

PLANS AND DOCUMENTS referred to in the PDA DEVELOPMENT APPROVAL



Approval no: DEV2022/1321

Date: 27 February 2023

CARSELDINE VILLAGE STAGE V

ENGINEERING SERVICES REPORT





DOCUMENT REGISTER

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INTRODUCTION

KN Group have been commissioned by Economic Development Queensland – Urban Development (EDQ UD) to prepare an engineering services report for the proposed Stage V of Carseldine Village located at 520 Beams Road, Carseldine.

The proposed Stage V development proposes:

- 3 new commercial lots;
- 1 public plaza lot;
- 1 open space/bushland lot;
- an access easement;
- new road;
- boundary realignment with Lot 322 on SP311781; and
- works in Lot 322 on SP311781 related to earthworks retaining, pedestrian connectivity and stormwater infrastructure.

Refer to the Appendix A RPS Plan of Subdivision Plan Reference 128180-123 & 124.

This report addresses the proposed development of Stage V of the Carseldine Village development only however continuity with the masterplan of the overall development has been considered. The proposed commercial lots will be the subject of future development application(s) by third party developers.

The town planning application is in accordance with the existing overall Masterplan Approval (amended) granted in September 2021 (EDQ Ref: DEV2018/932/3) and reflects the intent of the approval.

The PDA development application seeks PDA development approval from the Minister for Economic Development Queensland (MEDQ) for:

 Development Permit for Reconfiguring a Lot (Stage V of Carseldine Village - 3 commercial lots, 1 public plaza lot, 1 open space/bushland lot, an access easement, new road reserve, boundary realignment and works in Lot 322 on SP311781).

The proposed development is located within the Brisbane City Council (BCC) local government area with Urban Utilities (UU) the designated retail water authority.

This report identifies civil infrastructure required to service the proposed development. The civil infrastructure identified within this report includes bulk earthworks, roads, stormwater drainage, water and sewer reticulation and other service utilities.



SITE CHARACTERISTICS

The site is currently unoccupied state land and is located within the Fitzgibbon Priority Development Area (PDA) under Economic Development Queensland Fitzgibbon PDA Development Scheme (2011). Located within Carseldine Village at 520 Beams Road, Carseldine, the site is within the BCC local government catchment.

Within Carseldine Village Stages S (sport and recreation precinct), 1 and 2 have reached construction completion, and Stages 3A, & 4A are close to practical completion. The proposed Stage V development is contained within the western part of Lot 7002 on SP311913, comprising of approximately 2.493 hectares of the total 5.83 hectares.

The larger Carseldine Village development site is bound by Beams Road to the north, Cabbage Tree Creek to the south, North Coast Railway to the east and Dorville Road to the west.

LAND TOPOGRAPHY AND SITE DRAINAGE

Stage V contains the Carseldine Village sales and information centre, C&K child care centre encompassed by bushland and grass cover and an existing private access driveway. The pre-development terrain is relatively varied between approximately RL26.0 to RL13.5 AHD, with the site falling northeast at an approximate grade of 7.0% from southern west boundary.

The proposed stage of works will be filled to the range of RL18 to RL13.5 (excluding the southern batter in proposed Lot V002 down to the proposed road corridor, grading to an approximate invert of RL16.5), with approximately 5,000m³ of select fill imported from off site into the stage.

Site drainage within the stage will discharge primarily to the proposed road corridor (extension of Meander Street) and be collected by the piped stormwater system, connecting to the existing network on Plaza Place. Existing upstream stormwater constructed as part of previous development works will be adequately tied in as part of the proposed drainage works.

EROSION AND SEDIMENT CONTROL

During the construction phase of the development, erosion and sediment control measures will be implemented and maintained. An erosion and sediment control strategy will be created during the Operational Works phase of the development to recognise the potential risks and control measures to be designed accordingly.

The contractor will prepare an Erosion and Sediment Control Plan (ESCP) certified by an RPEQ or an accredited professional in erosion and sediment control (CPESC) generally in accordance with the following guidelines:

- Urban Stormwater Quality Planning Guidelines, dated 2010, prepared by the former Department of Environment and Heritage Protection;
- Best Practice Erosion and Sediment Control, dated November 2008, prepared by the International Erosion Control Association Australasia (as amended from time to time);
- State Planning Policy (DILGP, 2017);
- Appendix B (IECA, 2018); and
- Complying with the SPP Technical Note for Government Development Assessment & Compliance Officers (Healthy Land and Water, 2018).



In accordance with the State Planning Policy (DILGP, 2017), Type 1 sediment controls (sediment basins) are designed to achieve 80% hydrologic efficiency (HE) and are deemed to comply. A range of approaches are considered acceptable to achieve compliance with the 80% HE objective, being:

- High Efficiency Sediment (HES) Basins in accordance with IECA (2018);
- Large Traditional Sediment Basins (in accordance with Table 2 of HLW,2018);
- Total Capture hold all water on site;
- Alternative Innovative Measures; and
- Erosion Control.

The contractor will be required to implement the certified ESCP and maintain a register of inspections and testing results which must be available for review by the MEDQ or another relevant authority at any time during construction.

INFRASTRUCTURE FOR DEVELOPMENT

5.1 ROADWORKS

The proposed development features a 19m road corridor with a 6m wide access street, intersecting the site linking the existing Beams Road / Meander Street intersection with the existing Plaza Place / Meander Street intersection (NB. both Meander Street intersection stubs were created with Stage 1 works). The road provides potential for direct vehicular and pedestrian access to each individual allotment within the site including sufficient width for future concrete footpaths for pedestrian access, including additional roadside parking to be constructed with the proposed Stage v works. All verge works are to be in accordance with the proposed typical cross-sections for commercial streets.

Proposed road and path typology is in accordance with the Technical Traffic Memorandum prepared by Cardno, to support Stage V of the Carseldine Village development.

Appendix B demonstrates the proposed road network and hierarchy for the proposed development. The design of roadworks will be in accordance with BCC requirements, Austroads Guidelines and all other relevant standards and specifications.

5.2 EARTHWORKS

A number of environmental and geo-technical reports have been conducted across the site which will be implemented as required, these include:

- SGS Geotechnical Investigation Report, dated 29th May 2018;
- Golder Asbestos Remediation Strategy during Stormwater Pipe Removal dated 30th September 2020;
- Gallagher Environmental Dispersive Soil Management Plan (DSMP), dated 22nd April 2020; and
- Gallagher Environmental Acid Sulfate Soil (ASS) Review, dated 22nd December 2020.

The above reports can be found in Appendix F and Appendix G of this report.

A further, more detailed geotechnical investigation report has been commissioned by EDQ UD and will be provided to the MEDQ shortly for review.



Localised filling within the development will occur in accordance with AS 3798 under Level 1 supervision. An assessment of the Brisbane City Council *Brisbane City Plan 2014* Filling and excavation code has been included in Appendix H to demonstrate compliance with relevant requirements.

A preliminary bulk earthworks plan has been included in Appendix B. Earthworks will be required to achieve suitable road grades throughout the proposed development site and for finished surface levels in the proposed development to tie into the surrounding land at the boundary of the proposed development site.

5.3 STORMWATER QUANTITY, FLOOD MANAGEMENT AND QUALITY

A Stormwater Technical Memorandum has been prepared by DesignFlow to confirm the stormwater management measures proposed to support the proposed Stage V development.

Previous stormwater treatment strategy and flood impact assessments have been assessed and approved as part of previous whole of site stormwater modelling, which have been updated through recent stages of development over the site. Specifically, Stage 1 works are completed including all required water quality treatment and flood mitigation measures.

The Stormwater Management Technical Memorandum is located within RPS Planning report.

5.5 STORMWATER DRAINAGE INFRASTRUCTURE

A complete underground piped stormwater system will be provided as a part of the proposed development. The stormwater system will capture stormwater runoff for the minor event in gullies and field inlets and convey it through underground infrastructure. Surface water from the major event is directed to the roadway and conveyed off site overland.

Passive irrigation of street trees from stormwater runoff is also proposed and will achieve additional WSUD outcomes in addition to the overall masterplan strategy. Refer the Landscape design drawings prepared by Saunders Havill for further details.

A catch drain, and associated maintenance access driveway is proposed to be constructed immediately south of proposed Lot V002, in Lot 322 on SP311781, to manage stormwater from the upstream catchment. This catch drain is a Phase 2 works component connecting into the Phase 1 component which was constructed with the Stage 2 works.

Concept plans of the catch drain have been prepared and included in Appendix C.

The design of all stormwater infrastructure will be in accordance with Queensland Urban Design Manual (QUDM) and Brisbane City Council (BCC) standard drawings. A preliminary stormwater layout plan is included in Appendix B of this report indicating the proposed layout of stormwater infrastructure for the proposed development.

5.6 SEWERAGE

The proposed sewer network will be in accordance with the Services Advice Notice dated 15th October 2018 and Urban Utilities Water and Wastewater Analysis dated 15th June 2020, Refer Appendix D for copy of these notices.



The development will be serviced with a new sewer reticulation main, connecting to each individual allotment. The gravity sewerage mains will connect to the existing DN160 dia sewer main constructed as part of Stage 1.

A preliminary sewer layout plan has been included in Appendix B which shows the proposed sewer infrastructure to be constructed as part of the proposed development. All sewer infrastructure will be designed in accordance with the SEQ Water Supply and Sewerage Design and Construction Code and UU Design Criteria.

5.7 WATER RETICULATION

The proposed water network will be in accordance with Services Advice Notice dated 15th October 2018 and Urban Utilities Water and Wastewater Analysis dated 15th June 2020, Refer Appendix E for copy of these notices.

A new DN250 water reticulation main will be constructed to service the proposed development with potable water. The proposed watermain will connect into the existing DN300 watermain along Beams Road and the existing DN250 watermain along Plaza place. It will provide connection to all commercial lots within the stage where each individual allotment will be provided individual service connections and meters.

A preliminary water reticulation layout has been included in Appendix B. All water reticulation will be designed in accordance with the SEQ Water Supply and Sewerage Design and Construction Code and UU Design Criteria.

5.8 ELECTRICAL, TELECOMMUNICATIONS AND GAS

All proposed allotments will be serviced with underground electricity and telecommunication (NBN) services. New infrastructure in relation to these utilities will be constructed as a part of the proposed development to service individual allotments. All electrical, NBN and gas infrastructure will be constructed in accordance with the relevant authorities and service providers. Further information in regards to the services will be provided as a part of the Operational Works application. Refer Appendix D for Dial Before You Dig (DBYD) existing services search.

SUMMARY

This Engineering Services Report relating to the proposed Carseldine Village Stage V development has demonstrated the following:

- The proposal is for the construction of 3 commercial lots, 1 public plaza lot, 1 open space/bushland lot, an access easement, new road reserve, boundary realignment and works in Lot 322 on SP311781;
- The proposed road network will connect into preceding Stages 1, 2, 3A and 4A;
- Each individual allotment will have direct access to the proposed road network;
- Earthworks will be necessary throughout the proposed development area to satisfy design lot pad levels, road grades and for the installation of underground infrastructure;
- New stormwater infrastructure will be constructed as a part of the new development. Stormwater flows
 will be conveyed through the proposed development site, discharging into the existing piped drainage
 network.
- Passive irrigation of street trees from stormwater runoff is proposed and will achieve additional WSUD outcomes for the development;
- New sewerage infrastructure will be constructed to service individual allotments. Gravity sewer mains will connect to existing infrastructure constructed as part of Stage 1;



- New water reticulation infrastructure will be constructed to service individual allotments. Reticulation mains will connect to existing infrastructure constructed as part of Stage 1; and
- The information presented in this report demonstrates that the proposed development may be constructed in accordance with the *Economic Development Act 2012* relevant standards, guidelines and manuals outlined within the EDQ Engineering Standards PDA Guideline No. 13. with respect to civil engineering matters.



APPENDIX A PLAN OF SUBDIVISION

KEY MAP

Scale: 1: 10,000

URBAN DESIGN Level 4 HQ South 520 Wedham Street PO Box 1559 Forttude Valley QLD 4006 T 7461 7 3539 9500 W rpsgroup.com

