc   | Ped   | Cyc   | Ped   | Cyc   | Ped   | Cyc      | Ped     | Cyc   | Ped   | Cyc   | Ped   | Cyc   |
| 3:15 PM      | 0     | 0      | 0       | 0     | 7     | 0    | 7      | 0     | 273   | 4    | 277     | 0     | 0     | 0     | 0       | 0     | 252   | 5    | 257     | 0     | 1     | 0     | 1       | 0     | 1            | 0    | 1       | 0     | 2     | 0    | 2      | 0     | 0     | 0     | 0     | 0     | 0     | 0        | 0       | 0     | 0     | 1     | 0     | 0     |
| 3:30 PM      | 0     | 0      | 0       | 0     | 8     | 0    | 8      | 0     | 274   | 8    | 282     | 0     | 0     | 0     | 0       | 0     | 307   | 5    | 312     | 0     | 1     | 1     | 2       | 0     | 1            | 1    | 2       | 0     | 6     | 0    | 6      | 0     | 0     | 0     | 0     | 0     | 0     | 0        | 0       | 0     | 0     | 0     | 0     | 0     |
| 3:45 PM      | 0     | 0      | 0       | 0     | 4     | 0    | 4      | 0     | 304   | 5    | 309     | 0     | 0     | 0     | 0       | 0     | 338   | 6    | 344     | 0     | 4     | 0     | 4       | 0     | 3            | 0    | 3       | 0     | 9     | 0    | 9      | 0     | 0     | 0     | 0     | 0     | 0     | 0        | 0       | 0     | 0     | 0     | 0     | 0     |
| 4:00 PM      | 1     | 0      | 1       | 0     | 6     | 0    | 6      | 0     | 301   | 5    | 306     | 0     | 0     | 0     | 0       | 0     | 312   | 10   | 322     | 0     | 8     | 1     | 9       | 0     | 2            | 0    | 2       | 0     | 4     | 0    | 4      | 0     | 0     | 0     | 0     | 0     | 0     | 0        | 0       | 0     | 0     | 0     | 0     | 0     |
| 4:15 PM      | 0     | 0      | 0       | 0     | 3     | 0    | 3      | 0     | 253   | 6    | 259     | 1     | 0     | 0     | 0       | 0     | 306   | 5    | 311     | 0     | 3     | 0     | 3       | 0     | 2            | 0    | 2       | 0     | 12    | 0    | 12     | 0     | 0     | 0     | 0     | 0     | 0     | 0        | 0       | 0     | 0     | 0     | 0     | 0     |
| 4:30 PM      | 0     | 0      | 0       | 0     | 3     | 0    | 3      | 0     | 260   | 8    | 268     | 0     | 0     | 0     | 0       | 0     | 407   | 6    | 413     | 0     | 4     | 0     | 4       | 0     | 3            | 0    | 3       | 0     | 5     | 0    | 5      | 0     | 0     | 0     | 0     | 0     | 0     | 0        | 0       | 0     | 0     | 0     | 0     | 0     |
| 4:45 PM      | 0     | 0      | 0       | 0     | 2     | 0    | 2      | 0     | 307   | 5    | 312     | 0     | 0     | 0     | 0       | 0     | 364   | 4    | 368     | 0     | 1     | 0     | 1       | 0     | 4            | 0    | 4       | 0     | 4     | 0    | 4      | 0     | 0     | 0     | 0     | 0     | 0     | 0        | 0       | 0     | 0     | 1     | 0     | 0     |
| 5:00 PM      | 0     | 0      | 0       | 0     | 3     | 0    | 3      | 0     | 304   | 3    | 307     | 0     | 0     | 0     | 0       | 0     | 381   | 2    | 383     | 0     | 2     | 0     | 2       | 0     | 1            | 0    | 1       | 0     | 5     | 0    | 5      | 0     | 0     | 0     | 0     | 0     | 0     | 0        | 0       | 0     | 0     | 0     | 1     | 0     |
| 5:15 PM      | 0     | 0      | 0       | 0     | 5     | 0    | 5      | 0     | 317   | 2    | 319     | 0     | 0     | 0     | 0       | 0     | 370   | 3    | 373     | 0     | 6     | 0     | 6       | 0     | 1            | 0    | 1       | 0     | 5     | 0    | 5      | 0     | 0     | 0     | 0     | 0     | 0     | 0        | 0       | 0     | 3     | 0     | 0     | 0     |
| 5:30 PM      | 0     | 0      | 0       | 0     | 5     | 0    | 5      | 0     | 320   | 3    | 323     | 0     | 0     | 0     | 0       | 0     | 396   | 4    | 400     | 0     | 0     | 0     | 0       | 0     | 2            | 0    | 2       | 0     | 2     | 0    | 2      | 0     | 0     | 0     | 0     | 0     | 0     | 0        | 0       | 0     | 2     | 0     | 0     | 0     |
| 5:45 PM      | 0     | 0      | 0       | 0     | 2     | 0    | 2      | 0     | 273   | 2    | 275     | 0     | 0     | 0     | 0       | 0     | 374   | 4    | 378     | 0     | 1     | 0     | 1       | 0     | 0            | 0    | 0       | 0     | 3     | 0    | 3      | 0     | 0     | 0     | 0     | 0     | 0     | 0        | 0       | 0     | 1     | 0     | 0     | 0     |
| 6:00 PM      | 0     | 0      | 0       | 0     | 5     | 0    | 5      | 0     | 253   | 3    | 256     | 0     | 0     | 0     | 0       | 0     | 375   | 2    | 377     | 0     | 0     | 0     | 0       | 0     | 2            | 0    | 2       | 0     | 1     | 0    | 1      | 0     | 0     | 0     | 0     | 0     | 0     | 0        | 0       | 0     | 2     | 0     | 0     | 0     |
| tal          | -     | •      | -       | •     | 53    | •    | 53     | •     | 439   | 54   | 493     | -     | •     | •     | •       | •     | 182   | 56   | 238     | •     | 31    | 2     | 33      | •     | 22           | -    | 23      | •     | 58    | •    | 58     | •     | °     | •     | •     | •     | •     | •        | •       | •     | œ     | 7     | -     | •     |
| r To         |       |        |         |       |       |      |        |       | ň     |      | ň       |       |       |       |         |       | 4     |      | 4       |       |       |       |         |       |              |      |         |       |       |      |        |       |       |       |       |       |       |          |         |       |       |       |       |       |
| 31           |       |        |         |       |       |      |        |       |       |      |         |       |       |       |         |       |       |      |         |       |       |       |         |       |              |      |         |       |       |      |        |       |       |       |       |       |       |          |         |       |       |       |       |       |
| ¥            | •     | •      | •       | •     | 15    | •    | 15     | •     | 84    | 13   | 61      | •     | •     | •     | •       | •     | =     | 12   | 54      | •     | 6     | •     | റ       | •     | <sup>∞</sup> | •    | ø       | •     | 16    | •    | 16     | •     | •     | •     | •     | •     | •     | •        | •       | •     | 5     | -     | -     | •     |
| Pes          |       |        |         |       |       |      |        |       | 12    |      | 12      |       |       |       |         |       | 15    |      | 15      |       |       |       |         |       |              |      |         |       |       |      |        |       |       |       |       |       |       |          |         |       |       |       |       |       |
| MA           |       |        |         |       |       |      |        |       |       |      |         |       |       |       |         |       |       |      |         |       |       |       |         |       |              |      |         |       |       |      |        |       |       |       |       |       |       |          |         |       |       |       |       |       |
|              |       |        |         |       |       |      |        |       |       |      |         |       |       |       |         |       |       |      |         |       |       |       |         |       |              |      |         |       |       |      |        |       | 1     |       |       |       |       |          |         |       |       |       |       |       |

### AUSTRAFFIC VIDEO INTERSECTION COUNT

Burrows Street (north)



Site No.:3Weather: FineLocation:Burrows Street/Taylor Street, Bowen HillsDay/Date:Tuesday, 22 November 2022AM Peak:Hour ending - & 8:15 AMPM Peak:Hour ending - 5:45 PM



|              |             | Μονο         | mont 1 |        |             | Μονο         | mont 2 |        |             | Move         | mont 3    |        |             | Μονο         | mont 4 |        |             | Move         | mont 5  |        |             | Move         | mont 6  |        |             | Move         | oment 7 |        |             | Move         | mont 8  |        |             |        |           |        | P         | edestriar | n Moverr  | ents   |           |        |           |        |
|--------------|-------------|--------------|--------|--------|-------------|--------------|--------|--------|-------------|--------------|-----------|--------|-------------|--------------|--------|--------|-------------|--------------|---------|--------|-------------|--------------|---------|--------|-------------|--------------|---------|--------|-------------|--------------|---------|--------|-------------|--------|-----------|--------|-----------|-----------|-----------|--------|-----------|--------|-----------|--------|
| TIME         |             | more         |        |        |             | move         |        |        |             | move         | inicint o |        |             | more         | ment 4 |        |             | more         | inent o |        |             | more         | inent o |        |             | more         |         |        |             | more         | inent e |        | A ·         | - В    | В         | - A    | E         | 8 - C     | 0         | с-В    | с         | - D    | D         | )-C    |
| (1/4 hr end) | ht Vehicles | avy Vehicles | tal    | clists | ht Vehicles | avy Vehicles | tal    | clists | ht Vehicles | avy Vehicles | tal       | clists | ht Vehicles | avy Vehicles | tal    | clists | ht Vehicles | avy Vehicles | tal     | clists | ht Vehicles | avy Vehicles | tal     | clists | ht Vehicles | avy Vehicles | tal     | clists | ht Vehicles | avy Vehicles | tal     | clists | de strian s | clists | destrians | clists | destrians | olists    | destrians | clists | destrians | clists | destrians | clists |
|              | Lig         | He           | To     | ð      | Lig         | He           | To     | ð      | Lig         | He           | To        | Ś      | Lig         | He           | To     | ð      | Lig         | He           | 70      | ð      | Lig         | He           | To      | ð      | Lig         | He           | To      | ð      | Lig         | He           | To      | ð      | Pe          | ò      | Pe        | Š      | Pe        | Ś         | Pe        | Ś      | Pe        | ð      | Pe        | Č      |
| 7:15 AM      | 0           | 0            | 0      | 0      | 229         | 3            | 232    | 0      | 4           | 0            | 4         | 0      | 1           | 0            | 1      | 0      | 3           | 0            | 3       | 0      | 1           | 0            | 1       | 0      | 0           | 0            | 0       | 0      | 118         | 3            | 121     | 0      | 1           | 0      | 2         | 0      | 4         | 0         | 1         | 0      | 0         | 0      | 0         | 0      |
| 7:30 AM      | 0           | 0            | 0      | 0      | 250         | 1            | 251    | 0      | 5           | 0            | 5         | 0      | 3           | 1            | 4      | 0      | 9           | 1            | 10      | 0      | 1           | 0            | 1       | 0      | 1           | 0            | 1       | 0      | 146         | 4            | 150     | 0      | 1           | 0      | 2         | 0      | 0         | 0         | 2         | 0      | 0         | 0      | 1         | 0      |
| 7:45 AM      | 0           | 0            | 0      | 0      | 259         | 3            | 262    | 0      | 4           | 0            | 4         | 0      | 5           | 0            | 5      | 0      | 8           | 0            | 8       | 0      | 2           | 0            | 2       | 0      | 2           | 0            | 2       | 0      | 159         | 4            | 163     | 0      | 1           | 0      | 3         | 0      | 1         | 0         | 1         | 0      | 0         | 0      | 0         | 0      |
| 8:00 AM      | 0           | 0            | 0      | 0      | 268         | 5            | 273    | 0      | 5           | 0            | 5         | 0      | 4           | 0            | 4      | 0      | 6           | 1            | 7       | 0      | 1           | 0            | 1       | 0      | 3           | 0            | 3       | 0      | 154         | 5            | 159     | 0      | 1           | 0      | 0         | 0      | 0         | 0         | 1         | 0      | 0         | 0      | 0         | 0      |
| 8:15 AM      | 0           | 0            | 0      | 0      | 247         | 2            | 249    | 0      | 8           | 0            | 8         | 0      | 5           | 0            | 5      | 0      | 4           | 0            | 4       | 0      | 0           | 0            | 0       | 0      | 4           | 0            | 4       | 0      | 155         | 7            | 162     | 0      | 0           | 0      | 0         | 0      | 0         | 0         | 1         | 0      | 0         | 0      | 0         | 0      |
| 8:30 AM      | 0           | 0            | 0      | 0      | 228         | 5            | 233    | 0      | 3           | 0            | 3         | 0      | 8           | 0            | 8      | 0      | 7           | 0            | 7       | 0      | 2           | 0            | 2       | 0      | 7           | 0            | 7       | 0      | 146         | 1            | 147     | 0      | 0           | 0      | 0         | 0      | 0         | 1         | 0         | 0      | 0         | 0      | 0         | 0      |
| 8:45 AM      | 0           | 0            | 0      | 0      | 222         | 2            | 224    | 1      | 9           | 0            | 9         | 0      | 4           | 1            | 5      | 0      | 5           | 0            | 5       | 0      | 0           | 0            | 0       | 0      | 2           | 0            | 2       | 0      | 160         | 3            | 163     | 0      | 1           | 0      | 0         | 0      | 1         | 0         | 0         | 0      | 2         | 0      | 0         | 0      |
| 9.00 AM      | 0           | 0            | 0      | 0      | 223         | 7            | 230    | 1      | 2           | 0            | 2         | 0      | 4           | 0            | 4      | 0      | 7           | 1            | 8       | 0      | 1           | 0            | 1       | 0      | 0           | 0            | 0       | 0      | 151         | 2            | 153     | 0      | 1           | 0      | 1         | 0      | 2         | 0         | 1         | 0      | 0         | 0      | 0         | 0      |
| 2 hr Total   | 0           | 0            | 0      | 0      | 1926        | 28           | 1954   | 0      | 40          | 0            | 40        | 0      | 34          | 0            | 36     | •      | 49          | e<br>e       | 52      | 0      | 8           | 0            | 8       | •      | 19          | 0            | 19      | •      | 1189        | 5            | 1218    | e      | 9           | 0      | 8         | 0      | ŵ         | -         | 2         | 0      | 6         | o      | F         | •      |
| AM Peak      | 0           | 0            | 0      | 0      | 1024        | 11           | 1035   | 0      | 22          | 0            | 22        | 0      | 11          | 4            | 18     | 0      | 27          | 2            | 29      | 0      | 4           | 0            | 4       | 0      | 10          | 0            | 10      | 0      | 614         | 20           | 634     | 0      | 3           | 0      | ũ         | 0      | 6         | 0         | 2         | 0      | 0         | 0      | -         | 0      |

|              |                | Moyo           | mont 1  |          |                | Move           | mont 2   |          |                | Movo           | mont 3   |          |                | Movo           | mont 4 |          |                | Moyo           | mont 5 |          |                | Movo           | mont 6 |          |                | Movo           | mont 7 |          |                | Movo           | mont 8   |          |             |          |             |          | Ped         | lestrian | Moveme      | ents     |             |          |             |          |
|--------------|----------------|----------------|---------|----------|----------------|----------------|----------|----------|----------------|----------------|----------|----------|----------------|----------------|--------|----------|----------------|----------------|--------|----------|----------------|----------------|--------|----------|----------------|----------------|--------|----------|----------------|----------------|----------|----------|-------------|----------|-------------|----------|-------------|----------|-------------|----------|-------------|----------|-------------|----------|
| ТІМЕ         |                | WOVE           | inent i |          |                | WOVE           | illent 2 |          |                | WOVE           | illent 3 |          |                | WOVE           | ment 4 |          |                | WOVE           | ment 5 |          |                | WOVE           | ment o |          |                | WOVE           | ment / |          |                | MOVE           | illent o |          | A           | ·В       | В           | - A      | В-          | C        | С           | - B      | С           | - D      | D -         | - C      |
| (1/4 hr end) |                |                |         |          |                |                |          |          |                |                |          |          |                |                |        |          |                |                |        |          |                |                |        |          |                |                |        |          |                |                |          |          |             |          |             |          |             |          |             |          |             |          |             | 1        |
|              | Light Vehicles | Heavy Vehicles | Total   | Cyclists | Light Vehicles | Heavy Vehicles | Total    | Cyclists | Light Vehicles | Heavy Vehicles | Total    | Cyclists | Light Vehicles | Heavy Vehicles | Total  | Cyclists | Light Vehicles | Heavy Vehicles | Total  | Cyclists | Light Vehicles | Heavy Vehicles | Total  | Cyclists | Light Vehicles | Heavy Vehicles | Total  | Cyclists | Light Vehicles | Heavy Vehicles | Total    | Cyclists | Pedestrians | Cyclists |
| 3:15 PM      | 0              | 0              | 0       | 0        | 129            | 2              | 131      | 1        | 4              | 0              | 4        | 0        | 4              | 0              | 4      | 0        | 8              | 0              | 8      | 0        | 1              | 0              | 1      | 0        | 3              | 0              | 3      | 0        | 214            | 2              | 216      | 1        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 0        |
| 3:30 PM      | 0              | 0              | 0       | 0        | 136            | 3              | 139      | 0        | 3              | 0              | 3        | 0        | 5              | 0              | 5      | 0        | 7              | 0              | 7      | 0        | 0              | 0              | 0      | 0        | 2              | 1              | 3      | 0        | 176            | 3              | 179      | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 1           | 0        | 0           | 0        | 1           | 0        |
| 3:45 PM      | 0              | 0              | 0       | 0        | 152            | 3              | 155      | 0        | 1              | 0              | 1        | 0        | 3              | 0              | 3      | 0        | 6              | 1              | 7      | 0        | 1              | 0              | 1      | 0        | 7              | 0              | 7      | 0        | 241            | 6              | 247      | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 1           | 1        | 0           | 0        | 0           | 0        |
| 4:00 PM      | 0              | 0              | 0       | 0        | 137            | 6              | 143      | 0        | 2              | 0              | 2        | 0        | 2              | 1              | 3      | 0        | 10             | 0              | 10     | 0        | 1              | 0              | 1      | 0        | 3              | 0              | 3      | 0        | 249            | 5              | 254      | 0        | 1           | 0        | 0           | 0        | 0           | 0        | 0           | 1        | 0           | 0        | 0           | 0        |
| 4:15 PM      | 0              | 0              | 0       | 0        | 142            | 3              | 145      | 0        | 5              | 0              | 5        | 0        | 7              | 0              | 7      | 0        | 7              | 0              | 7      | 0        | 1              | 0              | 1      | 0        | 9              | 0              | 9      | 0        | 268            | 5              | 273      | 0        | 1           | 0        | 0           | 1        | 0           | 0        | 1           | 1        | 0           | 0        | 0           | 0        |
| 4:30 PM      | 0              | 0              | 0       | 0        | 146            | 3              | 149      | 0        | 4              | 0              | 4        | 0        | 7              | 0              | 7      | 0        | 10             | 0              | 10     | 0        | 0              | 0              | 0      | 0        | 5              | 0              | 5      | 0        | 284            | 2              | 286      | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 0           | 1        | 0           | 0        | 0           | 0        |
| 4:45 PM      | 0              | 0              | 0       | 0        | 159            | 0              | 159      | 0        | 0              | 0              | 0        | 0        | 2              | 0              | 2      | 0        | 4              | 0              | 4      | 0        | 1              | 0              | 1      | 0        | 4              | 0              | 4      | 0        | 262            | 2              | 264      | 0        | 1           | 0        | 0           | 0        | 0           | 0        | 0           | 1        | 0           | 0        | 0           | 0        |
| 5:00 PM      | 0              | 0              | 0       | 0        | 173            | 0              | 173      | 0        | 5              | 0              | 5        | 0        | 0              | 0              | 0      | 0        | 5              | 0              | 5      | 0        | 0              | 0              | 0      | 0        | 1              | 0              | 1      | 0        | 330            | 4              | 334      | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 2           | 0        | 0           | 0        | 0           | 0        |
| 5:15 PM      | 0              | 0              | 0       | 0        | 163            | 0              | 163      | 0        | 1              | 0              | 1        | 0        | 10             | 0              | 10     | 0        | 13             | 0              | 13     | 0        | 1              | 0              | 1      | 0        | 4              | 0              | 4      | 0        | 299            | 3              | 302      | 3        | 0           | 0        | 0           | 1        | 0           | 0        | 0           | 1        | 0           | 0        | 0           | 0        |
| 5:30 PM      | 0              | 0              | 0       | 0        | 201            | 2              | 203      | 0        | 1              | 0              | 1        | 0        | 2              | 0              | 2      | 0        | 4              | 0              | 4      | 0        | 0              | 0              | 0      | 0        | 2              | 0              | 2      | 0        | 327            | 1              | 328      | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 1           | 1        | 0           | 0        | 0           | 0        |
| 5:45 PM      | 0              | 0              | 0       | 0        | 133            | 2              | 135      | 0        | 0              | 0              | 0        | 0        | 4              | 0              | 4      | 0        | 2              | 0              | 2      | 0        | 0              | 0              | 0      | 0        | 2              | 0              | 2      | 0        | 342            | 1              | 343      | 1        | 0           | 0        | 0           | 0        | 0           | 0        | 1           | 1        | 0           | 0        | 0           | 0        |
| 6:00 PM      | 0              | 0              | 0       | 0        | 173            | 1              | 174      | 0        | 1              | 0              | 1        | 0        | 6              | 0              | 6      | 0        | 1              | 0              | 1      | 0        | 0              | 0              | 0      | 0        | 2              | 0              | 2      | 0        | 276            | 1              | 277      | 0        | 0           | 0        | 0           | 0        | 0           | 0        | 1           | 0        | 0           | 0        | 0           | 0        |
| 3 hr Total   | 0              | 0              | •       | 0        | 1844           | 25             | 1869     |          | 27             | 0              | 27       |          | 52             | -              | 23     | •        | 17             | -              | 78     |          | 9              | •              | 9      | 0        | 44             | -              | 45     |          | 3268           | 35             | 3303     | Ω.       | 3           | 0        | •           | 5        | 0           | 0        | 8           | 8        | 0           | 0        | -           | 8        |
| PM Peak      | 0              | 0              | 0       | 0        | 670            | 4              | 674      | 0        | 2              | 0              | 2        | 0        | 16             | 0              | 16     | 0        | 24             | 0              | 24     | 0        | -              | 0              | 1      | 0        | 6              | 0              | 6      | 0        | 1298           | 6              | 1307     | 4        | 0           | 0        | 0           | -        | 0           | 0        | 4           | e        | 0           | 0        | 0           | 0        |



APPENDIX B INTERSECTION ANALYSES

# SITE LAYOUT

## Site: 101 [AM 2022 Existing Conditions (Site Folder: General)]

Abbotsford Road / Gebbie Street Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



# PHASING SUMMARY

### Site: 101 [AM 2022 Existing Conditions (Site Folder: General)]

Abbotsford Road / Gebbie Street Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time)

Timings based on settings in the Site Phasing & Timing dialog Phase Times determined by the program Phase Sequence: Leading Right Turn Reference Phase: Phase B Input Phase Sequence: A, B, C Output Phase Sequence: A, B, C

#### Phase Timing Summary

| Phase                   | Α   | В   | С   |
|-------------------------|-----|-----|-----|
| Phase Change Time (sec) | 24  | 0   | 12  |
| Green Time (sec)        | 90  | 6   | 6   |
| Phase Time (sec)        | 96  | 12  | 12  |
| Phase Split             | 80% | 10% | 10% |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than 100%.

#### **Output Phase Sequence**



Other Movement Class (MC) Running
 Mixed Running & Stopped MCs
 Other Movement Class (MC) Stopped



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# **NETWORK LAYOUT**

## ■ Network: N101 [AM 2022 Existing Conditions (Network

Folder: General)]

#### New Network Network Category: (None)

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



| SITES IN N   | IETWORK |                             |
|--------------|---------|-----------------------------|
| Site ID      | CCG ID  | Site Name                   |
| 101          | NA      | AM 2022 Existing Conditions |
| <b>▽</b> 102 | NA      | AM 2022 Existing Conditions |

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V Site: 102 [AM 2022 Existing Conditions (Site Folder: General)]

# Network: N101 [AM 2022 Existing Conditions (Network Folder: General)]

Abbotsford Road / Taylor Street Site Category: (None) Give-Way (Two-Way)

| Vehi      | cle Mo  | vement                           | Perfo                 | rmanc                           | e                     |                     |                       |                     |                              |                                |              |                            |                    |                        |
|-----------|---------|----------------------------------|-----------------------|---------------------------------|-----------------------|---------------------|-----------------------|---------------------|------------------------------|--------------------------------|--------------|----------------------------|--------------------|------------------------|
| Mov<br>ID | Turn    | DEMA<br>FLO\<br>[ Total<br>veh/h | AND<br>NS<br>HV]<br>% | ARRI<br>FLO<br>[ Total<br>veh/h | VAL<br>WS<br>HV]<br>% | Deg.<br>Satn<br>v/c | Aver.<br>Delay<br>sec | Level of<br>Service | 95% I<br>QI<br>[ Veh.<br>veh | BACK OF<br>UEUE<br>Dist ]<br>m | Prop.<br>Que | EffectiveA<br>Stop<br>Rate | ver. No.<br>Cycles | Aver.<br>Speed<br>km/h |
| South     | : Abbot | tsford Ro                        | ad                    |                                 |                       |                     |                       |                     |                              |                                |              |                            |                    |                        |
| 1         | L2      | 12                               | 9.1                   | 12                              | 9.1                   | 0.245               | 2.7                   | LOS A               | 0.0                          | 0.0                            | 0.00         | 0.01                       | 0.00               | 56.0                   |
| 2         | T1      | 933                              | 2.9                   | 933                             | 2.9                   | 0.245               | 0.0                   | LOS A               | 0.0                          | 0.0                            | 0.00         | 0.01                       | 0.00               | 59.8                   |
| Appro     | bach    | 945                              | 3.0                   | 945                             | 3.0                   | 0.245               | 0.0                   | NA                  | 0.0                          | 0.0                            | 0.00         | 0.01                       | 0.00               | 59.8                   |
| North     | : Abbot | sford Roa                        | ad                    |                                 |                       |                     |                       |                     |                              |                                |              |                            |                    |                        |
| 8         | T1      | 1958                             | 2.4                   | 1958                            | 2.4                   | 0.363               | 0.4                   | LOS A               | 9.7                          | 69.3                           | 0.05         | 0.01                       | 0.06               | 58.8                   |
| 9         | R2      | 42                               | 5.3                   | 42                              | 5.3                   | 0.363               | 12.4                  | LOS B               | 9.7                          | 69.3                           | 0.18         | 0.05                       | 0.22               | 52.8                   |
| Appro     | bach    | 2000                             | 2.5                   | 2000                            | 2.5                   | 0.363               | 0.7                   | NA                  | 9.7                          | 69.3                           | 0.05         | 0.01                       | 0.07               | 58.5                   |
| West      | Taylor  | Street                           |                       |                                 |                       |                     |                       |                     |                              |                                |              |                            |                    |                        |
| 10        | L2      | 7                                | 0.0                   | 7                               | 0.0                   | 0.008               | 6.4                   | LOS A               | 0.0                          | 0.2                            | 0.44         | 0.55                       | 0.44               | 48.6                   |
| 12        | R2      | 1                                | 0.0                   | 1                               | 0.0                   | 0.059               | 95.7                  | LOS F               | 0.1                          | 0.5                            | 0.97         | 0.99                       | 0.97               | 14.0                   |
| Appro     | bach    | 8                                | 0.0                   | 8                               | 0.0                   | 0.059               | 17.6                  | LOS C               | 0.1                          | 0.5                            | 0.51         | 0.61                       | 0.51               | 41.6                   |
| All Ve    | hicles  | 2953                             | 2.6                   | 2953                            | 2.6                   | 0.363               | 0.5                   | NA                  | 9.7                          | 69.3                           | 0.04         | 0.01                       | 0.05               | 58.8                   |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Network Data dialog (Network tab).

Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Project: P:\2022-23\23-114 254-270 Abbotsford Road, Bowen Hills\Calcs\Revised Abbotsford Road.sip9

Site: 101 [AM 2022 Existing Conditions (Site Folder: General)]

### Abbotsford Road / Gebbie Street

Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time)

| Vehi      | cle Mo  | vement                           | Perfo                 | rmanc                           | e:                    |                     |                       |                     |                             |                                |              |                                    |                    |                        |
|-----------|---------|----------------------------------|-----------------------|---------------------------------|-----------------------|---------------------|-----------------------|---------------------|-----------------------------|--------------------------------|--------------|------------------------------------|--------------------|------------------------|
| Mov<br>ID | Turn    | DEMA<br>FLO\<br>[ Total<br>veh/h | AND<br>NS<br>HV]<br>% | ARRI<br>FLO<br>[ Total<br>veh/h | VAL<br>WS<br>HV]<br>% | Deg.<br>Satn<br>v/c | Aver.<br>Delay<br>sec | Level of<br>Service | 95%  <br>Q<br>[ Veh.<br>veh | BACK OF<br>UEUE<br>Dist ]<br>m | Prop.<br>Que | Effective <i>A</i><br>Stop<br>Rate | ver. No.<br>Cycles | Aver.<br>Speed<br>km/h |
| South     | n: Abbo | tsford Ro                        | ad                    |                                 |                       |                     |                       |                     |                             |                                |              |                                    |                    |                        |
| 2         | T1      | 942                              | 2.9                   | 942                             | 2.9                   | 0.297               | 1.9                   | LOS A               | 5.5                         | 39.4                           | 0.22         | 0.19                               | 0.22               | 56.5                   |
| 3         | R2      | 19                               | 0.0                   | 19                              | 0.0                   | *0.209              | 68.3                  | LOS E               | 1.1                         | 7.9                            | 0.99         | 0.70                               | 0.99               | 26.9                   |
| Appro     | bach    | 961                              | 2.8                   | 961                             | 2.8                   | 0.297               | 3.2                   | LOS A               | 5.5                         | 39.4                           | 0.23         | 0.20                               | 0.23               | 54.3                   |
| East:     | Gebbie  | e Street                         |                       |                                 |                       |                     |                       |                     |                             |                                |              |                                    |                    |                        |
| 4         | L2      | 10                               | 0.0                   | 10                              | 0.0                   | 0.064               | 57.2                  | LOS E               | 0.7                         | 5.0                            | 0.93         | 0.68                               | 0.93               | 29.0                   |
| 6         | R2      | 2                                | 50.0                  | 2                               | 50.0                  | *0.064              | 57.6                  | LOS E               | 0.7                         | 5.0                            | 0.93         | 0.68                               | 0.93               | 19.7                   |
| Appro     | bach    | 13                               | 8.3                   | 13                              | 8.3                   | 0.064               | 57.2                  | LOS E               | 0.7                         | 5.0                            | 0.93         | 0.68                               | 0.93               | 27.8                   |
| North     | : Abbot | sford Roa                        | ad                    |                                 |                       |                     |                       |                     |                             |                                |              |                                    |                    |                        |
| 7         | L2      | 8                                | 0.0                   | 8                               | 0.0                   | 0.461               | 8.7                   | LOS A               | 4.6                         | 32.6                           | 0.41         | 0.38                               | 0.41               | 42.9                   |
| 8         | T1      | 1950                             | 2.4                   | 1950                            | 2.4                   | *0.461              | 6.0                   | LOS A               | 4.6                         | 32.6                           | 0.41         | 0.38                               | 0.41               | 50.5                   |
| Appro     | bach    | 1958                             | 2.4                   | 1958                            | 2.4                   | 0.461               | 6.0                   | LOS A               | 4.6                         | 32.6                           | 0.41         | 0.38                               | 0.41               | 50.4                   |
| All Ve    | hicles  | 2932                             | 2.6                   | 2932                            | 2.6                   | 0.461               | 5.3                   | LOS A               | 5.5                         | 39.4                           | 0.35         | 0.32                               | 0.35               | 51.3                   |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

\* Critical Movement (Signal Timing)

| Pedestrian Mov    | vement | Perform | nance    |              |              |         |              |        |        |       |
|-------------------|--------|---------|----------|--------------|--------------|---------|--------------|--------|--------|-------|
| Mov               | Dem.   | Aver.   | Level of | AVERAGE      | BACK OF      | Prop. E | Effective    | Travel | Travel | Aver. |
| ID Crossing       | Flow   | Delay   | Service  | QUE<br>[ Ped | UE<br>Dist ] | Que     | Stop<br>Rate | Time   | Dist.  | Speed |
|                   | ped/h  | sec     |          | ped          | m            |         |              | sec    | m      | m/sec |
| South: Abbotsford | d Road |         |          |              |              |         |              |        |        |       |
| P1 Full           | 11     | 54.2    | LOS E    | 0.0          | 0.0          | 0.95    | 0.95         | 223.5  | 220.1  | 0.98  |
| East: Gebbie Stre | et     |         |          |              |              |         |              |        |        |       |
| P2 Full           | 11     | 54.2    | LOS E    | 0.0          | 0.0          | 0.95    | 0.95         | 216.3  | 210.8  | 0.97  |
| All Pedestrians   | 21     | 54.2    | LOS E    | 0.0          | 0.0          | 0.95    | 0.95         | 219.9  | 215.5  | 0.98  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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Site: 101 [PM 2022 Existing Conditions (Site Folder: General)]

### Abbotsford Road / Gebbie Street

Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time)

| Vehio     | cle Mo  | vement                  | Perfo            | rmanc                  | e:               |              |                |                     |                       |                          |              |                                    |                    |                |
|-----------|---------|-------------------------|------------------|------------------------|------------------|--------------|----------------|---------------------|-----------------------|--------------------------|--------------|------------------------------------|--------------------|----------------|
| Mov<br>ID | Turn    | DEMA<br>FLO\<br>[ Total | AND<br>NS<br>HV] | ARRI<br>FLO<br>[ Total | VAL<br>WS<br>HV] | Deg.<br>Satn | Aver.<br>Delay | Level of<br>Service | 95% B<br>QU<br>[ Veh. | ACK OF<br>IEUE<br>Dist ] | Prop.<br>Que | Effective <i>A</i><br>Stop<br>Rate | ver. No.<br>Cycles | Aver.<br>Speed |
| South     | : Abbo  | tsford Ro               | ad               | VCH/H                  | 70               | v/C          | 300            |                     | VCII                  |                          |              |                                    |                    | KI11/11        |
| 2         | T1      | 1550                    | 0.9              | 1550                   | 0.9              | *0.477       | 2.4            | LOS A               | 11.3                  | 79.4                     | 0.27         | 0.25                               | 0.27               | 55.7           |
| 3         | R2      | 11                      | 18.2             | 11                     | 18.2             | 0.141        | 68.4           | LOS E               | 0.7                   | 5.4                      | 0.98         | 0.68                               | 0.98               | 26.9           |
| Appro     | ach     | 1562                    | 1.0              | 1562                   | 1.0              | 0.477        | 2.8            | LOS A               | 11.3                  | 79.4                     | 0.28         | 0.25                               | 0.28               | 54.9           |
| East:     | Gebbie  | e Street                |                  |                        |                  |              |                |                     |                       |                          |              |                                    |                    |                |
| 4         | L2      | 30                      | 0.0              | 30                     | 0.0              | 0.218        | 60.7           | LOS E               | 2.2                   | 15.2                     | 0.96         | 0.73                               | 0.96               | 28.2           |
| 6         | R2      | 9                       | 0.0              | 9                      | 0.0              | *0.218       | 60.7           | LOS E               | 2.2                   | 15.2                     | 0.96         | 0.73                               | 0.96               | 19.0           |
| Appro     | ach     | 39                      | 0.0              | 39                     | 0.0              | 0.218        | 60.7           | LOS E               | 2.2                   | 15.2                     | 0.96         | 0.73                               | 0.96               | 26.5           |
| North     | : Abbot | sford Roa               | ad               |                        |                  |              |                |                     |                       |                          |              |                                    |                    |                |
| 7         | L2      | 7                       | 0.0              | 7                      | 0.0              | 0.301        | 7.8            | LOS A               | 4.6                   | 32.6                     | 0.35         | 0.31                               | 0.35               | 43.8           |
| 8         | T1      | 1284                    | 1.0              | 1284                   | 1.0              | 0.301        | 5.1            | LOS A               | 4.6                   | 32.6                     | 0.35         | 0.31                               | 0.35               | 51.7           |
| Appro     | ach     | 1291                    | 1.0              | 1291                   | 1.0              | 0.301        | 5.1            | LOS A               | 4.6                   | 32.6                     | 0.35         | 0.31                               | 0.35               | 51.7           |
| All Ve    | hicles  | 2891                    | 1.0              | 2891                   | 1.0              | 0.477        | 4.6            | LOS A               | 11.3                  | 79.4                     | 0.32         | 0.29                               | 0.32               | 52.2           |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

\* Critical Movement (Signal Timing)

| Pedestrian Mov    | vement | Perform | nance    |              |              |         |              |        |        |       |
|-------------------|--------|---------|----------|--------------|--------------|---------|--------------|--------|--------|-------|
| Mov               | Dem.   | Aver.   | Level of | AVERAGE      | BACK OF      | Prop. E | Effective    | Travel | Travel | Aver. |
| ID Crossing       | Flow   | Delay   | Service  | QUE<br>[ Ped | UE<br>Dist ] | Que     | Stop<br>Rate | Time   | Dist.  | Speed |
|                   | ped/h  | sec     |          | ped          | m            |         |              | sec    | m      | m/sec |
| South: Abbotsford | d Road |         |          |              |              |         |              |        |        |       |
| P1 Full           | 11     | 54.2    | LOS E    | 0.0          | 0.0          | 0.95    | 0.95         | 223.5  | 220.1  | 0.98  |
| East: Gebbie Stre | et     |         |          |              |              |         |              |        |        |       |
| P2 Full           | 11     | 54.2    | LOS E    | 0.0          | 0.0          | 0.95    | 0.95         | 216.3  | 210.8  | 0.97  |
| All Pedestrians   | 21     | 54.2    | LOS E    | 0.0          | 0.0          | 0.95    | 0.95         | 219.9  | 215.5  | 0.98  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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V Site: 102 [PM 2022 Existing Conditions (Site Folder: General)]

### ■ Network: N101 [PM 2022 Existing Conditions (Network Folder: General)]

#### Abbotsford Road / Taylor Street Site Category: (None) Give-Way (Two-Way)

| Vehio     | cle Mo  | vement                           | Perfo                 | rmanc                           | e                     |                     |                       |                     |                             |                                |              |                                    |                    |                        |
|-----------|---------|----------------------------------|-----------------------|---------------------------------|-----------------------|---------------------|-----------------------|---------------------|-----------------------------|--------------------------------|--------------|------------------------------------|--------------------|------------------------|
| Mov<br>ID | Turn    | DEMA<br>FLOV<br>[ Total<br>veh/h | AND<br>WS<br>HV]<br>% | ARRI<br>FLO<br>[ Total<br>veh/h | VAL<br>WS<br>HV]<br>% | Deg.<br>Satn<br>v/c | Aver.<br>Delay<br>sec | Level of<br>Service | 95%  <br>Q<br>[ Veh.<br>veh | BACK OF<br>UEUE<br>Dist ]<br>m | Prop.<br>Que | Effective <i>A</i><br>Stop<br>Rate | ver. No.<br>Cycles | Aver.<br>Speed<br>km/h |
| South     | : Abbo  | tsford Ro                        | ad                    |                                 |                       |                     |                       |                     |                             |                                |              |                                    |                    |                        |
| 1         | L2      | 9                                | 0.0                   | 9                               | 0.0                   | 0.398               | 2.7                   | LOS A               | 0.0                         | 0.0                            | 0.00         | 0.01                               | 0.00               | 56.7                   |
| 2         | T1      | 1550                             | 0.9                   | 1550                            | 0.9                   | 0.398               | 0.0                   | LOS A               | 0.0                         | 0.0                            | 0.00         | 0.00                               | 0.00               | 59.7                   |
| Appro     | bach    | 1560                             | 0.9                   | 1560                            | 0.9                   | 0.398               | 0.0                   | NA                  | 0.0                         | 0.0                            | 0.00         | 0.00                               | 0.00               | 59.7                   |
| North     | : Abbot | sford Roa                        | ad                    |                                 |                       |                     |                       |                     |                             |                                |              |                                    |                    |                        |
| 8         | T1      | 1283                             | 1.0                   | 1283                            | 1.0                   | 0.238               | 0.7                   | LOS A               | 3.3                         | 23.4                           | 0.05         | 0.01                               | 0.06               | 58.3                   |
| 9         | R2      | 15                               | 0.0                   | 15                              | 0.0                   | 0.238               | 20.8                  | LOS C               | 3.2                         | 22.9                           | 0.19         | 0.03                               | 0.21               | 52.0                   |
| Appro     | bach    | 1298                             | 1.0                   | 1298                            | 1.0                   | 0.238               | 0.9                   | NA                  | 3.3                         | 23.4                           | 0.05         | 0.01                               | 0.06               | 58.1                   |
| West:     | Taylor  | Street                           |                       |                                 |                       |                     |                       |                     |                             |                                |              |                                    |                    |                        |
| 10        | L2      | 16                               | 0.0                   | 16                              | 0.0                   | 0.026               | 8.7                   | LOS A               | 0.1                         | 0.6                            | 0.57         | 0.72                               | 0.57               | 47.2                   |
| 12        | R2      | 8                                | 0.0                   | 8                               | 0.0                   | 0.743               | 329.3                 | LOS F               | 1.0                         | 7.1                            | 0.99         | 1.04                               | 1.19               | 5.1                    |
| Appro     | bach    | 24                               | 0.0                   | 24                              | 0.0                   | 0.743               | 115.5                 | LOS F               | 1.0                         | 7.1                            | 0.71         | 0.83                               | 0.78               | 17.6                   |
| All Ve    | hicles  | 2882                             | 0.9                   | 2882                            | 0.9                   | 0.743               | 1.4                   | NA                  | 3.3                         | 23.4                           | 0.03         | 0.01                               | 0.03               | 57.2                   |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Network Data dialog (Network tab).

Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Project: P:\2022-23\23-114 254-270 Abbotsford Road, Bowen Hills\Calcs\Revised Abbotsford Road.sip9

Site: 101 [AM 2025 Pre Development (Site Folder: General)]

#### ■ Network: N101 [AM 2025 Pre Development (Network Folder: General)]

#### Abbotsford Road / Gebbie Street

Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time)

| Vehi      | cle Mo  | vement                           | Perfo                | rmanc                           | e:                    |                     |                       |                     |                              |                                |              |                                    |                    |                        |
|-----------|---------|----------------------------------|----------------------|---------------------------------|-----------------------|---------------------|-----------------------|---------------------|------------------------------|--------------------------------|--------------|------------------------------------|--------------------|------------------------|
| Mov<br>ID | Turn    | DEMA<br>FLOV<br>[ Total<br>veh/h | ND<br>VS<br>HV]<br>% | ARRI<br>FLO<br>[ Total<br>veh/h | VAL<br>WS<br>HV]<br>% | Deg.<br>Satn<br>v/c | Aver.<br>Delay<br>sec | Level of<br>Service | 95% [<br>QI<br>[ Veh.<br>veh | BACK OF<br>JEUE<br>Dist ]<br>m | Prop.<br>Que | Effective <i>A</i><br>Stop<br>Rate | ver. No.<br>Cycles | Aver.<br>Speed<br>km/h |
| South     | : Abbo  | tsford Ro                        | ad                   |                                 |                       |                     |                       |                     |                              |                                |              |                                    |                    |                        |
| 2         | T1      | 974                              | 2.9                  | 974                             | 2.9                   | 0.307               | 1.9                   | LOS A               | 5.7                          | 41.2                           | 0.22         | 0.20                               | 0.22               | 56.5                   |
| 3         | R2      | 20                               | 0.0                  | 20                              | 0.0                   | *0.221              | 68.4                  | LOS E               | 1.2                          | 8.3                            | 0.99         | 0.70                               | 0.99               | 26.9                   |
| Appro     | bach    | 994                              | 2.8                  | 994                             | 2.8                   | 0.307               | 3.2                   | LOS A               | 5.7                          | 41.2                           | 0.23         | 0.21                               | 0.23               | 54.2                   |
| East:     | Gebbie  | e Street                         |                      |                                 |                       |                     |                       |                     |                              |                                |              |                                    |                    |                        |
| 4         | L2      | 10                               | 0.0                  | 10                              | 0.0                   | 0.064               | 57.2                  | LOS E               | 0.7                          | 5.0                            | 0.93         | 0.68                               | 0.93               | 29.0                   |
| 6         | R2      | 2                                | 50.0                 | 2                               | 50.0                  | *0.064              | 57.6                  | LOS E               | 0.7                          | 5.0                            | 0.93         | 0.68                               | 0.93               | 19.7                   |
| Appro     | bach    | 13                               | 8.3                  | 13                              | 8.3                   | 0.064               | 57.2                  | LOS E               | 0.7                          | 5.0                            | 0.93         | 0.68                               | 0.93               | 27.8                   |
| North     | : Abbot | sford Roa                        | ad                   |                                 |                       |                     |                       |                     |                              |                                |              |                                    |                    |                        |
| 7         | L2      | 8                                | 0.0                  | 8                               | 0.0                   | 0.476               | 8.8                   | LOS A               | 4.6                          | 32.6                           | 0.42         | 0.39                               | 0.42               | 42.8                   |
| 8         | T1      | 2015                             | 2.4                  | 2015                            | 2.4                   | *0.476              | 6.1                   | LOS A               | 4.6                          | 32.6                           | 0.42         | 0.39                               | 0.42               | 50.3                   |
| Appro     | bach    | 2023                             | 2.4                  | 2023                            | 2.4                   | 0.476               | 6.1                   | LOS A               | 4.6                          | 32.6                           | 0.42         | 0.39                               | 0.42               | 50.3                   |
| All Ve    | hicles  | 3029                             | 2.6                  | 3029                            | 2.6                   | 0.476               | 5.4                   | LOS A               | 5.7                          | 41.2                           | 0.36         | 0.33                               | 0.36               | 51.2                   |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

\* Critical Movement (Signal Timing)

| Pedestrian Mov    | vement | Perform | nance    |              |              |         |              |        |        |       |
|-------------------|--------|---------|----------|--------------|--------------|---------|--------------|--------|--------|-------|
| Mov               | Dem.   | Aver.   | Level of | AVERAGE      | BACK OF      | Prop. E | Effective    | Travel | Travel | Aver. |
| ID Crossing       | Flow   | Delay   | Service  | QUE<br>[ Ped | UE<br>Dist ] | Que     | Stop<br>Rate | Time   | Dist.  | Speed |
|                   | ped/h  | sec     |          | ped          | m            |         |              | sec    | m      | m/sec |
| South: Abbotsford | d Road |         |          |              |              |         |              |        |        |       |
| P1 Full           | 11     | 54.2    | LOS E    | 0.0          | 0.0          | 0.95    | 0.95         | 223.5  | 220.1  | 0.98  |
| East: Gebbie Stre | et     |         |          |              |              |         |              |        |        |       |
| P2 Full           | 11     | 54.2    | LOS E    | 0.0          | 0.0          | 0.95    | 0.95         | 216.3  | 210.8  | 0.97  |
| All Pedestrians   | 21     | 54.2    | LOS E    | 0.0          | 0.0          | 0.95    | 0.95         | 219.9  | 215.5  | 0.98  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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V Site: 102 [AM 2025 Pre Development (Site Folder: General)]

Abbotsford Road / Taylor Street Site Category: (None) Give-Way (Two-Way)

| Vehi      | cle Mo  | vement                           | Perfo                 | rmanc                           | e                     |                     |                       |                     |                             |                                |              |                                    |                    |                        |
|-----------|---------|----------------------------------|-----------------------|---------------------------------|-----------------------|---------------------|-----------------------|---------------------|-----------------------------|--------------------------------|--------------|------------------------------------|--------------------|------------------------|
| Mov<br>ID | Turn    | DEMA<br>FLO\<br>[ Total<br>veh/h | AND<br>WS<br>HV]<br>% | ARRI<br>FLO<br>[ Total<br>veh/h | VAL<br>WS<br>HV]<br>% | Deg.<br>Satn<br>v/c | Aver.<br>Delay<br>sec | Level of<br>Service | 95%  <br>Q<br>[ Veh.<br>veh | BACK OF<br>UEUE<br>Dist ]<br>m | Prop.<br>Que | Effective <i>F</i><br>Stop<br>Rate | ver. No.<br>Cycles | Aver.<br>Speed<br>km/h |
| South     | : Abbo  | tsford Ro                        | ad                    |                                 |                       |                     |                       |                     |                             |                                |              |                                    |                    |                        |
| 1         | L2      | 12                               | 9.1                   | 12                              | 9.1                   | 0.253               | 2.7                   | LOS A               | 0.0                         | 0.0                            | 0.00         | 0.01                               | 0.00               | 56.0                   |
| 2         | T1      | 964                              | 2.9                   | 964                             | 2.9                   | 0.253               | 0.0                   | LOS A               | 0.0                         | 0.0                            | 0.00         | 0.01                               | 0.00               | 59.8                   |
| Appro     | bach    | 976                              | 3.0                   | 976                             | 3.0                   | 0.253               | 0.0                   | NA                  | 0.0                         | 0.0                            | 0.00         | 0.01                               | 0.00               | 59.8                   |
| North     | : Abbot | sford Roa                        | ad                    |                                 |                       |                     |                       |                     |                             |                                |              |                                    |                    |                        |
| 8         | T1      | 2023                             | 2.4                   | 2023                            | 2.4                   | 0.379               | 0.5                   | LOS A               | 10.4                        | 74.6                           | 0.06         | 0.01                               | 0.08               | 58.5                   |
| 9         | R2      | 43                               | 5.3                   | 43                              | 5.3                   | 0.379               | 14.3                  | LOS B               | 10.4                        | 74.6                           | 0.22         | 0.05                               | 0.28               | 52.4                   |
| Appro     | bach    | 2066                             | 2.5                   | 2066                            | 2.5                   | 0.379               | 0.8                   | NA                  | 10.4                        | 74.6                           | 0.07         | 0.01                               | 0.08               | 58.2                   |
| West:     | Taylor  | Street                           |                       |                                 |                       |                     |                       |                     |                             |                                |              |                                    |                    |                        |
| 10        | L2      | 7                                | 0.0                   | 7                               | 0.0                   | 0.008               | 6.6                   | LOS A               | 0.0                         | 0.2                            | 0.45         | 0.58                               | 0.45               | 48.5                   |
| 12        | R2      | 1                                | 0.0                   | 1                               | 0.0                   | 0.097               | 149.7                 | LOS F               | 0.1                         | 0.8                            | 0.98         | 0.99                               | 0.98               | 9.9                    |
| Appro     | bach    | 8                                | 0.0                   | 8                               | 0.0                   | 0.097               | 24.5                  | LOS C               | 0.1                         | 0.8                            | 0.51         | 0.63                               | 0.51               | 38.4                   |
| All Ve    | hicles  | 3050                             | 2.6                   | 3050                            | 2.6                   | 0.379               | 0.6                   | NA                  | 10.4                        | 74.6                           | 0.05         | 0.01                               | 0.06               | 58.6                   |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Network Data dialog (Network tab).

Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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### Site: 101 [AM 2025 Post Development (Site Folder: General)]

### Abbotsford Road / Gebbie Street

Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time)

| Vehio     | cle Mo  | vement                  | Perfo            | rmanc                  | e                |              |                |                     |                       |                           |              |                                    |                    |                |
|-----------|---------|-------------------------|------------------|------------------------|------------------|--------------|----------------|---------------------|-----------------------|---------------------------|--------------|------------------------------------|--------------------|----------------|
| Mov<br>ID | Turn    | DEMA<br>FLOV<br>[ Total | ND<br>NS<br>HV ] | ARRI<br>FLO<br>[ Total | VAL<br>WS<br>HV] | Deg.<br>Satn | Aver.<br>Delay | Level of<br>Service | 95% I<br>Ql<br>[ Veh. | BACK OF<br>UEUE<br>Dist ] | Prop.<br>Que | Effective <i>A</i><br>Stop<br>Rate | ver. No.<br>Cycles | Aver.<br>Speed |
| 0 11      |         | ven/n                   | %                | veh/h                  | %                | V/C          | sec            | _                   | ven                   | m                         | _            | _                                  | _                  | Km/h           |
| South     | : Abboi | tsford Roa              | ad               |                        |                  |              |                |                     |                       |                           |              |                                    |                    |                |
| 2         | T1      | 992                     | 2.9              | 992                    | 2.9              | 0.313        | 1.9            | LOS A               | 5.9                   | 42.2                      | 0.22         | 0.20                               | 0.22               | 56.5           |
| 3         | R2      | 20                      | 0.0              | 20                     | 0.0              | *0.221       | 68.4           | LOS E               | 1.2                   | 8.3                       | 0.99         | 0.70                               | 0.99               | 26.9           |
| Appro     | ach     | 1012                    | 2.8              | 1012                   | 2.8              | 0.313        | 3.2            | LOS A               | 5.9                   | 42.2                      | 0.23         | 0.21                               | 0.23               | 54.2           |
| East:     | Gebbie  | e Street                |                  |                        |                  |              |                |                     |                       |                           |              |                                    |                    |                |
| 4         | L2      | 10                      | 0.0              | 10                     | 0.0              | 0.064        | 57.2           | LOS E               | 0.7                   | 5.0                       | 0.93         | 0.68                               | 0.93               | 29.0           |
| 6         | R2      | 2                       | 50.0             | 2                      | 50.0             | *0.064       | 57.6           | LOS E               | 0.7                   | 5.0                       | 0.93         | 0.68                               | 0.93               | 19.7           |
| Appro     | ach     | 13                      | 8.3              | 13                     | 8.3              | 0.064        | 57.2           | LOS E               | 0.7                   | 5.0                       | 0.93         | 0.68                               | 0.93               | 27.8           |
| North     | : Abbot | sford Roa               | ad               |                        |                  |              |                |                     |                       |                           |              |                                    |                    |                |
| 7         | L2      | 8                       | 0.0              | 8                      | 0.0              | 0.474        | 8.8            | LOS A               | 4.6                   | 32.6                      | 0.42         | 0.38                               | 0.42               | 42.8           |
| 8         | T1      | 2007                    | 2.4              | 2007                   | 2.4              | *0.474       | 6.1            | LOS A               | 4.6                   | 32.6                      | 0.42         | 0.38                               | 0.42               | 50.4           |
| Appro     | bach    | 2016                    | 2.4              | 2016                   | 2.4              | 0.474        | 6.1            | LOS A               | 4.6                   | 32.6                      | 0.42         | 0.38                               | 0.42               | 50.3           |
| All Ve    | hicles  | 3040                    | 2.6              | 3040                   | 2.6              | 0.474        | 5.4            | LOS A               | 5.9                   | 42.2                      | 0.36         | 0.33                               | 0.36               | 51.2           |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

\* Critical Movement (Signal Timing)

| Pedestrian Mov    | vement | Perform | nance    |              |              |         |              |        |        |       |
|-------------------|--------|---------|----------|--------------|--------------|---------|--------------|--------|--------|-------|
| Mov               | Dem.   | Aver.   | Level of | AVERAGE      | BACK OF      | Prop. E | Effective    | Travel | Travel | Aver. |
| ID Crossing       | Flow   | Delay   | Service  | QUE<br>[ Ped | UE<br>Dist ] | Que     | Stop<br>Rate | Time   | Dist.  | Speed |
|                   | ped/h  | sec     |          | ped          | m            |         |              | sec    | m      | m/sec |
| South: Abbotsford | d Road |         |          |              |              |         |              |        |        |       |
| P1 Full           | 11     | 54.2    | LOS E    | 0.0          | 0.0          | 0.95    | 0.95         | 223.5  | 220.1  | 0.98  |
| East: Gebbie Stre | et     |         |          |              |              |         |              |        |        |       |
| P2 Full           | 11     | 54.2    | LOS E    | 0.0          | 0.0          | 0.95    | 0.95         | 216.3  | 210.8  | 0.97  |
| All Pedestrians   | 21     | 54.2    | LOS E    | 0.0          | 0.0          | 0.95    | 0.95         | 219.9  | 215.5  | 0.98  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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V Site: 102 [AM 2025 Post Development (Site Folder: General)]

Abbotsford Road / Taylor Street Site Category: (None) Give-Way (Two-Way)

| Vehio     | cle Mo  | vement                          | Perfo                 | rmanc                           | e                     |                     |                       |                     |                              |                               |              |                                    |                    |                        |
|-----------|---------|---------------------------------|-----------------------|---------------------------------|-----------------------|---------------------|-----------------------|---------------------|------------------------------|-------------------------------|--------------|------------------------------------|--------------------|------------------------|
| Mov<br>ID | Turn    | DEM/<br>FLO<br>[ Total<br>veh/h | AND<br>WS<br>HV]<br>% | ARRI<br>FLO<br>[ Total<br>veh/h | VAL<br>WS<br>HV]<br>% | Deg.<br>Satn<br>v/c | Aver.<br>Delay<br>sec | Level of<br>Service | 95%  <br>Q <br>[ Veh.<br>veh | BACK OF<br>UEUE<br>Dist]<br>m | Prop.<br>Que | Effective <i>A</i><br>Stop<br>Rate | ver. No.<br>Cycles | Aver.<br>Speed<br>km/h |
| South     | : Abbo  | tsford Ro                       | ad                    |                                 |                       |                     |                       |                     |                              |                               |              |                                    |                    |                        |
| 1         | L2      | 36                              | 9.1                   | 36                              | 9.1                   | 0.258               | 2.7                   | LOS A               | 0.0                          | 0.0                           | 0.00         | 0.04                               | 0.00               | 55.8                   |
| 2         | T1      | 957                             | 2.9                   | 957                             | 2.9                   | 0.258               | 0.0                   | LOS A               | 0.0                          | 0.0                           | 0.00         | 0.02                               | 0.00               | 59.7                   |
| Appro     | bach    | 993                             | 3.1                   | 993                             | 3.1                   | 0.258               | 0.1                   | NA                  | 0.0                          | 0.0                           | 0.00         | 0.02                               | 0.00               | 59.5                   |
| North     | : Abbot | sford Ro                        | ad                    |                                 |                       |                     |                       |                     |                              |                               |              |                                    |                    |                        |
| 8         | T1      | 2016                            | 2.4                   | 2016                            | 2.4                   | 0.391               | 0.8                   | LOS A               | 10.4                         | 74.0                          | 0.08         | 0.02                               | 0.11               | 58.0                   |
| 9         | R2      | 64                              | 5.3                   | 64                              | 5.3                   | 0.391               | 14.5                  | LOS B               | 10.3                         | 74.0                          | 0.33         | 0.08                               | 0.43               | 51.4                   |
| Appro     | bach    | 2079                            | 2.5                   | 2079                            | 2.5                   | 0.391               | 1.2                   | NA                  | 10.4                         | 74.0                          | 0.09         | 0.02                               | 0.12               | 57.5                   |
| West:     | Taylor  | Street                          |                       |                                 |                       |                     |                       |                     |                              |                               |              |                                    |                    |                        |
| 10        | L2      | 24                              | 0.0                   | 24                              | 0.0                   | 0.027               | 6.5                   | LOS A               | 0.1                          | 0.7                           | 0.44         | 0.61                               | 0.44               | 48.5                   |
| 12        | R2      | 1                               | 0.0                   | 1                               | 0.0                   | 0.105               | 161.4                 | LOS F               | 0.1                          | 0.9                           | 0.99         | 0.99                               | 0.99               | 9.3                    |
| Appro     | bach    | 25                              | 0.0                   | 25                              | 0.0                   | 0.105               | 13.0                  | LOS B               | 0.1                          | 0.9                           | 0.47         | 0.63                               | 0.47               | 44.5                   |
| All Ve    | hicles  | 3097                            | 2.7                   | 3097                            | 2.7                   | 0.391               | 0.9                   | NA                  | 10.4                         | 74.0                          | 0.07         | 0.03                               | 0.08               | 57.9                   |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Network Data dialog (Network tab).

Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Site: 101 [PM 2025 Pre Development (Site Folder: General)]

#### ■ Network: N101 [PM2025 Pre Development (Network Folder: General)]

#### Abbotsford Road / Gebbie Street

Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time)

| Vehic     | cle Mo  | vement                           | Perfo                | rmanc                           | e:                    |                     |                       |                     |                              |                               |              |                                    |                    |                        |
|-----------|---------|----------------------------------|----------------------|---------------------------------|-----------------------|---------------------|-----------------------|---------------------|------------------------------|-------------------------------|--------------|------------------------------------|--------------------|------------------------|
| Mov<br>ID | Turn    | DEMA<br>FLO\<br>[ Total<br>veh/h | ND<br>NS<br>HV]<br>% | ARRI<br>FLO<br>[ Total<br>veh/h | VAL<br>WS<br>HV]<br>% | Deg.<br>Satn<br>v/c | Aver.<br>Delay<br>sec | Level of<br>Service | 95% E<br>Ql<br>[ Veh.<br>veh | BACK OF<br>JEUE<br>Dist]<br>m | Prop.<br>Que | Effective <i>A</i><br>Stop<br>Rate | ver. No.<br>Cycles | Aver.<br>Speed<br>km/h |
| South     | : Abboi | tsford Ro                        | ad                   |                                 |                       |                     |                       |                     |                              |                               |              |                                    |                    |                        |
| 2         | T1      | 1602                             | 0.9                  | 1602                            | 0.9                   | <b>*</b> 0.493      | 2.4                   | LOS A               | 11.9                         | 83.9                          | 0.28         | 0.26                               | 0.28               | 55.6                   |
| 3         | R2      | 11                               | 18.2                 | 11                              | 18.2                  | 0.141               | 68.4                  | LOS E               | 0.7                          | 5.4                           | 0.98         | 0.68                               | 0.98               | 26.9                   |
| Appro     | ach     | 1613                             | 1.0                  | 1613                            | 1.0                   | 0.493               | 2.9                   | LOS A               | 11.9                         | 83.9                          | 0.28         | 0.26                               | 0.28               | 54.8                   |
| East:     | Gebbie  | e Street                         |                      |                                 |                       |                     |                       |                     |                              |                               |              |                                    |                    |                        |
| 4         | L2      | 31                               | 0.0                  | 31                              | 0.0                   | 0.221               | 59.8                  | LOS E               | 2.2                          | 15.5                          | 0.96         | 0.73                               | 0.96               | 28.4                   |
| 6         | R2      | 9                                | 0.0                  | 9                               | 0.0                   | *0.221              | 59.8                  | LOS E               | 2.2                          | 15.5                          | 0.96         | 0.73                               | 0.96               | 19.2                   |
| Appro     | ach     | 40                               | 0.0                  | 40                              | 0.0                   | 0.221               | 59.8                  | LOS E               | 2.2                          | 15.5                          | 0.96         | 0.73                               | 0.96               | 26.7                   |
| North     | : Abbot | sford Roa                        | ad                   |                                 |                       |                     |                       |                     |                              |                               |              |                                    |                    |                        |
| 7         | L2      | 7                                | 0.0                  | 7                               | 0.0                   | 0.311               | 7.8                   | LOS A               | 4.6                          | 32.6                          | 0.35         | 0.32                               | 0.35               | 43.7                   |
| 8         | T1      | 1327                             | 1.0                  | 1327                            | 1.0                   | 0.311               | 5.1                   | LOS A               | 4.6                          | 32.6                          | 0.35         | 0.31                               | 0.35               | 51.7                   |
| Appro     | ach     | 1334                             | 1.0                  | 1334                            | 1.0                   | 0.311               | 5.1                   | LOS A               | 4.6                          | 32.6                          | 0.35         | 0.31                               | 0.35               | 51.6                   |
| All Ve    | hicles  | 2987                             | 1.0                  | 2987                            | 1.0                   | 0.493               | 4.6                   | LOS A               | 11.9                         | 83.9                          | 0.32         | 0.29                               | 0.32               | 52.1                   |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

\* Critical Movement (Signal Timing)

| Pedestrian Mov    | vement | Perform | nance    |              |              |         |              |        |        |       |
|-------------------|--------|---------|----------|--------------|--------------|---------|--------------|--------|--------|-------|
| Mov               | Dem.   | Aver.   | Level of | AVERAGE      | BACK OF      | Prop. E | Effective    | Travel | Travel | Aver. |
| ID Crossing       | Flow   | Delay   | Service  | QUE<br>[ Ped | UE<br>Dist ] | Que     | Stop<br>Rate | Time   | Dist.  | Speed |
|                   | ped/h  | sec     |          | ped          | m            |         |              | sec    | m      | m/sec |
| South: Abbotsford | d Road |         |          |              |              |         |              |        |        |       |
| P1 Full           | 11     | 54.2    | LOS E    | 0.0          | 0.0          | 0.95    | 0.95         | 223.5  | 220.1  | 0.98  |
| East: Gebbie Stre | et     |         |          |              |              |         |              |        |        |       |
| P2 Full           | 11     | 54.2    | LOS E    | 0.0          | 0.0          | 0.95    | 0.95         | 216.3  | 210.8  | 0.97  |
| All Pedestrians   | 21     | 54.2    | LOS E    | 0.0          | 0.0          | 0.95    | 0.95         | 219.9  | 215.5  | 0.98  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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V Site: 102 [PM 2025 Pre Development (Site Folder: General)]

### ■ Network: N101 [PM2025 Pre Development (Network Folder: General)]

Abbotsford Road / Taylor Street Site Category: (None) Give-Way (Two-Way)

| Vehi      | cle Mo   | vement                           | Perfo                 | rmanc                           | e                     |                     |                       |                     |                           |                                |              |                                    |                    |                        |
|-----------|----------|----------------------------------|-----------------------|---------------------------------|-----------------------|---------------------|-----------------------|---------------------|---------------------------|--------------------------------|--------------|------------------------------------|--------------------|------------------------|
| Mov<br>ID | Turn     | DEMA<br>FLOV<br>[ Total<br>veh/h | AND<br>WS<br>HV]<br>% | ARRI<br>FLO<br>[ Total<br>veh/h | VAL<br>WS<br>HV]<br>% | Deg.<br>Satn<br>v/c | Aver.<br>Delay<br>sec | Level of<br>Service | 95%<br>Q<br>[ Veh.<br>veh | BACK OF<br>UEUE<br>Dist ]<br>m | Prop.<br>Que | Effective <i>F</i><br>Stop<br>Rate | ver. No.<br>Cycles | Aver.<br>Speed<br>km/h |
| South     | n: Abbot | tsford Ro                        | ad                    |                                 |                       |                     |                       |                     |                           |                                |              |                                    |                    |                        |
| 1         | L2       | 9                                | 0.0                   | 9                               | 0.0                   | 0.411               | 2.7                   | LOS A               | 0.0                       | 0.0                            | 0.00         | 0.01                               | 0.00               | 56.7                   |
| 2         | T1       | 1602                             | 0.9                   | 1602                            | 0.9                   | 0.411               | 0.0                   | LOS A               | 0.0                       | 0.0                            | 0.00         | 0.00                               | 0.00               | 59.7                   |
| Appro     | bach     | 1611                             | 0.9                   | 1611                            | 0.9                   | 0.411               | 0.0                   | NA                  | 0.0                       | 0.0                            | 0.00         | 0.00                               | 0.00               | 59.7                   |
| North     | : Abbot  | sford Roa                        | ad                    |                                 |                       |                     |                       |                     |                           |                                |              |                                    |                    |                        |
| 8         | T1       | 1326                             | 1.0                   | 1326                            | 1.0                   | 0.248               | 0.8                   | LOS A               | 3.7                       | 25.8                           | 0.06         | 0.01                               | 0.07               | 58.0                   |
| 9         | R2       | 16                               | 0.0                   | 16                              | 0.0                   | 0.248               | 22.1                  | LOS C               | 3.6                       | 25.3                           | 0.21         | 0.03                               | 0.24               | 51.6                   |
| Appro     | bach     | 1342                             | 1.0                   | 1342                            | 1.0                   | 0.248               | 1.1                   | NA                  | 3.7                       | 25.8                           | 0.06         | 0.01                               | 0.07               | 57.9                   |
| West      | : Taylor | Street                           |                       |                                 |                       |                     |                       |                     |                           |                                |              |                                    |                    |                        |
| 10        | L2       | 17                               | 0.0                   | 17                              | 0.0                   | 0.029               | 8.9                   | LOS A               | 0.1                       | 0.7                            | 0.59         | 0.74                               | 0.59               | 47.0                   |
| 12        | R2       | 8                                | 0.0                   | 8                               | 0.0                   | 0.861               | 430.9                 | LOS F               | 1.2                       | 8.6                            | 0.99         | 1.07                               | 1.31               | 4.0                    |
| Appro     | bach     | 25                               | 0.0                   | 25                              | 0.0                   | 0.861               | 143.9                 | LOS F               | 1.2                       | 8.6                            | 0.72         | 0.84                               | 0.82               | 15.2                   |
| All Ve    | hicles   | 2979                             | 0.9                   | 2979                            | 0.9                   | 0.861               | 1.7                   | NA                  | 3.7                       | 25.8                           | 0.03         | 0.01                               | 0.04               | 56.6                   |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Network Data dialog (Network tab).

Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Site: 101 [PM 2025 Post Development (Site Folder: General)]

### Abbotsford Road / Gebbie Street

Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time)

| Vehio     | cle Mo  | vement                           | Perfo                 | rmanc                           | e                |                     |                       |                     |                              |                               |              |                                    |                    |                        |
|-----------|---------|----------------------------------|-----------------------|---------------------------------|------------------|---------------------|-----------------------|---------------------|------------------------------|-------------------------------|--------------|------------------------------------|--------------------|------------------------|
| Mov<br>ID | Turn    | DEMA<br>FLO\<br>[ Total<br>veh/h | AND<br>NS<br>HV]<br>% | ARRI<br>FLO<br>[ Total<br>veh/h | VAL<br>WS<br>HV] | Deg.<br>Satn<br>v/c | Aver.<br>Delay<br>sec | Level of<br>Service | 95% E<br>Ql<br>[ Veh.<br>veh | BACK OF<br>JEUE<br>Dist]<br>m | Prop.<br>Que | Effective <i>A</i><br>Stop<br>Rate | ver. No.<br>Cycles | Aver.<br>Speed<br>km/h |
| South     | : Abbo  | tsford Ro                        | ad                    |                                 |                  |                     |                       |                     |                              |                               |              |                                    |                    |                        |
| 2         | T1      | 1620                             | 0.9                   | 1620                            | 0.9              | *0.498              | 2.4                   | LOS A               | 12.1                         | 85.5                          | 0.28         | 0.26                               | 0.28               | 55.6                   |
| 3         | R2      | 11                               | 18.2                  | 11                              | 18.2             | 0.141               | 68.4                  | LOS E               | 0.7                          | 5.4                           | 0.98         | 0.68                               | 0.98               | 26.9                   |
| Appro     | ach     | 1631                             | 1.0                   | 1631                            | 1.0              | 0.498               | 2.9                   | LOS A               | 12.1                         | 85.5                          | 0.29         | 0.26                               | 0.29               | 54.8                   |
| East:     | Gebbie  | e Street                         |                       |                                 |                  |                     |                       |                     |                              |                               |              |                                    |                    |                        |
| 4         | L2      | 31                               | 0.0                   | 31                              | 0.0              | 0.221               | 59.8                  | LOS E               | 2.2                          | 15.5                          | 0.96         | 0.73                               | 0.96               | 28.4                   |
| 6         | R2      | 9                                | 0.0                   | 9                               | 0.0              | *0.221              | 59.8                  | LOS E               | 2.2                          | 15.5                          | 0.96         | 0.73                               | 0.96               | 19.2                   |
| Appro     | ach     | 40                               | 0.0                   | 40                              | 0.0              | 0.221               | 59.8                  | LOS E               | 2.2                          | 15.5                          | 0.96         | 0.73                               | 0.96               | 26.7                   |
| North     | : Abbot | sford Roa                        | ad                    |                                 |                  |                     |                       |                     |                              |                               |              |                                    |                    |                        |
| 7         | L2      | 7                                | 0.0                   | 7                               | 0.0              | 0.311               | 7.8                   | LOS A               | 4.6                          | 32.6                          | 0.35         | 0.32                               | 0.35               | 43.7                   |
| 8         | T1      | 1327                             | 1.0                   | 1327                            | 1.0              | 0.311               | 5.1                   | LOS A               | 4.6                          | 32.6                          | 0.35         | 0.31                               | 0.35               | 51.7                   |
| Appro     | ach     | 1334                             | 1.0                   | 1334                            | 1.0              | 0.311               | 5.1                   | LOS A               | 4.6                          | 32.6                          | 0.35         | 0.31                               | 0.35               | 51.6                   |
| All Ve    | hicles  | 3004                             | 1.0                   | 3004                            | 1.0              | 0.498               | 4.6                   | LOS A               | 12.1                         | 85.5                          | 0.32         | 0.29                               | 0.32               | 52.1                   |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

\* Critical Movement (Signal Timing)

| Pedestrian Mov    | vement | Perform | nance    |              |              |         |              |        |        |       |
|-------------------|--------|---------|----------|--------------|--------------|---------|--------------|--------|--------|-------|
| Mov               | Dem.   | Aver.   | Level of | AVERAGE      | BACK OF      | Prop. E | Effective    | Travel | Travel | Aver. |
| ID Crossing       | Flow   | Delay   | Service  | QUE<br>[ Ped | UE<br>Dist ] | Que     | Stop<br>Rate | Time   | Dist.  | Speed |
|                   | ped/h  | sec     |          | ped          | m            |         |              | sec    | m      | m/sec |
| South: Abbotsford | d Road |         |          |              |              |         |              |        |        |       |
| P1 Full           | 11     | 54.2    | LOS E    | 0.0          | 0.0          | 0.95    | 0.95         | 223.5  | 220.1  | 0.98  |
| East: Gebbie Stre | et     |         |          |              |              |         |              |        |        |       |
| P2 Full           | 11     | 54.2    | LOS E    | 0.0          | 0.0          | 0.95    | 0.95         | 216.3  | 210.8  | 0.97  |
| All Pedestrians   | 21     | 54.2    | LOS E    | 0.0          | 0.0          | 0.95    | 0.95         | 219.9  | 215.5  | 0.98  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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V Site: 102 [PM 2025 Post Development (Site Folder: General)]

Abbotsford Road / Taylor Street Site Category: (None) Give-Way (Two-Way)

| Vehio     | cle Mo  | vement                           | Perfo                 | rmanc                           | e                     |                     |                       |                     |                             |                                |              |                                    |                    |                        |
|-----------|---------|----------------------------------|-----------------------|---------------------------------|-----------------------|---------------------|-----------------------|---------------------|-----------------------------|--------------------------------|--------------|------------------------------------|--------------------|------------------------|
| Mov<br>ID | Turn    | DEMA<br>FLO\<br>[ Total<br>veh/h | AND<br>WS<br>HV]<br>% | ARRI<br>FLO<br>[ Total<br>veh/h | VAL<br>WS<br>HV]<br>% | Deg.<br>Satn<br>v/c | Aver.<br>Delay<br>sec | Level of<br>Service | 95%  <br>Q<br>[ Veh.<br>veh | BACK OF<br>UEUE<br>Dist ]<br>m | Prop.<br>Que | Effective <i>A</i><br>Stop<br>Rate | ver. No.<br>Cycles | Aver.<br>Speed<br>km/h |
| South     | : Abbot | tsford Ro                        | ad                    |                                 |                       |                     |                       |                     |                             |                                |              |                                    |                    |                        |
| 1         | L2      | 26                               | 0.0                   | 26                              | 0.0                   | 0.416               | 2.7                   | LOS A               | 0.0                         | 0.0                            | 0.00         | 0.02                               | 0.00               | 56.6                   |
| 2         | T1      | 1602                             | 0.9                   | 1602                            | 0.9                   | 0.416               | 0.0                   | LOS A               | 0.0                         | 0.0                            | 0.00         | 0.01                               | 0.00               | 59.6                   |
| Appro     | bach    | 1629                             | 0.9                   | 1629                            | 0.9                   | 0.416               | 0.1                   | NA                  | 0.0                         | 0.0                            | 0.00         | 0.01                               | 0.00               | 59.6                   |
| North     | : Abbot | sford Roa                        | ad                    |                                 |                       |                     |                       |                     |                             |                                |              |                                    |                    |                        |
| 8         | T1      | 1326                             | 1.0                   | 1326                            | 1.0                   | 0.262               | 1.3                   | LOS A               | 3.7                         | 25.8                           | 0.09         | 0.01                               | 0.10               | 57.0                   |
| 9         | R2      | 28                               | 0.0                   | 28                              | 0.0                   | 0.262               | 22.1                  | LOS C               | 3.6                         | 25.1                           | 0.37         | 0.06                               | 0.44               | 49.5                   |
| Appro     | bach    | 1354                             | 1.0                   | 1354                            | 1.0                   | 0.262               | 1.7                   | NA                  | 3.7                         | 25.8                           | 0.09         | 0.02                               | 0.11               | 56.7                   |
| West:     | Taylor  | Street                           |                       |                                 |                       |                     |                       |                     |                             |                                |              |                                    |                    |                        |
| 10        | L2      | 30                               | 0.0                   | 30                              | 0.0                   | 0.048               | 8.9                   | LOS A               | 0.2                         | 1.2                            | 0.59         | 0.76                               | 0.59               | 47.0                   |
| 12        | R2      | 8                                | 0.0                   | 8                               | 0.0                   | 0.872               | 440.7                 | LOS F               | 1.3                         | 8.8                            | 0.99         | 1.08                               | 1.32               | 3.9                    |
| Appro     | bach    | 38                               | 0.0                   | 38                              | 0.0                   | 0.872               | 102.3                 | LOS F               | 1.3                         | 8.8                            | 0.67         | 0.83                               | 0.74               | 19.9                   |
| All Ve    | hicles  | 3020                             | 0.9                   | 3020                            | 0.9                   | 0.872               | 2.1                   | NA                  | 3.7                         | 25.8                           | 0.05         | 0.02                               | 0.06               | 56.0                   |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Network Data dialog (Network tab).

Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Site: 101 [AM 2035 Pre Development (Site Folder: General)]

#### ■ Network: N101 [AM2035 Pre Development (Network Folder: General)]

#### Abbotsford Road / Gebbie Street

Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time)

| Vehi      | cle Mo  | vement                           | Perfo                 | rmanc                           | e:                    |                     |                       |                     |                              |                                |              |                                    |                    |                        |
|-----------|---------|----------------------------------|-----------------------|---------------------------------|-----------------------|---------------------|-----------------------|---------------------|------------------------------|--------------------------------|--------------|------------------------------------|--------------------|------------------------|
| Mov<br>ID | Turn    | DEMA<br>FLO\<br>[ Total<br>veh/h | AND<br>NS<br>HV]<br>% | ARRI<br>FLO<br>[ Total<br>veh/h | VAL<br>WS<br>HV]<br>% | Deg.<br>Satn<br>v/c | Aver.<br>Delay<br>sec | Level of<br>Service | 95% E<br>Ql<br>[ Veh.<br>veh | BACK OF<br>JEUE<br>Dist ]<br>m | Prop.<br>Que | Effective <i>A</i><br>Stop<br>Rate | ver. No.<br>Cycles | Aver.<br>Speed<br>km/h |
| South     | n: Abbo | tsford Ro                        | ad                    |                                 |                       |                     |                       |                     |                              |                                |              |                                    |                    |                        |
| 2         | T1      | 1087                             | 2.9                   | 1087                            | 2.9                   | 0.343               | 2.0                   | LOS A               | 6.7                          | 48.0                           | 0.23         | 0.21                               | 0.23               | 56.4                   |
| 3         | R2      | 22                               | 0.0                   | 22                              | 0.0                   | *0.244              | 68.5                  | LOS E               | 1.3                          | 9.2                            | 0.99         | 0.71                               | 0.99               | 26.9                   |
| Appro     | bach    | 1109                             | 2.8                   | 1109                            | 2.8                   | 0.343               | 3.3                   | LOS A               | 6.7                          | 48.0                           | 0.24         | 0.22                               | 0.24               | 54.1                   |
| East:     | Gebbie  | e Street                         |                       |                                 |                       |                     |                       |                     |                              |                                |              |                                    |                    |                        |
| 4         | L2      | 13                               | 0.0                   | 13                              | 0.0                   | 0.071               | 56.2                  | LOS E               | 0.8                          | 5.8                            | 0.92         | 0.69                               | 0.92               | 29.2                   |
| 6         | R2      | 2                                | 50.0                  | 2                               | 50.0                  | *0.071              | 56.6                  | LOS E               | 0.8                          | 5.8                            | 0.92         | 0.69                               | 0.92               | 19.9                   |
| Appro     | bach    | 15                               | 7.1                   | 15                              | 7.1                   | 0.071               | 56.3                  | LOS E               | 0.8                          | 5.8                            | 0.92         | 0.69                               | 0.92               | 28.2                   |
| North     | : Abbot | sford Roa                        | ad                    |                                 |                       |                     |                       |                     |                              |                                |              |                                    |                    |                        |
| 7         | L2      | 9                                | 0.0                   | 9                               | 0.0                   | 0.531               | 9.2                   | LOS A               | 4.6                          | 32.6                           | 0.45         | 0.41                               | 0.45               | 42.4                   |
| 8         | T1      | 2248                             | 2.4                   | 2248                            | 2.4                   | *0.531              | 6.5                   | LOS A               | 4.6                          | 32.6                           | 0.45         | 0.41                               | 0.45               | 49.8                   |
| Appro     | bach    | 2257                             | 2.4                   | 2257                            | 2.4                   | 0.531               | 6.5                   | LOS A               | 4.6                          | 32.6                           | 0.45         | 0.41                               | 0.45               | 49.8                   |
| All Ve    | hicles  | 3381                             | 2.6                   | 3381                            | 2.6                   | 0.531               | 5.7                   | LOS A               | 6.7                          | 48.0                           | 0.38         | 0.35                               | 0.38               | 50.8                   |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

\* Critical Movement (Signal Timing)

| Pedestrian Mov    | vement | Perform | nance    |              |              |         |              |        |        |       |
|-------------------|--------|---------|----------|--------------|--------------|---------|--------------|--------|--------|-------|
| Mov               | Dem.   | Aver.   | Level of | AVERAGE      | BACK OF      | Prop. E | Effective    | Travel | Travel | Aver. |
| ID Crossing       | Flow   | Delay   | Service  | QUE<br>[ Ped | UE<br>Dist ] | Que     | Stop<br>Rate | Time   | Dist.  | Speed |
|                   | ped/h  | sec     |          | ped          | m            |         |              | sec    | m      | m/sec |
| South: Abbotsford | d Road |         |          |              |              |         |              |        |        |       |
| P1 Full           | 11     | 54.2    | LOS E    | 0.0          | 0.0          | 0.95    | 0.95         | 223.5  | 220.1  | 0.98  |
| East: Gebbie Stre | et     |         |          |              |              |         |              |        |        |       |
| P2 Full           | 11     | 54.2    | LOS E    | 0.0          | 0.0          | 0.95    | 0.95         | 216.3  | 210.8  | 0.97  |
| All Pedestrians   | 21     | 54.2    | LOS E    | 0.0          | 0.0          | 0.95    | 0.95         | 219.9  | 215.5  | 0.98  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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V Site: 102 [AM 2035 Pre Development (Site Folder: General)]

Abbotsford Road / Taylor Street Site Category: (None) Give-Way (Two-Way)

| Vehi      | cle Mo  | vement                           | Perfo                 | rmanc                           | e                     |                     |                       |                     |                              |                                |              |                                    |                    |                        |
|-----------|---------|----------------------------------|-----------------------|---------------------------------|-----------------------|---------------------|-----------------------|---------------------|------------------------------|--------------------------------|--------------|------------------------------------|--------------------|------------------------|
| Mov<br>ID | Turn    | DEMA<br>FLO\<br>[ Total<br>veh/h | AND<br>NS<br>HV]<br>% | ARRI<br>FLO<br>[ Total<br>veh/h | VAL<br>WS<br>HV]<br>% | Deg.<br>Satn<br>v/c | Aver.<br>Delay<br>sec | Level of<br>Service | 95% I<br>QI<br>[ Veh.<br>veh | BACK OF<br>UEUE<br>Dist ]<br>m | Prop.<br>Que | Effective <i>A</i><br>Stop<br>Rate | ver. No.<br>Cycles | Aver.<br>Speed<br>km/h |
| South     | : Abbot | sford Ro                         | ad                    |                                 |                       |                     |                       |                     |                              |                                |              |                                    |                    |                        |
| 1         | L2      | 14                               | 9.1                   | 14                              | 9.1                   | 0.282               | 2.7                   | LOS A               | 0.0                          | 0.0                            | 0.00         | 0.01                               | 0.00               | 56.0                   |
| 2         | T1      | 1075                             | 2.9                   | 1075                            | 2.9                   | 0.282               | 0.0                   | LOS A               | 0.0                          | 0.0                            | 0.00         | 0.01                               | 0.00               | 59.8                   |
| Appro     | bach    | 1089                             | 3.0                   | 1089                            | 3.0                   | 0.282               | 0.0                   | NA                  | 0.0                          | 0.0                            | 0.00         | 0.01                               | 0.00               | 59.7                   |
| North     | : Abbot | sford Roa                        | ad                    |                                 |                       |                     |                       |                     |                              |                                |              |                                    |                    |                        |
| 8         | T1      | 2257                             | 2.4                   | 2257                            | 2.4                   | 0.427               | 0.7                   | LOS A               | 13.3                         | 95.3                           | 0.07         | 0.01                               | 0.10               | 58.1                   |
| 9         | R2      | 48                               | 5.3                   | 48                              | 5.3                   | 0.427               | 16.6                  | LOS C               | 13.3                         | 95.3                           | 0.27         | 0.05                               | 0.36               | 51.8                   |
| Appro     | bach    | 2305                             | 2.5                   | 2305                            | 2.5                   | 0.427               | 1.1                   | NA                  | 13.3                         | 95.3                           | 0.08         | 0.01                               | 0.10               | 57.8                   |
| West      | Taylor  | Street                           |                       |                                 |                       |                     |                       |                     |                              |                                |              |                                    |                    |                        |
| 10        | L2      | 8                                | 0.0                   | 8                               | 0.0                   | 0.010               | 6.9                   | LOS A               | 0.0                          | 0.2                            | 0.47         | 0.60                               | 0.47               | 48.3                   |
| 12        | R2      | 1                                | 0.0                   | 1                               | 0.0                   | 0.166               | 270.5                 | LOS F               | 0.2                          | 1.4                            | 0.99         | 1.00                               | 1.00               | 6.0                    |
| Appro     | bach    | 9                                | 0.0                   | 9                               | 0.0                   | 0.166               | 36.2                  | LOS E               | 0.2                          | 1.4                            | 0.53         | 0.65                               | 0.53               | 34.1                   |
| All Ve    | hicles  | 3404                             | 2.6                   | 3404                            | 2.6                   | 0.427               | 0.8                   | NA                  | 13.3                         | 95.3                           | 0.05         | 0.01                               | 0.07               | 58.2                   |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Network Data dialog (Network tab).

Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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### Site: 101 [AM 2035 Post Development (Site Folder: General)]

### Abbotsford Road / Gebbie Street

Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time)

| Vehio                  | Vehicle Movement Performance |                         |                  |                        |                  |              |                |                     |                       |                           |                |                            |                    |                |
|------------------------|------------------------------|-------------------------|------------------|------------------------|------------------|--------------|----------------|---------------------|-----------------------|---------------------------|----------------|----------------------------|--------------------|----------------|
| Mov<br>ID              | Turn                         | DEMA<br>FLOV<br>[ Total | AND<br>WS<br>HV] | ARRI<br>FLO<br>[ Total | VAL<br>WS<br>HV] | Deg.<br>Satn | Aver.<br>Delay | Level of<br>Service | 95% E<br>Ql<br>[ Veh. | BACK OF<br>JEUE<br>Dist ] | Prop.<br>Que   | EffectiveA<br>Stop<br>Rate | ver. No.<br>Cycles | Aver.<br>Speed |
| South: Abbotsford Road |                              |                         |                  |                        |                  |              |                |                     |                       |                           | <u>KIII/II</u> |                            |                    |                |
| 2                      | T1                           | 1104                    | 2.9              | 1104                   | 2.9              | 0.348        | 2.0            | LOS A               | 6.8                   | 49.0                      | 0.23           | 0.21                       | 0.23               | 56.3           |
| 3                      | R2                           | 22                      | 0.0              | 22                     | 0.0              | *0.244       | 68.5           | LOS E               | 1.3                   | 9.2                       | 0.99           | 0.71                       | 0.99               | 26.9           |
| Appro                  | ach                          | 1126                    | 2.8              | 1126                   | 2.8              | 0.348        | 3.3            | LOS A               | 6.8                   | 49.0                      | 0.24           | 0.22                       | 0.24               | 54.1           |
| East: Gebbie Street    |                              |                         |                  |                        |                  |              |                |                     |                       |                           |                |                            |                    |                |
| 4                      | L2                           | 13                      | 0.0              | 13                     | 0.0              | 0.071        | 56.2           | LOS E               | 0.8                   | 5.8                       | 0.92           | 0.69                       | 0.92               | 29.2           |
| 6                      | R2                           | 2                       | 50.0             | 2                      | 50.0             | *0.071       | 56.6           | LOS E               | 0.8                   | 5.8                       | 0.92           | 0.69                       | 0.92               | 19.9           |
| Appro                  | ach                          | 15                      | 7.1              | 15                     | 7.1              | 0.071        | 56.3           | LOS E               | 0.8                   | 5.8                       | 0.92           | 0.69                       | 0.92               | 28.2           |
| North                  | Abbot                        | sford Roa               | ad               |                        |                  |              |                |                     |                       |                           |                |                            |                    |                |
| 7                      | L2                           | 9                       | 0.0              | 9                      | 0.0              | 0.529        | 9.2            | LOS A               | 4.6                   | 32.6                      | 0.45           | 0.41                       | 0.45               | 42.4           |
| 8                      | T1                           | 2241                    | 2.4              | 2241                   | 2.4              | *0.529       | 6.5            | LOS A               | 4.6                   | 32.6                      | 0.45           | 0.41                       | 0.45               | 49.8           |
| Appro                  | ach                          | 2250                    | 2.4              | 2250                   | 2.4              | 0.529        | 6.5            | LOS A               | 4.6                   | 32.6                      | 0.45           | 0.41                       | 0.45               | 49.8           |
| All Ve                 | hicles                       | 3390                    | 2.6              | 3390                   | 2.6              | 0.529        | 5.7            | LOS A               | 6.8                   | 49.0                      | 0.38           | 0.35                       | 0.38               | 50.8           |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

\* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |        |       |          |                     |     |         |              |        |        |       |  |  |  |
|---------------------------------|--------|-------|----------|---------------------|-----|---------|--------------|--------|--------|-------|--|--|--|
| Mov                             | Dem.   | Aver. | Level of | AVERAGE BACK OF     |     | Prop. E | Effective    | Travel | Travel | Aver. |  |  |  |
| ID Crossing                     | Flow   | Delay | Service  | QUEUE<br>[Ped Dist] |     | Que     | Stop<br>Rate | Time   | Dist.  | Speed |  |  |  |
|                                 | ped/h  | sec   |          | ped                 | m   |         |              | sec    | m      | m/sec |  |  |  |
| South: Abbotsford               | d Road |       |          |                     |     |         |              |        |        |       |  |  |  |
| P1 Full                         | 11     | 54.2  | LOS E    | 0.0                 | 0.0 | 0.95    | 0.95         | 223.5  | 220.1  | 0.98  |  |  |  |
| East: Gebbie Stre               | et     |       |          |                     |     |         |              |        |        |       |  |  |  |
| P2 Full                         | 11     | 54.2  | LOS E    | 0.0                 | 0.0 | 0.95    | 0.95         | 216.3  | 210.8  | 0.97  |  |  |  |
| All Pedestrians                 | 21     | 54.2  | LOS E    | 0.0                 | 0.0 | 0.95    | 0.95         | 219.9  | 215.5  | 0.98  |  |  |  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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V Site: 102 [AM 2035 Post Development (Site Folder: General)]

Abbotsford Road / Taylor Street Site Category: (None) Give-Way (Two-Way)

| Vehio                  | Vehicle Movement Performance |                                 |                       |                                 |                       |                     |                       |                     |                           |                                |              |                                    |                     |                        |
|------------------------|------------------------------|---------------------------------|-----------------------|---------------------------------|-----------------------|---------------------|-----------------------|---------------------|---------------------------|--------------------------------|--------------|------------------------------------|---------------------|------------------------|
| Mov<br>ID              | Turn                         | DEM/<br>FLO<br>[ Total<br>veh/h | AND<br>WS<br>HV]<br>% | ARRI<br>FLO<br>[ Total<br>veh/h | VAL<br>WS<br>HV]<br>% | Deg.<br>Satn<br>v/c | Aver.<br>Delay<br>sec | Level of<br>Service | 95%<br>Q<br>[ Veh.<br>veh | BACK OF<br>UEUE<br>Dist ]<br>m | Prop.<br>Que | Effective <i>l</i><br>Stop<br>Rate | Aver. No.<br>Cycles | Aver.<br>Speed<br>km/h |
| South: Abbotsford Road |                              |                                 |                       |                                 |                       |                     |                       |                     |                           |                                |              |                                    |                     |                        |
| 1                      | L2                           | 38                              | 9.1                   | 38                              | 9.1                   | 0.287               | 2.7                   | LOS A               | 0.0                       | 0.0                            | 0.00         | 0.04                               | 0.00                | 55.8                   |
| 2                      | T1                           | 1069                            | 2.9                   | 1069                            | 2.9                   | 0.287               | 0.0                   | LOS A               | 0.0                       | 0.0                            | 0.00         | 0.02                               | 0.00                | 59.7                   |
| Appro                  | bach                         | 1107                            | 3.1                   | 1107                            | 3.1                   | 0.287               | 0.1                   | NA                  | 0.0                       | 0.0                            | 0.00         | 0.02                               | 0.00                | 59.5                   |
| North: Abbotsford Road |                              |                                 |                       |                                 |                       |                     |                       |                     |                           |                                |              |                                    |                     |                        |
| 8                      | T1                           | 2250                            | 2.4                   | 2250                            | 2.4                   | 0.441               | 1.0                   | LOS A               | 13.2                      | 94.6                           | 0.10         | 0.02                               | 0.13                | 57.5                   |
| 9                      | R2                           | 69                              | 5.3                   | 69                              | 5.3                   | 0.441               | 16.7                  | LOS C               | 13.2                      | 94.7                           | 0.39         | 0.09                               | 0.53                | 50.6                   |
| Appro                  | bach                         | 2319                            | 2.5                   | 2319                            | 2.5                   | 0.441               | 1.5                   | NA                  | 13.2                      | 94.7                           | 0.10         | 0.02                               | 0.14                | 57.1                   |
| West:                  | Taylor                       | Street                          |                       |                                 |                       |                     |                       |                     |                           |                                |              |                                    |                     |                        |
| 10                     | L2                           | 25                              | 0.0                   | 25                              | 0.0                   | 0.030               | 6.9                   | LOS A               | 0.1                       | 0.7                            | 0.47         | 0.64                               | 0.47                | 48.3                   |
| 12                     | R2                           | 1                               | 0.0                   | 1                               | 0.0                   | 0.184               | 309.3                 | LOS F               | 0.2                       | 1.5                            | 0.99         | 1.00                               | 1.00                | 5.4                    |
| Appro                  | bach                         | 26                              | 0.0                   | 26                              | 0.0                   | 0.184               | 19.0                  | LOS C               | 0.2                       | 1.5                            | 0.49         | 0.65                               | 0.49                | 41.4                   |
| All Ve                 | hicles                       | 3452                            | 2.7                   | 3452                            | 2.7                   | 0.441               | 1.2                   | NA                  | 13.2                      | 94.7                           | 0.07         | 0.03                               | 0.10                | 57.5                   |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Network Data dialog (Network tab).

Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Site: 101 [PM 2035 Pre Development (Site Folder: General)]

#### ■ Network: N101 [PM 2035 Pre Development (Network Folder: General)]

### Abbotsford Road / Gebbie Street

Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time)

| Vehio     | Vehicle Movement Performance |                                  |                       |                                 |                       |                     |                       |                     |                           |                                |              |                                    |                     |                        |
|-----------|------------------------------|----------------------------------|-----------------------|---------------------------------|-----------------------|---------------------|-----------------------|---------------------|---------------------------|--------------------------------|--------------|------------------------------------|---------------------|------------------------|
| Mov<br>ID | Turn                         | DEMA<br>FLOV<br>[ Total<br>veh/h | AND<br>WS<br>HV]<br>% | ARRI<br>FLO<br>[ Total<br>veh/h | VAL<br>WS<br>HV]<br>% | Deg.<br>Satn<br>v/c | Aver.<br>Delay<br>sec | Level of<br>Service | 95%<br>Q<br>[ Veh.<br>veh | BACK OF<br>UEUE<br>Dist ]<br>m | Prop.<br>Que | Effective <i>l</i><br>Stop<br>Rate | Aver. No.<br>Cycles | Aver.<br>Speed<br>km/h |
| South     | : Abbot                      | sford Ro                         | ad                    |                                 |                       |                     |                       |                     |                           |                                |              |                                    |                     |                        |
| 2         | T1                           | 1787                             | 0.9                   | 1787                            | 0.9                   | <b>*</b> 0.550      | 2.6                   | LOS A               | 14.5                      | 102.3                          | 0.30         | 0.28                               | 0.30                | 55.2                   |
| 3         | R2                           | 13                               | 18.2                  | 13                              | 18.2                  | 0.166               | 68.7                  | LOS E               | 0.8                       | 6.4                            | 0.99         | 0.69                               | 0.99                | 26.8                   |
| Appro     | bach                         | 1801                             | 1.0                   | 1801                            | 1.0                   | 0.550               | 3.1                   | LOS A               | 14.5                      | 102.3                          | 0.31         | 0.29                               | 0.31                | 54.4                   |
| East:     | Gebbie                       | Street                           |                       |                                 |                       |                     |                       |                     |                           |                                |              |                                    |                     |                        |
| 4         | L2                           | 34                               | 0.0                   | 34                              | 0.0                   | 0.244               | 60.9                  | LOS E               | 2.5                       | 17.2                           | 0.97         | 0.74                               | 0.97                | 28.2                   |
| 6         | R2                           | 10                               | 0.0                   | 10                              | 0.0                   | *0.244              | 60.9                  | LOS E               | 2.5                       | 17.2                           | 0.97         | 0.74                               | 0.97                | 19.0                   |
| Appro     | bach                         | 44                               | 0.0                   | 44                              | 0.0                   | 0.244               | 60.9                  | LOS E               | 2.5                       | 17.2                           | 0.97         | 0.74                               | 0.97                | 26.5                   |
| North     | : Abbot                      | sford Roa                        | ad                    |                                 |                       |                     |                       |                     |                           |                                |              |                                    |                     |                        |
| 7         | L2                           | 8                                | 0.0                   | 8                               | 0.0                   | 0.346               | 8.0                   | LOS A               | 4.6                       | 32.6                           | 0.36         | 0.33                               | 0.36                | 43.5                   |
| 8         | T1                           | 1480                             | 1.0                   | 1477                            | 1.0                   | 0.346               | 5.3                   | LOS A               | 4.6                       | 32.6                           | 0.36         | 0.33                               | 0.36                | 51.4                   |
| Appro     | bach                         | 1488                             | 1.0                   | 1486 <sup>N</sup><br>1          | 1.0                   | 0.346               | 5.3                   | LOS A               | 4.6                       | 32.6                           | 0.36         | 0.33                               | 0.36                | 51.4                   |
| All Ve    | hicles                       | 3333                             | 1.0                   | 3330 <sup>N</sup>               | 1.0                   | 0.550               | 4.9                   | LOS A               | 14.5                      | 102.3                          | 0.34         | 0.31                               | 0.34                | 51.8                   |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

\* Critical Movement (Signal Timing)

N1 Arrival Flow value is reduced due to capacity constraint at oversaturated upstream lanes.

| Pedestrian Movement Performance |       |       |          |                       |     |                 |              |        |        |       |  |  |  |
|---------------------------------|-------|-------|----------|-----------------------|-----|-----------------|--------------|--------|--------|-------|--|--|--|
| Mov                             | Dem.  | Aver. | Level of | AVERAGE BACK OF       |     | Prop. Effective |              | Travel | Travel | Aver. |  |  |  |
| ID Crossing                     | Flow  | Delay | Service  | QUEUE<br>[ Ped Dist ] |     | Que             | Stop<br>Rate | Time   | Dist.  | Speed |  |  |  |
|                                 | ped/h | sec   |          | ped                   | m   |                 |              | sec    | m      | m/sec |  |  |  |
| South: Abbotsford               | Road  |       |          |                       |     |                 |              |        |        |       |  |  |  |
| P1 Full                         | 11    | 54.2  | LOS E    | 0.0                   | 0.0 | 0.95            | 0.95         | 223.5  | 220.1  | 0.98  |  |  |  |
| East: Gebbie Stre               | et    |       |          |                       |     |                 |              |        |        |       |  |  |  |
| P2 Full                         | 11    | 54.2  | LOS E    | 0.0                   | 0.0 | 0.95            | 0.95         | 216.3  | 210.8  | 0.97  |  |  |  |
| All Pedestrians                 | 21    | 54.2  | LOS E    | 0.0                   | 0.0 | 0.95            | 0.95         | 219.9  | 215.5  | 0.98  |  |  |  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.
V Site: 102 [PM 2035 Pre Development (Site Folder: General)]

Abbotsford Road / Taylor Street Site Category: (None) Give-Way (Two-Way)

| Vehi      | cle Mo  | vement                           | Perfo                 | rmanc                           | e                     |                     |                       |                     |                           |                                |              |                                    |                    |                        |
|-----------|---------|----------------------------------|-----------------------|---------------------------------|-----------------------|---------------------|-----------------------|---------------------|---------------------------|--------------------------------|--------------|------------------------------------|--------------------|------------------------|
| Mov<br>ID | Turn    | DEMA<br>FLOV<br>[ Total<br>veh/h | AND<br>NS<br>HV]<br>% | ARRI<br>FLO<br>[ Total<br>veh/h | VAL<br>WS<br>HV]<br>% | Deg.<br>Satn<br>v/c | Aver.<br>Delay<br>sec | Level of<br>Service | 95%<br>Q<br>[ Veh.<br>veh | BACK OF<br>UEUE<br>Dist ]<br>m | Prop.<br>Que | Effective <i>F</i><br>Stop<br>Rate | ver. No.<br>Cycles | Aver.<br>Speed<br>km/h |
| South     | : Abbo  | tsford Ro                        | ad                    |                                 |                       |                     |                       |                     |                           |                                |              |                                    |                    |                        |
| 1         | L2      | 10                               | 0.0                   | 10                              | 0.0                   | 0.459               | 2.7                   | LOS A               | 0.0                       | 0.0                            | 0.00         | 0.01                               | 0.00               | 56.7                   |
| 2         | T1      | 1787                             | 0.9                   | 1787                            | 0.9                   | 0.459               | 0.0                   | LOS A               | 0.0                       | 0.0                            | 0.00         | 0.00                               | 0.00               | 59.6                   |
| Appro     | bach    | 1798                             | 0.9                   | 1798                            | 0.9                   | 0.459               | 0.0                   | NA                  | 0.0                       | 0.0                            | 0.00         | 0.00                               | 0.00               | 59.6                   |
| North     | : Abbot | sford Roa                        | ad                    |                                 |                       |                     |                       |                     |                           |                                |              |                                    |                    |                        |
| 8         | T1      | 1479                             | 1.0                   | 1479                            | 1.0                   | 0.281               | 1.2                   | LOS A               | 4.9                       | 34.9                           | 0.07         | 0.01                               | 0.08               | 57.3                   |
| 9         | R2      | 17                               | 0.0                   | 17                              | 0.0                   | 0.281               | 27.5                  | LOS D               | 4.9                       | 34.3                           | 0.25         | 0.03                               | 0.30               | 50.4                   |
| Appro     | bach    | 1496                             | 1.0                   | 1496                            | 1.0                   | 0.281               | 1.5                   | NA                  | 4.9                       | 34.9                           | 0.07         | 0.01                               | 0.08               | 57.1                   |
| West:     | Taylor  | Street                           |                       |                                 |                       |                     |                       |                     |                           |                                |              |                                    |                    |                        |
| 10        | L2      | 18                               | 0.0                   | 18                              | 0.0                   | 0.034               | 9.9                   | LOS A               | 0.1                       | 0.8                            | 0.64         | 0.79                               | 0.64               | 46.5                   |
| 12        | R2      | 9                                | 0.0                   | 9                               | 0.0                   | 1.633               | 1077.7                | LOS F               | 4.2                       | 29.5                           | 1.00         | 1.35                               | 2.47               | 1.5                    |
| Appro     | bach    | 27                               | 0.0                   | 27                              | 0.0                   | 1.633               | 365.8                 | LOS F               | 4.2                       | 29.5                           | 0.76         | 0.97                               | 1.25               | 6.7                    |
| All Ve    | hicles  | 3321                             | 0.9                   | 3321                            | 0.9                   | 1.633               | 3.7                   | NA                  | 4.9                       | 34.9                           | 0.04         | 0.01                               | 0.05               | 53.0                   |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Network Data dialog (Network tab).

Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Site: 101 [PM 2035 Post Development (Site Folder: General)]

#### Abbotsford Road / Gebbie Street

Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time)

| Vehio     | cle Mo  | vement                           | Perfo                 | rmanc                           | :e                    |                     |                       |                     |                              |                                |              |                                    |                    |                        |
|-----------|---------|----------------------------------|-----------------------|---------------------------------|-----------------------|---------------------|-----------------------|---------------------|------------------------------|--------------------------------|--------------|------------------------------------|--------------------|------------------------|
| Mov<br>ID | Turn    | DEMA<br>FLO\<br>[ Total<br>veh/h | AND<br>NS<br>HV]<br>% | ARRI<br>FLO<br>[ Total<br>veh/h | VAL<br>WS<br>HV]<br>% | Deg.<br>Satn<br>v/c | Aver.<br>Delay<br>sec | Level of<br>Service | 95% [<br>Ql<br>[ Veh.<br>veh | BACK OF<br>UEUE<br>Dist ]<br>m | Prop.<br>Que | Effective <i>F</i><br>Stop<br>Rate | ver. No.<br>Cycles | Aver.<br>Speed<br>km/h |
| South     | : Abbot | sford Ro                         | ad                    |                                 |                       |                     |                       |                     |                              |                                |              |                                    |                    |                        |
| 2         | T1      | 1805                             | 0.9                   | 1805                            | 0.9                   | *0.555              | 2.7                   | LOS A               | 14.8                         | 104.1                          | 0.31         | 0.29                               | 0.31               | 55.2                   |
| 3         | R2      | 13                               | 18.2                  | 13                              | 18.2                  | 0.166               | 68.7                  | LOS E               | 0.8                          | 6.4                            | 0.99         | 0.69                               | 0.99               | 26.8                   |
| Appro     | bach    | 1818                             | 1.0                   | 1818                            | 1.0                   | 0.555               | 3.1                   | LOS A               | 14.8                         | 104.1                          | 0.31         | 0.29                               | 0.31               | 54.4                   |
| East:     | Gebbie  | Street                           |                       |                                 |                       |                     |                       |                     |                              |                                |              |                                    |                    |                        |
| 4         | L2      | 34                               | 0.0                   | 34                              | 0.0                   | 0.244               | 60.9                  | LOS E               | 2.5                          | 17.2                           | 0.97         | 0.74                               | 0.97               | 28.2                   |
| 6         | R2      | 10                               | 0.0                   | 10                              | 0.0                   | *0.244              | 60.9                  | LOS E               | 2.5                          | 17.2                           | 0.97         | 0.74                               | 0.97               | 19.0                   |
| Appro     | bach    | 44                               | 0.0                   | 44                              | 0.0                   | 0.244               | 60.9                  | LOS E               | 2.5                          | 17.2                           | 0.97         | 0.74                               | 0.97               | 26.5                   |
| North     | : Abbot | sford Roa                        | ad                    |                                 |                       |                     |                       |                     |                              |                                |              |                                    |                    |                        |
| 7         | L2      | 8                                | 0.0                   | 8                               | 0.0                   | 0.346               | 8.0                   | LOS A               | 4.6                          | 32.6                           | 0.36         | 0.33                               | 0.36               | 43.5                   |
| 8         | T1      | 1480                             | 1.0                   | 1477                            | 1.0                   | 0.346               | 5.3                   | LOS A               | 4.6                          | 32.6                           | 0.36         | 0.33                               | 0.36               | 51.4                   |
| Appro     | bach    | 1488                             | 1.0                   | 1486 <sup>N</sup><br>1          | 1.0                   | 0.346               | 5.3                   | LOS A               | 4.6                          | 32.6                           | 0.36         | 0.33                               | 0.36               | 51.4                   |
| All Ve    | hicles  | 3350                             | 1.0                   | <mark>3347</mark> N             | 1.0                   | 0.555               | 4.9                   | LOS A               | 14.8                         | 104.1                          | 0.34         | 0.31                               | 0.34               | 51.8                   |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

\* Critical Movement (Signal Timing)

N1 Arrival Flow value is reduced due to capacity constraint at oversaturated upstream lanes.

| Pedestrian Mov    | /ement | Perform | nance    |              |               |         |              |        |        |       |
|-------------------|--------|---------|----------|--------------|---------------|---------|--------------|--------|--------|-------|
| Mov               | Dem.   | Aver.   | Level of | AVERAGE      | BACK OF       | Prop. E | ffective     | Travel | Travel | Aver. |
| ID Crossing       | Flow   | Delay   | Service  | QUE<br>[ Ped | EUE<br>Dist ] | Que     | Stop<br>Rate | Time   | Dist.  | Speed |
|                   | ped/h  | sec     |          | ped          | m             |         |              | sec    | m      | m/sec |
| South: Abbotsford | Road   |         |          |              |               |         |              |        |        |       |
| P1 Full           | 11     | 54.2    | LOS E    | 0.0          | 0.0           | 0.95    | 0.95         | 223.5  | 220.1  | 0.98  |
| East: Gebbie Stre | et     |         |          |              |               |         |              |        |        |       |
| P2 Full           | 11     | 54.2    | LOS E    | 0.0          | 0.0           | 0.95    | 0.95         | 216.3  | 210.8  | 0.97  |
| All Pedestrians   | 21     | 54.2    | LOS E    | 0.0          | 0.0           | 0.95    | 0.95         | 219.9  | 215.5  | 0.98  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

V Site: 102 [PM 2035 Post Development (Site Folder: General)]

Abbotsford Road / Taylor Street Site Category: (None) Give-Way (Two-Way)

| Vehio     | cle Mo  | vement                           | Perfo                 | rmanc                           | e                     |                     |                       |                     |                           |                                |              |                                    |                    |                        |
|-----------|---------|----------------------------------|-----------------------|---------------------------------|-----------------------|---------------------|-----------------------|---------------------|---------------------------|--------------------------------|--------------|------------------------------------|--------------------|------------------------|
| Mov<br>ID | Turn    | DEMA<br>FLOV<br>[ Total<br>veh/h | AND<br>WS<br>HV]<br>% | ARRI<br>FLO<br>[ Total<br>veh/h | VAL<br>WS<br>HV]<br>% | Deg.<br>Satn<br>v/c | Aver.<br>Delay<br>sec | Level of<br>Service | 95%<br>Q<br>[ Veh.<br>veh | BACK OF<br>UEUE<br>Dist ]<br>m | Prop.<br>Que | Effective <i>F</i><br>Stop<br>Rate | ver. No.<br>Cycles | Aver.<br>Speed<br>km/h |
| South     | : Abbot | tsford Ro                        | ad                    |                                 |                       |                     |                       |                     |                           |                                |              |                                    |                    |                        |
| 1         | L2      | 27                               | 0.0                   | 27                              | 0.0                   | 0.464               | 2.7                   | LOS A               | 0.0                       | 0.0                            | 0.00         | 0.02                               | 0.00               | 56.6                   |
| 2         | T1      | 1787                             | 0.9                   | 1787                            | 0.9                   | 0.464               | 0.0                   | LOS A               | 0.0                       | 0.0                            | 0.00         | 0.01                               | 0.00               | 59.6                   |
| Appro     | bach    | 1815                             | 0.9                   | 1815                            | 0.9                   | 0.464               | 0.1                   | NA                  | 0.0                       | 0.0                            | 0.00         | 0.01                               | 0.00               | 59.5                   |
| North     | : Abbot | sford Roa                        | ad                    |                                 |                       |                     |                       |                     |                           |                                |              |                                    |                    |                        |
| 8         | T1      | 1479                             | 1.0                   | 1479                            | 1.0                   | 0.301               | 1.9                   | LOS A               | 4.9                       | 34.9                           | 0.10         | 0.02                               | 0.12               | 56.0                   |
| 9         | R2      | 31                               | 0.0                   | 31                              | 0.0                   | 0.301               | 27.3                  | LOS D               | 4.9                       | 34.2                           | 0.46         | 0.07                               | 0.55               | 47.4                   |
| Appro     | bach    | 1510                             | 1.0                   | 1510                            | 1.0                   | 0.301               | 2.4                   | NA                  | 4.9                       | 34.9                           | 0.11         | 0.02                               | 0.13               | 55.6                   |
| West:     | Taylor  | Street                           |                       |                                 |                       |                     |                       |                     |                           |                                |              |                                    |                    |                        |
| 10        | L2      | 32                               | 0.0                   | 32                              | 0.0                   | 0.058               | 9.9                   | LOS A               | 0.2                       | 1.4                            | 0.64         | 0.82                               | 0.64               | 46.5                   |
| 12        | R2      | 9                                | 0.0                   | 9                               | 0.0                   | 1.631               | 1076.3                | LOS F               | 4.2                       | 29.4                           | 1.00         | 1.35                               | 2.48               | 1.5                    |
| Appro     | bach    | 41                               | 0.0                   | 41                              | 0.0                   | 1.631               | 249.8                 | LOS F               | 4.2                       | 29.4                           | 0.72         | 0.94                               | 1.05               | 9.7                    |
| All Ve    | hicles  | 3365                             | 0.9                   | 3365                            | 0.9                   | 1.631               | 4.1                   | NA                  | 4.9                       | 34.9                           | 0.06         | 0.02                               | 0.07               | 52.4                   |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Network Data dialog (Network tab).

Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## SITE LAYOUT

**▽** Site: 101 [AM 2022 Existing Conditions (Site Folder: General)]

Burrows Street / Taylor Street Site Category: (None) Give-Way (Two-Way)

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



## V Site: 101 [AM 2022 Existing Conditions (Site Folder: General)]

Burrows Street / Taylor Street Site Category: (None) Give-Way (Two-Way)

| Vehi         | icle M  | ovemen           | t Perfoi  | rmance           |          |       |       |          |               |             |       |           |        |        |
|--------------|---------|------------------|-----------|------------------|----------|-------|-------|----------|---------------|-------------|-------|-----------|--------|--------|
| Mov          | Turn    | INP              | UT        | DEM              | AND      | Deg.  | Aver. | Level of | 95% BA        | ACK OF      | Prop. | Effective | Aver.  | Aver.  |
| ID           |         |                  | IMES      | FLO              | WS       | Satn  | Delay | Service  | QUE           | EUE         | Que   | Stop      | No.    | Speed  |
|              |         | l Iolai<br>veh/h | HV ]<br>% | [ IOlai<br>veh/h | HV]<br>% | v/c   | Sec   |          | į ven.<br>veh | DISL J<br>m |       | Rale      | Cycles | km/h   |
| Sout         | h: Burr | ows Stre         | et        | VOII/II          |          | 10    |       |          | VOIT          |             |       |           |        | KI1/11 |
| 2            | T1      | 634              | 3.2       | 650              | 3.2      | 0.183 | 0.4   | LOS A    | 0.3           | 2.3         | 0.06  | 0.01      | 0.06   | 59.4   |
| 3            | R2      | 14               | 0.0       | 14               | 0.0      | 0.183 | 12.6  | LOS B    | 0.3           | 2.3         | 0.12  | 0.03      | 0.12   | 52.9   |
| Appr         | oach    | 648              | 3.1       | 664              | 3.1      | 0.183 | 0.7   | NA       | 0.3           | 2.3         | 0.06  | 0.01      | 0.06   | 59.2   |
| East         | : Taylo | r Street         |           |                  |          |       |       |          |               |             |       |           |        |        |
| 4            | L2      | 29               | 6.9       | 30               | 6.9      | 0.170 | 7.2   | LOS A    | 0.5           | 4.0         | 0.71  | 0.82      | 0.71   | 42.7   |
| 6            | R2      | 18               | 5.6       | 18               | 5.6      | 0.170 | 31.6  | LOS D    | 0.5           | 4.0         | 0.71  | 0.82      | 0.71   | 42.7   |
| Appr         | oach    | 47               | 6.4       | 48               | 6.4      | 0.170 | 16.5  | LOS C    | 0.5           | 4.0         | 0.71  | 0.82      | 0.71   | 42.7   |
| North        | n: Burr | ows Stree        | et        |                  |          |       |       |          |               |             |       |           |        |        |
| 7            | L2      | 22               | 0.0       | 23               | 0.0      | 0.282 | 5.6   | LOS A    | 0.0           | 0.0         | 0.00  | 0.03      | 0.00   | 58.0   |
| 8            | T1      | 1035             | 1.1       | 1060             | 1.1      | 0.282 | 0.1   | LOS A    | 0.0           | 0.0         | 0.00  | 0.01      | 0.00   | 59.7   |
| Appr         | oach    | 1057             | 1.1       | 1083             | 1.1      | 0.282 | 0.2   | NA       | 0.0           | 0.0         | 0.00  | 0.01      | 0.00   | 59.7   |
| All<br>Vehio | cles    | 1752             | 2.0       | 1795             | 2.0      | 0.282 | 0.8   | NA       | 0.5           | 4.0         | 0.04  | 0.03      | 0.04   | 58.9   |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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#### V Site: 101 [AM 2025 Pre Development (Site Folder: General)]

Burrows Street / Taylor Street Site Category: (None) Give-Way (Two-Way)

| Vehi         | cle M   | ovemen                          | t Perfor                | mance  |                       |                     |                       |                     |                                |                             |              |                           |                        |                        |
|--------------|---------|---------------------------------|-------------------------|--|-----------------------|---------------------|-----------------------|---------------------|--------------------------------|-----------------------------|--------------|---------------------------|------------------------|------------------------|
| Mov<br>ID    | Turn    | INP<br>VOLL<br>[ Total<br>veh/h | PUT<br>JMES<br>HV]<br>% | DEM/<br>FLO <sup>V</sup><br>[ Total<br>veh/h | AND<br>NS<br>HV]<br>% | Deg.<br>Satn<br>v/c | Aver.<br>Delay<br>sec | Level of<br>Service | 95% BA<br>QUI<br>[ Veh.<br>veh | ACK OF<br>EUE<br>Dist]<br>m | Prop.<br>Que | Effective<br>Stop<br>Rate | Aver.<br>No.<br>Cycles | Aver.<br>Speed<br>km/h |
| South        | n: Burr | ows Stre                        | et                      |  |                       |                     |                       |                     |                                |                             |              |                           |                        |                        |
| 2            | T1      | 655                             | 3.2                     | 671  | 3.2                   | 0.189               | 0.4                   | LOS A               | 0.3                            | 2.5                         | 0.06         | 0.01                      | 0.06                   | 59.3                   |
| 3            | R2      | 14                              | 0.0                     | 14   | 0.0                   | 0.189               | 13.1                  | LOS B               | 0.3                            | 2.5                         | 0.13         | 0.03                      | 0.13                   | 52.8                   |
| Appro        | oach    | 669                             | 3.1                     | 685  | 3.1                   | 0.189               | 0.7                   | NA                  | 0.3                            | 2.5                         | 0.06         | 0.01                      | 0.06                   | 59.2                   |
| East:        | Taylor  | Street                          |                         |  |                       |                     |                       |                     |                                |                             |              |                           |                        |                        |
| 4            | L2      | 30                              | 6.9                     | 31   | 6.9                   | 0.191               | 7.3                   | LOS A               | 0.6                            | 4.5                         | 0.74         | 0.84                      | 0.74                   | 42.1                   |
| 6            | R2      | 19                              | 5.6                     | 19   | 5.6                   | 0.191               | 33.9                  | LOS D               | 0.6                            | 4.5                         | 0.74         | 0.84                      | 0.74                   | 42.1                   |
| Appro        | bach    | 49                              | 6.4                     | 50   | 6.4                   | 0.191               | 17.6                  | LOS C               | 0.6                            | 4.5                         | 0.74         | 0.84                      | 0.74                   | 42.1                   |
| North        | : Burro | ows Stree                       | et                      |  |                       |                     |                       |                     |                                |                             |              |                           |                        |                        |
| 7            | L2      | 23                              | 0.0                     | 24   | 0.0                   | 0.292               | 5.6                   | LOS A               | 0.0                            | 0.0                         | 0.00         | 0.03                      | 0.00                   | 58.0                   |
| 8            | T1      | 1070                            | 1.1                     | 1096   | 1.1                   | 0.292               | 0.1                   | LOS A               | 0.0                            | 0.0                         | 0.00         | 0.01                      | 0.00                   | 59.7                   |
| Appro        | bach    | 1093                            | 1.1                     | 1120   | 1.1                   | 0.292               | 0.2                   | NA                  | 0.0                            | 0.0                         | 0.00         | 0.01                      | 0.00                   | 59.7                   |
| All<br>Vehic | les     | 1811                            | 2.0                     | 1856   | 2.0                   | 0.292               | 0.9                   | NA                  | 0.6                            | 4.5                         | 0.04         | 0.04                      | 0.04                   | 58.8                   |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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#### V Site: 101 [AM 2025 Post Development (Site Folder: General)]

Burrows Street / Taylor Street Site Category: (None) Give-Way (Two-Way)

| Vehi         | cle M   | ovemen      | t Perfor    | mance       |           |              |                |                     |             |               |              |                   |              |                |
|--------------|---------|-------------|-------------|-------------|-----------|--------------|----------------|---------------------|-------------|---------------|--------------|-------------------|--------------|----------------|
| Mov<br>ID    | Turn    | INP<br>VOLU | PUT<br>JMES | DEM/<br>FLO | AND<br>WS | Deg.<br>Satn | Aver.<br>Delay | Level of<br>Service | 95% BA      | ACK OF<br>EUE | Prop.<br>Que | Effective<br>Stop | Aver.<br>No. | Aver.<br>Speed |
|              |         | veh/h       | нvј<br>%    | veh/h       | нvј<br>%  | v/c          | sec            |                     | ven.<br>veh | m Dist        |              | Rate              | Cycles       | km/h           |
| Sout         | h: Burr | ows Stre    | et          |             |           |              |                |                     |             |               |              |                   |              |                |
| 2            | T1      | 655         | 3.2         | 671         | 3.2       | 0.194        | 0.6            | LOS A               | 0.5         | 3.4           | 0.08         | 0.02              | 0.08         | 59.1           |
| 3            | R2      | 19          | 0.0         | 19          | 0.0       | 0.194        | 13.2           | LOS B               | 0.5         | 3.4           | 0.17         | 0.04              | 0.17         | 52.4           |
| Appr         | oach    | 674         | 3.1         | 691         | 3.1       | 0.194        | 0.9            | NA                  | 0.5         | 3.4           | 0.08         | 0.02              | 0.08         | 58.9           |
| East         | Taylo   | Street      |             |             |           |              |                |                     |             |               |              |                   |              |                |
| 4            | L2      | 63          | 6.9         | 65          | 6.9       | 0.323        | 9.4            | LOS A               | 1.2         | 9.1           | 0.72         | 0.92              | 0.89         | 41.7           |
| 6            | R2      | 30          | 5.6         | 31          | 5.6       | 0.323        | 37.8           | LOS E               | 1.2         | 9.1           | 0.72         | 0.92              | 0.89         | 41.7           |
| Appr         | oach    | 93          | 6.5         | 95          | 6.5       | 0.323        | 18.6           | LOS C               | 1.2         | 9.1           | 0.72         | 0.92              | 0.89         | 41.7           |
| North        | n: Burr | ows Stree   | ət          |             |           |              |                |                     |             |               |              |                   |              |                |
| 7            | L2      | 36          | 0.0         | 37          | 0.0       | 0.294        | 5.6            | LOS A               | 0.0         | 0.0           | 0.00         | 0.04              | 0.00         | 57.9           |
| 8            | T1      | 1065        | 1.1         | 1091        | 1.1       | 0.294        | 0.1            | LOS A               | 0.0         | 0.0           | 0.00         | 0.02              | 0.00         | 59.7           |
| Appr         | oach    | 1101        | 1.1         | 1128        | 1.1       | 0.294        | 0.3            | NA                  | 0.0         | 0.0           | 0.00         | 0.02              | 0.00         | 59.6           |
| All<br>Vehio | cles    | 1868        | 2.1         | 1914        | 2.1       | 0.323        | 1.4            | NA                  | 1.2         | 9.1           | 0.06         | 0.06              | 0.07         | 58.1           |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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#### V Site: 101 [AM 2035 Pre Development (Site Folder: General)]

Burrows Street / Taylor Street Site Category: (None) Give-Way (Two-Way)

| Vehi         | cle M    | ovemen                 | t Perfor           | mance                  |                  |              |                |                     |                         |                         |              |                           |                        |                |
|--------------|----------|------------------------|--------------------|------------------------|------------------|--------------|----------------|---------------------|-------------------------|-------------------------|--------------|---------------------------|------------------------|----------------|
| Mov<br>ID    | Turn     | INF<br>VOLU<br>[ Total | PUT<br>JMES<br>HV] | لDEM<br>FLO<br>[ Total | AND<br>WS<br>HV] | Deg.<br>Satn | Aver.<br>Delay | Level of<br>Service | 95% BA<br>QUI<br>[ Veh. | ACK OF<br>EUE<br>Dist ] | Prop.<br>Que | Effective<br>Stop<br>Rate | Aver.<br>No.<br>Cycles | Aver.<br>Speed |
|              |          | veh/h                  | %                  | veh/h                  | %                | v/c          | sec            |                     | veh                     | m                       |              |                           |                        | km/h           |
| Sout         | n: Burr  | ows Stre               | et                 |                        |                  |              |                |                     |                         |                         |              |                           |                        |                |
| 2            | T1       | 731                    | 3.2                | 749                    | 3.2              | 0.214        | 0.6            | LOS A               | 0.5                     | 3.6                     | 0.07         | 0.01                      | 0.07                   | 59.1           |
| 3            | R2       | 16                     | 0.0                | 16                     | 0.0              | 0.214        | 15.0           | LOS B               | 0.5                     | 3.6                     | 0.15         | 0.03                      | 0.16                   | 52.5           |
| Appr         | oach     | 747                    | 3.1                | 765                    | 3.1              | 0.214        | 0.9            | NA                  | 0.5                     | 3.6                     | 0.07         | 0.01                      | 0.08                   | 59.0           |
| East:        | Taylo    | Street                 |                    |                        |                  |              |                |                     |                         |                         |              |                           |                        |                |
| 4            | L2       | 33                     | 6.9                | 34                     | 6.9              | 0.269        | 9.7            | LOS A               | 0.9                     | 6.6                     | 0.80         | 0.94                      | 0.91                   | 39.4           |
| 6            | R2       | 21                     | 5.6                | 22                     | 5.6              | 0.269        | 45.8           | LOS E               | 0.9                     | 6.6                     | 0.80         | 0.94                      | 0.91                   | 39.4           |
| Appro        | oach     | 54                     | 6.4                | 55                     | 6.4              | 0.269        | 23.8           | LOS C               | 0.9                     | 6.6                     | 0.80         | 0.94                      | 0.91                   | 39.4           |
| North        | n: Burro | ows Stree              | ət                 |                        |                  |              |                |                     |                         |                         |              |                           |                        |                |
| 7            | L2       | 25                     | 0.0                | 26                     | 0.0              | 0.325        | 5.6            | LOS A               | 0.0                     | 0.0                     | 0.00         | 0.02                      | 0.00                   | 58.0           |
| 8            | T1       | 1193                   | 1.1                | 1222                   | 1.1              | 0.325        | 0.1            | LOS A               | 0.0                     | 0.0                     | 0.00         | 0.01                      | 0.00                   | 59.7           |
| Appr         | oach     | 1218                   | 1.1                | 1248                   | 1.1              | 0.325        | 0.2            | NA                  | 0.0                     | 0.0                     | 0.00         | 0.01                      | 0.00                   | 59.7           |
| All<br>Vehic | les      | 2019                   | 2.0                | 2069                   | 2.0              | 0.325        | 1.1            | NA                  | 0.9                     | 6.6                     | 0.05         | 0.04                      | 0.05                   | 58.6           |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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#### V Site: 101 [AM 2035 Post Development (Site Folder: General)]