Saleable Allotments

Total Stage Area

Land Use

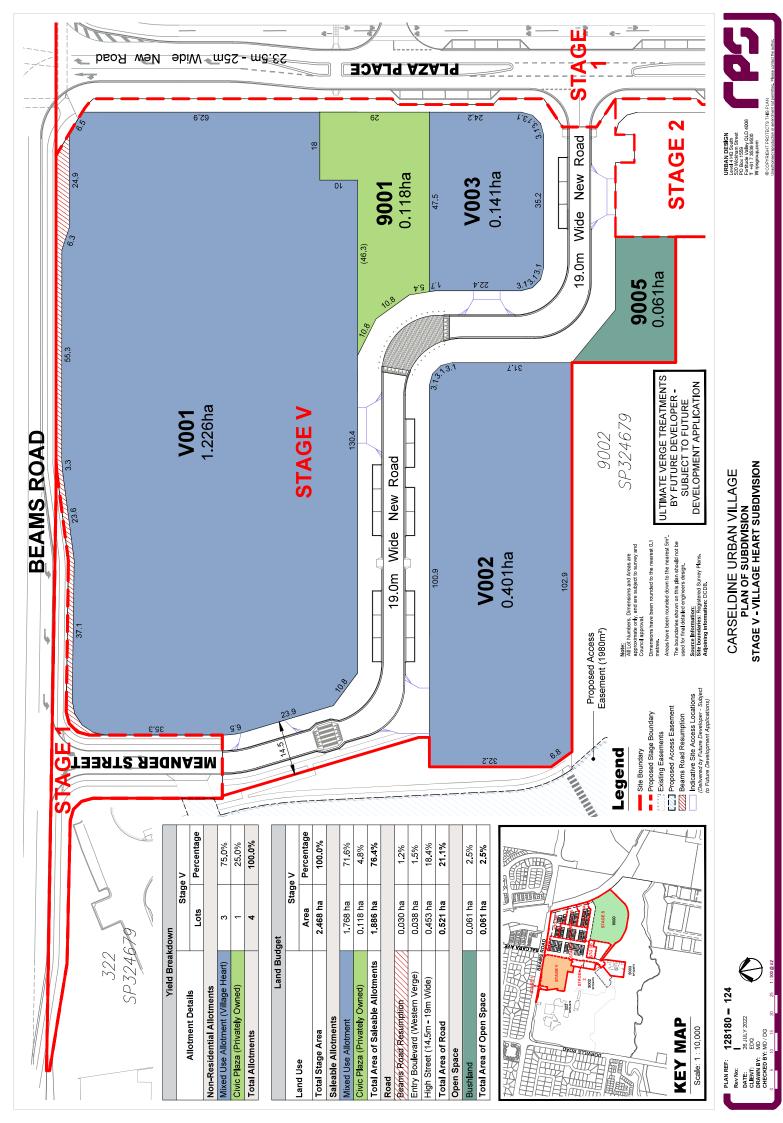
Total Allotments

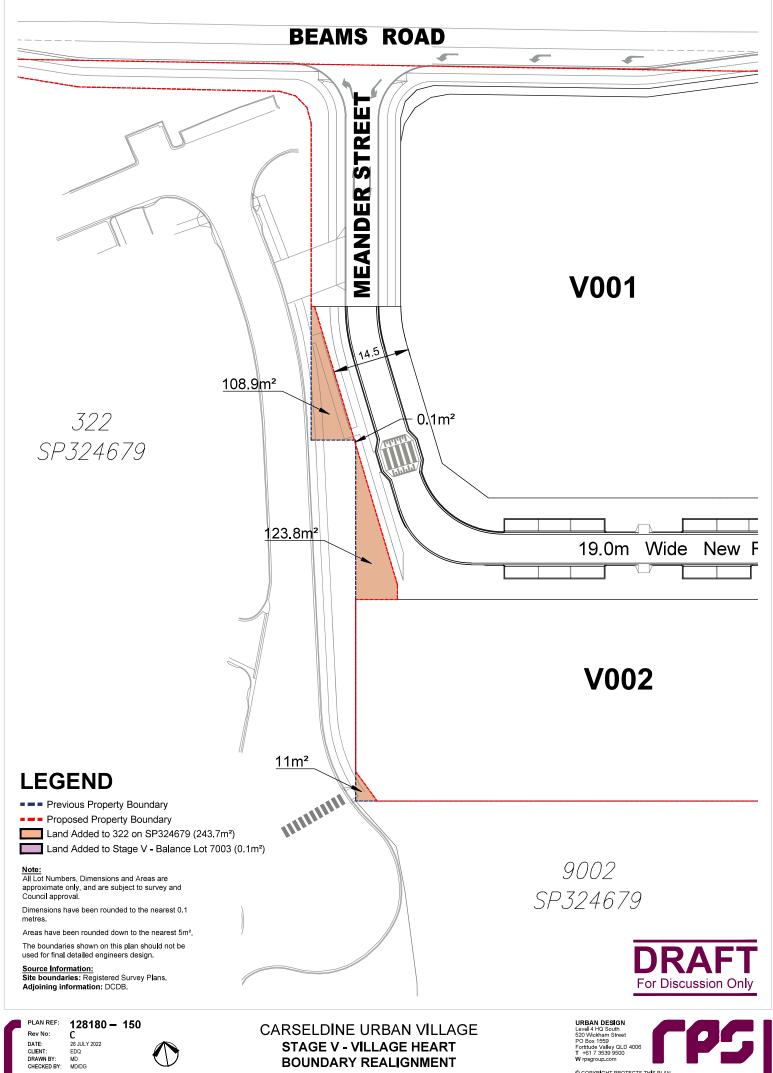
Aixed Use Allotment

Road

Total Area of Road

Open Space





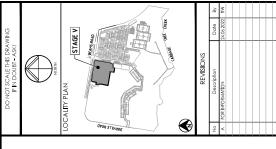


BOUNDARY REALIGNMENT





APPENDIX B CIVIL FUNCTIONALS



ECONOMIC DEVELOPMENT QUEENSLAND (EDQ)

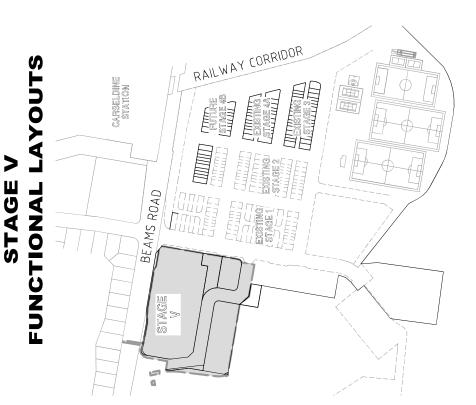
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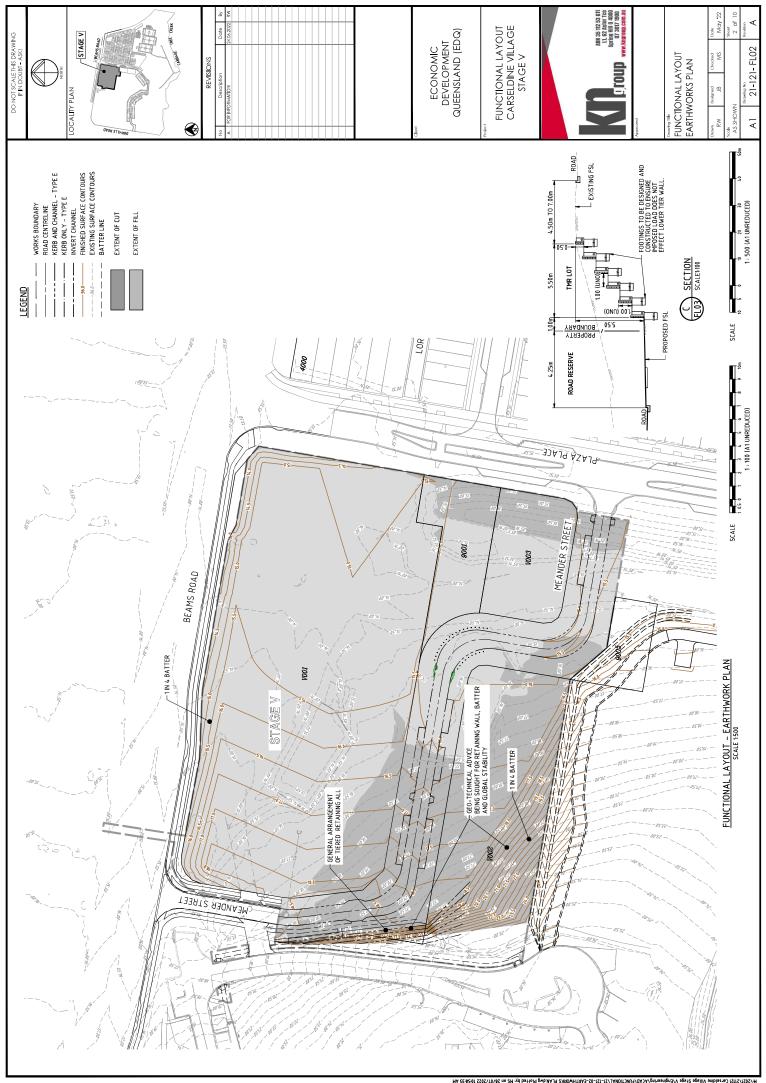
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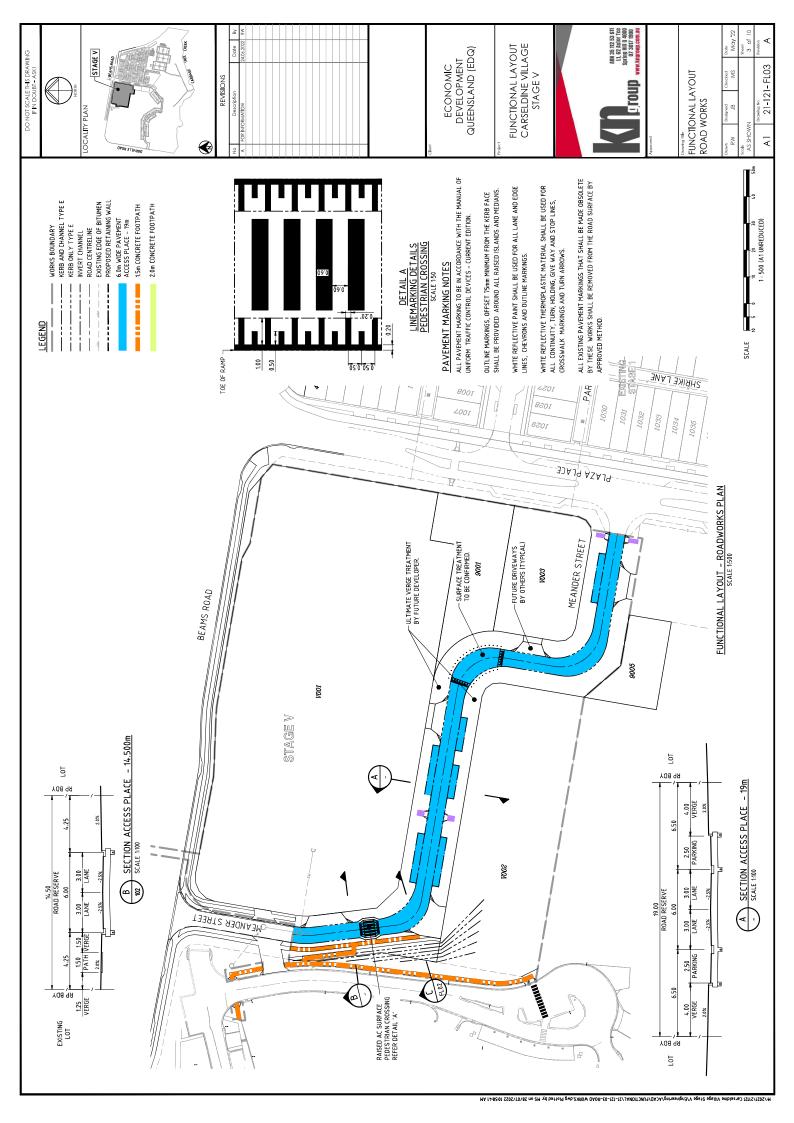
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report FUNCTIONAL LAYOUT CARSELDINE VILLAGE STAGE V	dno.jó Jy
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CARSELDINE VILLAGE