Burrows Street / Taylor Street Site Category: (None) Give-Way (Two-Way)

| Vehi         | cle M    | ovemen           | t Perfor    | mance            |           |              |                |                     |               |               |              |                   |              |                |
|--------------|----------|------------------|-------------|------------------|-----------|--------------|----------------|---------------------|---------------|---------------|--------------|-------------------|--------------|----------------|
| Mov<br>ID    | Turn     | INF<br>VOLU      | PUT<br>JMES | DEM/<br>FLO      | AND<br>WS | Deg.<br>Satn | Aver.<br>Delay | Level of<br>Service | 95% B/<br>QUI | ACK OF<br>EUE | Prop.<br>Que | Effective<br>Stop | Aver.<br>No. | Aver.<br>Speed |
|              |          | [ Iotal<br>veh/h | HV J<br>%   | [ Iotal<br>veh/h | HV J<br>% | v/c          | sec            |                     | [ Veh.<br>veh | Dist J<br>m   |              | Rate              | Cycles       | km/h           |
| Sout         | h: Burr  | ows Stre         | et          |                  |           |              |                |                     |               |               |              |                   |              |                |
| 2            | T1       | 731              | 3.2         | 749              | 3.2       | 0.216        | 0.6            | LOS A               | 0.5           | 3.9           | 0.08         | 0.02              | 0.08         | 59.1           |
| 3            | R2       | 20               | 0.0         | 20               | 0.0       | 0.216        | 14.0           | LOS B               | 0.5           | 3.9           | 0.18         | 0.04              | 0.19         | 52.3           |
| Appr         | oach     | 751              | 3.1         | 769              | 3.1       | 0.216        | 1.0            | NA                  | 0.5           | 3.9           | 0.08         | 0.02              | 0.09         | 58.9           |
| East:        | Taylo    | Street           |             |                  |           |              |                |                     |               |               |              |                   |              |                |
| 4            | L2       | 66               | 6.9         | 68               | 6.9       | 0.348        | 10.2           | LOS B               | 1.3           | 9.9           | 0.76         | 0.96              | 0.96         | 41.3           |
| 6            | R2       | 32               | 5.6         | 33               | 5.6       | 0.348        | 38.5           | LOS E               | 1.3           | 9.9           | 0.76         | 0.96              | 0.96         | 41.3           |
| Appr         | oach     | 98               | 6.5         | 100              | 6.5       | 0.348        | 19.5           | LOS C               | 1.3           | 9.9           | 0.76         | 0.96              | 0.96         | 41.3           |
| North        | n: Burro | ows Stree        | et          |                  |           |              |                |                     |               |               |              |                   |              |                |
| 7            | L2       | 38               | 0.0         | 39               | 0.0       | 0.328        | 5.6            | LOS A               | 0.0           | 0.0           | 0.00         | 0.04              | 0.00         | 57.9           |
| 8            | T1       | 1189             | 1.1         | 1218             | 1.1       | 0.328        | 0.1            | LOS A               | 0.0           | 0.0           | 0.00         | 0.02              | 0.00         | 59.6           |
| Appr         | oach     | 1227             | 1.1         | 1257             | 1.1       | 0.328        | 0.3            | NA                  | 0.0           | 0.0           | 0.00         | 0.02              | 0.00         | 59.6           |
| All<br>Vehic | cles     | 2076             | 2.1         | 2127             | 2.1       | 0.348        | 1.4            | NA                  | 1.3           | 9.9           | 0.07         | 0.06              | 0.08         | 58.1           |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## V Site: 101 [PM 2022 Existing Conditions (Site Folder: General)]

Burrows Street / Taylor Street Site Category: (None) Give-Way (Two-Way)

| Vehi         | cle M    | ovemen    | t Perfor | rmance  |     |              |       |          |        |        |       |           |        |       |
|--------------|----------|-----------|----------|---------|-----|--------------|-------|----------|--------|--------|-------|-----------|--------|-------|
| Mov          | Turn     |           |          |         | AND | Deg.<br>Sata | Aver. | Level of | 95% BA |        | Prop. | Effective | Aver.  | Aver. |
|              |          | [ Total   | HV ]     | [ Total |     | Call         | Delay | OCIVICC  | [Veh.  | Dist ] | Que   | Rate      | Cycles | opecu |
|              |          | veh/h     | %        | veh/h   | %   | v/c          | sec   |          | veh    | m      |       |           | ·      | km/h  |
| Sout         | h: Burr  | ows Stree | et       |         |     |              |       |          |        |        |       |           |        |       |
| 2            | T1       | 1307      | 0.7      | 1327    | 0.7 | 0.348        | 0.1   | LOS A    | 0.2    | 1.5    | 0.02  | 0.00      | 0.02   | 59.8  |
| 3            | R2       | 10        | 0.0      | 10      | 0.0 | 0.348        | 10.2  | LOS B    | 0.2    | 1.5    | 0.03  | 0.01      | 0.04   | 53.7  |
| Appr         | oach     | 1317      | 0.7      | 1337    | 0.7 | 0.348        | 0.2   | NA       | 0.2    | 1.5    | 0.02  | 0.00      | 0.02   | 59.7  |
| East:        | : Tayloi | Street    |          |         |     |              |       |          |        |        |       |           |        |       |
| 4            | L2       | 24        | 0.0      | 24      | 0.0 | 0.178        | 5.9   | LOS A    | 0.6    | 3.9    | 0.68  | 0.75      | 0.68   | 41.4  |
| 6            | R2       | 16        | 0.0      | 16      | 0.0 | 0.178        | 40.0  | LOS E    | 0.6    | 3.9    | 0.68  | 0.75      | 0.68   | 41.3  |
| Appr         | oach     | 40        | 0.0      | 41      | 0.0 | 0.178        | 19.5  | LOS C    | 0.6    | 3.9    | 0.68  | 0.75      | 0.68   | 41.4  |
| North        | n: Burro | ows Stree | et       |         |     |              |       |          |        |        |       |           |        |       |
| 7            | L2       | 7         | 0.0      | 7       | 0.0 | 0.179        | 5.6   | LOS A    | 0.0    | 0.0    | 0.00  | 0.01      | 0.00   | 58.2  |
| 8            | T1       | 674       | 0.6      | 684     | 0.6 | 0.179        | 0.0   | LOS A    | 0.0    | 0.0    | 0.00  | 0.01      | 0.00   | 59.9  |
| Appr         | oach     | 681       | 0.6      | 691     | 0.6 | 0.179        | 0.1   | NA       | 0.0    | 0.0    | 0.00  | 0.01      | 0.00   | 59.8  |
| All<br>Vehic | cles     | 2038      | 0.6      | 2069    | 0.6 | 0.348        | 0.6   | NA       | 0.6    | 3.9    | 0.02  | 0.02      | 0.03   | 59.3  |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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#### V Site: 101 [PM 2025 Pre Development (Site Folder: General)]

Burrows Street / Taylor Street Site Category: (None) Give-Way (Two-Way)

| Vehi         | cle M   | ovemen                 | t Perfor            | mance                  |                   |              |                |                     |                         |                         |              |                           |                        |                |
|--------------|---------|------------------------|---------------------|------------------------|-------------------|--------------|----------------|---------------------|-------------------------|-------------------------|--------------|---------------------------|------------------------|----------------|
| Mov<br>ID    | Turn    | INP<br>VOLL<br>[ Total | PUT<br>JMES<br>HV ] | DEM/<br>FLO<br>[ Total | AND<br>WS<br>HV ] | Deg.<br>Satn | Aver.<br>Delay | Level of<br>Service | 95% BA<br>QUI<br>[ Veh. | ACK OF<br>EUE<br>Dist ] | Prop.<br>Que | Effective<br>Stop<br>Rate | Aver.<br>No.<br>Cycles | Aver.<br>Speed |
|              |         | veh/h                  | %                   | veh/h                  | %                 | v/c          | sec            |                     | veh                     | m                       |              |                           |                        | km/h           |
| Sout         | h: Burr | ows Stre               | et                  |                        |                   |              |                |                     |                         |                         |              |                           |                        |                |
| 2            | T1      | 1351                   | 0.7                 | 1372                   | 0.7               | 0.360        | 0.1            | LOS A               | 0.2                     | 1.5                     | 0.02         | 0.00                      | 0.02                   | 59.8           |
| 3            | R2      | 10                     | 0.0                 | 10                     | 0.0               | 0.360        | 10.5           | LOS B               | 0.2                     | 1.5                     | 0.03         | 0.01                      | 0.04                   | 53.7           |
| Appr         | oach    | 1361                   | 0.7                 | 1382                   | 0.7               | 0.360        | 0.2            | NA                  | 0.2                     | 1.5                     | 0.02         | 0.00                      | 0.02                   | 59.7           |
| East:        | Taylo   | r Street               |                     |                        |                   |              |                |                     |                         |                         |              |                           |                        |                |
| 4            | L2      | 25                     | 0.0                 | 25                     | 0.0               | 0.204        | 6.1            | LOS A               | 0.6                     | 4.4                     | 0.71         | 0.77                      | 0.71                   | 40.6           |
| 6            | R2      | 17                     | 0.0                 | 17                     | 0.0               | 0.204        | 43.6           | LOS E               | 0.6                     | 4.4                     | 0.71         | 0.77                      | 0.71                   | 40.5           |
| Appr         | oach    | 42                     | 0.0                 | 43                     | 0.0               | 0.204        | 21.3           | LOS C               | 0.6                     | 4.4                     | 0.71         | 0.77                      | 0.71                   | 40.6           |
| North        | n: Burr | ows Stree              | et                  |                        |                   |              |                |                     |                         |                         |              |                           |                        |                |
| 7            | L2      | 7                      | 0.0                 | 7                      | 0.0               | 0.185        | 5.6            | LOS A               | 0.0                     | 0.0                     | 0.00         | 0.01                      | 0.00                   | 58.2           |
| 8            | T1      | 696                    | 0.6                 | 707                    | 0.6               | 0.185        | 0.0            | LOS A               | 0.0                     | 0.0                     | 0.00         | 0.01                      | 0.00                   | 59.9           |
| Appr         | oach    | 703                    | 0.6                 | 714                    | 0.6               | 0.185        | 0.1            | NA                  | 0.0                     | 0.0                     | 0.00         | 0.01                      | 0.00                   | 59.8           |
| All<br>Vehio | cles    | 2106                   | 0.6                 | 2138                   | 0.6               | 0.360        | 0.6            | NA                  | 0.6                     | 4.4                     | 0.02         | 0.02                      | 0.03                   | 59.2           |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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#### V Site: 101 [PM 2025 Post Development (Site Folder: General)]

Burrows Street / Taylor Street Site Category: (None) Give-Way (Two-Way)

| Vehi         | icle M   | ovemen           | t Perfor  | mance            |          |       |       |          |               |        |       |           |        |        |
|--------------|----------|------------------|-----------|------------------|----------|-------|-------|----------|---------------|--------|-------|-----------|--------|--------|
| Mov          | Turn     | INP              | TUT       | DEM              | AND      | Deg.  | Aver. | Level of | 95% BA        | ACK OF | Prop. | Effective | Aver.  | Aver.  |
| ID           |          |                  | JMES      | FLO              | WS       | Satn  | Delay | Service  | QUI           | EUE    | Que   | Stop      | No.    | Speed  |
|              |          | [ IOlai<br>veh/h | HV J<br>% | [ IOlai<br>veh/h | HV]<br>% | vic   | 200   |          | į ven.<br>veh | DISL]  |       | Rale      | Cycles | km/h   |
| Sout         | h: Burr  | ows Stre         | et        | VOII/II          | /0       | 10    | 000   |          | VOIT          |        |       |           |        | K11/11 |
| 2            | T1       | 1351             | 0.7       | 1372             | 0.7      | 0.363 | 0.2   | LOS A    | 0.3           | 2.3    | 0.02  | 0.01      | 0.03   | 59.7   |
| 3            | R2       | 15               | 0.0       | 15               | 0.0      | 0.363 | 10.6  | LOS B    | 0.3           | 2.3    | 0.05  | 0.01      | 0.06   | 53.5   |
| Appr         | oach     | 1366             | 0.7       | 1387             | 0.7      | 0.363 | 0.3   | NA       | 0.3           | 2.3    | 0.03  | 0.01      | 0.03   | 59.6   |
| East         | : Tayloi | Street           |           |                  |          |       |       |          |               |        |       |           |        |        |
| 4            | L2       | 46               | 0.0       | 47               | 0.0      | 0.313 | 8.8   | LOS A    | 1.1           | 7.9    | 0.68  | 0.82      | 0.82   | 39.9   |
| 6            | R2       | 25               | 0.0       | 25               | 0.0      | 0.313 | 48.4  | LOS E    | 1.1           | 7.9    | 0.68  | 0.82      | 0.82   | 39.9   |
| Appr         | oach     | 71               | 0.0       | 72               | 0.0      | 0.313 | 22.8  | LOS C    | 1.1           | 7.9    | 0.68  | 0.82      | 0.82   | 39.9   |
| North        | n: Burro | ows Stree        | et        |                  |          |       |       |          |               |        |       |           |        |        |
| 7            | L2       | 16               | 0.0       | 16               | 0.0      | 0.188 | 5.6   | LOS A    | 0.0           | 0.0    | 0.00  | 0.03      | 0.00   | 58.1   |
| 8            | T1       | 696              | 0.6       | 707              | 0.6      | 0.188 | 0.0   | LOS A    | 0.0           | 0.0    | 0.00  | 0.01      | 0.00   | 59.8   |
| Appr         | oach     | 712              | 0.6       | 723              | 0.6      | 0.188 | 0.2   | NA       | 0.0           | 0.0    | 0.00  | 0.01      | 0.00   | 59.7   |
| All<br>Vehio | cles     | 2149             | 0.6       | 2182             | 0.6      | 0.363 | 1.0   | NA       | 1.1           | 7.9    | 0.04  | 0.04      | 0.05   | 58.7   |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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#### V Site: 101 [PM 2035 Pre Development (Site Folder: General)]

Burrows Street / Taylor Street Site Category: (None) Give-Way (Two-Way)

| Vehi                  | Vehicle Movement Performance |             |          |             |           |              |                |                     |               |               |              |                   |              |                |
|-----------------------|------------------------------|-------------|----------|-------------|-----------|--------------|----------------|---------------------|---------------|---------------|--------------|-------------------|--------------|----------------|
| Mov<br>ID             | Turn                         | INP<br>VOLU |          | DEM,<br>FLO | AND<br>WS | Deg.<br>Satn | Aver.<br>Delay | Level of<br>Service | 95% BA<br>QUI | ACK OF<br>EUE | Prop.<br>Que | Effective<br>Stop | Aver.<br>No. | Aver.<br>Speed |
|                       |                              | veh/h       | пvј<br>% | veh/h       | пvј<br>%  | v/c          | sec            |                     | ven.<br>veh   | m Dist        |              | Rale              | Cycles       | km/h           |
| South: Burrows Street |                              |             |          |             |           |              |                |                     |               |               |              |                   |              |                |
| 2                     | T1                           | 1507        | 0.7      | 1530        | 0.7       | 0.403        | 0.2            | LOS A               | 0.3           | 2.2           | 0.02         | 0.00              | 0.03         | 59.7           |
| 3                     | R2                           | 12          | 0.0      | 12          | 0.0       | 0.403        | 11.8           | LOS B               | 0.3           | 2.2           | 0.04         | 0.01              | 0.06         | 53.6           |
| Appr                  | oach                         | 1519        | 0.7      | 1542        | 0.7       | 0.403        | 0.3            | NA                  | 0.3           | 2.2           | 0.02         | 0.00              | 0.03         | 59.7           |
| East:                 | Taylo                        | Street      |          |             |           |              |                |                     |               |               |              |                   |              |                |
| 4                     | L2                           | 28          | 0.0      | 28          | 0.0       | 0.297        | 10.3           | LOS B               | 1.0           | 6.8           | 0.78         | 0.87              | 0.90         | 36.6           |
| 6                     | R2                           | 18          | 0.0      | 18          | 0.0       | 0.297        | 63.5           | LOS F               | 1.0           | 6.8           | 0.78         | 0.87              | 0.90         | 36.6           |
| Appr                  | oach                         | 46          | 0.0      | 47          | 0.0       | 0.297        | 31.1           | LOS D               | 1.0           | 6.8           | 0.78         | 0.87              | 0.90         | 36.6           |
| North                 | n: Burr                      | ows Stree   | et       |             |           |              |                |                     |               |               |              |                   |              |                |
| 7                     | L2                           | 8           | 0.0      | 8           | 0.0       | 0.207        | 5.6            | LOS A               | 0.0           | 0.0           | 0.00         | 0.01              | 0.00         | 58.2           |
| 8                     | T1                           | 777         | 0.6      | 789         | 0.6       | 0.207        | 0.1            | LOS A               | 0.0           | 0.0           | 0.00         | 0.01              | 0.00         | 59.8           |
| Appr                  | oach                         | 785         | 0.6      | 797         | 0.6       | 0.207        | 0.1            | NA                  | 0.0           | 0.0           | 0.00         | 0.01              | 0.00         | 59.8           |
| All<br>Vehio          | cles                         | 2350        | 0.6      | 2386        | 0.6       | 0.403        | 0.8            | NA                  | 1.0           | 6.8           | 0.03         | 0.02              | 0.04         | 59.0           |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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#### V Site: 101 [PM 2035 Post Development (Site Folder: General)]

Burrows Street / Taylor Street Site Category: (None) Give-Way (Two-Way)

| Vehi         | Vehicle Movement Performance |                  |             |                  |           |              |                |                     |               |             |              |                   |             |                |
|--------------|------------------------------|------------------|-------------|------------------|-----------|--------------|----------------|---------------------|---------------|-------------|--------------|-------------------|-------------|----------------|
| Mov<br>ID    | Turn                         | INF<br>Vol I     | PUT<br>IMES | DEM.<br>FLO      | AND<br>WS | Deg.<br>Satn | Aver.<br>Delav | Level of<br>Service | 95% BA        |             | Prop.<br>Que | Effective<br>Stop | Aver.<br>No | Aver.<br>Speed |
|              |                              | [ Total<br>veh/h | HV ]<br>%   | [ Total<br>veh/h | HV ]<br>% | v/c          | sec            |                     | [ Veh.<br>veh | Dist ]<br>m | Que          | Rate              | Cycles      | km/h           |
| Sout         | South: Burrows Street        |                  |             |                  |           |              |                |                     |               |             |              |                   |             |                |
| 2            | T1                           | 1507             | 0.7         | 1530             | 0.7       | 0.405        | 0.2            | LOS A               | 0.4           | 3.0         | 0.03         | 0.01              | 0.04        | 59.7           |
| 3            | R2                           | 16               | 0.0         | 16               | 0.0       | 0.405        | 11.9           | LOS B               | 0.4           | 3.0         | 0.06         | 0.01              | 0.08        | 53.5           |
| Appr         | oach                         | 1523             | 0.7         | 1546             | 0.7       | 0.405        | 0.4            | NA                  | 0.4           | 3.0         | 0.03         | 0.01              | 0.04        | 59.6           |
| East:        | Taylor                       | Street           |             |                  |           |              |                |                     |               |             |              |                   |             |                |
| 4            | L2                           | 49               | 0.0         | 50               | 0.0       | 0.458        | 16.9           | LOS C               | 1.8           | 12.5        | 0.77         | 0.96              | 1.11        | 34.6           |
| 6            | R2                           | 27               | 0.0         | 27               | 0.0       | 0.458        | 72.8           | LOS F               | 1.8           | 12.5        | 0.77         | 0.96              | 1.11        | 34.6           |
| Appr         | oach                         | 76               | 0.0         | 77               | 0.0       | 0.458        | 36.8           | LOS E               | 1.8           | 12.5        | 0.77         | 0.96              | 1.11        | 34.6           |
| North        | n: Burro                     | ows Stree        | et          |                  |           |              |                |                     |               |             |              |                   |             |                |
| 7            | L2                           | 16               | 0.0         | 16               | 0.0       | 0.209        | 5.6            | LOS A               | 0.0           | 0.0         | 0.00         | 0.02              | 0.00        | 58.1           |
| 8            | T1                           | 777              | 0.6         | 789              | 0.6       | 0.209        | 0.1            | LOS A               | 0.0           | 0.0         | 0.00         | 0.01              | 0.00        | 59.8           |
| Appr         | oach                         | 793              | 0.6         | 805              | 0.6       | 0.209        | 0.2            | NA                  | 0.0           | 0.0         | 0.00         | 0.01              | 0.00        | 59.7           |
| All<br>Vehic | cles                         | 2392             | 0.6         | 2428             | 0.6       | 0.458        | 1.4            | NA                  | 1.8           | 12.5        | 0.04         | 0.04              | 0.06        | 58.3           |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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APPENDIX C DEVELOPMENT LAYOUT PLANS



|    | 2000 1000  | GENERAL KEY:   |   |  |  |  |
|----|--|--|---|--|--|--|
|    |  | YELLOW PAINTED DIRECT  | FIONAL ARROW  |  |  |  |
|    | Ġ.   | WHITE "SYMBOL OF ACCE<br>SQUARE 1200mm SQ. TO<br>AS1428.1                            | ESS" 900mm ON BLUE<br>COMPLY WITH                                     |  |  |  |
|    |  | PROPRIETARY WHEEL ST   | OPS   |  |  |  |
|    |  | BLACK CONCRETE TO DR<br>THRU ORDER STATION, A<br>5% BLACK OXIDE, BORAL               | IVE-THRU LANE, DRIVE<br>LL KERBS AND CHANNELS.<br>MINOX B100 OR EQUAL |  |  |  |
|    |  | BOUNDARY LINE  |   |  |  |  |
| VE | B  | BIN WITH CONCRETE BAS  | E   |  |  |  |
| NG | KR   | KERB RAMP  |   |  |  |  |
|    | Ο  | SAFETY BOLLARDS, REFE<br>EXTERNAL FINISHES SCH                                       | ER TO<br>EDULE  |  |  |  |
|    | _  | ILLUMINATED RED LIGHT  | BOX   |  |  |  |
|    |  | 1.2m HIGH PERFORATED SCREEN ALONG DRIVE<br>THRU, REFER TO EXTERNAL FINISHES SCHEDULE |   |  |  |  |
|    |  | 2m HIGH XF12 SLATTED S<br>EXTERNAL FINISHES SCH                                      | SCREENS, REFER TO<br>EDULE  |  |  |  |
|    |  | LANDSCAPE - REFER TO I   | ANDSCAPE DRAWINGS   |  |  |  |
|    | AREA SCHEDULE  |  |   |  |  |  |
|    | LOT SIZE:<br>GFA   |  | 1925m <sup>2</sup><br>244 m <sup>2</sup>                              |  |  |  |
|    | BIN ROOM<br>PLANT  |  | 18 m²<br>9 m²   |  |  |  |
|    | ACCESSIBLE PAR<br>CAR SPACES PRO<br>DELIVERY PARKIN<br>STAFF SPACES P<br>CUSTOMER WAIT | KING:<br>DVIDED:<br>NG:<br>ROVIDED:<br>ING SPACE:                                    | 1 SPACES<br>5 SPACES<br>2 SPACES<br>3 SPACES<br>2 SPACES              |  |  |  |
|    | TOTAL CAR PARKIN   | G  | 13 SPACES   |  |  |  |
|    | MOTORBIKE/EV SCC<br>BICYCLE PARKING  | OOTER PARKING  | 4 SPACES<br>4 SPACES  |  |  |  |
|    | GFA (GROSS FLOOF<br>FROM THE OUTSIDE   | R AREA FOR QLD) - MEASUR<br>OF EXTERNAL WALLS.                                       | RED   |  |  |  |
|    | NOTE 1:  |  |   |  |  |  |
|    | PAVEMENT LEVEL AT DRIV<br>FFL FOR EASE OF OPERA  | /E-THRU SERVICE WINDOW<br>TIONS  | /S TO MATCH INTERNAL  |  |  |  |
|    | NOTE: SITE PLAN IS DRAW<br>THIS IS ONLY CONCEPT D                                      | IN BASED ON CAD FROM O<br>ESIGN. CHECK SURVEY DR                                     | THERS.<br>AWINGS <b>N</b>   |  |  |  |

NOT FOR CONSTRUCTION



PROJECT HUNGRY JACK'S

#### ALBION

254-270 ABBOTSFORD ROAD BOWEN HILLS QLD 4006

# PROPOSED SITE & SIGNAGE LOCATION PLAN

PROJECT NO. 211106

DRAWING

SCALE As indicated@A3

DA01

DRAWING NO.

REV.



APPENDIX D VEHICLE SWEPT PATHS



| HICKEY OATLEY |                     |                 |      |                       |                 |  |  |  |
|---------------|---------------------|-----------------|------|-----------------------|-----------------|--|--|--|
|               | DATE:<br>20/07/2023 | SCALE:<br>1:200 | )@A3 | DRAWN:<br>CB          | APPROVED:<br>JG |  |  |  |
| J             | DRAWING NO. 23-114  | 4-001           | REV  | <sup>ЈОВ NO.</sup> 23 | 8-114           |  |  |  |



| Ì |                     |                 |      |                        |                 |  |  |  |  |  |
|---|---------------------|-----------------|------|------------------------|-----------------|--|--|--|--|--|
|   | DATE:<br>20/07/2023 | SCALE:<br>1:200 | )@A3 | DRAWN:<br>CB           | APPROVED:<br>JG |  |  |  |  |  |
| J | DRAWING NO. 23-114  | 4-002           | REV  | <sup>ЈОВ NO.</sup> 23- | -114            |  |  |  |  |  |



| HICKEY OATLEY |                     |                    |                          |              |                 |  |  |  |
|---------------|---------------------|--------------------|--------------------------|--------------|-----------------|--|--|--|
|               | DATE:<br>20/07/2023 | scale:<br>1:250@A3 |                          | DRAWN:<br>CB | APPROVED:<br>JG |  |  |  |
| J             | DRAWING NO. 23-114  | REV                | <sup>ЈОВ NO.</sup><br>23 | -114         |                 |  |  |  |



APPENDIX E TURNING MOVEMENT FORECASTS
































# **Stormwater Management Plan**

# SUPPORTING DOCUMENT





Ref. (22224)

PROPOSED COMMERICAL DEVELOPMENT 254 & 270 ABBOTSFORD ROAD, BOWEN HILLS

# STORMWATER MANAGEMENT PLAN REVISION 3



Prepared For HICKEY OATLEY PLANNING & DEVELOPMENT



PO Box 7214, Redland Bay Qld 4165 55-57 Jardine Dr, Redland Bay QLD Tel: (07) **3829 1399** Email: mail@hce-engineers.com.au Web: www.hce-engineers.com.au



## **REPORT CONTROL SHEET**

| HCE Ref. No.: | 22224                                  |
|---------------|--|
| Site:         | 254 & 270 Abbotsford Road, Bowen Hills |
| Report Title: | Stormwater Management Plan             |

| Rev No. | Date     | Written By | Reviewed By | Authorised<br>By | Signed |
|---------|----------|------------|-------------|------------------|--------|
| 3       | 20/07/23 | MB         | GH          | GH               |        |
|         |          |            |             |                  |        |
|         |          |            |             |                  |        |
|         |          |            |             |                  |        |

| DISTRIBUTION                         |          |                      |             |             |             |             |   |   |   |   |
|--------------------------------------|----------|----------------------|-------------|-------------|-------------|-------------|---|---|---|---|
| Destination                          | Date     | Date Revision Number |             |             |             |             |   |   |   |   |
| Destination                          | Sent     | Draft                | 0           | 1           | 2           | 3           | 4 | 5 | 6 | 7 |
| HCE - File                           | -        | $\boxtimes$          | $\boxtimes$ | $\boxtimes$ | $\boxtimes$ | $\boxtimes$ |   |   |   |   |
| Hickey Oatley Planning & Development | 17/01/23 | $\boxtimes$          |             |             |             |             |   |   |   |   |
| Hickey Oatley Planning & Development | 09/02/23 |                      | $\boxtimes$ |             |             |             |   |   |   |   |
| Hickey Oatley Planning & Development | 13/07/23 |                      |             | $\boxtimes$ |             |             |   |   |   |   |
| Hickey Oatley Planning & Development | 14/07/23 |                      |             |             | $\boxtimes$ |             |   |   |   |   |
| Hickey Oatley Planning & Development | 20/07/23 |                      |             |             |             | $\boxtimes$ |   |   |   |   |
|                                      |          |                      |             |             |             |             |   |   |   |   |
|                                      |          |                      |             |             |             |             |   |   |   |   |
|                                      |          |                      |             |             |             |             |   |   |   |   |



### **INDEX**

- 1. Introduction
- 2. Existing Site and Catchment Description
- 3. Water Quantity Management
- 4. Water Quality Management
- 5. Flooding
- 6. Conclusions
- Appendix A Flood Overlay Code

Appendix B – Coastal Hazard Overlay Code



#### 1. INTRODUCTION

HCE Engineers have been engaged to prepare a Stormwater Management Plan to accompany the development application for the commercial development at 254 & 270 Abbotsford Road, Bowen Hills.

This report identifies stormwater quality and quantity management measures that should be incorporated into the proposed site in order to satisfy Brisbane City Council's Planning Scheme Policy, the Queensland Urban Drainage Manual and items outlined in Economic Development Queensland's pre-lodgement meeting minutes dated 13<sup>th</sup> July 2022.

Information presented in this report should not be applied to properties or developments other than the subject development. No responsibility is accepted for use of any part of this report in any other context or for any other purposes or by any third party.

Revision 3 of this report has been created to reflect the updated site layout. Refer to drawing 22224-SK01.

#### 2. EXISTING SITE AND CATCHMENT DESCRIPTION

The site is bound by Abbotsford Road to the east, Taylor Street to the north, Hadwen Lane to the south and existing light industrial to the west. The site is currently developed with light industrial buildings, and generally falls towards Abbotsford Road.



Image 1: Site Location (image from Nearmap.com)



#### 3. WATER QUANTITY MANAGEMENT

Existing discharge from the site currently discharges to Abbotsford Road, Hadwen Lane and Taylor Street as surface flow. Existing surface contours indicate that surface flows are ultimately conveyed to the existing sag gully in Taylor Street.

It is proposed to capture and convey on site stormwater to the existing stormwater gully in Taylor Street as shown on concept design drawings in accordance with Brisbane City Councils Infrastructure Design Planning Scheme Policy.