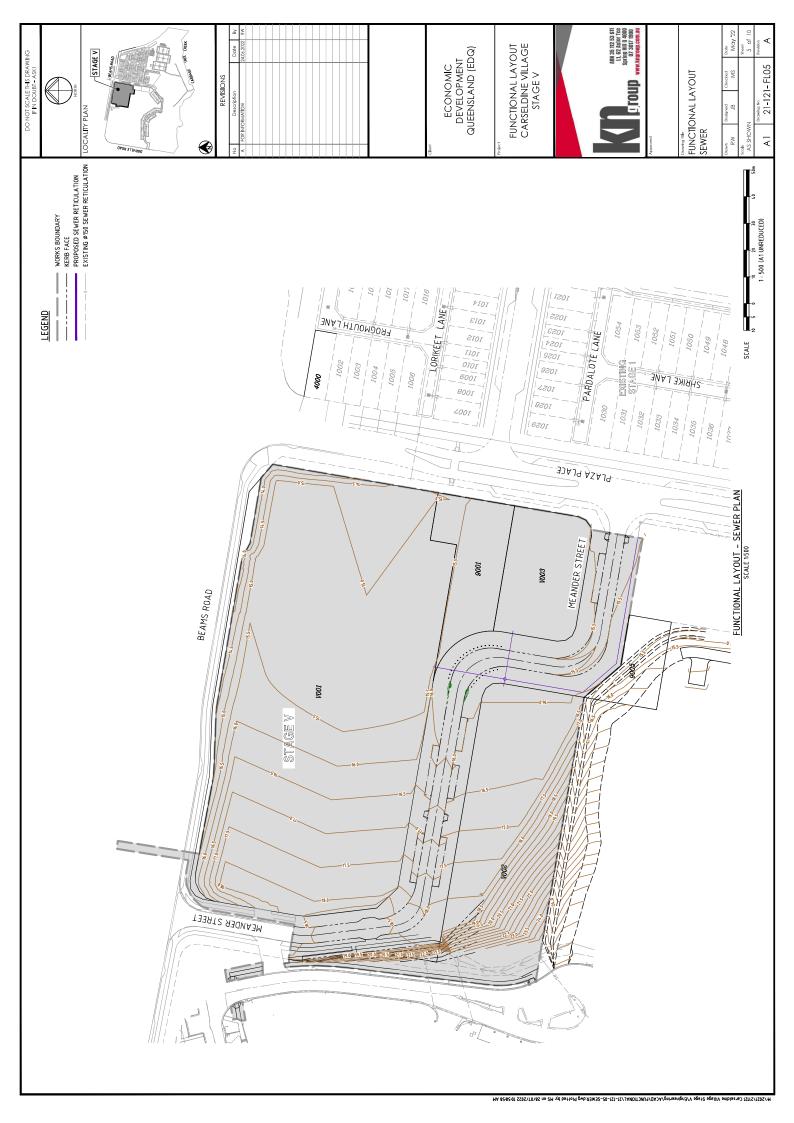


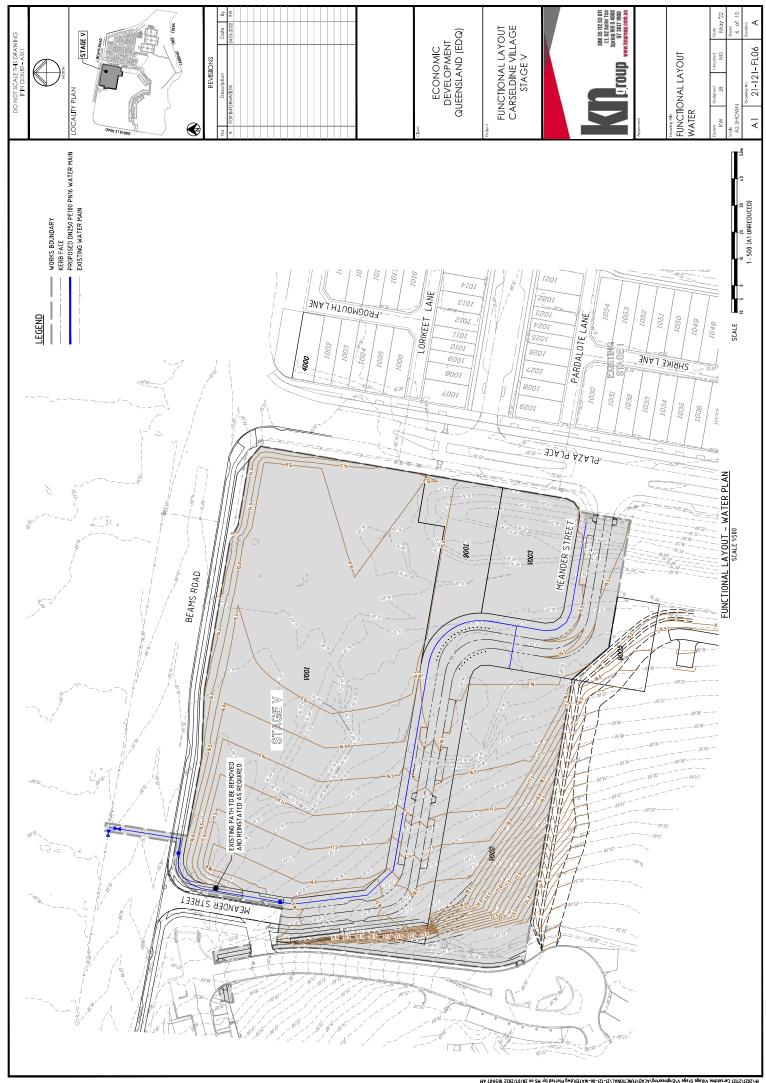
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	DRAWING NO.	21-121-FL01	21-121-FL02	21-121-FL03	21-121-FL04	21-121-FL05	21-121-FL06	21-121-FL07	21-121-FL08	21-121-FL09	21-121-FL10
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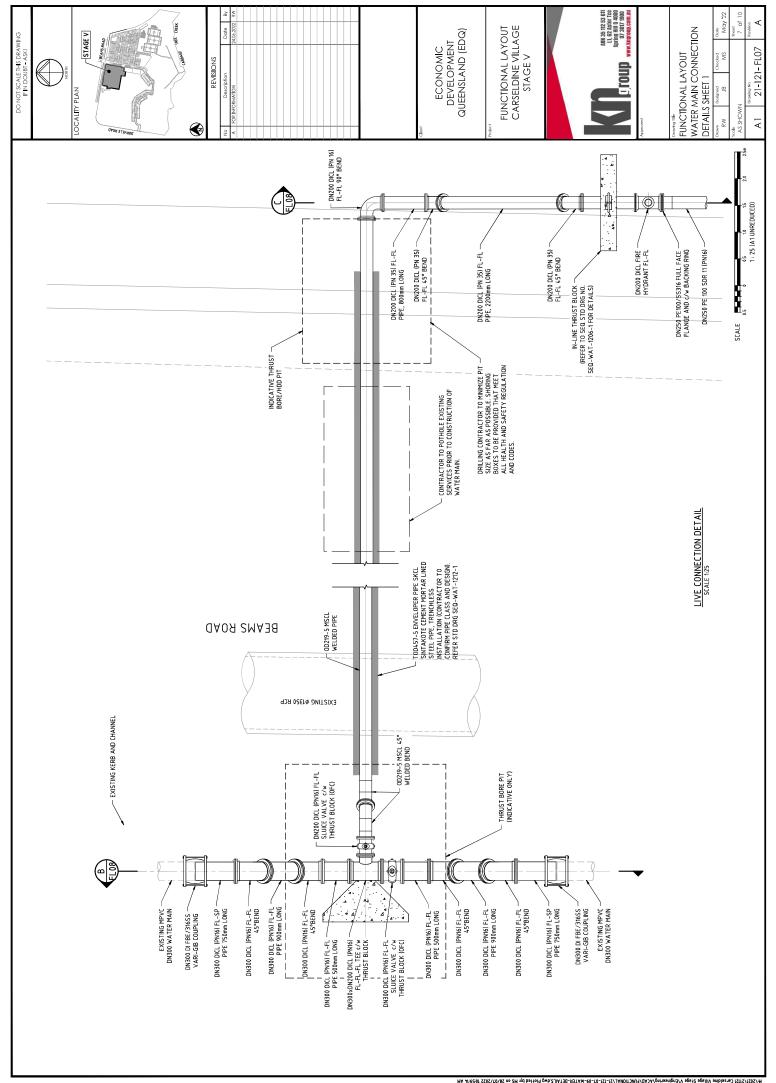


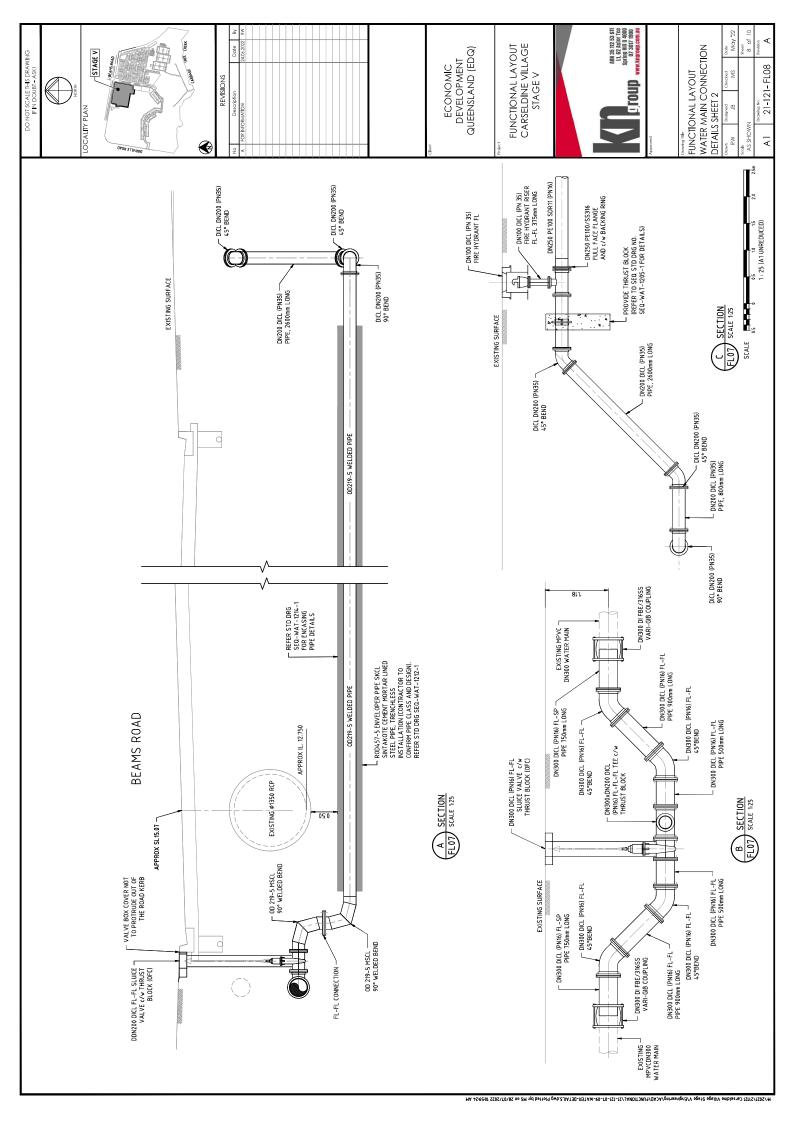












ASSET REGISTER - WATER RETICULATION STAGE V STAGE V STAGE V STE ADDRESS STATE/STAGE CARRELDNE VILLAGE - STAGE V STE ADDRESS STATE/STAGE CARRELDNE VILLAGE - STAGE V STE ADDRESS STATE/STAGE CARRELDNE VILLAGE CAR		No.	77	2	19										•			_	
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SERVICE DETAILS	LOT NUMBERS	-	-	-
	SIZE	40mm	32mm	25mm
	No.	77	5	19

ALL ENVIRONMENT PROTECTION MEASURES SHALL BE IMPLEMENTED PRIOR TO ANY CONSTRUCTION WORK, INCLUDING CLEARING, COMMENCING.

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NOTE:
ALL CONSTRUCTION WORK SHALL COMPLY WITH THE
REQUIREMENTS OF THE QUERENSLAND WORK HEALTH AND
RETTY ACT 2011 CONTACT THE WISHON ON WORKPLACE
HEALTH AND SAFETY FOR MICHANTION; PHONE 1300 362 728.

ALL WATER AND SEWER CONSTRUCTION WORK UNDERTAKEN BY THE CONTRACTOR SHALL COMPLY WITH ALL APPLICABLE WORKPLACE HEALTH AND SAFETY LEGISLATION.

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ENERAL NOTES

- 1. ALL WORK AND WITERIALS SHALL BE IN ACCIDIANCE WITH CURRENT SOUTH EAST WATER SUPPLY CODE SPECIFICATIONS AND STANDARDS & URBAN UTH LIFE TERNIKAL GOIDEINE. DESON AND DOCOMENTATION OF MATTER RETUGLATION AND WASTEWATER (SEWERAGE) NATER RETUGLATION.
- UNLESS SPECIFIED OTHERWISE ALL MATERIALS AND WORK SHALL COMPLY WITH THE RELEVANT AUSTRALIAN STANDARDS.
- ADOPT LIP OF KERB OR SHOULDER OF ROAD AS PERMANENT LEVEL.
- COVER OWNER MANNEY FROM PERMANENT LEVEL OBE AS SHOWN IN 23. WI STANDRADD BRANNEN NO. SEG. WAT-YOU'S. S. STANDRADD BRANNEN SEG. WAT-YOU'S. F. S. STANDRADD BRANNEN NO. SEG. WAT-YOU'S. F. CONSTRUCT BYBEDMENT AND TRENCHELL TO SEG. "WAT-720-2". 1201-1
 - CONSTRUCT EMBEDMENT AND TRENCHEIL TO SEQ.-WAT-1200-2, 1201-1
 TO SEQ.-WAT-1200-11 PIPE D SUPPORT UNIESS GEGTEMENTAL
 MINESTERATIONS DEPONSTRATE HAT TYPE C SUPPORT IS ABEQUATE
 AND PSWICH CITY COUNCIL STANDARDS FOR ROADWAY CROSSINGS.

 24. WHICHEVER IS WORE ONEROUS.
 - CONSTRUCT THRUST BLOCKS ON ALL VALVES, BENDS, TEES, TAPERS, DEAD ENDS, AND TRANSITIONS TO UNRESTRAINED PIPEWORK TO SEG-WAT-1205-1 TO SEG-WAT-1207-1.

. 6

- SLG-WAT-1259-1 10 SLG-WAT-1207-1.
 WATER SERVICES UNDER ROADS MUST BE PLACED WITHIN A ¢100mm
 CONDUIT REFER TO SEG-WAT-1107-1
- A WATER METER SUPPLED AT THE DEVELOPER'S COST, IS TO BE INSTALLED AT THE SERVICE POINT OF EACH LOT IN ACCORDANCE WITH STANDARD DRAWING NO. SEQ.-WAT-1107-3.

6

- ALL MATERIALS USED IN THE WORKS SHALL COMPLY WITH THE URBAN UTILITIES FAM ACCEPTED PRODUCTS AND MATERIALS LIST ALL CAST IRON HITHOS SHALL BE TO ASSSA4, WITH SOCKET ENDS DESIGNED FOR USE WITH DUCTILE IRON PIPES AND FOR WATER SUPPLY PURPOSES SHALL BE L'UGHT LEND IN THE SUPPLY PURPOSES SHALL BE L'UGHT L'EMBNI LINED.
- OTHER TYPES AND CLASSES OF PIPES SHALL NOT BE INSTALLED.
- CAST IRON GATE (SLUICE) VALVES SHALL CONFORM TO AS2638.
 ALL VALVES AND HYDRANTS SHALL BE COATED INTERNALLY AND
 EXTERNALLY WITH A FUSION BONDED EPOXY.
- -ALL NUTS AND WASHERS SHALL BE STANLESS STEEL GRADE 316.
 ALL STANLESS STEEL NUTS AND BOUTS WIST BE ASSEMBLE DWITH AN ANT-GALLING COMPOUND 'UDRALAC' OR APPROVED EQUIVALENT AS PRESTE WATER SUPPLY CODE LANSE, AMD DRAWNIG
 - SEQ-WAT-1313-1. All concrete footpaths to be clear of water mains (where applicable).

6

- CONSTRUCT TEST POINTS TO SEQ.-WAT.-Ku0-1AT THE ENDS OF ALL
 NEW TAMNS BEROBE THE SCOUR AND WHERE REQUIRED DOR
 COMMISSIONNE URPORSES, UBBAUTILITES PREFERENCES TO AVOID
 TAPPING BANDS FOR TEST POINTS AND PROVIDE ETHER A TEMPORARY
 RESTRANKED DUCKFOOTH YPRANT OR FLANKED SHORT PIPE WITH A
 TEMPORARY TAPPED BLANK FLANGE. TESTING AGAINST LIVE MAINS
 AND VALVES IS NOT PERMITTED.
- TESTING LOCATIONS AND TEMPORARY FITTINGS ARE REQUIRED ON REPRETES DUES TO NO. LINGO MULTES, SAFRONCED IN WITHING FIRM WORKS TO BE UNDETRAKEN AS LIVE WORKS. TESTING AND AS-CONSTRUCTED REQUIREMENTS TO BE DOCUMENTED ON DRAWINGS.

12

- MARKERS SHALL BE INSTALLED FOR ALL SERVICE (ROSSINGS, HYDRANTS AND VALVES IN ACCORDANCE WITH STANDARD DRAWING Nos. SEQ-WAT-1107-1, SEQ-WAT-1300-1 AND SEQ-WAT-1300-2.
- THE CONSTRUCTION OF THE WATER RETICULATION WORK SHOWN ON THIS DRAWING MUST BE SUPERVISED BY AN ENGINEER WHO HAS R.P.E.Q. REGISTRATION, WORKS ON'T COMPLYING WITH THIS REQUIREMENT WILL WITH BE PRAMITED TO CONNECT TO THE RETICULATION SYSTEM.

7

MA 45.82.01 S2057/00AEL NO BM 746 Bettel DETAILS.ANG Plotted by MS on 28/07/2021 10.82.4. MS

- WATER MAIN SHALL BE LAID AT 2.500m ALIGNMENT FROM PROPERTY BOUNDARY UNLESS NOTES OTHERWISE.
- WHERE PERMANENT HYDRANTS ARE NOT INSTALLED AT END OF MAINS OF EACH STAGE, A TEMPORARY HYDRANT WILL BE INSTALLED INSTEAD. PROVIDE BULKHEADS/TRENCHSTOPS IN ACCORDANCE WITH SEQ WATER

₽.

- SUPPLY CODE TABLE 7.5 AND SEQ.-WAT-1209-1 AND 1210-1.

 18. CONSTRUCT SMALL DIAMETER PROPERTY SERVICES TO
- 19. INSTALL DETECTABLE MARKER TAPE ON ALL WATER MAINS AND PROPERTY SERVICES.

 CONSTRUCT FIRE HYDRANTS AND STOP VALVES TO SEQ-WAT-1301-1, 1302-1, 1303-2, 1305-1, 1306-1 AND 14.09-1.