The site is currently developed with light industrial buildings and hardstand areas with a fraction impervious of between 90-100%. The proposed development is expected to have an impervious area of 80% per the architectural drawings. The proposed reduction in impervious area is expected to reduce the total peak discharge from the proposed development site.

The capture and conveyance of runoff from the proposed development to the existing stormwater network will reduce surface flow to Hadwen Lane, Abbotsford Road and Taylor Street. This reduction of surface flow to the existing road network will reduce any nuisance ponding that may occur in the existing road network.

As the development will reduce peak flows, and discharge to existing stormwater drainage under control of the local authority, the discharge to the existing stormwater infrastructure in Taylor Street is considered lawful per Section 3.9.1 of the Queensland Urban Drainage Manual.

#### 4. WATER QUALITY MANAGEMENT

The State Planning Policy (SPP) requires on site treatment to comply with the Water Quality Objectives where the development site is:

- a. a material change of use for an urban purpose which involves greater than 2,500m<sup>2</sup> of land that:
  - i. will result in an impervious area greater than 25% of the net developable area; or
  - ii. will result in 6 or more dwellings.
- b. reconfiguring a lot for an urban purpose that involves greater than 2,500m<sup>2</sup> of land and will result in 6 or more lots;
- c. operational work for an urban purpose which involves disturbing greater than 2,500m<sup>2</sup> of land.

The site has a development area of 1875m2, and therefore is not required to meet the Water Quality Objectives outlined in the SPP.

Water quality treatment on site is to be undertaken by implementation of best management practices. It is proposed to install gross pollutant traps on all inlets within carparking areas to capture pollutants prior to discharge. Refer to concept design drawings for additional information.



#### 5. <u>FLOODING</u>

Review of Brisbane City Plan 2014 indicates the site is subject to the Brisbane River Flood Planning Area sub-categories 4 and 5, and the Creek/waterway Flood Planning Area sub-category 5. The site is also in the Costal Hazard Overlay, medium storm-site inundation area sub-category.

As outlined in Economic Development Queensland's Pre-lodgement meeting minutes dated 13<sup>th</sup> July 2022, the minimum floor level for the development is to be 3.0m AHD, with essential electrical services being raised to 3.50m AHD.

It is proposed the minimum floor level for the proposed building is 3.50m AHD, meeting the requirements of Brisbane City Councils Flood Overlay Code.

Code Response to Councils Flood Overlay Code and Coastal Hazard Overlay Code are attached as appendices.

#### 6. <u>CONCLUSIONS</u>

The proposed commercial development at 254 & 270 Abbotsford Road, Bowen Hills can lawfully discharge stormwater to the existing stormwater drainage in Taylor Street in accordance with the concept design drawings.

The development of the site will reduce the overall impervious area of the development site, ensuing peak flow is reduced, and the development will cause actionable nuisance to surrounding properties or the existing road network.

A best management approach to stormwater quality treatment is proposed, and new stormwater drainage inlets are to be fitted with Gross Pollutant Traps to reduce contaminants discharging into receiving waterways.

It is proposed the minimum floor level for the proposed building is 3.50m AHD, meeting the requirements of Brisbane City Councils Flood Overlay Code.



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| LEVELS AMENDED | 20/07/23  | Drawing No.                   |             |                   |        | Rev.        |
|                |           |                               | 222         | 224-SK01          |        | I E I       |



#### APPENDIX A – FLOOD OVERLAY CODE

#### 8.2.11 Flood overlay code

#### 8.2.11.1

#### Application

- 1. This code applies to assessing development in the Flood overlay, if:
  - a. accepted development subject to compliance with identified requirements, where acceptable outcomes of this code are identified requirements in a table of assessment for an overlay (section 5.10); or
  - b. assessable development where this code is an applicable code identified in the assessment benchmarks column of a table of assessment for an overlay (section 5.10); or
  - c. impact assessable development.
- 2. Land in the Flood overlay is identified on the Flood overlay map and is included in the following sub-categories:
  - a. Brisbane River flood planning area 1 sub-category;
  - b. Brisbane River flood planning area 2a sub-category;
  - c. Brisbane River flood planning area 2b sub-category;
  - d. Brisbane River flood planning area 3 sub-category;
  - e. Brisbane River flood planning area 4 sub-category;
  - f. Brisbane River flood planning area 5 sub-category;
  - g. Creek/waterway flood planning area 1 sub-category;
  - h. Creek/waterway flood planning area 2 sub-category;
  - i. Creek/waterway flood planning area 3 sub-category;
  - j. Creek/waterway flood planning area 4 sub-category;
  - k. Creek/waterway flood planning area 5 sub-category;
  - I. Overland flow flood planning area sub-category.

Editor's note—For the purposes of the overlay, the Pine and South Pine rivers are treated as Creek/waterway flood planning area sub-categories.

Note—The Flood overlay is a 'natural hazard area' for the purpose of the State Planning Policy. Within this area, susceptibility to flooding has been identified. The natural hazard area identified on the Flood overlay map may not reflect the full extent of the flood affected area.

3. When using this code, reference should be made to section 1.5 and section 5.3.3.

Note—The following purpose, overall outcomes, performance outcomes and acceptable outcomes comprise the assessment benchmarks of this code.

Note—Where this code includes performance outcomes or acceptable outcomes that relate to:

- management of flood hazard or hydraulic hazard, guidance is provided in the Flood planning scheme policy;
- filling or excavation within the Creek/waterway flood planning area sub-categories, guidance is provided in the Compensatory earthworks planning scheme policy;
- handling or storage of hazardous materials, guidance is provided in the Management of hazardous chemicals in flood affected areas planning scheme policy;
- standards and specifications for public assets in a park, guidance is provided in the Infrastructure design planning scheme policy;
- standards and specifications for stormwater drainage assets, guidance is provided in the Infrastructure design planning scheme policy.

Editor's note—For a proposal to be accepted development subject to compliance with identified requirements, it must meet all the identified acceptable outcomes of this code that relate to the applicable sub-category

Page 1 of 28 Print Date: 08/12/2022 cityplan.brisbane.qld.gov.au and any other applicable code. Where it does not meet all identified acceptable outcomes, the proposal becomes assessable development and a development application is required. Where a development application is required, only the specific acceptable outcomes that the proposal fails to meet need to be assessed against the corresponding assessable acceptable outcomes or performance outcomes and relevant overall outcomes. Other identified acceptable outcomes that are met are not assessed as part of the development application.

#### 8.2.11.2

#### Purpose

- 1. The purpose of the Flood overlay code is to:
  - a. Implement the policy direction in the Strategic framework, in particular:
    - i. Theme 2: Brisbane's outstanding lifestyle, and Element 2.3 Brisbane's healthy and safe communities;
    - ii. Theme 4: Brisbane's highly effective transport and infrastructure networks, and Element 4.3 Brisbane's coordinated infrastructure planning and delivery.
  - b. Provide for the assessment of the suitability of development in the Flood overlay.
- 2. The purpose of the Flood overlay code will be achieved through the following overall outcomes:
  - a. Development minimises exposure of people and property to unacceptable risk from flood hazard in all flood events.
  - b. Development and infrastructure mitigates the flood risk through its location, siting, design, construction and operation whilst maintaining amenity.
  - c. Development does not unduly burden the city's counter-disaster response capacity, including emergency services access during a flood emergency.
  - d. Development provides for efficient evacuation and access for evacuation resources including emergency services during flood events, or otherwise plans for the prospect and impact of isolation or hindered evacuation during flooding.
  - e. Development involving essential community infrastructure remains functional during and immediately after flood events.
  - f. Development ensures that emergency management plans respond to the number and capacity of future users of the development to safely participate in emergency measures such as evacuation.
  - g. Development ensures that essential building services or services essential for the development are designed, located and operated to minimise the flood risk to people, minimise damage to property, disruption to building function, and re-establishment time after a flood event.
  - h. Development involving hazardous materials manufactured, handled or stored in bulk does not adversely impact on public safety and the environment as a result of the impacts of floodwater.
  - i. Development does not, directly or cumulatively, cause or increase adverse impacts on other properties or land within the floodplain from flooding.
  - j. Development and infrastructure mitigates the impacts of hydraulic hazard due to predictable future increases in rainfall intensity on flooding.
  - k. Development prioritises, in order, the safety of people, protection of public infrastructure and protection of private property, in the management of the economic, social and environmental impacts of flooding.

#### 8.2.11.3 Performance outcomes and acceptable outcomes

#### Table 8.2.11.3.A—Performance outcomes and acceptable outcomes

| Performance outcomes                                 | Acceptable outcomes | Comments |
|--|---------------------|----------|
| Section A—If for accepted development subject to con |                     |          |

| outcomes only) or assessable development for a dwel<br>Note—Development for a dwelling house does not require assessment a   |  |                                     |
|--|--|-------------------------------------|
| <ul> <li>PO1</li> <li>Development involving any habitable or non-habitable part of a dwelling house, including any secondary dwelling, is located and designed to: <ul> <li>a. minimise the risk to people from flood hazard;</li> <li>b. achieve acceptable flood immunity;</li> <li>c. minimise property impacts from a flood event up to and including the defined flood event;</li> <li>d. minimise disruption to residents, recovery time and rebuilding or restoration costs after a flood event up to and including the defined flood event.</li> </ul> </li> </ul> | <ul> <li>AO1.1</li> <li>Development for a dwelling house including any secondary dwelling: <ul> <li>a. is not located in the Brisbane River flood planning area 1, 2a or 2b sub-categories or the Creek/waterway flood planning area 1 or 2 sub-categories; or</li> <li>b. is only located in these sub-categories, if a Registered Professional Engineer Queensland certifies that the dwelling house and any secondary dwelling are structurally designed to be able to resist hydrostatic and hydrodynamic loads associated with flooding up to and including the defined flood event.</li> </ul> </li> </ul> | Not applicable to this development. |
|  | AO1.2<br>Development for a dwelling house and any secondary<br>dwelling complies with the minimum flood planning levels<br>in Table 8.2.11.3.B.<br>Note—If located in an area that has no flood level information available<br>from the Council such as an overland flow path, a Registered<br>Professional Engineer of Queensland with expertise in undertaking<br>flood studies is to certify that the flood level and development levels for<br>the dwelling house and any secondary dwelling achieve the required<br>flood planning levels in Table 8.2.11.3.B.  |                                     |
|  | AO1.3<br>Development involving a building undercroft complies<br>with the minimum clearance requirements in Table<br>8.2.11.3.E.<br>Editor's note—For creek/waterway, storm-tide and river flooding,<br>applicable flood planning information is available from Council's<br>FloodWise Property Report.<br>Note—The Flood planning scheme policy provides guidance on<br>undercroft design.  |                                     |

| <ul> <li>PO2 Development within the Creek/waterway flood planning area sub-categories or Overland flow flood planning area sub-category: <ul> <li>a. maintains the conveyance of flood waters to allow flow and debris to pass predominantly unimpeded through the site;</li> <li>b. does not concentrate, intensify or divert floodwater onto upstream, downstream or adjacent properties;</li> <li>c. will not result in a material increase in flood levels or flood hazard on upstream, downstream or adjacent properties.</li> </ul> </li> </ul> | <ul> <li>AO2</li> <li>Development: <ul> <li>a. is not located within the Creek/waterway flood planning area 1, 2 or 3 sub-categories or the Overland flow flood planning area sub-category; or</li> <li>b. provides an open undercroft area from natural ground level to habitable floor level for any area inundated by the defined flood event; or</li> </ul> </li> <li>Note—This undercroft area is not suitable for providing non-habitable rooms, secure storage of valuables, or future enclosing for storage or car parking. The clear area may include structural elements such as columns and floor substructure. The Flood planning scheme policy provides guidance on undercroft design.</li> <li>Editor's note—An open undercroft design may be achieved through a 'valance' treatment around the perimeter of an otherwise internally clear undercroft.</li> <li>Editor's note—For Creek/waterway, storm-tide and river flooding, applicable flood planning information is available from Council's FloodWise Property Report.</li> <li>c. a report from a Registered Professional Engineer Queensland certifies that the development in the Creek/waterway flood planning area or Overland flow flood planning area sub-categories will not result in a material increase in flood level or flood hazard on upstream, downstream or adjacent properties.</li> <li>Note—Flood studies demonstrate that the development and engineering design methods conform to the principles within the Flood planning scheme policy.</li> </ul> | Not applicable to this development.  |
|---|--|--|
| Section B—If accepted development subject to compli-<br>outcomes only) or assessable development other than<br>Note—If development that is accepted development subject to compliand<br>this part, no further assessment against this code is required.   | ance with identified requirements (acceptable<br>for a dwelling house or reconfiguring a lot<br>with identified requirements complies with the acceptable outcomes of  |  |
| PO3<br>Development:<br>a. is compatible with flood hazard in a defined flood<br>event;  | <b>AO3</b><br>Development for a material change of use is identified in<br>Table 8.2.11.3.C as compatible with the flood hazard in<br>the relevant flood planning area.  | The Acceptable Outcome can be and is proposed to be met, as identified on the accompanying drawings. |

Page 4 of 28 Print Date: 08/12/2022 cityplan.brisbane.qld.gov.au

| <ul> <li>b. minimises the risk to people from flood hazard;</li> <li>c. does not reduce the ability of evacuation resources including emergency services to access and evacuate the site in a flood emergency, with consideration to the scale of the development;</li> <li>d. minimises impacts on property from flooding;</li> <li>e. minimises disruption to residents, business or site operations and recovery time due to flooding;</li> <li>f. minimises the need to rebuild structures after a flood event greater than the defined flood event.</li> <li>Note—Where Table 8.2.11.3.C identifies that a flood risk assessment is required, compliance with this performance outcome can be achieved by submitting a flood risk assessment, which may be included within a flood study, addressing the criteria within this performance solution.</li> <li>Preparing flood risk assessments and flood studies is required to be in accordance with the Flood planning scheme policy.</li> <li>Note—An emergency management plan prepared in accordance with the Flood planning scheme policy, which sets out procedures for evacuation due to flooding may be used to demonstrate compliance with this performance outcome.</li> </ul> |   |  |
|---|---|--|
| <ul> <li>PO4</li> <li>Development for a park ensures that the design of a park and location of structures and facilities responds to the flood hazard and balances the safety of intended users with: <ul> <li>a. maintaining continuity of operations;</li> <li>b. impacts of flooding on asset life and ongoing maintenance costs;</li> <li>c. efficient recovery after flood events;</li> <li>d. recreational benefits to the city;</li> <li>e. availability of suitable land within the park.</li> </ul> </li> </ul>  | <ul> <li>AO4.1 Development involving a building or structure in a park complies with the flood planning levels specified in Table 8.2.11.3.D.</li> <li>AO4.2 Development involving a building or structure in a park where Table 8.2.11.3.D does not apply: <ul> <li>a. is not located within the 20% AEP flood extent of any creek/waterway or overland flow path; or</li> <li>b. is located above the 20% AEP flood level of any creek/waterway or overland flow path.</li> </ul> </li> </ul> | Not applicable to this development.  |
| Section C—If for assessable development other than f  |   |  |
| PO5<br>Development is located and designed to:<br>a. minimise the risk to people from flood hazard on the   | AO5.1<br>Development complies with the flood planning levels<br>specified in Table 8.2.11.3.D.  | The Acceptable Outcome can be and is proposed to be met, as identified on the accompanying drawings. |

| <ul> <li>site;</li> <li>b. minimise flood damage to the development and contents of buildings up to the defined flood event;</li> <li>c. provide suitable amenity;</li> <li>d. minimise disruption to residents, recovery time and the need to rebuild structures after a flood event up to and including the defined flood event.</li> </ul> | <ul> <li>Note—If located in an area with no Council-derived flood levels such as an overland flow path, a Registered Professional Engineer Queensland with expertise in undertaking flood studies is to derive the applicable flood level and certify that the development meets the required flood planning levels in Table 8.2.11.3.D. The study is to demonstrate that the development and engineering design methods conform to the principles within the Flood planning scheme policy and the Infrastructure design planning scheme policy.</li> <li>AO5.2</li> <li>Development is: <ul> <li>a. not located in the:</li> <li>i. Brisbane River flood planning area 1, 2a, or 2b sub-categories;</li> <li>ii. Creek/waterway flood planning area 1 or 2 sub-categories;</li> <li>iii. Overland flow flood planning area sub-category; or</li> </ul> </li> <li>b. only located in these sub-categories if a Registered Professional Engineer Queensland with expertise in undertaking flood studies certifies that: <ul> <li>i. the development design, siting and any mitigation measures will ensure the development is structurally adequate to resist hydrostatic, hydrodynamic and debris impact loads associated with flooding up to the defined flood event; and</li> <li>ii. the risk to people is managed to an acceptable level.</li> </ul> </li> </ul> |  |
|---|--|--|
| <b>PO6</b><br>Development involving essential electrical services or a<br>basement storage area is suitably located and designed<br>to ensure public safety and minimise flood recovery and<br>economic consequences of damage during a flood.  | <ul> <li>AO6.1</li> <li>Development ensures that: <ul> <li>a. all areas containing essential electrical services comply with the flood planning levels in Table 8.2.11.3.D; or</li> <li>b. if a basement contains essential electrical services or a private basement storage area, the basement is a waterproof structure with walls and floors</li> </ul> </li> </ul>  | The Acceptable Outcome can be and is proposed to be met, as identified on the accompanying drawings. |

|  | <ul> <li>impermeable to the passage of water with all entry points and services located at or above the relevant flood planning level in Table 8.2.11.3.D.</li> <li>Note—A basement storage area does not include a bike storage room, change room, building maintenance storage and non-critical electrical services.</li> <li>AO6.2</li> <li>Development involving a basement that relies on a pumping solution to manage floodwater ingress or for dewatering after a flood provides a secondary pump system with a backup power source for the pump.</li> </ul>   |  |
|--|---|--|
| PO7<br>Development does not directly or indirectly create a<br>material adverse impact on flood behaviour or drainage<br>on properties that are upstream, downstream or adjacen<br>to the development. | <ul> <li>A07.1</li> <li>Development: <ul> <li>a. does not block, or divert floodwaters for any area affected by creek/waterway or overland flow flooding, excluding storm-tide flooding and Brisbane River flooding sources; or</li> <li>b. does not result in a material increase in flood level or hydraulic hazard on upstream, downstream or adjacent properties.</li> </ul> </li> <li>Note—Compliance with this acceptable solution can be demonstrated by the submission of a flood study by a Registered Professional Engineer of Queensland with expertise in undertaking flood studies demonstrating that the development and engineering design methods conform to the principles within the Flood planning scheme policy and the Infrastructure design planning scheme policy.</li> <li>A07.2</li> <li>Development retains existing overland flow paths and does not rely wholly on piped solutions to manage major</li> </ul> | The Acceptable Outcome can be and is proposed to be met, as identified on the accompanying drawings. |
|  | flows.<br><b>A07.3</b><br>Development which creates a new overland flow path or<br>significantly modifies an existing overland flow path via<br>earthworks does not materially worsen hydraulic hazard<br>on the site from existing conditions.   |  |

| PO8<br>Development for filling or excavation in an area affected<br>by creek/waterway flooding does not directly, indirectly or<br>cumulatively cause any material increase in flooding or<br>hydraulic hazard or involve significant redistribution of<br>flood storage from high to lower areas in the floodplain.<br>Note—This can be demonstrated by undertaking earthworks in<br>compliance with the Compensatory earthworks planning scheme policy.   | Note—Compliance with this acceptable solution can be demonstrated<br>by the submission of a flood study by a Registered Professional<br>Engineer of Queensland with expertise in undertaking flood studies<br>demonstrating that the development and engineering design methods<br>conform to the principles within the Flood planning scheme policy and<br>the Infrastructure design planning scheme policy.<br><b>AO8</b><br>Development ensures that no filling or excavation greater<br>than 100mm is located in the Creek/waterway flood<br>planning area 1, 2 or 3 sub-categories if contained in the<br>5% AEP flood extent of any Creek/waterway flood<br>planning area sub-category for which no waterway<br>corridor has been mapped in the Waterway corridors<br>overlay.  | The Acceptable Outcome can be and is proposed to be met, as identified on the accompanying drawings. |
|---|---|--|
| dwelling house and any secondary dwelling which involves filling or<br>excavation, whether or not the development application comprises a<br>separate development application for operational work involving filling<br>or excavation.  |   |  |
| <ul> <li>PO9</li> <li>Development ensures that the building and site design: <ul> <li>a. maintains the conveyance capacity of existing overland flow paths and creek/waterways;</li> <li>b. ensures floodwaters and flood debris can pass predominantly unimpeded under a structure or building to minimise property or building damage, including for a flood larger than the defined flood event;</li> <li>c. mitigates flood impacts by ensuring that filling, excavation and location of services are designed to allow for the conveyance of floodwater across the site.</li> </ul> </li> <li>Note—The Flood planning scheme policy provides guidance on relevant considerations in determining minimum undercroft clearances and treatment of ground level in undercroft areas where floodwater conveyance is required underneath development.</li> </ul> | <ul> <li>AO9.1 Development involving a building undercroft in the Creek/waterway flood planning area sub-categories or the Overland flow flood planning area sub-category: <ul> <li>a. complies with the minimum building undercroft clearance requirements in Table 8.2.11.3.E;</li> <li>b. not located directly above any part of a waterway corridor as mapped in the Waterway corridors overlay.</li> </ul> </li> <li>AO9.2 Development involving a building undercroft in the Creek/waterway flood planning area sub-categories or the Overland flow flood planning area sub category: <ul> <li>a. has a ground level within the undercroft area that is free draining;</li> <li>b. does not involve excavation below ground level of more than 300mm within the undercroft area.</li> </ul> </li> </ul> | Not applicable to this development.  |

| <ul> <li>PO10 Development for vulnerable uses, difficult to evacuate uses or assembly uses optimises vehicular access and efficient evacuation from the development to parts of the road network unaffected by flood hazard, in order to: <ul> <li>a. protect safety of users and emergency services personnel;</li> <li>b. support efficient emergency services access and site evacuation with consideration to the scale of development.</li> </ul> </li> <li>Note—A flood risk assessment may be required to address the performance outcomes or acceptable solutions which deal with evacuation and isolation arrangements, and the ability to take refuge. The Flood planning scheme policy provides information for undertaking flood risk assessments.</li> </ul> | <ul> <li>AO10</li> <li>Development for vulnerable uses, difficult to evacuate uses or assembly uses: <ul> <li>a. is not isolated in any event up to the relevant flood planning level specified in Table 8.2.11.3.L; or</li> <li>b. has direct vehicle access to a critical route or interim critical route in the Critical infrastructure and movement network overlay for evacuation in a flood; or</li> <li>c. can achieve vehicular evacuation to a suitable flood-free location.</li> </ul> </li> <li>Note—A suitable flood-free location is of a size and nature sufficient to provide for the size and characteristics of the population likely to need evacuation to that area.</li> </ul>                               | Not applicable to this development.   |
|---|--|---|
| PO11<br>Development has access which, having regard to<br>hydraulic hazard, provides for safe vehicular and<br>pedestrian movement and emergency services access to<br>adjoining roads.   | <ul> <li>AO11.1 Development provides an access or driveway into the site which is: <ul> <li>a. trafficable during the defined flood event;</li> <li>b. not located in the Creek/waterway flood planning area 1 sub-category;</li> <li>c. not located in the Overland flow flood planning area sub-category if the hydraulic hazard is unsafe in the defined flood event;</li> <li>d. the access or driveway is not inundated by a 10% AEP flood.</li> </ul> </li> <li>AO11.2 Development located in the Creek/waterway flood planning area 1, 2, 3 or 4 sub-categories locates any disabled access in the highest part of the site. Note—explanation of hydraulic hazard provided in the Flood planning scheme policy.</li></ul> | The Acceptable Outcome can be and is proposed to<br>be met, as identified on the accompanying drawings. |
| <b>PO12</b><br>Development involving a new road, a bridge or culvert is designed to minimise impacts to flood behaviour,  | <b>AO12</b><br>Development involving a new road complies with the<br>flood planning levels in Table 8.2.11.3.F.  | Not applicable to this development.   |

| minimise disruption to traffic during a flood and allow for emergency access.  |  |                                     |
|--|--|-------------------------------------|
| <ul> <li>PO13</li> <li>Development for pedestrian and cyclist paths: <ul> <li>a. provides a suitable level of trafficability;</li> <li>b. manages the impacts of flooding on asset life and ongoing maintenance costs;</li> <li>c. balances route availability with recreational and transport connectivity benefits to the city.</li> </ul> </li> </ul> | AO13.1<br>Development for cyclist and pedestrian facilities other<br>than on public roads, including those traversing through a<br>park and adjacent to a watercourse and overland flow<br>path, are located above the 39% AEP (2 year ARI) flood<br>immunity from all flooding sources.<br>Note—If the site is subject to more than one type of flooding, the<br>requirement that affords the greatest level of protection will apply.            | Not applicable to this development. |
|  | <b>AO13.2</b><br>All new on-road cyclist and pedestrian facilities comply<br>with the flood planning levels and trafficability standards<br>for the applicable category of road in Table 8.2.11.3.F or<br>Table 8.2.11.3.K.  |                                     |
| <b>PO14</b><br>Development which increases the residential population<br>within the Brisbane River flood planning area sub-<br>categories minimises the risk to people in all flood events<br>with consideration to flood hazard, including warning<br>time.   | AO14<br>Development in the Brisbane River flood planning area<br>sub-categories in areas where the residential flood level<br>is greater than 12.8m AHD involving:<br>a. an increase in the number of residential dwellings;<br>or<br>b. additional residential lots<br>is not subject to an unsafe hydraulic hazard in the 0.2%<br>AEP flood event.<br>Note—Explanation of a hydraulic hazard is provided in the Flood<br>planning scheme policy. | Not applicable to this development. |
| Additional performance outcomes and acceptable out   | comes for essential community infrastructure   |                                     |
| <ul> <li>PO15</li> <li>Development involving essential community infrastructure:</li> <li>a. remains functional to serve community need during and immediately after a flood event, or is part of a network that is able to maintain the function of the</li> </ul>  | <ul> <li>AO15</li> <li>Development involving essential community infrastructure: <ul> <li>a. is ancillary to and not relied upon for the provision of the essential service during a flood; or</li> <li>b. is located above the flood planning levels in Table</li> </ul> </li> </ul>  | Not applicable to this development. |

| <ul> <li>essential community infrastructure when parts of the development are unable to function during or after a flood;</li> <li>b. is designed, sited and operated to avoid adverse impacts on the community or the environment due to the impacts of flooding on infrastructure, facilities or access and egress routes;</li> <li>c. is able to remain functional or is part of a network which is able to remain functional even when other infrastructure or services (such as electricity supply) may be compromised in a flood event;</li> <li>d. contains mitigation measures which are not entirely dependent on human activation to respond to a flood event.</li> <li>Note—Protection of function is required up to and including the flood event in Table 8.2.11.3.G.</li> </ul> | <ul> <li>8.2.11.3.G;</li> <li>c. has access to or provides the necessary back-up emergency electricity and communications supply in times of flood;</li> <li>d. is designed and constructed to resist hydrostatic and hydrodynamic forces as a result of inundation by the flood event listed for the development type in Table 8.2.11.3.G;</li> <li>e. that services a local area: <ul> <li>i. is able to be accessed in times of flood to service local community needs up to the event listed for that development type in Table 8.2.11.3.G; or</li> <li>ii. has a service continuity plan that demonstrates the continued provision of service during the relevant flood event.</li> </ul> </li> </ul>                    |                                     |
|---|---|-------------------------------------|
| <ul> <li>PO16</li> <li>Development involving the storage and handling of hazardous materials avoids or minimises risks to public health and safety and the environment, by: <ul> <li>a. protecting underground tanks for hazardous materials against the forces of buoyancy, velocity flow and debris impacts;</li> <li>b. securing above-ground tanks for hazardous materials against flotation and lateral movement;</li> <li>c. preventing damage to hazardous materials pipework or entry of floodwater into hazardous materials pipework;</li> <li>d. preventing damage to or off-site release of packages, drums or containers storing hazardous materials.</li> </ul> </li> </ul>  | <ul> <li>AO16 <ul> <li>a. Development does not include the storage or handling of hazardous chemicals that exceed the hazardous chemicals flood hazard threshold quantities in Table 8.2.11.3.M.</li> <li>b. Development involving the processes listed in Table 8.2.11.3.H: <ul> <li>i. where located in the Flood overlay area, occurs only in the Creek/waterway flood planning area 5 sub-category or the Brisbane River flood planning area 5 sub-category; or</li> <li>ii. is consistent with the standards contained in the Management of hazardous chemicals in flood affected areas planning scheme policy and can operate without risk of environmental harm during a flood event.</li> </ul> </li> </ul></li></ul> | Not applicable to this development. |

| planning scheme policy can assist in demonstrating achievement of this performance outcome.<br>Note—A pump drainage system is not an acceptable measure to meet the performance outcome.  | Note—The Management of hazardous chemicals in flood affected<br>areas planning scheme policy sets out further information and<br>processes including risk assessment for the management of hazardous<br>chemicals in flood planning areas.   |                                     |
|---|--|-------------------------------------|
| Additional performance outcomes and acceptable out  | comes for reconfiguring a lot  |                                     |
| <ul> <li>PO17 Development locates and designs all lots resulting from reconfiguring a lot to: <ul> <li>a. minimise the risk to people from flood hazard;</li> <li>b. minimise damage to property from flood hazard;</li> <li>c. facilitate safe and efficient evacuation.</li> </ul> </li> <li>Note— <ul> <li>Consideration of all floods up to the probable maximum flood is relevant to minimising the risk to people.</li> </ul> </li> <li>Flood warning time is not considered sufficient in the Creek/waterway planning area sub-categories or the Overland flow flood planning area sub-category.</li> <li>Filling above the flood planning level for a flood event greater than the defined flood event cannot be assumed to mitigate the flood hazard.</li> </ul> | <ul> <li>AO17.1         Development creating new lots is identified in Table 8.2.11.3.1 as suitable within the relevant flood planning area.     </li> <li>AO17.2         Development provides for reconfiguring a lot design that achieves a road and lot layout which:         <ul> <li>a. provides trafficable vehicular egress for evacuation during a defined flood event;</li> <li>b. optimises hazard-free movement away from sources of flood hazard within the development.</li> </ul> </li> <li>Note—Further advice on road and lot layout is contained in the Flood planning scheme policy.</li> <li>AO17.3         Development which creates a new residential lot in an area subject to Brisbane River flooding, if the residential     </li> </ul> | Not applicable to this development. |
|   | flood level is greater than 12.8m AHD is not subject to a<br>hydraulic hazard greater than 0.6m <sup>2</sup> /s DV or 0.6m deep<br>in a 0.2% AEP flood.<br>Note—Refer to the Flood planning scheme policy for further explanation<br>on the 0.2% AEP flood.  |                                     |
| <ul> <li>PO18</li> <li>Development involving reconfiguring a lot: <ul> <li>a. minimises the risk to people from flood hazard;</li> <li>b. creates safe evacuation routes or avoids isolation of the development during a flood greater than the defined flood event;</li> <li>c. minimises damage to property and services;</li> </ul> </li> </ul>  | <ul> <li>AO18.1 Development involving reconfiguring a lot ensures: <ul> <li>a. all lots comply with the flood planning levels in Table 8.2.11.3.J;</li> <li>b. a new road complies with the flood planning levels in Table 8.2.11.3.F.</li> </ul> </li> <li>AO18.2</li> </ul>  | Not applicable to this development. |

| <ul> <li>d. provides lots and roads that are not frequently flooded or subject to nuisance ponding or seepage;</li> <li>e. ensures lots created for park or private open space minimise the risk to people from flood hazard and are fit for purpose;</li> <li>f. provides a lot that is not substantially burdened by flood mitigation infrastructure.</li> </ul> | Development involving reconfiguring a lot creating more<br>than 6 residential lots or a lot for industry ensures the<br>flood planning levels of a dedicated road fronting the<br>development or providing primary access within 200m of<br>the development:<br>a. complies with Table 8.2.11.3.K; or<br>b. has acceptable trafficability in accordance with the<br>requirements in the Flood planning scheme policy<br>and the Queensland Urban Drainage Manual.<br>Note—The Flood planning scheme policy contains supporting<br>information about trafficability on existing roads and serviceability<br>during floods. |  |
|--|---|--|
|  | <ul> <li>AO18.3</li> <li>Development protects the conveyance of flood hazard area by providing an easement over the:</li> <li>a. 2% AEP flood extent for overland flow flooding;</li> <li>b. 1% AEP flood extent for creek/waterway flooding.</li> </ul>  |  |

#### Table 8.2.11.3.B—Flood planning levels for a dwelling house (BCA building classification 1a)

| Flooding<br>source | Minimum habitable floor level |  | Minimum non-habitable floor level (i.e. utility areas, garage, laundry, storage room and basement entries)  |                            |  |  |  |  |
|--------------------|-------------------------------|--|---|----------------------------|--|--|--|--|
| Brisbane River     |                               | RFL + 500mm  |   | 2% AEP flood level + 300mm |  |  |  |  |
| Creek/<br>waterway |                               | 1% AEP flood level + 500mm   | 1   | 1% AEP flood level + 300mm |  |  |  |  |
| Overland flow      |                               | 2% AEP flood level + 500mm   | 1   | 2% AEP level + 300mm       |  |  |  |  |
|                    |                               | Note—Where no detailed flood leve<br>Queensland with expertise in flood s<br>including any secondary dwelling, m | Where no detailed flood level information is available from the Council such as an overland flow path, a Registered Professional Engineer<br>Jeensland with expertise in flood studies is to derive the relevant flood level and certify that the development level for the dwelling house,<br>cluding any secondary dwelling, meets the required flood immunity standards. |                            |  |  |  |  |

Note—

• Where the site is subject to more than one flooding source, the minimum flood planning level is the highest level determined from these flooding sources.