7

- CONSTRUCT SCOURS TO SEQ.-WAT-1907-2 WHERE WECESSARY, SCOURS WITH PSCHMET TO CROUGE, GENOWINGST DISCHARGE BIND AN OPEN STORMATIES CULLY PIT, NOT TO THE WIVER OF KERS AND CHANNEL. DISCHARGE TO KERS AND CHANNEL. VIA A STANDARD KERS ADAPTOR THOUGH THE FACE OF THE KERS IS NOT ACCEPTED BY URBAN UTILITIES.
- 316SS BACKING RINGS SHALL BE USED WITH FULL-FACE PE FLANGES. PE STUB-FLANGES ARE NOT ACCEPTED.

75

- WHEN JOINING TO EXISTING UNRESTRAINED PPELINES, PROVIDE A DICL SHORT PIPE WITH THRUST FLANGE AND THRUST BLOCK, BOLT ON UNI NAMES SHALL ON THE GESDE AS THRUST FLANGES. THRUST PRODCE) FLANGES SHALL BE AN APPROVED PEFFABRICATED DICL/MSCL SHORT PIPE WITH PREFABRICATED THANGS.
- AC MAINS SHALL BE REPLACED COLLAR-COLLAR
- 25. ALL DISISED SERVICES SHALL BE PLUGGED AT THE MAIN AND FERRULE CLOSES OR LAPPING BAND REMOVED AND SECTION OF WAIN SUBSTITUTED AS LIVE WORKS, LARGE DAWFITER SERVICES SHALL BE SUBSTITUTED AS LIVE WORKS, LARGE DAWFITER SERVICES SHALL BE DOING TO COMMETCION TO THE MAIN INCLUDING VALVE), AND INTERNALING ARE ANK FLANGE DIRECTLY ON THE TEE (DO THERWISE REMOVET HE TEE ALTOGETHER AND REPLACE WITH STRAIGHT PIPE).

 26. PROVIDE MILLIPSE ANTER SERVICES FOR ROAD CROSSINGS SERVICING.
- THOU DWELLINGS. PROUDE DUSTONE CHRONIC SERVICING THOU DWELLINGS. PROUDE DUSTONE WATER SERVICES OF ROAD CROSSINGS. SERVICING. A SMOKE DWELLING. IF THE LONG TIEMS STANT OF THE PROPERTY SERVICE IS LESS. THAN 350. APR 353.00 (R. PROUSER) YERVICE IS LESS. THAN 350. APR 353.00 (R. PROUSER). THE MINIMUM SIZE OF PROPERTY SERVICE STANDING STAN
- URBAN UTILITIES WATER METERS AND FIRE HYDRANTS MUST BE LOCATED CLEAR OF ENERGEX PILLARS.

27.

VEGETATION PROTECTION

- A. TREES LOCATED ALONG THE FOOTPATH SHALL BE, TRANSPLANTED PRIOR TO CONSTRUCTION, OR REPLACED IF DESTROYED.
- WHEN WORKING WITHIN 4.m OF TREES, RUBBER OR HARDWOOD GIRDLES SHALL BE CONSIGNED TO MINING MAIN THE MAINTER CLOSEY STATED AND ARRANGED VERTICALLY FROM GROUND LEVEL. GREEKE SHALL BE STRAPPED TO TREES PRIOR TO CONSTRUCTION AND REPAIN UNTIL. COPPLETION.
- TREE ROOTS SHALL BE TUNNELLED UNDER, RATHER THAN SEVERED. IF ROOTS ARE SEVERED THE DARAGED AREA SHALL BE TREATED WITH A SULTABLE FUNGIODE. CONTACT RELEVANT COUNCIL ARBORIST FOR FURTHER AUVICE.
- ANY TREE LOPPING REQUIRED SHOULD BE UNDERTAKEN BY AN APPROVED ARBORIST.

ECONOMIC

SOIL

TOPSOIL AND SUBSOIL SHALL BE STOCKPULED SEPARATELY.

CARE SHALL ID FARKEN TO PREVENT SEDDINENT RROW ENTERMIG THE
STORMWATTER SYSTEM. THIS MAY INVOLVE PLACING APPROPRATE
SEDINENT CONTROL AROUND STOCKPULES.

CREEK CROSSINGS

- .. SILTATION CONTROL MEASURES SHALL BE PLACED DOWNSTREAM OF ANY EXCAVATION WORK.
- APPROPRIATE SEDIMENT CONTROLS SHALL BE USED TO PREVENT SEDIMENT FROM ENTERING THE CREEK.
 - NO SOIL SHALL BE STOCKPILED WITHIN 5m OF CREEK.

REHABILITATION

- A. PREDISTURBANCE SOIL PROFILES AND COMPACTION LEVELS SHALL BE REINSTATED.
- PREDISTURBANCE VEGETATION PATTERNS SHALL BE RESTORED.









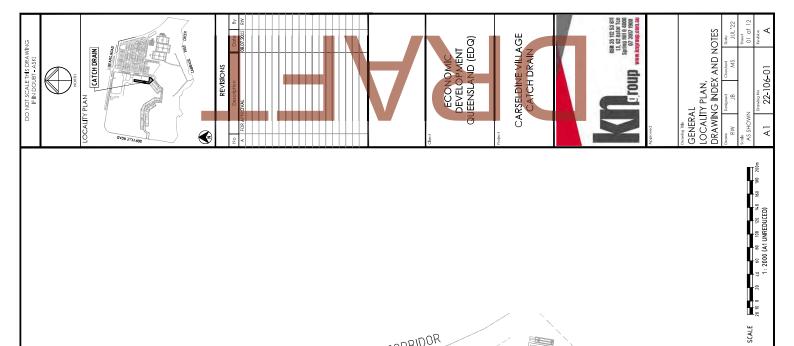
8	FUNCTIONAL LAYOUT	WATER MAIN CONNECTION	Ų
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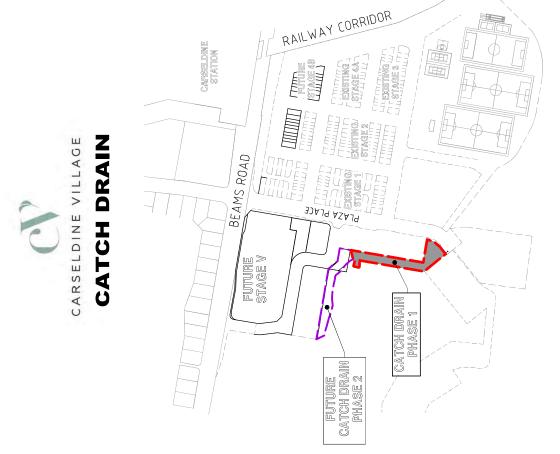
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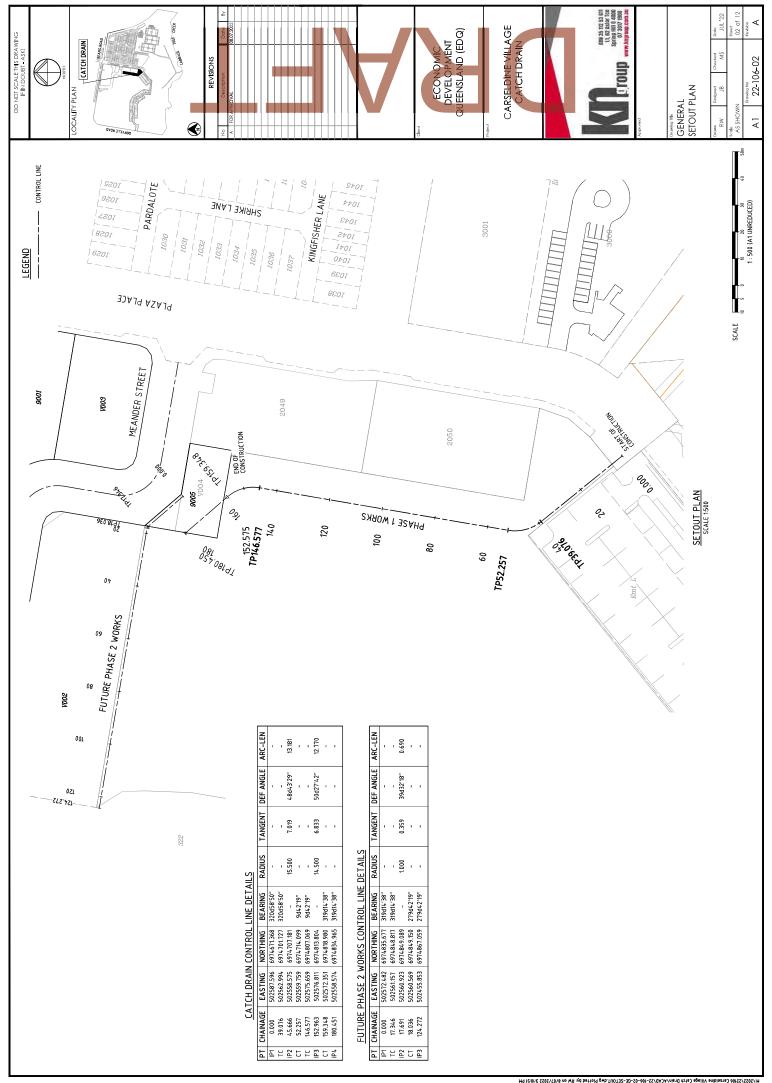
APPENDIX C CATCH DRAIN CONCEPT PLANS