• Flood planning levels for a dwelling house from storm-tide inundation are located in the Coastal hazard overlay code.

• A flood event with an AEP of 1% is the equivalent of a 100 year ARI flood event.

Page 13 of 28 Print Date: 08/12/2022 cityplan.brisbane.qld.gov.au • A flood event with an AEP of 2% is the equivalent of a 50 year ARI flood event.

#### Table 8.2.11.3.C—Land use compatibility with flood hazard

C – Land use is compatible with the flood hazard subject to meeting all other relevant requirements.

# – Flood risk assessment in accordance with requirements of the Flood planning scheme policy is required to demonstrate the use is compatible with the flood hazard.

| Accommodation<br>activities     | Brisbane River<br>flood planning area<br>sub-category |   |   |    |    |   |   | Creek/waterway<br>flood planning area<br>sub-category |   |   |   |   |
|---------------------------------|---|---|---|----|----|---|---|---|---|---|---|---|
|                                 | 5   | 4 | 3 | 2B | 2A | 1 | 5 | 4   | 3 | 2 | 1 |   |
| Community residence             | С   | # | # | #  | #  | # | С | #   | # | # | # | # |
| Dual occupancy                  | С   | С | # | #  | #  | # | С | #   | # | # | # | С |
| Dwelling unit                   | С   | С | # | #  | #  | # | С | #   | # | # | # | С |
| Multiple dwelling (1–3 storeys) | С   | С | # | #  | #  | # | С | #   | # | # | # | С |
| Multiple dwelling (4+ storeys)  | С   | С | С | #  | #  | # | С | #   | # | # | # | С |
| Nature-based tourism            | С   | С | С | #  | #  | # | С | #   | # | # | # | С |
| Relocatable home park           | С   | # | # | #  | #  | # | С | #   | # | # | # | С |
| Residential care facility       | #   | # | # | #  | #  | # | # | #   | # | # | # | # |
| Resort complex                  | С   | С | С | #  | #  | # | С | #   | # | # | # | С |
| Retirement facility             | С   | # | # | #  | #  | # | # | #   | # | # | # | С |
| Rooming                         | С   | С | # | #  | #  | # | С | #   | # | # | # | С |

Page 14 of 28 Print Date: 08/12/2022 cityplan.brisbane.qld.gov.au

| accommodation,<br>short-term<br>accommodation or<br>hotel where including<br>accommodation (1–3<br>storeys)           |   |                           |   |    |    |   |   |   |   |   |   |   |
|---|---|---------------------------|---|----|----|---|---|---|---|---|---|---|
| Rooming<br>accommodation,<br>short-term<br>accommodation or<br>hotel where including<br>accommodation (4+<br>storeys) | С                                       | С                         | С | #  | #  | # | С   | # | # | # | # | C   |
| Tourist park  | С                                       | С                         | # | #  | #  | # | С   | С | # | # | # | С   |
| Commercial land<br>uses   | Brisbane F<br>flood planı<br>sub-catego | River<br>ning area<br>ory |   |    |    |   | Creek/waterway<br>flood planning area<br>sub-category |   |   |   |   | Overland<br>flow flood<br>planning<br>area sub-<br>category |
|   | 5                                       | 4                         | 3 | 2B | 2A | 1 | 5   | 4 | 3 | 2 | 1 |   |
| Agricultural supplies store   | С                                       | С                         | # | #  | #  | # | С   | # | # | # | # | С   |
| Animal husbandry  | С                                       | С                         | # | #  | #  | # | С   | # | # | # | # | С   |
| Animal keeping  | С                                       | С                         | # | #  | #  | # | С   | # | # | # | # | С   |
| Aquaculture   | С                                       | С                         | # | #  | #  | # | С   | # | # | # | # | С   |
| Bulk landscape  | С                                       | С                         | С | С  | С  | С | С   | С | С | # | # | С   |

| Car park ancillary to another use               | С | С | С | С | С | # | С | С | # | # | # | С |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| Car wash  | С | С | С | С | С | # | С | С | # | # | # | С |
| Food and drink outlet                           | С | С | # | # | # | # | С | С | # | # | # | С |
| Function facility                               | С | С | # | # | # | # | С | # | # | # | # | С |
| Garden centre                                   | С | С | С | # | # | # | С | С | # | # | # | С |
| Hardware and trade supplies                     | С | С | # | # | # | # | С | С | # | # | # | С |
| Home-based business                             | С | С | # | # | # | # | С | # | # | # | # | С |
| Hotel (where not<br>including<br>accommodation) | С | С | # | # | # | # | С | # | # | # | # | С |
| Market  | С | С | С | # | # | # | С | С | # | # | # | С |
| Nightclub<br>entertainment facility             | С | С | # | # | # | # | С | # | # | # | # | С |
| Office  | С | С | # | # | # | # | С | # | # | # | # | С |
| Outdoor sales                                   | С | С | # | # | # | # | С | С | # | # | # | С |
| Parking station                                 | С | С | С | С | С | # | С | С | # | # | # | С |
| Roadside stalls                                 | С | С | С | # | # | # | С | С | # | # | # | С |
| Sales office                                    | С | С | # | # | # | # | С | С | # | # | # | С |
| Shop, Adult store                               | С | С | # | # | # | # | С | # | # | # | # | С |
| Shopping centre                                 | С | # | # | # | # | # | С | # | # | # | # | С |
| Showroom  | С | С | # | # | # | # | С | С | # | # | # | С |

| Theatre   | С                                      | С                         | # | #  | #  | # | С                                      | # | #   | # | # | С |
|---|--|---------------------------|---|----|----|---|--|---|---|---|---|---|
| Tourist attraction  | С                                      | С                         | С | #  | #  | # | С                                      | С | #   | # | # | С |
| Veterinary service  | С                                      | С                         | # | #  | #  | # | С                                      | # | #   | # | # | С |
| Wholesale nursery   | С                                      | С                         | С | С  | С  | С | С                                      | С | С   | # | # | С |
| Community land<br>uses  | Brisbane F<br>flood plan<br>sub-catege | River<br>ning area<br>ory |   |    |    |   | Creek/wate<br>flood plan<br>sub-catego |   | Overland<br>flow<br>flood<br>planning<br>area<br>sub-<br>category |   |   |   |
|   | 5                                      | 4                         | 3 | 2B | 2A | 1 | 5                                      | 4 | 3   | 2 | 1 |   |
| Childcare centre  | С                                      | #                         | # | #  | #  | # | С                                      | # | #   | # | # | # |
| Club  | С                                      | С                         | # | #  | #  | # | С                                      | С | #   | # | # | С |
| Community care centre   | С                                      | #                         | # | #  | #  | # | С                                      | # | #   | # | # | С |
| Community use   | С                                      | #                         | # | #  | #  | # | С                                      | С | #   | # | # | С |
| Educational<br>establishment<br>(and outdoor<br>education centre) | С                                      | #                         | # | #  | #  | # | С                                      | # | #   | # | # | С |
| Environment facility  | С                                      | С                         | С | С  | С  | С | С                                      | С | С   | С | С | С |
| Health care service   | С                                      | #                         | # | #  | #  | # | С                                      | # | #   | # | # | С |
| Hospital  | #                                      | #                         | # | #  | #  | # | #                                      | # | #   | # | # | # |
| Indoor sport and recreation                                       | С                                      | С                         | # | #  | #  | # | С                                      | С | #   | # | # | С |

Page 17 of 28 Print Date: 08/12/2022 cityplan.brisbane.qld.gov.au

| Major sport, recreation<br>and entertainment<br>facility | С                                      | #                         | # | #  | #  | # | С   | С | # | # | # | С   |
|--|--|---------------------------|---|----|----|---|---|---|---|---|---|---|
| Motor sport facility                                     | С                                      | С                         | С | #  | #  | # | С   | С | С | # | # | С   |
| Outdoor sport and recreation                             | С                                      | С                         | С | #  | #  | # | С   | С | # | # | # | С   |
| Park   | С                                      | С                         | С | С  | С  | С | С   | С | С | С | С | С   |
| Place of worship   | С                                      | #                         | # | #  | #  | # | С   | С | # | # | # | С   |
| Special purpose land<br>uses                             | Brisbane F<br>flood plan<br>sub-catego | River<br>ning area<br>ory |   |    |    |   | Creek/waterway<br>flood planning area<br>sub-category |   |   |   |   | Overland<br>flow<br>flood<br>planning<br>area<br>sub-<br>category |
|  | 5                                      | 4                         | 3 | 2B | 2A | 1 | 5   | 4 | 3 | 2 | 1 |   |
| Air service  | С                                      | #                         | # | #  | #  | # | С   | # | # | # | # | С   |
| Cemetery   | С                                      | С                         | С | #  | #  | # | С   | С | # | # | # | С   |
| Crematorium  | С                                      | #                         | # | #  | #  | # | С   | # | # | # | # | С   |
| Detention facility                                       | #                                      | #                         | # | #  | #  | # | #   | # | # | # | # | С   |
| Emergency services                                       | #                                      | #                         | # | #  | #  | # | #   | # | # | # | # | #   |
| Funeral parlour  | С                                      | #                         | # | #  | #  | # | С   | # | # | # | # | С   |
| Landing  | С                                      | С                         | С | С  | С  | С | С   | С | С | С | # | С   |
| Major electricity infrastructure                         | #                                      | #                         | # | #  | #  | # | #   | # | # | # | # | #   |

| Port service                     | С   | С | С | #  | #  | # | С | С   | С | С | # | С |  |
|----------------------------------|---|---|---|----|----|---|---|---|---|---|---|---|--|
| Substation                       | С   | # | # | #  | #  | # | С | #   | # | # | # | # |  |
| Telecommunications facility      | С   | # | # | #  | #  | # | С | #   | # | # | # | # |  |
| Utility installation             | С   | # | # | #  | #  | # | # | #   | # | # | # | # |  |
| Industry land uses               | Brisbane River<br>flood planning area<br>sub-category |   |   |    |    |   |   | Creek/waterway<br>flood planning area<br>sub-category |   |   |   |   |  |
|                                  | 5   | 4 | 3 | 2B | 2A | 1 | 5 | 4   | 3 | 2 | 1 |   |  |
| Extractive industry              | С   | С | С | #  | #  | # | С | С   | С | # | # | С |  |
| High impact industry             | С   | С | # | #  | #  | # | С | С   | # | # | # | С |  |
| Intensive animal industry        | С   | С | # | #  | #  | # | С | #   | # | # | # | С |  |
| Intensive horticulture           | С   | С | С | #  | #  | # | С | С   | # | # | # | С |  |
| Low impact industry              | С   | С | # | #  | #  | # | С | С   | # | # | # | С |  |
| Marine industry                  | С   | С | С | #  | #  | # | С | С   | # | # | # | С |  |
| Medium impact<br>industry        | С   | С | # | #  | #  | # | С | С   | # | # | # | С |  |
| Research and technology industry | С   | # | # | #  | #  | # | С | #   | # | # | # | С |  |
| Rural industry                   | С   | С | С | С  | С  | С | С | С   | С | # | # | С |  |

| Service industry   | С | С | # | # | # | # | С | С | # | # | # | С |
|--------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Service station    | С | # | # | # | # | # | С | # | # | # | # | С |
| Special industries | С | # | # | # | # | # | # | # | # | # | # | С |
| Transport depot    | С | # | # | # | # | # | С | # | # | # | # | С |
| Warehouse          | С | С | # | # | # | # | С | # | # | # | # | С |

Note—Caretaker's accommodation and home-based business are considered ancillary to the dominant land use.

#### Table 8.2.11.3.D—Flood planning categories for development types

| BCA building classification <sup>(1)</sup> | Development types and design levels, assigned design floor or pavement levels                                    | Category – refer to Table 8.2.11.3.L for flood planning levels  |
|--|--|---|
| Class 1–4                                  | Habitable room <sup>(2)</sup>  | Category A  |
|  | Non-habitable room including patio and courtyard   | Category B  |
|  | Non-habitable part of a Class 2 or Class 3 building excluding the essential services <sup>(2)</sup> control room | Category B<br>Risk management approach to Brisbane River flooding is permitted (refer to Flood<br>planning scheme policy) |
|  | Parking located in the building undercroft of a multiple dwelling  | Category C  |
|  | Carport <sup>(4)</sup> , unroofed car park; vehicular manoeuvring area   | Category D  |
|  | Essential electrical services <sup>(2)</sup> of a Class 2 or Class 3 building only                               | Category A <sup>(6)</sup>   |
|  | Basement parking entry <sup>(3)</sup>  | Category C + 300mm  |
| Class 5,<br>Class 6, or<br>Class 8         | Building floor level   | Category C<br>Risk management approach to Brisbane River flooding is permitted (refer to Flood<br>planning scheme policy) |
|  | Garage or car park located in the building undercroft <sup>(3)</sup>   | Category C  |

|           | Carport <sup>(4)</sup> or unroofed car park   | Category D  |  |  |
|-----------|---|---|--|--|
|           | Vehicular access and manoeuvring areas  | Category D  |  |  |
|           | Basement parking entry <sup>(3)</sup>   | Category C  |  |  |
|           | Essential electrical services <sup>(2)</sup>  | Class 8 – Category C <sup>(6)</sup><br>Class 5 & 6 – Category A <sup>(6)</sup>  |  |  |
| Class 7a  | Refer to the relevant building class specified in this table  |   |  |  |
| Class 7b  | Building floor level  | Category C<br>Risk management approach to Brisbane River flooding is permitted (refer to Flood<br>planning scheme policy) |  |  |
|           | Vehicular access and manoeuvring area   | Category D  |  |  |
|           | Essential electrical services <sup>(2)</sup>  | Category C  |  |  |
| Class 9   | Building floor level  | Category A  |  |  |
|           | Building floor level for habitable rooms in Class 9a or 9c where for a residential care facility          | 0.2% AEP flood  |  |  |
|           | Building floor level for habitable rooms in Class 9b where involving children, such as a childcare centre | 0.2% AEP flood  |  |  |
|           | Garage or car park located in the building undercroft <sup>(3)</sup>                                      | Category C  |  |  |
|           | Carport <sup>(5)</sup> or unroofed car park   | Category D  |  |  |
|           | Vehicular access and manoeuvring areas  | Category D  |  |  |
|           | Essential electrical services <sup>(2)</sup>  | Category A  |  |  |
| Class 10a | Car parking facility  | Refer to the relevant building class specified in this table  |  |  |
|           | Shed <sup>(5)</sup> or the like   | Category D  |  |  |

| Class 10b | Swimming pool                                       | Category E                         |  |
|-----------|---|------------------------------------|--|
|           | Associated mechanical and electrical pool equipment | Category C                         |  |
|           | Other structures                                    | Flood planning levels do not apply |  |

Notes-

<sup>(1)</sup> Refer to the Building Code of Australia for definitions of building classifications.

<sup>(2)</sup> Essential electrical services include any area or room used for fire control panel, telephone PABX, sensitive substation equipment including transformers, low voltage switch gear, high voltage switch gear, battery chargers, protection control and communication equipment, low voltage cables, high voltage cables, and lift or pump controls.

<sup>(3)</sup> Basement car parks must be suitably waterproofed and all air vents, air-conditioning ducts, pedestrian access and entry and exit ramps into the basement must comply with the applicable flood planning levels in this table.

<sup>(4)</sup> A shelter for a motor vehicle, which has a roof and one or more open sides, and which can be built against the side of a building.

<sup>(5)</sup> A slight or rough structure built for shelter and storage; or a large strongly built structure, often open at the sides or end.

<sup>(6)</sup> Where essential electrical services are proposed in a basement below the specified flood planning level, the flood immunity of all air vents, air-conditioning ducts, pedestrian access, lift shafts and entry/exit ramps at the basement entrance and any other openings into that basement must conform with the flood planning levels for Category A for Residential development, and the relevant basement entry level of all other uses. To ensure flood immunity, basements require a waterproof basement design to prevent flood waters entering the basement.

• A flood event with an AEP of 2% is the equivalent of a 50 year ARI flood event.

- A flood event with an AEP of 0.2% is the equivalent of a 500 year ARI flood event.
- Where a building has a combination of uses that includes a component of classes 2, 3 or 9, the essential services for that building shall comply with the requirements of the building class with the greatest flood planning level requirement.
- Use classes for residential development also include basement storage.

#### Table 8.2.11.3.E— Building undercroft clearances

| Flooding source  | Minimum clearance requirement <sup>(1)(3)</sup>   |
|--|---|
| Overland flow– Hydraulic Hazard (DV <0.6 m <sup>2</sup> /s and depth <600mm in 2% AEP flood event) | Lowest floor level is to be 1.5m <sup>(2)</sup> above the highest ground elevation in undercroft area |
| Overland flow– Hydraulic Hazard (DV >0.6 m <sup>2</sup> /s or depth >600mm in 2% AEP flood event)  | Lowest floor level is to be 2.5m <sup>(2)</sup> above the highest ground elevation in undercroft area |
| Creek/waterway (Flood planning area 1, 2 or 3 sub-categories)                                      | Lowest floor level is to be 2.5m <sup>(2)</sup> above the highest ground elevation in undercroft area |
| Creek/waterway (Flood planning area 4 sub-category)  | Lowest flood level is to be 1.5m <sup>(2)</sup> above the highest ground elevation in undercroft area |
| Notes—   |   |

<sup>(1)</sup> The minimum undercroft only relates to the minimum clearance requirements from ground level to the finished floor level and not minimum flood planning levels. Where the flood planning level requirement with freeboard results in a higher finished floor level that higher level needs to be adopted.

<sup>(2)</sup> Refer to the Flood planning scheme policy for explanatory material regarding clearances and considerations.

<sup>(3)</sup> The minimum undercroft clearance only applies to the area of undercroft above the relevant flood extent or flood planning area sub-category.

#### Table 8.2.11.3.F—Flood planning levels for a new road

| Flooding                         | Minimum design levels at the crown of the road (m AHD) <sup>(2)</sup> |                                      |  |
|----------------------------------|---|--------------------------------------|--|
| source                           | Residential development   | Industrial or commercial development |  |
| Brisbane<br>River <sup>(3)</sup> | Defined flood level   | 5% AEP flood level                   |  |
| Creek/waterway                   | 1% AEP flood level  | 2% AEP flood level                   |  |
| Overland flow                    | 2% AEP flood level  | 2% AEP flood level                   |  |

Notes—

<sup>(1)</sup> Where the road is subject to more than one flooding source, the minimum flood planning level is the highest level determined from these sources.

<sup>(2)</sup> Where flood levels are not available from Council's FloodWise Property Report, such as for overland flow flooding, a suitably qualified Registered Professional Engineer Queensland with expertise in undertaking flood studies is required to estimate the relevant flood level.

<sup>(3)</sup> A risk management approach determining flood planning levels of roads for Brisbane River flooding can be applied as an alternative to Table 8.2.11.3.F. Typically such roads would have a flood immunity no worse than the surrounding roads that support a similar land use, otherwise a Flood Risk Assessment which complies with the relevant requirements of the Flood planning scheme policy is provided.

#### Table 8.2.11.3.G—Flood planning levels for essential community infrastructure

| Type of essential community infrastructure  | Minimum design levels |
|---|-----------------------|
| Emergency services  | 0.2% AEP flood        |
| Emergency services, where for an emergency shelter  | 0.5% AEP flood        |
| Emergency services, where for police facilities   | 0.5% AEP flood        |
| Hospital and health care service where associated with a hospital   | 0.2% AEP flood        |
| Community facility where involving storage of valuable records or items of historic or cultural significance (e.g. galleries and libraries) | 0.5% AEP flood        |

| State-controlled roads<br>Major or minor electricity infrastructure not otherwise listed in this table<br>Utility installation where for rail transport services<br>Air service<br>Telecommunications facility | No specific recommended level but development proponents should ensure that the infrastructure is optimally located and designed to achieve suitable levels of service, having regard to the processes and policies of the administering government agency. |
|--|---|
| Power stations (as defined in the <i>Electricity Act 1994</i> ) or renewable energy facility.  | 0.2% AEP flood  |
| Major electricity infrastructure where a major switch yard   | 0.2% AEP flood  |
| Substations  | 0.5% AEP flood  |
| Utility installation where for a sewage treatment plant  | Defined flood event   |
| Utility installation where for a water treatment plant   | 0.5% AEP flood  |

Note—A flood event with an AEP of 0.2% is the equivalent of a 500 year ARI flood event.

Note—A flood event with an AEP of 0.5% is the equivalent of a 200 year ARI flood event.

#### Table 8.2.11.3.H—Table of processes requiring additional assessment in a flood planning area

| Process  |
|--|
| (1) Oil refining or processing   |
| (2) Producing, refining or processing gas or fuel gas  |
| (3) Power station, including the activity of generating electricity by using fuel  |
| (4) Producing, quenching, cutting, crushing or grading coke  |
| (5) Waste incinerator, including thermal treatment of waste  |
| (6) Pulp or paper manufacturing  |
| (7) Tannery or works for curing animal skins, hides or finishing leather   |
| (8) Textile manufacturing, including carpet manufacturing, wool scouring or carbonising, cotton milling, or textile bleaching, dyeing or finishing |
| (9) Rendering plant, including meat processing   |

(10) Manufacturing chemicals, poisons and explosives

(11) Manufacturing fertilisers involving ammonia

(12) Manufacturing polyvinyl chloride plastic

(13) Major hazard facilities for the storage and handling of dangerous goods

(14) Storage of hazardous chemicals in quantities that would exceed the hazardous chemicals flood hazard threshold set out in Table 8.2.11.3.M

(15) Manufacturing medium-density fibreboard, chipboard, particle board, plywood, laminated board or wood veneer products

(16) Manufacturing or processing plaster

(17) Enamelling workshop

(18) Galvanising works

(19) Anodising or electroplating workshop

(20) Powder coating workshop

(21) Treating timber for preservation using chemicals including copper, chromium, arsenic, borax and creosote

(22) Manufacturing soil conditioners by receiving, blending, storing, processing, drying or composting organic material or organic waste, including animal manures, sewage, septic sludges and domestic waste

(23) Manufacturing tyres, asbestos products, asphalt, cement, glass or glass fibre, mineral wool or ceramic fibre

(24) Abattoir, including meat processing

(25) Recycling chemicals, oils or solvents

(26) Waste disposal activity (other than waste incinerator), including waste transfer station operation

(27) Recycling, storing or reprocessing regulated waste, including regulated waste treatment

(28) Manufacturing batteries and battery recycling

(29) Drum and container reconditioning

#### (30) Water treatment

(31) Sewage treatment

#### Table 8.2.11.3.I—Suitability of reconfiguring a lot within a flood planning area

C – Reconfiguring a lot is suitable within a flood planning area

# – Flood risk assessment in accordance with the requirements of the Flood planning scheme policy is required to demonstrate the mitigation of risk from flood hazard

| Flood planning area | Creek/waterway flood planning area sub-categories |            | Brisbane River flood planning area<br>sub-categories |             |            |       |
|---------------------|---|------------|--|-------------|------------|-------|
|                     | Residential                                       | Industrial | Other  | Residential | Industrial | Other |
| 1                   | #   | #          | #  | #           | #          | #     |
| 2/2a;2b             | #   | #          | #  | #           | С          | #     |
| 3                   | #   | #          | #  | #           | С          | С     |
| 4                   | С   | С          | С  | С           | С          | С     |
| 5                   | С   | С          | С  | С           | С          | С     |

Notes—

• A flood risk assessment is required for residential reconfiguring a lot development where creating more than two new lots in the overland flow flood planning area sub-category.

Additional requirements apply for the Brisbane River flood planning area sub-category if the residential flood level is greater than 12.8m AHD.

• Minimum site levels, requirements for no adverse off site impacts and other provisions in the planning scheme still apply.

#### Table 8.2.11.3.J—Flood planning levels for reconfiguring a lot

| Flooding source <sup>(1)</sup> | Minimum lot levels (m AHD) <sup>(2)</sup>              |  |                        |  |  |
|--------------------------------|--|--|------------------------|--|--|
|                                | Residential (creating 6 or less lots with no new road) | Residential (creating more than 6 lots), or a new road | Other than residential |  |  |
| Brisbane River                 | 2% AEP flood level + 300mm                             | RFL + 0.3m   | 1% AEP flood level     |  |  |
| Creek/waterway | Minimum $300m^2$ area at the 1% AEP flood level + $300mm^{(3)}$ | 1% AEP flood level + 300mm | 2% AEP flood level |
|----------------|---|----------------------------|--------------------|
| Overland flow  | Minimum $300m^2$ area at the 2% AEP flood level + $300mm^{(3)}$ | 2% AEP flood level + 300mm | 2% AEP flood level |

Notes-

<sup>(1)</sup> Where the site is subject to more than one flooding source, the minimum flood planning level is the highest level determined from these sources.

<sup>(2)</sup> Where flood levels are not available from Council's FloodWise Property Report such as for overland flow flooding, a suitably qualified Registered Professional Engineer Queensland with expertise in undertaking flood studies is required to estimate the relevant flood level.

<sup>(3)</sup> The 300m<sup>2</sup> area is considered suitable for siting a dwelling house with open space area at or above the nominated flood planning level.

### Table 8.2.11.3.K—Flood planning levels for existing road providing access to or fronting a development

| Flooding source <sup>(1)</sup> | Minimum design levels at the crown of the road (m AHD) <sup>(2)(3)</sup> |                    |   |
|--------------------------------|--|--------------------|---|
|                                | Local road   | Neighbourhood road | District road, suburban road, arterial road |
| Brisbane River                 | 5% AEP flood level   | 2% AEP flood level | 2% AEP flood level                          |
| Creek/waterway                 | 5% AEP flood level   | 2% AEP flood level | 2% AEP flood level                          |
| Overland flow                  | 5% AEP flood level   | 5% AEP flood level | 5% AEP flood level                          |

Notes-

<sup>(1)</sup> Where the site is subject to more than one flooding source, the minimum flood planning level is the highest level determined from these sources.

<sup>(2)</sup> Where flood levels are not available from Council's FloodWise Property Report such as overland flow flooding a suitably qualified Registered Professional Engineer in Queensland with expertise in undertaking flood studies is required to estimate the relevant flood level. The Flood planning scheme policy sets out the requirements for a flood risk assessment process.

<sup>(3)</sup> The design standard for industry access is the 5% AEP flood level for all flooding sources.

### Table 8.2.11.3.L—Categories of flood planning levels

| Flooding source <sup>(1)</sup> | Minimum design floor or pavement levels (m AHD) <sup>(2)</sup><br>(refer to Table 8.2.11.3.D for assignment of these categories) |            |            |            |            |
|--------------------------------|--|------------|------------|------------|------------|
|                                | Category A   | Category B | Category C | Category D | Category E |

| Brisbane River     | RFL<br>+ 500mm                | RFL<br>+ 300mm                | DFL                | 5% AEP flood level | 5% AEP flood level |
|--------------------|-------------------------------|-------------------------------|--------------------|--------------------|--------------------|
| Creek/<br>waterway | 1% AEP flood level<br>+ 500mm | 1% AEP flood level<br>+ 300mm | 1% AEP flood level | 1% AEP flood level | 5% AEP flood level |
| Overland flow      | 2% AEP flood level<br>+ 500mm | 2% AEP flood level<br>+ 300mm | 2% AEP flood level | 2% AEP flood level | 5% AEP flood level |

Notes-

<sup>(1)</sup> Where the site is subject to more than one type of flooding that is overland flow flooding, creek or waterway flooding or river flooding, the minimum flood immunity level is the highest level determined from these sources.

<sup>(2)</sup> Where flood levels are not available from Council's FloodWise Property Report such as overland flow flooding, the applicant will need to engage a suitably qualified Registered Professional Engineer Queensland with expertise in undertaking flood studies required to estimate the relevant flood level. The Flood planning scheme policy sets out the requirements for a flood risk assessment process.

- A flood event with an AEP of 1% is the equivalent of a 100 year ARI flood event.

• A flood event with an AEP of 2% is the equivalent of a 50 year ARI flood event.

• A flood event with an AEP of 5% is the equivalent of a 20 year ARI flood event.

#### Table 8.2.11.3.M—Hazardous chemicals flood hazard threshold

Hazardous chemicals flood hazard threshold means any of the following:

A hazardous chemical listed in schedule 11 of the Work Health and Safety Regulation 2011 in a quantity that exceeds a threshold quantity stated in column 5 of schedule 11

A chemical classified as hazardous to the aquatic environment under the Australian Dangerous Goods Code in the Acute I or Chronic I category that exceeds 2500 litres or kilograms

A chemical classified as hazardous to the aquatic environment under the Australian Dangerous Goods Code in the Chronic II category that exceeds 10,000 litres or kilograms

A chemical classified as hazardous to the aquatic environment under the Australian Dangerous Goods Code and assigned to Packing Group III that exceeds 10,000 litres or kilograms

A chemical classified as hazardous to the aquatic environment under the Globally Harmonised System of Classification and Labelling of Chemicals that exceeds 10,000 litres or kilograms



# APPENDIX B – COASTAL HAZARD OVERLAY CODE

# 8.2.6 Coastal hazard overlay code

### 8.2.6.1

#### Application

- 1. This code applies to assessing development in the Coastal hazard overlay, if:
  - a. accepted development subject to compliance with identified requirements, where acceptable outcomes of this code are identified requirements in a table of assessment for an overlay (section 5.10); or
  - b. assessable development where this code is an applicable code identified in the assessment benchmarks column of a table of assessment for an overlay (section 5.10); or
  - c. impact assessable development.
- 2. Land in the Coastal hazard overlay is identified on the Coastal hazard overlay map and is included in the following sub-categories:
  - a. Erosion prone area coastal erosion sub-category;
  - b. Erosion prone area permanent inundation due to sea-level rise at 2100 sub-category;
  - c. High storm-tide inundation area sub-category;
  - d. Medium storm-tide inundation area sub-category;
  - e. Coastal management district sub-category.
- 3. When using this code, reference should be made to section 1.5 and section 5.3.3.

Note—The following purpose, overall outcomes, performance outcomes and acceptable outcomes comprise the assessment benchmarks of this code.

Editor's note—Where land is identified within a flood planning area on the Flood overlay map, and is identified within a storm-tide inundation area on the Coastal hazard overlay map, the assessment benchmark that provides the highest level of protection from any source of flooding applies.