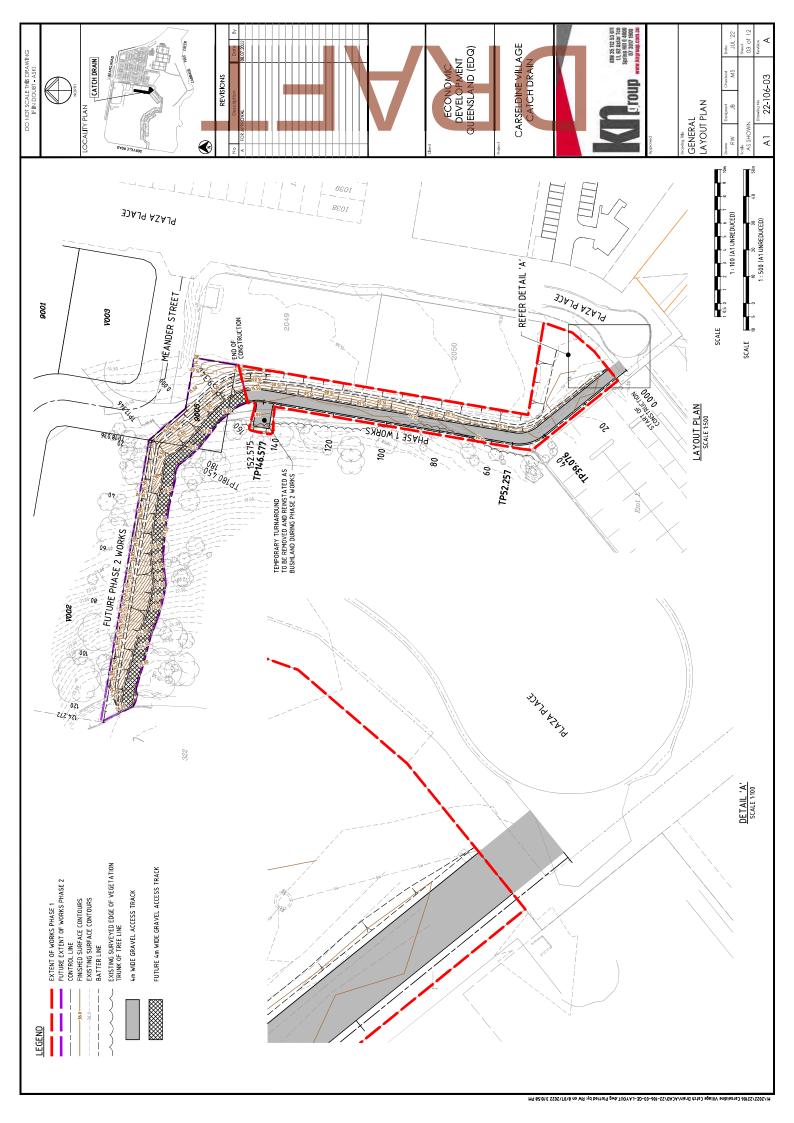


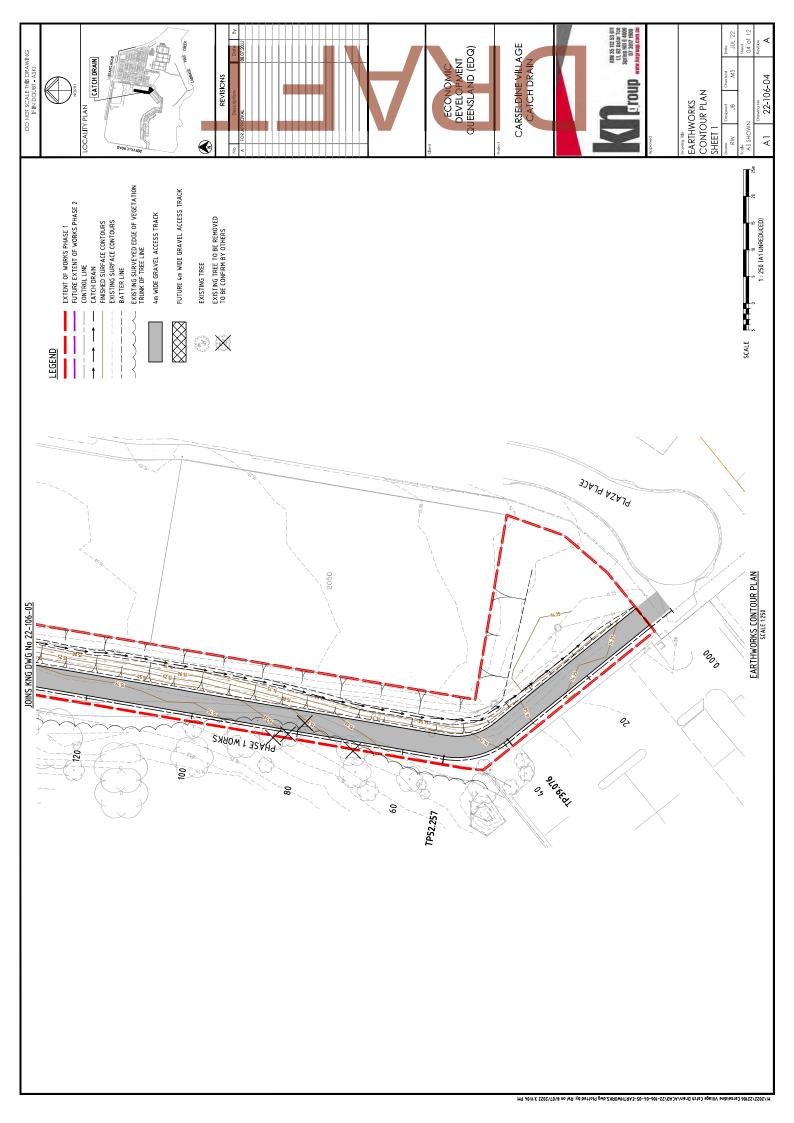


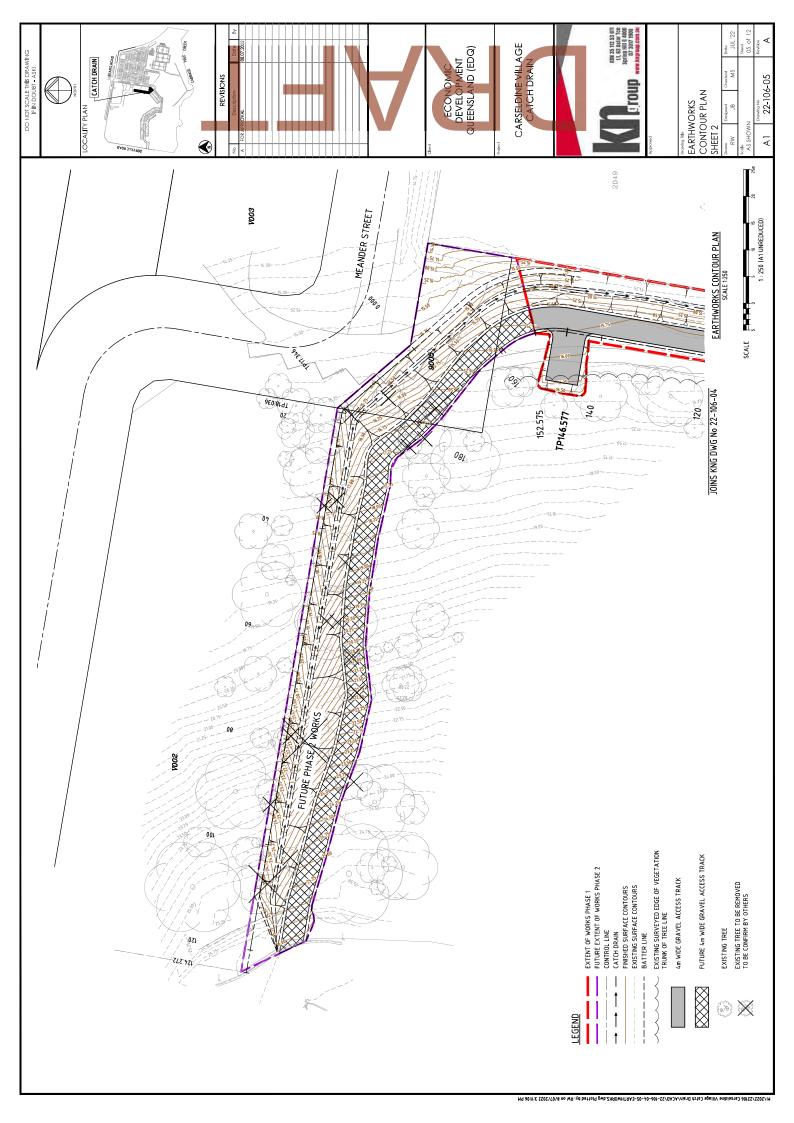
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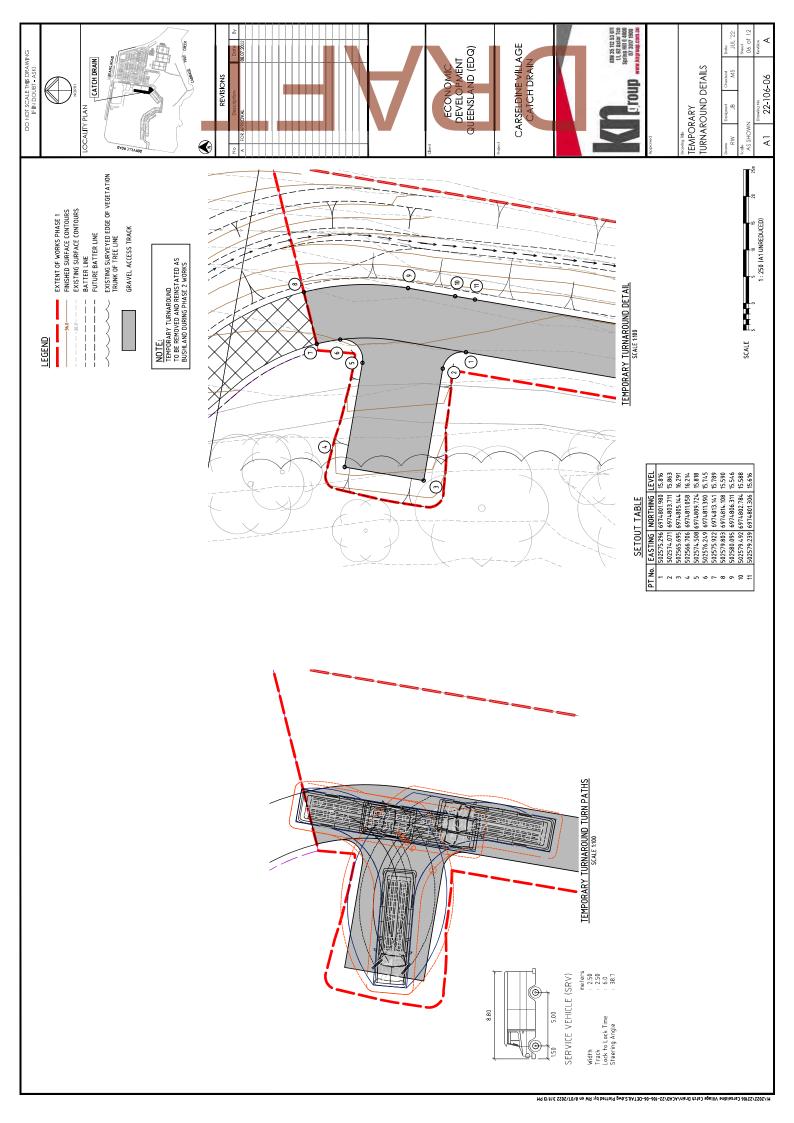
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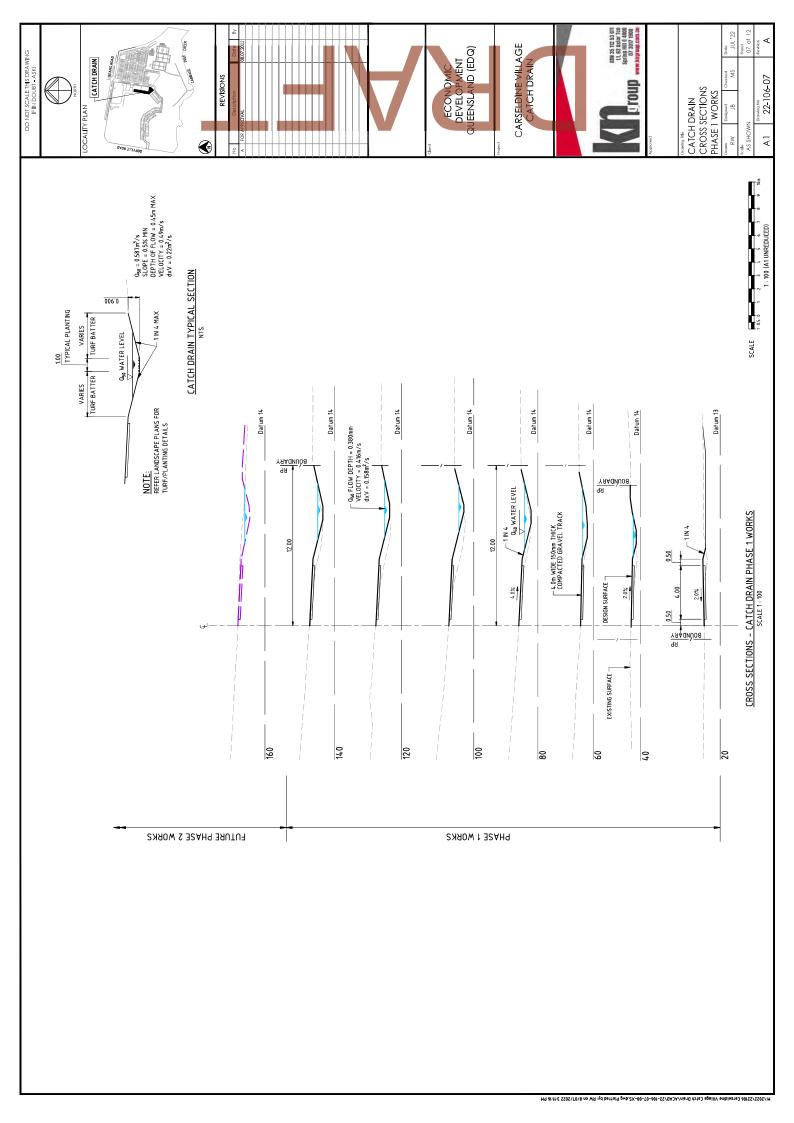


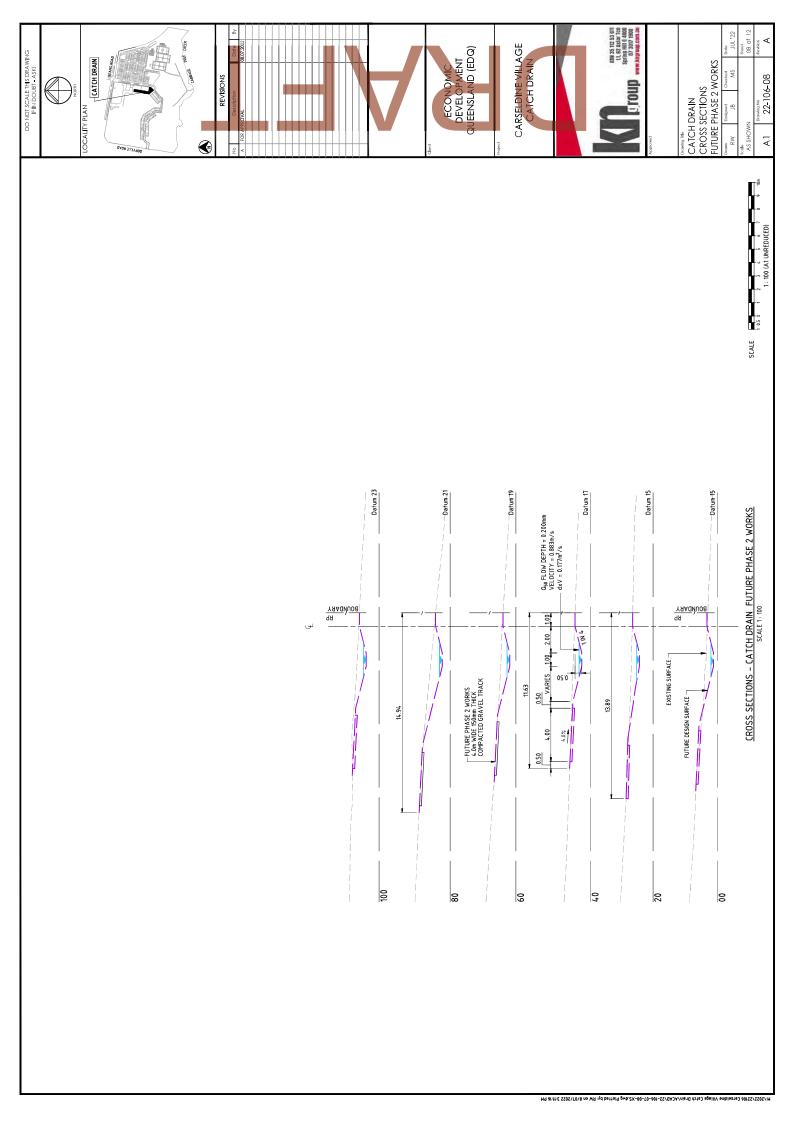


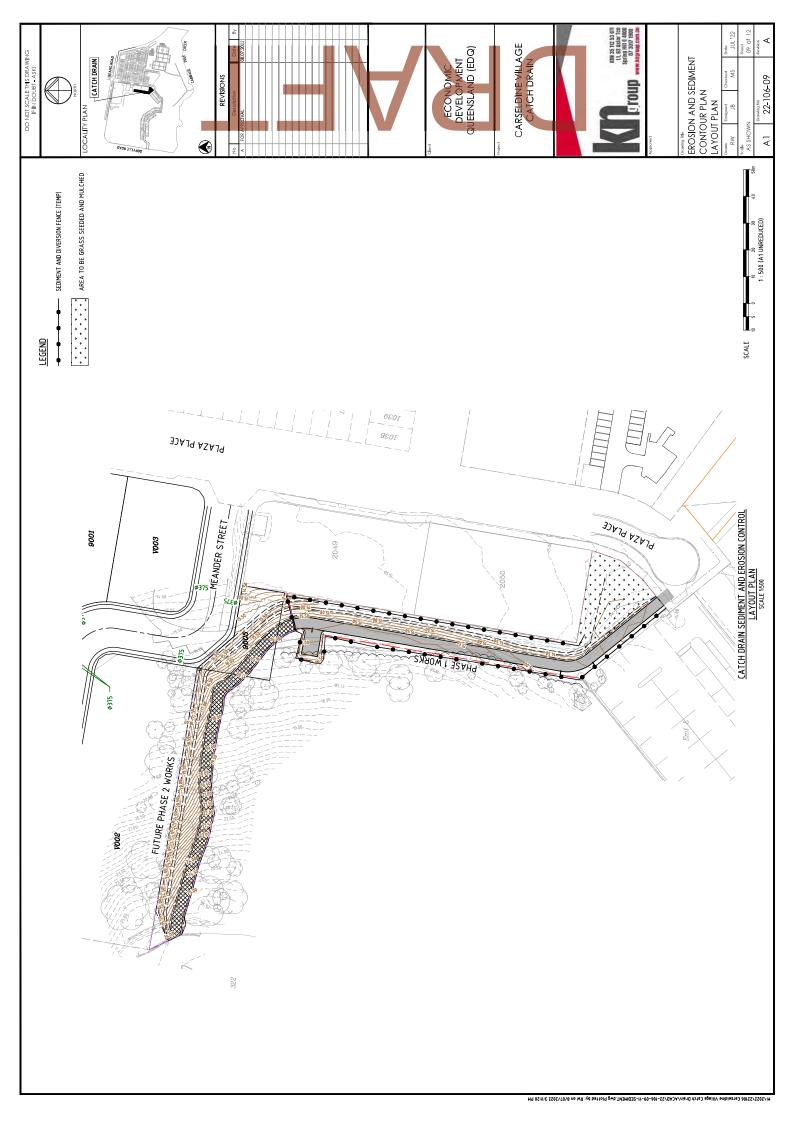












- EROSION AND SEDIMENT CONTROL PROGRAM 1. THIS PROGRAM AND ASSOCIATED PLANS SHOULD BE READ IN CONJUNCTION WITH THE SITE MANAGEMENT SPECIFICATION INCORPORATED IN THE CONTRACT DOCUMENTS. THE PROVISIONS OF THE SPECIFICATION ARE TO BE STRICTLY ADHERED TO.
 - THE BASIC OBJECTIVES OF THE EROSION AND SEDIMENT CONTROL ARE:

 I. IDENTIFY CRITICAL AREAS AND PROVIDE APPROPRIATE ATTENTION TO THOSE
- PLAN SITE LAYOUTS SO THAT ACCESS TO ALL REQUIRED DRAINAGE EROSION AND
- SEDIMENT CONTROL MEASURE IS MAINTAINED.

 THE XPOSURE THE BY PROGRAMMING TO MINIMSE THE AREA OF LAND EXPOSED
 TO POTENTIALLY ADVERSE WEATHER CONDITIONS AT ANY ONE TIME. I.E.

 PROGRESSIVELY CLEAR AND REVEGETAE.
 - IV. PRIVIDE CONTROL MEASURES INCLUDING TEMPORARY AND PERMANENT DRAINAGE, THE EROSION AND SEDMENT CONTROL SHALL COMPLY WITH BEST PRACTICE FOR EROSION AND SEDMENT CONTROL SHALL COMPLY WITH BEST PRACTICE FOR EROSION AND SEDMENT CONTROL SHALLAND, FIGH BEARS TORRIVAL AND AND SEDMENT CONTROL MANALE FIGH BEARS TORRIVAL AND HEAD AND THE SOLL EROSION AND ADDRESSED AND THE SOLL EROSION AND AND AGENTALLAND, AND THE SOLL EROSION AND ADDRESSED ADDRESSED AND ADDRESSED ADDRESSED
 - SEDIMENT CONTROL ENGINEERING GUIDELINES FOR QUEENSLAND (CURRENT EDITIONS). CONSTRUCTION SEQUENCE THE CONSTRUCTION SEQUENCE WILL GENERALLY BE: OBTAIN ALL NECESSARY PERMITS AND APPROVALS BEFORE SITE ESTABLISHMENTS.
 - STABILISE ALL CONSTRUCTION ACCESS ROUTES AND ENTRY/EXIT POINTS. ESTABLISH SEDIMENT CONTROL STRUCTURES AND TEMPORARY DRAINAGE HOLD A PRE-CONSTRUCTION CONFERENCE. <u>≡</u> ≥
 - CONTROL MEASURES AS NECESSARY.
 - CARRY OUT BULK EARTHWORK:
- MAINTAIN AND REPAIR DRAINAGE, EROSION AND SEDIMENT CONTROL MEASURES. REMOVE SEDIMENT CONTROL MEASURES WHEN THE SITE IS STABILISED. I.E. > 70% > ≥ ≥
- THE CONTRACTOR SHALL PREPARE A SUPPLEMENTARY EROSION AND SEDIMENT
 TOWN THE CONTROL PLAN TO SUIT HIS/HER, CONSTRUCTION METHODOLOGY, AND SUBMIT THIS
 CONTROL PLAN TO SUIT HIS/HER, CONSTRUCTION METHODOLOGY, AND SUBMIT THIS
 SIGNIFICAN IVARIATION TO THE SUPERINTENDENT. IT SHOULD BE NOTED THAT ANY
 SIGNIFICAN IVARIATION TO THE PLAN MAY REQUIRE RESUBMISSION TO COUNCIL. FOR APPROVAL. THE CLIENT SHALL NOT BE RESPONSIBLE FOR ANY SUCH ASSOCIATED DELAY. GROUND COVER THE CONTRACTO ₹

 - ALL ESC DEVICES ARE TO BE INSPECTED WEEKLY, PRIOR TO EXPECTED AND AFTER
 RAIM-ALL ANY DAMAGE IS TO BE REPARADA SA REQUEBED TO MANIFATH HEIR EFFCACY.
 THEOGRAPY ERGISION AND SEDIMENT CONTROL (ESC) MEASURE TO BE MAINTAINED AND
 FILLY OPERATIONAL DUBING THE MAINTENANCE PRIOD AND ARE TO BE REMOVED AFTER
 THE SATISFACTIONY COMPLETION OF AN OFF-MAINTENANCE INSPECTION BY COUNCIL AND
 PROOF TO THE CALL OF THE SATISFACTION OF AN OFF-MAINTENANCE BY COUNCIL.

 THE CALL OFFICE TO ARKEE "OFF FAMINTENANCE" BY COUNCIL.

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 TO SELECT THE SATISFACTION OF AN OFF-MAINTENANCE BY COUNCIL.

 THE SATISFACTION OF ANY OFF-MAINTENANCE BY COUNCIL.

 THE SATISFACTION OFF-MAINTENANCE BY COUNCIL.
 - PRIOR TO THE COMPENCEMENT OF CONSTRUCTION. THE CONTRACTOR IS TO PROVIDE A DETAILED PROGRAM TO THE SUPERINTENDENT SHOWING THE TIMING FOR ALL WORKS SOCIATED WITH HE PROJECT, MOMINATING, IN PARTICULAR, THE PROGRAM FOR
- INSTALLATION OF SOIL AND REDISOING OVAIROIL SYSTEMS. THE SITE IS MAINTAINED IN EARLINGMESS SHALL BE CARRED OLI IN SIGICA ANAINER THAT THE SITE IS MAINTAINED IN A WELL DRAINED CONDITION, AREAS OF LODGE SOIL ARE MINIMISED AND CONCENTRATIONS OF STORMANTER ARE MINIMISED. BULK EARTHWORKS WILL BE CARRIED OUT OVER THE BUTTLES SITE IN ONE STAGE.
 - A SHAKE DOWN AS DETAILED ON THE PLAN COMPRISING FREE DRANMAGE GRAVEL SHALL BE LLOCATED ADJACENT TO THE STREET SYSTEM FREQUEDS. THE WASH DOWN AREA SHALL BE PROPERTY TO THE STREET SYSTEM FREQUEDS. THE WASH DOWN AREA SHALL BE I FREE OF MUD.
 - FOR DETAILS OF ENTRY/EXIT SEDIMENT PAD REFER TO BEST PRACTICE EROSION & SEDIMENT CONTROL BOOK 1, PAGE 2.48, FIGURE ₽.
- SUPPLEMENTARY EROSION AND SEDIMENT CONTROL DEVICES MAY BE REQUIRED AT THE DISCRETION OF THE SUPERINTENDENT
- REFER BEST PRACTICE EROSION 8. SEDIMENT CONTROL BOOK 1, PAGE 2.50, FIGURE 2.8. WHERE SEDIMENT FEMCES ARE SHOWN TO BE CONSTRUCTED IN AREAS OF SIGNIFICANT EARTHWORKS, ERECTION OF THE FENCE MAY BE DEFERRED UNTIL COMPLETION OF THE BULK EARTHWORKS, SUBJECT TO ABSENCE OF RAIN. SEDIMENTATION FENCES TO BE PLACED AS SHOWN. FOR DETAILS OF SEDIMENT FENCE

ne Village Catch Drain/ACAD/22-106-09-11-SEDIMENT.dwg Plotted by: RW on 8/07/2022 3:11:51 PM

SITES. THIS MAY REQUIRE CONSULTATION AND GUIDANCE FROM A CLASS V CERTIFED ARRONISTA S THESE DOUSED THE IMMEDIATE WORK AREA MAY BE AFFECTED. RESURE COMPLIANCE WITH THE REQUIREMENTS OF THE 28 SOUTH ENVENOMENTAL FMP, INCLUDING IMPLEMENTING THE OPPOTECTION ZONES. TREES 1. ENSURE COMPLIANCE WITH THE REQUIREMENTS OF AS4970 - TREES ON CONSTRUCTION

1. STRIP AND STOCKPILE AVAILABLE TOPSOIL (ASSUMED AVERAGE DEPTH 150mm) FROM ALL DISTURBED AKEAS PROBE TO BULK ERRTHWORKS. GRADE EVENLY BETWEEN ALLOTMENT FINISHED SURFACE LEVELS AND ENSURE LOTS ARE PREE DRAINING.
2. MINISHED SURFACE LEVELS AND ENSURE LOTS ARE PREE DRAINING.
3. ALL FOOTPATHS, BATTERS, AND EARTHWORKS AFFECTED ALLOTMENTS ARE TO BE TO THE TOTAL TO A MINISHUM DEPTH OF 150mm (LIGHTLY COMPACTED) AND TUBFED WHERE

- EROSION AND SEDIMENT CONTROL NOTES

 1 NO DISTURBED REAL IS TO REPURN BENUDE UNGER THAN 80 DAYS.

 2 ALL EGROIN AND SIL ATION CONTROL MESSINESS ARE TO BE PLACED PRIOR TO DAS THE FIRST STEP IN CLEARING AND SIL ATION CONTROL MESSINESS ARE TO BE PLACED PRIOR TO DAS SELL'STORMATTER, SUMR IN ME AND SERVICES SIRENCHES NOT IN STREETS ARE TO BE MULCHED AND SEEDED WITHIN 10 DAYS AFTER BACKFILL, NO HORE THAN 150 METRES ARE TO BE PROFINED AND SELECTED BY AND ORD THE ANNO. SIL THE SELECTE SILENCHES NOT DAYS AFTER DAYS OF THE SLOPE AT THE BOOM OF SAFATOR SELECTED AND MULCHED FOR THEPOPRARY VEET THY COVER WITHIN 10 DAYS AFTER DAYS OF THE SLOPE AT THE END OF SAFATOR SEADING. SIRAW OR HAY MULCH IS REQUIRED.

 5. ALL CHE ENBANKHENTS ARE TO BE LEFT WITH A LIP AT THE TOP OF THE SLOPE AT THE END OF SAFATOR SAFATOR SEEDED AND MULCHED WITHIN 10 DAYS OF COMPLETION OF GRADING.

 6. ALL CHARLES ARE TO BE LEFT WITH A LIP AT THE TOP OF THE SLOPE AT THE ADDITIONAL SILL AND ENCOUNTROLS MAY BE REQUIRED AS ORDERED ON SITE BY THE SLOPE AT THE SAFATOR SAFATOR

- PERMANENTLY STABILIZED OR UNTIL NO LONGER REQUIRED.

PHASE 1 – CLEARING AND BULK EARTHWORKS CONSTRUCT AND MAIN AIN SILT SETS, STRAW BAZE IRASA, ALLOTMENT DRAINAGE BANKS, CATCH BORNS MAN HYDROWICLIAN BRAINE OF SEDIMENT AND REOSSION DUBING ELEARING CATCH DRAIN SAND HYDROWICH AND STRAWN S AND BULK EARTHWORKS.

PHASE 2 - TRENCH EXCAVATION CONSTRUCT AND MAINTAIN SILT FFNCFS STDAY

STRAW BALE TRAPS, ALLOTMENT DRAINAGE BANKS CONSTRUCT AND MAINTAIN SILT FENCES, STRAW BALE TRAPS, ALLOTMENT DRAINAGE BANKS AND CATCH DRAINS WHICH CONTROL SEDIMENTATION AND EROSION DURING TRENCHING WORK.

TURFING . PROVIDE TURFING TO ENTIRE WIDTH OF ALL SWALES, FOOTPATHS AND 1 IN 4 CUT AND FILL \boldsymbol{I} .

FOOTPATH BATTERS ARE TO BE STABILISED WITH TOPSOIL (AND TURFED) AS SOON AS PRACTICAL AFTER THE BATTERS HAVE BEEN COMPLETED.

THESE SHALL BE MAINTAINED IN A CLEAN CONDITION. IN THE EVENT OF HEAVY RAIN THEY SHALL BE REPOYED TO HIMINES THE POTIVILLA FOR ELOCIONG.
CHECKS OF SILT CONTROL DEVICES ARE TO BE MADE WEEK!, OR AFTER ANY SIGNIFICANT SOME YOUR DEVICES ARE TO BE MADE WEEK!, OR AFTER ANY SIGNIFICANT SOME EVENT TO ENSURE MITEGRITY AND PERFORMANCE.

Ŋ

INSTALLED AT ALL COMPLETED INLETS. REFER IPWEAQ STANDARD DRAWING D-0041.

SEDIMENT FENCES

1. SEDIMENT FENCE TO BE PLACED AS SHOWN. SEDIMENT FENCED TO BE REPARED AND

1. SEDIMENT FENCES TO BE PLACED AS SHOWN. SEDIMENT FENCED TO BE REPARED AND

2. OFF SEDIMENT DEPOSITS SHALL BE RENOVED ONCE CAPACITY FALLS BELOW 75%.

2. OFF DEPLAIS OF SEDIMENT FENCE REFER BEST PRACTICE ENOSION & SEDIMENT CONTROL

3. SEDIMENT FENCES TO BE REPARED AS REQUIRED AND EXCESSIVE SEDIMENT DEPOSITS

SHOULD BE REPROVED.

4. INSTALL KERB RIFETS WITH GRAVEL RANGING FROM 50mm TO 75mm IN SIZE SHALL BE

PHASE 3 – PAVEMENT CONSTRUCTION
CONSTRUCT AND MAINTAIN SILT FENCES, STRAW BALE TRAPS, ALLOTMENT DRAINAGE BANKS,
GOLLY INLET PROTECTION, AND IPPE MIET DOVILET PROPETION WHICH CONTROL
SEDIMENTATION AND RESCOROU DURING PAYERENT CONSTRUCTION. SAND BAGGINGT OBE
PLACED ACROSS PAVEMENT TO CONTROL RUNDEF IN PAYEMENT BOXING AS DIRECTED ON SITE.

PHASE 4 - MAINTENANCE PERIOD CONSTRUCT AND MAINTAIN CONTROLS AND VEG

CONSTRUCT AND MANTAIN CONTROLS. AND VGETATIVE TREATMENTS, WHICH CONTROL. SEDIMENTATION AND ERGOIN PRIOR TO THE ESTABLISHMENT OF GRASS COVER. PROTUDE GOADM WIDE GRASS HILTES STRIPS BEHIND KERB AND CHANMEL.