Note—Where this code includes performance outcomes or acceptable outcomes that relate to:

- coastal hazard assessment or evacuation, guidance is provided in the Coastal hazard planning scheme policy;
- flood risk assessment and flood immunity for reconfiguring a lot, guidance is provided in the Flood planning scheme policy;
- handling or storage of hazardous materials, guidance is provided in the Management of hazardous chemicals in flood affected areas planning scheme policy.
- standards and specifications for public assets in a park, guidance is provided in the Infrastructure design planning scheme policy.

Editor's note—For a proposal to be accepted development subject to compliance with identified requirements, it must meet all the identified acceptable outcomes of this code that relate to the applicable sub-category and any other applicable code. Where it does not meet all identified acceptable outcomes, the proposal becomes assessable development and a development application is required. Where a development application is triggered, only the specific acceptable outcomes that the proposal fails to meet need to be assessed against the corresponding assessable acceptable outcomes or performance outcomes and relevant overall outcomes. Other identified acceptable outcomes that are met are not assessed as part of the development application.

8.2.6.2

### Purpose

- 1. The purpose of the Coastal hazard overlay code is to:
  - a. Implement the policy direction in the Strategic framework, in particular:
    - i. Theme 2: Brisbane's outstanding lifestyle, and Element 2.3 Brisbane's healthy and safe communities;
    - ii. Theme 3: Brisbane's clean and green leading environmental performance, and Element 3.3 Brisbane's adaptation approaches;

Page 1 of 16 Print Date: 08/12/2022 cityplan.brisbane.qld.gov.au iii. Theme 4: Brisbane's highly effective transport and infrastructure networks, and Element 4.3 – Brisbane's coordinated infrastructure planning and delivery.

- b. Provide for the assessment of the suitability of development in the Coastal hazard overlay.
- 2. The purpose of the code will be achieved through the following overall outcomes:
  - a. Development minimises exposure of people and property to unacceptable risks from coastal hazards including storm-tide and permanent tidal inundation.
  - b. Development and infrastructure mitigates the risk of impacts from coastal hazard through its location, siting, design, construction and operation whilst maintaining amenity.
  - c. Development does not compromise the ability of the city's counter-disaster response capacity during a coastal hazard emergency.
  - d. Development provides for efficient evacuation and access for evacuation resources including emergency services during coastal hazard events or otherwise plans for the prospect and impact of isolation or hindered evacuation due to flooding from storm-tide and tidal inundation.
  - e. Development involving essential community infrastructure remains functional during and immediately after a coastal hazard event.
  - f. Development ensures that essential building services or services essential for the development are designed, located and operated to minimise the coastal hazard risk to people, minimise damage to property, disruption to building function and the re-establishment time after a storm-tide or tidal inundation event.
  - g. Development ensures that emergency management plans respond to the number and capacity of future users of the development to safely participate in emergency measures such as evacuation.
  - h. Development involving hazardous materials manufactured, handled or stored in bulk does not adversely impact on public safety and the environment as a result of the impacts of storm-tide and tidal inundation.
  - i. Development does not cause or increase adverse impacts on other premises from coastal hazard.
  - j. Development does not impact adversely on the ability of adjoining sites to implement future coastal hazard mitigation measures.
  - k. Development and infrastructure avoids or mitigates the impacts of predictable future coastal hazard due to increases in sea-level rise and cyclonic intensity.
  - I. Development in areas subject to coastal hazards protects biodiversity, the integrity of environmental networks and coastal resources.
  - m. Development prioritises, in order, the safety of people, protection of public infrastructure and protection of private property, in the management of the economic, social and environmental impacts of coastal hazards.
  - n. Development is designed and operated to withstand coastal hazards in order to avoid or defer the need for emergency assistance.
  - o. Development does not rely on Council undertaking specific coastal hazard mitigation actions or uncommitted future provision of services or infrastructure to ensure the protection of people, property or infrastructure, unless identified through an adaption strategy.

## 8.2.6.3 Performance outcomes and acceptable outcomes

### Table 8.2.6.3.A—Performance outcomes and acceptable outcomes

| Performance outcomes  | Acceptable outcomes   | Comments |
|---|---|----------|
| Section A—If for accepted development subject to con<br>outcomes only) or assessable development for a dwel | mpliance with identified requirements (acceptable<br>lling house including a secondary dwelling |          |

| <ul> <li>PO1</li> <li>Development involving any habitable or non-habitable part of the dwelling house, including any secondary dwelling, is: <ul> <li>a. located and designed to minimise the risk to people and structures from coastal hazards;</li> <li>b. located to minimise amenity impacts, disruption to residents, recovery time and rebuilding and restoration costs after a coastal hazard event.</li> </ul> </li> </ul>  | AO1<br>Development for a dwelling house including, any<br>secondary dwelling, complies with the flood planning<br>levels in Table 8.2.6.3.B.<br>Editor's note—Information about flooding from storm tide is provided in<br>Council's FloodWise Property Report.  | Not applicable to this development.  |
|--|--|--|
| Section B—If for accepted development subject to cor outcomes only) or assessable development other than   | npliance with identified requirements (acceptable<br>a for a dwelling house  |  |
| <ul> <li>PO2</li> <li>Development other than for a park is located and designed to: <ul> <li>a. minimise the risk to all persons from coastal hazards;</li> <li>b. minimise flood damages to the development and contents of buildings;</li> <li>c. provide suitable amenity;</li> <li>d. minimise disruption to residents, recovery time, and rebuilding or restoration costs after coastal hazard events.</li> </ul> </li> </ul>   | AO2<br>Development achieves minimum flood planning levels<br>consistent with Table 8.2.6.3.C.<br>Editor's note—Information about flooding from storm tide is provided in<br>Council's FloodWise Property Report.   | The Acceptable Outcome can be and is proposed to be met, as identified on the accompanying drawings. |
| <ul> <li>PO3</li> <li>Development for a park ensures that the design of the park and location of structures and facilities responds to coastal hazards and balances the safety of intended users with: <ul> <li>a. maintaining continuity of operations;</li> <li>b. impacts of flooding on asset life and ongoing maintenance costs;</li> <li>c. efficient recovery after flood events;</li> <li>d. recreational benefits to the city;</li> <li>e. availability of suitable land within the park.</li> </ul> </li> <li>Note—The Infrastructure design planning scheme policy provides more</li> </ul> | <ul> <li>AO3</li> <li>Development involving a building or structure in a park: <ul> <li>a. complies with the minimum flood planning levels in Table 8.2.6.3.C; or</li> <li>b. is not located below the 20% AEP storm-tide level if Table 8.2.6.3.C does not apply to the type of structure.</li> </ul> </li> </ul> | Not applicable to this development.  |

| detail on standards and specifications for public assets.   |  |  |
|---|--|--|
| Section C—If assessable development other than for a dwelling house   |  |  |
| General   |  |  |
| <b>PO4</b><br>Development has access which provides for safe<br>vehicular and pedestrian movement in the development,<br>including emergency services access during and after a<br>coastal hazard event.  | AO4<br>Development locates access points and driveways in the<br>flood free area (or the area of the lowest flood risk) of the<br>site.  | The Acceptable Outcome can be and is proposed to be met, as identified on the accompanying drawings. |
| <ul> <li>PO5</li> <li>Development for pedestrian and cyclist paths: <ul> <li>a. provides a suitable level of trafficability;</li> <li>b. manages the impacts of flooding on asset life and ongoing maintenance costs;</li> <li>c. balances route availability with recreational and transport connectivity benefits to the city.</li> </ul> </li> </ul> | <ul> <li>AO5.1 Development for off-road pedestrian and cyclist paths: <ul> <li>a. is not located in the Erosion prone area – coastal erosion subcategory; or</li> <li>b. complies with the minimum flood planning levels in Table 8.2.6.3.H.</li> </ul> Note—If the site is subject to more than 1 type of flooding, the requirement that affords the highest flood planning level will apply. AO5.2 All new on-road cyclist and pedestrian facilities comply with the road flood immunity and trafficability standards for the applicable category of road in Table 8.2.6.3.H</li></ul> | Not applicable to this development.  |
| <ul> <li>PO6</li> <li>Development does not: <ul> <li>a. impact adversely on the safety or amenity of an adjoining site;</li> <li>b. impact adversely on the ability of others to implement future coastal hazard adaptation actions.</li> </ul> </li> </ul>   | <b>AO6</b><br>Development does not concentrate, intensify or divert<br>floodwater, erosion impacts or cause nuisance ponding<br>onto other premises.   | The Acceptable Outcome can be and is proposed to be met, as identified on the accompanying drawings. |
| <b>PO7</b><br>Development involving essential electrical services or a basement storage area is suitably located and designed to ensure public safety and minimise the need for flood   | A07.1<br>Development ensures that:<br>a. all essential electrical services comply with the<br>flood planning levels in Table 8.2.6.3.C; or   | The Acceptable Outcome can be and is proposed to be met, as identified on the accompanying drawings. |

| recovery and economic consequences of damage during a flood.   | <ul> <li>b. if a basement contains essential electrical services or a private basement storage area, the basement is a waterproof structure with walls and floors impermeable to the passage of water and all entry points and services are located at or above the relevant flood immunity level in Table 8.2.6.3.C.</li> <li>Note—A basement storage area is a basement-level area for private storage, other than a bike storage room, change room, building maintenance storage and non-critical electrical services.</li> <li>AO7.2</li> <li>Development involving a basement that relies on a pumping solution to manage floodwater ingress or for dewatering after a flood, provides an appropriately flood protected backup power source for those pumps.</li> </ul> |                                     |
|--|--|-------------------------------------|
| <ul> <li>PO8</li> <li>Development involving the storage and handling of hazardous materials avoids or minimises risks to public health and safety and the environment, by: <ul> <li>a. protecting underground tanks for hazardous materials against the forces of buoyancy, velocity flow and debris impacts;</li> <li>b. securing above-ground tanks against flotation and lateral movement;</li> <li>c. preventing damage to pipework or entry of floodwater into pipework;</li> <li>d. preventing damage to or off-site release of packages, drums or containers.</li> </ul> </li> <li>Note—A chemical hazards flood risk report prepared in accordance with the Management of hazardous chemicals in flood affected areas planning scheme policy can assist in demonstrating achievement of this performance outcome.</li> </ul> | <ul> <li>AO8.1</li> <li>Development does not include the storage or handling of hazardous chemicals that exceed the hazardous chemicals flood hazard threshold quantities in Table 8.2.6.3.J.</li> <li>AO8.2</li> <li>Development involving the processes listed in Table 8.2.6.3.F is consistent with the standards contained in the Management of hazardous chemicals in flood affected areas planning scheme policy and can operate without risk of environmental harm during a coastal hazard.</li> <li>Note—The Management of hazardous chemicals in flood affected areas planning scheme policy sets out further information and processes including risk assessment for the management of hazardous chemicals in coastal hazard areas.</li> </ul>                     | Not applicable to this development. |
| Additional performance outcomes and acceptable outcomes for essential community infrastructure   |  |                                     |
| PO9  | AO9  |                                     |

| <ul> <li>Development involving essential community infrastructure: <ul> <li>a. maintains function during and immediately after a coastal hazard event or is part of a network that is able to maintain the function of the essential community infrastructure without parts of the development which are unable to function during a coastal hazard event;</li> <li>b. is designed and sited to avoid adverse impacts on the community or the environment due to the impacts of coastal hazard on infrastructure, facilities or access and egress routes;</li> <li>c. retains site access necessary to maintain function of the development during a coastal hazard event;</li> <li>d. maintains function or is part of a network which is able to remain functional even when other infrastructure may be compromised in a flood event;</li> <li>e. contains mitigation measures which are not entirely dependent on human activation to respond to a flood event.</li> </ul> </li> </ul> | <ul> <li>Development involving essential community infrastructure:</li> <li>a. is ancillary and is not relied upon for the provision of the essential service during a coastal hazard event; or</li> <li>b. is located above the flood immunity levels set out in Table 8.2.6.3.E;</li> <li>c. has access to, or provides, the necessary backup emergency electricity and communications supply in times of flood;</li> <li>d. if the essential community infrastructure has a city-wide emergency function, that part of the development is not located in an area that becomes isolated by a flood up to the event listed for that development type in Table 8.2.6.3.E.</li> </ul> |                                     |
|--|--|-------------------------------------|
| Additional performance outcomes and acceptable out<br>or assembly uses   | comes for vulnerable uses, difficult to evacuate uses  |                                     |
| PO10<br>Development for vulnerable or difficult to evacuate uses<br>and assembly uses optimises vehicular access and<br>efficient evacuation from the development to parts of the<br>road network unaffected by coastal hazard.<br>Note—A coastal hazard risk assessment may be required to address<br>the performance outcome or acceptable outcome that deals with<br>evacuation and isolation arrangements, and the ability to take refuge in<br>place.<br>Editor's note—Further guidance for risk assessment is contained in the<br>Coastal hazard planning scheme policy and the Flood planning scheme<br>policy.   | <ul> <li>AO10</li> <li>Development for vulnerable uses, difficult to evacuate uses or assembly uses: <ul> <li>a. is not isolated in any event up to the relevant flood planning level as specified in Table 8.2.6.3.D; or</li> <li>b. is supported by a critical route or interim critical route identified in the Critical infrastructure and movement network overlay; or</li> <li>c. can achieve vehicular evacuation to a suitable coastal hazard-free location.</li> </ul> </li> <li>Note—A suitable coastal hazard-free location is of a size and nature appropriate to provide for the size and characteristics of the population</li> </ul>                                  | Not applicable to this development. |

|  | likely to need evacuation to that area.  |                                     |
|--|--|-------------------------------------|
| Section D—If for reconfiguring a lot   |  |                                     |
| General  |  |                                     |
| <ul> <li>PO11 Development locates and designs all lots and roads resulting from reconfiguring a lot to: <ul> <li>a. ensure the safety of people;</li> <li>b. minimise damage to property and services;</li> <li>c. facilitate safe and efficient evacuation;</li> <li>d. avoid isolation during a coastal hazard event;</li> <li>e. provide suitable amenity in that it is not frequently flooded or subject to tidal inundation, or nuisance ponding.</li> </ul> </li> <li>Note— <ul> <li>Consideration of the 0.2% AEP flood is relevant to determining an acceptable level of safety for development.</li> </ul> </li> <li>Flood warning time is available for storm-tide flooding.</li> <li>Filling for flood immunity cannot be assumed to mitigate the flood hazard for a flood event greater than the defined flood event.</li> </ul> | <ul> <li>AO11.1<br/>Development ensures that the road and lot layout does<br/>not create new lots isolated by storm-tide flooding at the<br/>defined flood event.</li> <li>AO11.2<br/>Development involving reconfiguring a lot ensures flood<br/>immunity for all lots is provided in compliance with Table<br/>8.2.6.3.G.</li> </ul>   | Not applicable to this development. |
| <ul> <li>PO12 Development that results in 6 lots or less and no new road provides: <ul> <li>a. land with sufficient flood immunity to construct a dwelling house;</li> <li>b. an open space area that is safe and has suitable amenity in that it is not frequently flooded or subject to tidal inundation, nuisance ponding or seepage;</li> <li>c. a lot that is not substantially burdened by a stormwater easement or flood mitigation infrastructure;</li> <li>d. appropriate amenity for any adjoining residential area.</li> </ul> </li> </ul>  | AO12<br>Development for reconfiguring a lot that results in 6 lots<br>or less and no new road in the High storm-tide inundation<br>area sub-category or the Medium storm-tide inundation<br>area sub-category provides at least 80% of each new lot<br>at or above the flood planning levels in Table 8.2.6.3.G.<br>Note—This is to ensure that each new lot will not be affected by tidal<br>influences up to the highest astronomical tide event with an allowance<br>for 800mm of sea level increase through climate change. The<br>development will still need to meet the relevant flood immunity<br>standards. | Not applicable to this development. |
| PO13   | A013   |                                     |

| Development provides acceptable flood immunity for its<br>purpose that minimises the risk to people from coastal<br>hazard, creates safe access and evacuation routes,<br>minimises damage to property and services, and<br>provides suitable amenity.   | <ul> <li>Development involving reconfiguring a lot that results in more than 6 lots or a new road provides flood immunity for:</li> <li>a. all lots in compliance with Table 8.2.6.3.G;</li> <li>b. a new road in compliance with Table 8.2.6.3.H;</li> <li>c. an existing road fronting the development, or providing primary access within 200m of the development, in compliance with Table 8.2.6.3.I.</li> <li>Note—The Flood planning scheme policy contains supporting information about existing roads and serviceability during floods.</li> </ul> |                                     |
|--|--|-------------------------------------|
| <b>PO14</b><br>Development involving a new road, bridge or culvert is<br>designed to minimise impacts to flood behaviour,<br>minimise disruption to traffic during storm-tide inundation<br>and allow for emergency access and evacuation.   | <b>AO14</b><br>Development for a new road provides flood immunity in compliance with Table 8.2.6.3.H.  | Not applicable to this development. |
| <ul> <li>PO15</li> <li>Development for pedestrian and cyclist paths: <ul> <li>a. provides a suitable level of trafficability;</li> <li>b. manages the impacts of flooding on asset life and ongoing maintenance costs;</li> <li>c. balances route availability with recreational and transport connectivity benefits to the city.</li> </ul> </li> </ul>   | <ul> <li>AO15.1         Development for off-road pedestrian and cyclist paths:             <ul></ul></li></ul>   | Not applicable to this development. |
| <ul> <li>Section E—If for a material change of use, reconfiguration of a lot or operational works on a premises in an erosion prone area in a coastal management district where the chief executive is not identified as a referral agency under the Regulation</li> <li>Editor's note—Examples of development where the chief executive is not identified as a referral agency under the Regulation include operational work for:</li> <li>interfering with quarry material, as defined under the Coastal Act, on State coastal land above high-water mark; or</li> </ul> |  |                                     |

| <ul> <li>disposing of dredge spoil, or other solid waste material, in tidal water;</li> <li>constructing an artificial waterway; or</li> <li>removing or interfering with coastal dunes on land other than State cowhere that operational work only involves:</li> <li>prescribed tidal works in a canal; or</li> <li>tidal works that is for the installation, maintenance or repair of overhee</li> <li>for tidal works that is boring or tunnelling under the bed of tidal water,</li> </ul>   | or<br>pastal land,<br>ad cables or lines that extend over tidal water; or<br>works that do not disturb the bed of the tidal water. |                                     |
|---|--|-------------------------------------|
| <ul> <li>PO16 Development does not occur in an erosion prone area within a coastal management district unless the development cannot be feasible located elsewhere and is: <ul> <li>a. coastal dependant development; or</li> <li>b. temporary, readily relocatable or able to be abandoned development; or</li> <li>c. essential community infrastructure; or</li> <li>d. minor redevelopment (as defined in the SPP) of an existing permanent building or structure that cannot be relocated or abandoned.</li> </ul> The development mitigates the risks to people and property to an acceptable or tolerable level.</li></ul> | AO16<br>No acceptable outcome is prescribed.   | Not applicable to this development. |

# Table 8.2.6.3.B—Flood planning levels for a dwelling house

| Flooding Source   | Minimum ground level for house<br>pad after filling (where filling<br>permitted) | Minimum habitable floor level       | Minimum non-habitable floor level –<br>utility areas, garage, laundry and<br>storage room |
|---|--|-------------------------------------|---|
| Storm-tide flooding within the:<br>High storm-tide inundation area sub-category; or<br>Medium storm-tide inundation area sub-category | 2.5m AHD<br>(1% AEP)   | 2.5m AHD + 500mm<br>(1% AEP + 0.5m) | 2.5m AHD + 300mm<br>(1% AEP + 0.3m)   |

Note—Where subject to more than one flooding source, the highest immunity level as determined for each case applies.

# Table 8.2.6.3.C—Categories of flood planning levels

| Flooding Source   | Minimum design floor or pavement levels (m, AHD)<br>(refer Table 8.2.6.3.D for assignment of these categories) |  |                                    |              |              |
|---|--|--|------------------------------------|--------------|--------------|
|   | Category A   | Category B   | Category C                         | Category D   | Category E   |
| Storm-tide flooding within the:<br>High storm-tide inundation area sub-<br>category; or<br>Medium storm-tide inundation area sub-<br>category | 3.1m AHD + 0.5m<br>(1% AEP level at 2100 +<br>0.5m)  | 3.1m AHD + 0.3m<br>(1% AEP level at 2100<br>+0.3m) | 3.1m AHD (1% AEP<br>level at 2100) | 2% AEP level | 2% AEP level |

Note-

• Where the site is subject to more than one flooding source that is storm-tide flooding, overland flow flooding, creek/waterway flooding or river flooding, the minimum flood immunity level is the highest level determined from these sources.

• The Coastal hazard planning scheme policy and Flood planning scheme policy the set out the flood risk assessment process for coastal hazards.

### Table 8.2.6.3.D—Flood planning level categories for development types

| BCA building classification <sup>(1)</sup> | Development types and design levels, assigned design floor or pavement levels                                    | Category<br>refer to Table 8.2.6.3.C |
|--|--|--------------------------------------|
| Class 1-4 <sup>(7)</sup>                   | Habitable room <sup>(1)</sup>  | Category A                           |
|  | Non-habitable room<br>including patio and courtyard  | Category B                           |
|  | Non-habitable part of a Class 2 or Class 3 building excluding the essential services <sup>(2)</sup> control room | Category B                           |
|  | Parking located in the building undercroft of a multiple dwelling  | Category C                           |
|  | Carport <sup>(4)</sup> ; unroofed car park; vehicular manoeuvring area   | Category D                           |
|  | Essential electrical services <sup>(2)</sup> of a Class 2 or Class 3 building only                               | Category A <sup>(6)</sup>            |
|  | Basement parking entry <sup>(3)</sup>  | Category C + 300mm                   |
| Class 5,                                   | Building floor level   | Category C                           |

| Class 6, or            | Garage or car park located in the building undercroft <sup>(3)</sup>         | Category C   |
|------------------------|--|--|
|                        | Carport <sup>(4)</sup> or unroofed car park                                  | Category D   |
|                        | Vehicular access and manoeuvring area  | Category D   |
|                        | Basement parking entry <sup>(3)</sup>  | Category C   |
|                        | Essential electrical services <sup>(2)</sup>                                 | Class 8 – Category C <sup>(6)</sup><br>Class 5 and 6 – Category A <sup>(6)</sup> |
| Class 7a               | Refer to the relevant building class specified in this table                 |  |
| Class 7b               | Building floor level   | Category C   |
|                        | Vehicular access and manoeuvring area  | Category D   |
|                        | Essential electrical services <sup>(2)</sup>                                 | Category C   |
| Class 9 <sup>(7)</sup> | Building floor level   | Category A   |
|                        | Building floor level in Class 9a or 9c where for a residential care facility | 0.2% AEP flood   |
|                        | Garage or car park located in the building undercroft <sup>(3)</sup>         | Category C   |
|                        | Carport <sup>(4)</sup> or unroofed car park                                  | Category D   |
|                        | Vehicular access and manoeuvring area  | Category D   |
|                        | Essential electrical services <sup>(2)</sup>                                 | Category A   |
| Class 10a              | Car parking facility   | Refer to the relevant building class specified in this table                     |
|                        | Shed <sup>(5)</sup> or the like  | Category D   |
| Class 10b              | Swimming pool  | Category E   |
|                        | Associated mechanical and electrical pool equipment                          | Category C   |

Note—

(1) Refer to Building Code of Australia for definitions of building classifications and habitable rooms.

(2) Essential services include any room used for fire control panel, telephone PABX, sensitive substation equipment, including transformers, low voltage switch gear, high voltage switch gear, battery chargers, protection control and communication equipment, low voltage cables, high voltage cables, and lift controls. (3) Basement car parks must be suitably waterproofed and all air vents, air-conditioning ducts, pedestrian access and entry and exit ramps into the basement must comply with the applicable flood planning levels in this table.

(4) A shelter for a motor vehicle, which has a roof and one or more open sides, and which can be built against the side of a building.

(5) A slight or rough structure built for shelter and storage; or a large strongly built structure, often open at the sides or end.

(6) Where essential electrical services are proposed in a basement below the specified flood immunity level, the flood immunity of all air vents, air-conditioning ducts, pedestrian access, lift shafts and entry and exit ramps at the basement entrance and any other openings into that basement are to conform with the flood planning levels for Category A for residential development, and the relevant basement entry level of all other uses. To ensure flood immunity, basements require a waterproof design to prevent flood waters entering the basement.

(7) Where a building includes a combination of uses that includes a component of classes 2, 3 or 9, the essential services for that building shall comply with the requirements of the building class with the greatest flood planning level.

### Table 8.2.6.3.E—Flood planning levels for essential community infrastructure

| Type of essential community infrastructure  | Recommended planning levels for storm tide  |
|---|---|
| Community facility where involving storage of valuable records or items of historic or cultural significance, such as galleries and libraries | 0.5% AEP level  |
| Educational establishment   | 0.5% AEP level  |
| Emergency services where for an emergency shelter   | 0.5% AEP level or per Design Guidelines for Queensland Public Cyclone Shelters  |
| Emergency services where for police facilities <sup>(1)</sup>   | 0.5% AEP level  |
| Emergency services <sup>(1)</sup>   | 0.2% AEP level  |
| Hospitals and health care service where supporting a hospital   | 0.2% AEP level  |
| Major electricity infrastructure and substations <sup>(1)</sup>   | 0.5% AEP level  |
| Major or minor electricity infrastructure not otherwise listed in this table.<br>Telecommunications facilities                                | No specific recommended level but infrastructure is to be optimally located and designed to achieve suitable levels of service, having regard to the processes and policies of the relevant administering public sector entity. |
| Power stations as defined in the <i>Electricity Act 1994</i> or renewable energy facility   | 0.2% AEP level  |

| School facilities   | 0.5% AEP level  |
|---|-----------------|
| Utility installation where for a sewage treatment plant               | 0.01% AEP level |
| Utility installation where for a water treatment plant <sup>(1)</sup> | 0.5% AEP level  |

Note—

(1) This only applies to the electrical and other equipment that if damaged by floodwaters or debris, would prevent the infrastructure from functioning.

# Table 8.2.6.3.F—Table of processes requiring additional assessment in a coastal hazard area

| Process  |
|--|
| (1) Oil refining or processing   |
| (2) Producing, refining or processing gas or fuel gas  |
| (3) Power station, including the activity of generating electricity by using fuel  |
| (4) Producing, quenching, cutting, crushing or grading coke  |
| (5) Waste incinerator, including thermal treatment of waste  |
| (6) Pulp or paper manufacturing  |
| (7) Tannery or works for curing animal skins, hides or finishing leather   |
| (8) Textile manufacturing, including carpet manufacturing, wool scouring or carbonising, cotton milling, or textile bleaching, dyeing or finishing |
| (9) Rendering plant, including meat processing   |
| (10) Manufacturing chemicals, poisons and explosives   |
| (11) Manufacturing fertilisers involving ammonia   |
| (12) Manufacturing polyvinyl chloride plastic  |
| (13) Major hazard facilities for the storage and handling of dangerous goods   |
| (14) Storage of hazardous chemicals in quantities exceeding the hazardous chemicals flood hazard threshold in Table 8.2.6.3.J.                     |

| (15) Manufacturing medium-density fibreboard, chipboard, particle board, plywood, laminated board or wood veneer products   |
|---|
| (16) Manufacturing or processing plaster  |
| (17) Enamelling workshop  |
| (18) Galvanising works  |
| (19) Anodising or electroplating workshop   |
| (20) Powder-coating workshop  |
| (21) Treating timber for preservation using chemicals including copper, chromium, arsenic, borax and creosote   |
| (22) Manufacturing soil conditioners by receiving, blending, storing, processing, drying or composting organic material or organic waste, including animal manures, sewage, septic sludges and domestic waste |
| (23) Manufacturing tyres, asbestos products, asphalt, cement, glass or glass fibre, mineral wool or ceramic fibre   |
| (24) Abattoir, including meat processing  |
| (25) Recycling chemicals, oils or solvents  |
| (26) Waste disposal activity (other than waste incinerator), including waste transfer station operation   |
| (27) Recycling, storing or reprocessing regulated waste, including regulated waste treatment  |
| (28) Manufacturing batteries and battery recycling  |
| (29) Drum and container reconditioning  |
| (30) Water treatment  |
| (31) Sewage treatment   |
| Note—Further information and risk assessment concerning hazardous chemicals in coastal management areas is contained in Management of hazardous chemicals in flood affected areas planning scheme policy.     |

## Table 8.2.6.3.G—Flood planning levels for reconfiguring a lot

|--|

Page 14 of 16 Print Date: 08/12/2022 cityplan.brisbane.qld.gov.au

|   | Residential<br>(creating 6 or less lots with no<br>new road)        | Residential<br>(creating more than 6 lots), or<br>a new road | Other than residential                 |
|---|---|--|--|
| Storm-tide flooding within the:<br>High storm-tide inundation area sub-category; or<br>Medium storm-tide inundation area sub-category | 80% of each new lot at 2.5m<br>AHD <sup>(1)</sup><br>(1% AEP level) | 3.1m AHD + 0.3m<br>(1% AEP flood level at 2100 +<br>0.3m)    | 3.1m AHD<br>1% AEP flood level at 2100 |

Note—

(1) In addition to providing suitable flood immunity for a dwelling house to be constructed, this will ensure that each new lot will not be affected by tidal influences with an allowance for 800mm of sea level increase to 2100. The minimum area must have direct frontage to a road that will be used for accessing the lot.

Note—Where the site is subject to more than one flooding source the minimum flood planning level is the highest level determined from these sources.

#### Table 8.2.6.3.H—Flood planning levels for a new road and off-road paths

| Flooding type   | Minimum design levels at crown of road (m AHD) |                                      | Off-road pedestrian and cyclist |
|---|--|--------------------------------------|---------------------------------|
|   | Residential development                        | Industrial or commercial development | paths                           |
| Storm-tide flooding within the:<br>High storm-tide inundation area sub-category; or<br>Medium storm-tide inundation area sub-category | 3.1m AHD<br>1% AEP level at 2100               | 3.1m AHD<br>1% AEP level at 2100     | HAT + 0.3m <sup>(1)</sup>       |

Note—

(1) This is to ensure that new off-road paths will not be affected by highest astronomical tide (HAT) with an allowance for 300mm of sea level increase by 2050.

Note—Where the site is subject to more than one flooding source, the minimum flood planning level is the highest level determined from these sources.

### Table 8.2.6.3.I—Flood planning levels for existing road providing access to or fronting a development

| Flooding type   | Minimum design levels at the crown of the road (m AHD) |                    |   |
|---|--|--------------------|---|
|   | Local road   | Neighbourhood road | District road,<br>suburban road,<br>arterial road |
| Storm-tide flooding within the:<br>High storm-tide inundation area sub-category; or | 5% AEP   | 2% AEP             | 2% AEP  |

| Medium storm-tide inundation area sub-category |  |  |  |
|--|--|--|--|
|--|--|--|--|

Note—Where the site is subject to more than 1 flooding source the minimum flood planning level is the highest level determined from these sources.

Note—The design standard for an industrial access is the 5% AEP storm-tide level.

#### Table 8.2.6.3.J – Hazardous chemicals flood hazard threshold

Hazardous chemicals flood hazard threshold means any of the following:

A hazardous chemical listed in schedule 11 of the Work Health and Safety Regulation 2011 in a quantity that exceeds a threshold quantity stated in column 5 of schedule 11

A chemical classified as hazardous to the aquatic environment under the Australian Dangerous Goods Code in the Acute I or Chronic I category that exceeds 2500 litres or kilograms

A chemical classified as hazardous to the aquatic environment under the Australian Dangerous Goods Code in the Chronic II category that exceeds 10,000 litres or kilograms

A chemical classified as hazardous to the aquatic environment under the Australian Dangerous Goods Code and assigned to Packing Group III that exceeds 10,000 litres or kilograms

A chemical classified as hazardous to the aquatic environment under the Globally Harmonised System of Classification and Labelling of Chemicals that exceeds 10,000 litres or kilograms