NOTE: TURF TREATMENT IN CERTAIN AREAS BY LANDSCAPER. REFER TO LANDSCAPE DRAWING.

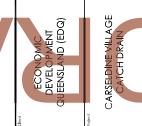
NOTE ALL VEHICLES EXITING FROM THE SITE ARE TO BE CLEANED AND TREATED TO PREVENT

MATERIAL BEING TRACKED OR DEPOSITED ONTO PUBLIC ROADS.

IF MATERIAL SE ACCIDENTE, DE POSITED ONTO PUBLIC ROADS IT SHALL BE REMOVED WITHOUT DEPOSITED ONTO PUBLIC ROADS IT SHALL BE REMOVED WITHOUT DEPOSITED ON TO BE INSEPECTIVE THE CONTRACTOR IS TO USE OTHERS HEARS TO PREVENT MATERIAL BEING DEPOSITED ONTO PUBLIC ROADS.

DO NOT SCALE THIS DRAWING IF IN DOUBT - ASK! CATCH DRAIN REVISIONS LOCALITY PLAN WITH DSCRIMER ETHER TO UNDISTORED DRAZE LANDS OF TO THE LROSS KADD DRAMAGE 8. SUPPLEMENTARY REOSION AND SEDIMENT CONTROL DEVISED MAY BE REQUIRED AT THE DISCRETION OF THE ENGINEER. 9. WATER QUALITY SAMPLES MUST BE TAKEN AND ANALYSED PRIOR TO THE RELEASE OF ANY WATER ROUGHTY SAMPLES MUST BE TAKEN AND ANALYSED PRIOR TO THE RELEASE OF ANY WATER ROUGHTY DATA MUST PORT WITHOUT DATA MUST POBLY CRITERIA. TSS-SOMOL, PH BETWERN 65 AND 85. ALL WATER QUALITY DATA MUST DATA MUST POBLY RELEASE WIST BE MANTANED IN AN ON-SITE REGISTER. THIS REGISTER IS TO BE MAINTAINED FOR THE DURATION OF THE APPROVED WORKS AND BE AVAILABLE ON SITE FOR INSPECTION BY COUNCIL DRETERS ON REQUIST. 11. EXPOSED AREA SO IL LOTS ARE TO BE SEEDED AND MULCHED IEG. HYDROMULCHED). MULCH STALLE APPLIED AT A MINIMUR NAT FOR TSTATM ALTERNATIVELY THEY SHALL BE DRILL-SEEDD AND IRRORATED SO AS TO RISINER. "JOX GROUND COVER WITHIN 14 DAYS FROM NOVEMBER TO APRIL, OR 30 DAYS FROM MY TO GTOBER. DURING CONSTRUCTION SEQUENCE: 1 TOPSOL STOKCHEES SHALL BE LESS THAN IN DEEP AND UNCOMPACTED. A SEDIMENTATION FENCE SHALL BE CONSTRUCTED ON THE DAS SIDE, OR THE STOCKPLE STABILISED WITH VEGET ATTON, MULLI, OR A SOLL STABILISED. SEDIMENTATION FENCES TO BE PLACED AS SHOWN. S. RECULARLY NISPECT BANKS AND REPAIR ANY SLUMPS, WHEEL TRACK DAMAGE OR LOSS OF FREEDADB. C. REMOVE SEDIMENT TO AVOID PONDING FROM CATCH DRAINS. S. REMOVE SECKESIVE SEDIMENT FROM IDESTREAM OF CHECK DAM. 6. ROAD RESERVET TO BE USED A SHALU RADM. 7. A CATCH DRAIN OF DAILS SHALL RADM. WITH DISCHARGE EITHER TO UNDISTURBED GRASS LANDS OR TO THE CROSS ROAD WITH DISCHARGE EITHER TO UNDISTURBED GRASS LANDS OR TO THE CROSS ROAD

ID (EDQ) **SEVELOP MENT** EENSL)



SEDIMENTATION FENCES TO BE MAN TAINED UNTIL TURFING IS COMPLETED.
SEDIMENT RASINS TO BE CHEKERD AFTER EVERY SIGNIFICANT STORM AND DESILIED ONCE
THE SETTLEMENT LIMIT HAS BEEN REACHED.

FOLLOWING CONSTRUCTION

THE AMOUNT OF AREA EXPOSED AT ANY ONE TIME TO BE MINIMISED BY STAGING THE WORKS WHEREVER POSSIBLE AND AIMING TO ACHIEVE FINISHED LEVEL IN EACH AREA AS

STABILISATION



THOSON, TO BE SPREAD TO CA-BURNY THE DISPERSIVE SUBSOILS.
TOPSOIL TO BE DRILL-SEEDED WITH A MYSTURE OF ANNUAL AND PERMUL GRASS
SPECIES (REFER TABLE) AND FERTILISEN WITH CROP-KING 80 (137-14).
WITH-BON MATT DE COVERT DUE FOR PAPILED COURSTING OF VITAL CHEMICALS
WITH-BON MATT PAT-VRI OR EQUIVALENT. QUICKLY AS POSSIBLE BEFORE OPENING NEW AREAS.

10950ILT OB ES TRIPPED MAD STOCKPILED SPEAARTEY TO SUB-SOILS.

3. STOCKPILES TO BE PROVIDED WITH SUPFACE COVEN USING, A CHEMICAL SUFFACE STABILISER SUCH AS VITAL CHEMICALS VITAL-BON MATT STONEWALL.

4. IF WORKS ARE DELAYED OFF OUT ON HOLD THEN TEMPORARY EROSION CONTROL COVENING.

10 BE PROVIDED USING VITAL CHEMICALS VITAL-BON MATT P47-VR1 OR EQUIVALENT.

5. ONCE AREAS REACH FINISHED LEVEL.

WATERING UNDERTAKEN AS NECESSARY UNTIL STABLE GRASS SURFACE COVER IS FCTAR ISHED

	SEED MIXES	WINTER BLEND (APPLICATIONS MAY AUGUST)	%57	%57
		MID SEASON BLEND (APPLICATIONS MAY AUGUST) SEPTEMBER/OCTOBER)	25%	25%
		SUMMER BLEND (APPLICATIONS NOVEMBER - DECEMBER)	25%	25%
LOT MUCIOILED.			UNHULLED GREEN COUCH (CYNODON DACTYLON) OR BLUE COACH IDIGITARIA DIDACYLA)	HULLED GREEN COUCH (CYNODON DACTYLON) OR BLUE COACH IDIGITARIA DIDACYLA)

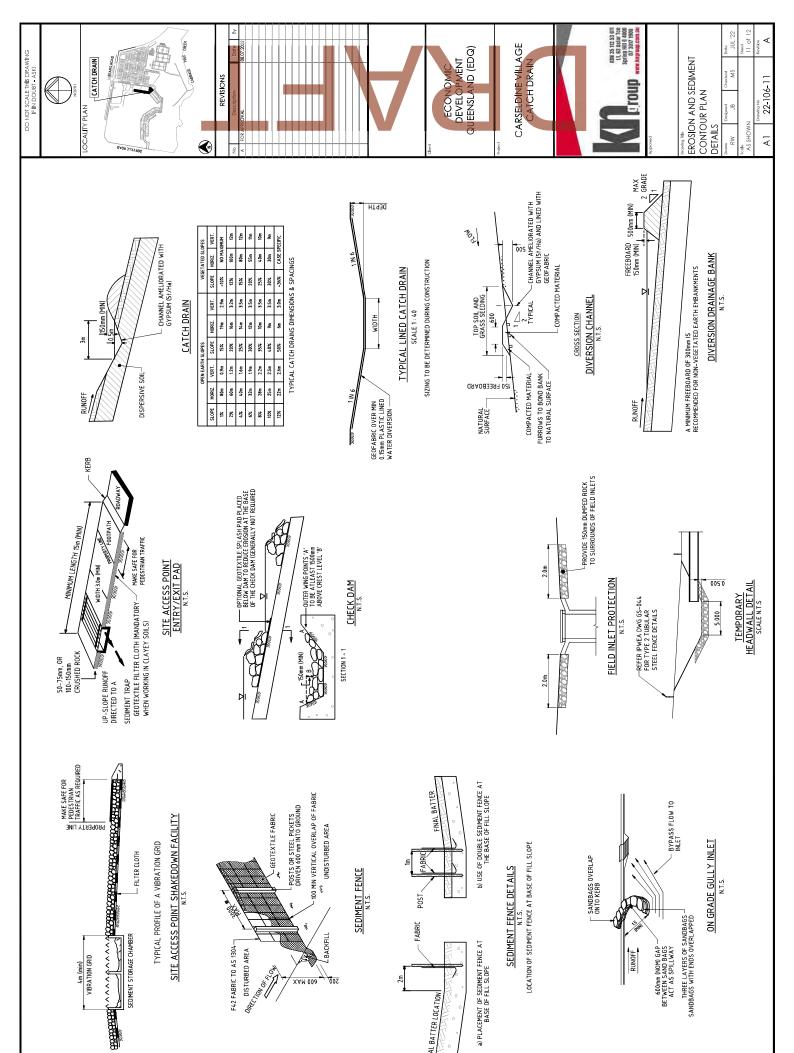
_	Date JUL '22	Sheet 10 of 12	Revision
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erosion and sediment Contour Plan Notes	Designed JB	7	DECOMING NO 22-106-10
EROSIO CONTO NOTES	Drawn RW	Scale AS SHOWN	A1

N/A 30% 20%

15 % 2 20 % 2 %

% ×

APANESE MILLET



FINAL BATTER LOCATION

DISTURBED AREA

4m (min) VIBRATION GRID

RUNOFF

DO NOT SCALE THIS DRAWING IF IN DOUBT - ASKI CATCH DRAIN

LOCALITY PLAN

Risk Manager

CABBAGE TREE CREEK

Complete Safety in Design Analysis by populating the table where applicable with all of the relevant safety issues for the project. For example:

Date: 10th June 2022 Date: 10th June 2022

Clant: ECONOMIC DEVELOPMENT QUEENSLAND (EDQ)
Project: CMSEDINI VILLAGE—CATCH DRAIN
Properated by Losso Button
Reviewed By: Mark Shaw
Safety in Design Analysis

| Slope Stability | Resident | Re

Project Specific Design Elements:

| Positioning of new services adjacent to existing live services Construction adjacent to existing road carriageways
| Pedestrians |
| Pedestrians |
| Richal Construction Workers |
| Richal Construction Workers |
| Work Place Health and Safety Constraints |
| Unusual material handling |
| Falls from heights |
| Service Installation |
| Communication Installation |
| Traffic Signal Installation |
| Traffic Sign

REVISIONS

Contractor

Contractor

Designer

Designer/ Contractor

Contractor

ECONOMIC DEVELOPMENT QUEENSLAND (EDQ)

CARSELDINE VILLAGE CATCH DRAIN

ABM 35 112 53 611
11, 62 851or Tce
Spring Hill @ 4000
07 3017 1900
WWW Kngroup.com.au Loud

SAFETY IN DESIGN

Sheet 12 of 12 bote JUL '22 Checked Designed cole AS SHOWN RW

22-106-12

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Page | 1

Risk Risk Rating (after design applied Σ 4 U Protection measures – that is fencing of all water retaining structures with side slopes greater than 1 in 5 as described in international Erosion Control Association (Australasian) Table R9 Mains located with safe working clearance to existing pressure mains, structures and battered embankments Depth of trenches minimized for both safety and cost efficiency Contractor to ensure works undertaken in a manner complying with safe work method statements TMP to be provided by Contractor to exclude pedes from work site Risk Control Measures TMP and SWMS required for all activities TMP and SWMS required for all activities Risk Rating I 4 Likelihood V < Maintenance Workers Construction of stormwater, sewer, water and wetland structures Public access to water retaining temporary sediment basins Underground Services (Existing) Identify any Potential Incident or Hazard Pedestrians Injury Civil Construction Workers – Injury rench depth Working adjacent to existing Infrastructure Service trench/ pipe installation Road/Earthworks Works Section of Works Silt and Erosion Control Works within Confined Spaces

			ш	S	M	_	_	_
			۵	s	s	Σ	_	1
¥			u	I	S	S	Σ	Σ
S: Significant Risk	Risk	atrix belo	8	Ξ	I	I	S	S
S: Sign	L: Low Risk	om the n	A	I	x	H	I	S
H: High Risk	M: Moderate Risk	Read the Risk Rating from the matrix below:	Risk Assessment Matrix	1	2	8	4	r.

Probable – means an event or situation that occurs or is likely to occur about ten times or more per year Possible – means an event or situation that occurs or is likely to occur about once per year Unlikely – means an event or situation that occurs or is likely to occur less frequently than once every ten years

RISK ASSESSMENT AND CONTROL

The following table summarises the safety in design issues considered.

∑List all relevant safety studies

Select one outcome i	Select one category from each of the columns below that best represents the likely outcome if the potential hazard actually did occur. For each consequence consider the most likely outcome and not the "absolute worst" case.	st repres	ents the likely ence consider the
	Consequence		Likelihood
A	Death – major environmental damage	1	Certain
8	Permanent Disability – severe environmental damage	2	Probable
U	Lost Time Injury – moderate environmental damage	3	Possible
Q	Medical Treatment Injury – minor environmental damage	4	Unlikely
ш	First Aid Treatment	2	Very Unlikely

RISK RATING

Certain - means an event or stuation that is happening more or less all the time, including continuous situations
Permanent Disability – means a disability, such as loss of a limb or eyesight, loss of hearing, chronic skin disorder, chronic back disorder, emphysema, and the like

Issued 10th June 2022 Rev - A



APPENDIX D DIAL BEFORE YOU DIG (DBYD)







Powerlink Queensland 33 Harold Street, Virginia, Qld, 4014 Phone: (07) 3866 1313 09/02/2021

To: ('Applicant')

KN Group - Mr Mark Shaw Level 2/71 Grey Street

South Brisbane QLD 4101

Email: mshaw@knpl.com.au Phone: 0488 044 500 Fax: Not Supplied Mobile: Not Supplied

Sequence No: 106379432

Enquiry Location: 532 Beams Road Carseldine

Enquiry Date: 09/02/2021 14:54

Dear Mr Mark Shaw

Thank you for your enquiry in relation to the Enquiry Location. Queensland Electricity Transmission Corporation Limited ACN 078 849 233 trading as Powerlink Queensland ("Powerlink") respond as follows:

Powerlink's records show that there ARE underground cables in the Enquiry Location.

A plan is attached showing the approximate location of Powerlink's assets in the vicinity of the Enquiry Location.

Should our response identify the presence of decommissioned Powerlink assets it should be noted that damage to these assets may result in an environmental hazard. As a precaution, all underground assets should be treated as live, and all necessary precautions should be taken to ensure that the cables are not damaged. Should damage occur, all work in the area surrounding the cables must be ceased immediately and Powerlink called on 07 3266 9410 to report the damage and get further advice.

Proposed works in close proximity to Powerlink's plant must undergo a detailed assessment by Powerlink. Please allow at least four to six weeks (more in complex situations) for Powerlink to process your application.

All work in close proximity to Powerlink's cables must be supervised by a Powerlink-appointed person and can be arranged by contacting Powerlink on (07) 3866 1313 at least seven days in advance.

The attached duty of care guidelines below must be observed at all times.

Yours faithfully,

Colin Langton

General Manager Community and Delivery Services Powerlink Queensland



Dial Before You Dig Terms and Conditions



"Duty of Care" for Everyone

Responsibilities When Working in the Vicinity of POWERLINK'S Plant

Everyone has a legal duty of care that must be observed, particularly when working in the vicinity of electrical plant. "Electrical plant" includes underground cables, conduits and other associated underground equipment. It should be noted that the placing or removal of soil by excavation, digging or by any other means is not allowed in a Powerlink-easement without prior written consent from Powerlink. In most cases it is unlikely that consent will be granted.

When discharging this duty of care in relation to Powerlink's plant, the following points must be considered:

- 1. It is the responsibility of the architect, consulting engineer, developer and head contractor in the project planning stages to design for minimal impact and adequate protection of Powerlink's plant. Powerlink will provide free plans showing the presence of its underground plant to assist.
- 2. It is the developer or constructor's responsibility to:
 - investigate whether Powerlink's plant is present in a particular location and obtain the most up to date plans available from Powerlink before commencing construction.
 - visually locate Powerlink's plant by hand digging where construction activities may be in close proximity to or interfere with Powerlink's plant.
 - contact Powerlink's Property Services Group on (07) 3866 1313 if Powerlink's plant is wholly or partly affected by planned development and construction activities.
- 3. As the alignment and boundaries of road ways with other properties (and roads within road ways) frequently change, the alignments and boundaries contained within Powerlink's plans and maps will frequently differ from present alignments and boundaries "on the ground". Accordingly, in every case where it appears that alignments and boundaries have shifted, or new road ways have been added, the constructor should obtain confirmation of the actual position of Powerlink's plant under or along the road ways. The constructor must never rely on statements made by third parties in relation to the position of Powerlink's plant.

Important Points to Note - Please Read

- Plans and details provided by Powerlink are current for one month from the Response Date and should be disposed of by shredding or any other secure disposal method after use.
- Powerlink's plans are diagrams only. They indicate the presence of underground plant in the general vicinity of the Enquiry Location. Exact ground cover and alignments cannot be given with any certainty, as such levels can change over time.
- To avoid damage or injury, Powerlink's plant must be carefully located under the supervision of a Powerlink-appointed person before excavation work or similar activities are undertaken near Powerlink's plant.
- Powerlink, its servants and agents will not be liable for any loss or damage caused or occasioned by the use of plans and or details so supplied to the applicant, its servants and agents, and the applicant agrees to indemnify Powerlink against any claim or demand for any such loss or damage.
- Where work commences prior to obtaining Powerlink's plans, or Powerlink's instructions are not followed, the developer/constructor is responsible for all damages sustained to Powerlink's plant.
- Powerlink reserves all rights to recover compensation for loss or damage caused by interference or damage, including consequential loss and damages to its cable network, or other property.
- All underground conduits and cover slabs must be presumed to contain asbestos. Refer to "Code of Practice for the Management and Control of Asbestos in Workplaces [NOHSC: 2018 (2005).]
- PCB (polychlorinated biphenyl) contamination may exist in some cables.





If requested, Powerlink may provide either remote over –the-phone or on-site location assistance with locating Powerlink's plant. This assistance may include guidance on visually locating and protecting Powerlink plant when excavating. Please note that any markings or pegs placed on the site by Powerlink during any such visit are indications of approximate cable locations only. The constructor is responsible for all hand digging (potholing) to visually locate and expose POWERLINK'S plant.

If the constructor is unable to locate Powerlink's plant within five metres of indicative plan locations, they must contact Powerlink's Regional Officer for Local Security for further advice. Contact details are as follows;

Officers for Local Security:

Region name	Contact's name	Telephone number	Mobile number
Southern	Bruce Muhling	(07) 3860 2305	0417 294 210
Central	Jeff Anstey	(07) 4931 2718	0418 785 743
Northern	Steve Cazzulino	(07) 4789 5561	0418 875 137

When working in the vicinity of Powerlink's plant, please observe the following conditions:

Records

The first step before any excavation commences is to obtain records of Powerlink's plant in the vicinity of the work. For new work, records should be obtained during the initial planning and design stage. The records provided by Powerlink must also be made available to all construction groups on site. Where plant information is transferred to plans for the proposed work, care must be exercised to ensure that important detail is not lost in the process.

Location of Cables

Examining the records is not sufficient, as reference points may change from the time of installation. Records must also be validated when working in close proximity to underground plant. The exact location of plant that maybe affected must be confirmed by use of an electronic cable locater followed by careful hand excavation to the level of cover slabs or conduits. Hand excavation must be used in advance of excavators. If doubt exists with respect to interpretation of cable records, Powerlink's Regional Officer for Local Security must be contacted. Refer to the contact details above.

Electrical Cable Covers

Powerlink's cables have underground cable warning tapes installed above the cables with the wording 'high voltage cable' and some may also have additional mechanical protection. Please note that some cables are known to be buried without covers.

Supervision

Any work in close proximity (within cable easement or five metres from the cable) to Powerlink's cables will always require on site supervision arranged by Powerlink.

Proposed works

No placing or removal of soil by excavation, digging or by any other means is allowed in Powerlink's easement without prior specific written consent from Powerlink.

Excavating Near Cables

For all work within five metres of where the plant is shown on Powerlink's plans, the constructor is required to hand dig (pothole) and expose the plant to confirm its exact location before work can commence.



ating Parallel to Cables



If construction work is parallel to Powerlink's cables, then hand digging (potholing) at least every four metres is required to establish the location of all cables to confirm the exact location of Powerlink's plant before work can commence. Generally, no restrictions are placed on excavations parallel to Powerlink's cables to a depth not exceeding that of the cable and the entire excavation is located outside Powerlink's easement. If an excavation exceeds the depth of the cables and is within five metres of the edge of the easement (or within ten metres of the cable) it is likely that the covers or bedding material around the cables or conduits will move, and Powerlink must be contacted. Design for the installation of parallel infrastructure will need to take into account electrical issues, including induction and transferred potential. Please note that cable depths may change suddenly.

Excavating Across Cables

A minimum clearance of 150 mm above, below, and to the sides of cables must be maintained. A standard clearance between services must be maintained as set down by the individual authorities. If the width or depth of the excavation is such that the cable warning tapes are exposed or the cables being unsupported, then Powerlink must be contacted to determine whether the cables should be taken out of service, or whether they need to be protected or supported. In the case of high voltage cables, it is unlikely that Powerlink will be able to take the cables out of service, and is definitely not an option without a lead time of at least 12 months. A cable cover must never be removed without prior specific written approval. A cable cover and the warning tapes may only be replaced under the supervision of a Powerlink officer. Protective cover strips must never be omitted to allow separation between Powerlink's cables and other services.

Directional Boring Near Cables

When boring parallel to cables, it is essential that trial holes are carefully hand dug at regular intervals to validate the actual location of the Powerlink's conduits or cables before using boring machinery. Where it is required to bore across the line of cables, the actual location of the cables must first be proven by hand digging. A trench must be excavated one metre from the side of the cables where the auger will approach to ensure a minimum clearance of 150 mm from cables can be maintained

Heavy Machinery Operation over Cables

If a heavy "crawler" or "vibration" type machinery is proposed to be operated over the top of cables, detailed engineering plans and supporting information must be submitted to Powerlink for its approval, or otherwise (in writing) prior to any on site work commencing.

Hot Work in Proximity to Exposed POWERLINK'S Plant and Underground Cables

Exposed underground electrical cables must be protected against the effects of heat by shielding or covering cables with a suitable material. Heating of exposed insulation is dangerous and must be avoided at all costs.

Explosives

Before using explosives in the vicinity of POWERLINK'S cables, clearances should be obtained from Powerlink's Design Engineer. If explosives are proposed to be used within 100 metres of cables, an engineering report demonstrating that no damage will be sustained to Powerlink's plant must be provided to Powerlink prior to using such explosives.

Damage Reporting

All damage to Powerlink's cables, conduits and pipes must be reported to Powerlink no matter how insignificant the damage appears to be. Even very minor damage to cable protective coverings can lead to eventual failure of cables through corrosion of metal sheaths and moisture ingress. Some cables contain oil, and damage may result in an oil leak which will seriously impact the performance of the cable and will be treated as an environmental incident. All work in the vicinity of any of Powerlink's plant that has been damaged should cease and the area should be vacated until a clearance to continue work has been obtained from an authorised Powerlink officer.

Please note that high voltage electrical cables, if damaged, can cause serious injury, or fatality. Extreme caution needs to be exercised at all times when working in close proximity to these cables.





Electricity emergencies all areas or after hours enquiries 24 Hours **1800 353 031**

Plant Solutions and Assistance

If Powerlink's plant location plans or visual location of Powerlink's plant by hand digging reveals that the location of this plant is situated wholly or partly where the developer or constructor plans to work, then Powerlink's Property Services Team must be contacted on (07) 3866 1313 to discuss possible engineering solutions.

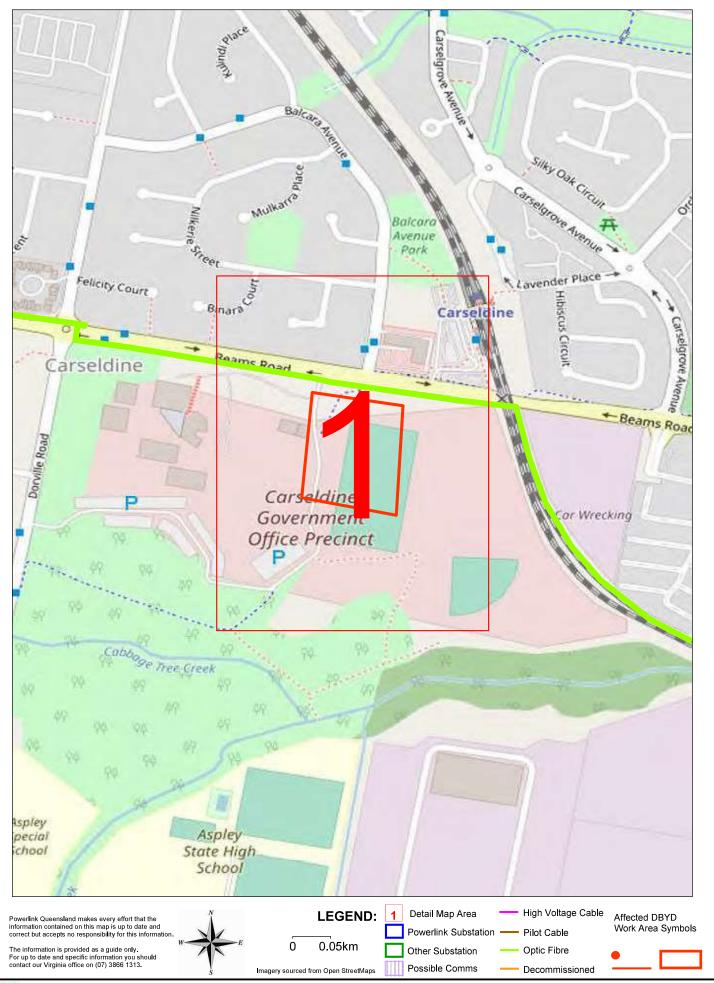
If detailed engineering assessment work, plant relocation, or protection works are part of the solution offered by Powerlink, then the cost of this work (the technical assessment and design, as well as the solution implementation cost) is recoverable by Powerlink from the principal developer or constructor. Powerlink will not commence work on the assessment and design until the developer or constructor provide a purchase order for these works. Powerlink will then provide a cost estimate for any proposed solution, and will not commence work on the solution until the developer or constructor provide a purchase order for the cost estimate.



Overview Map

Enquiry No: 106379432 532 Beams Road Carseldine

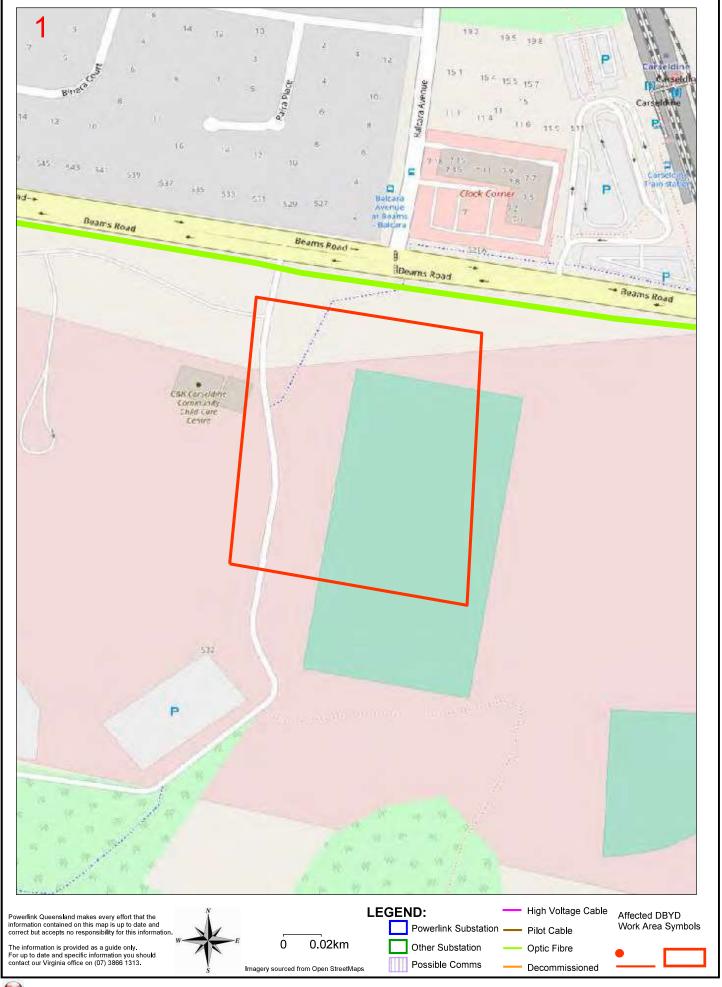


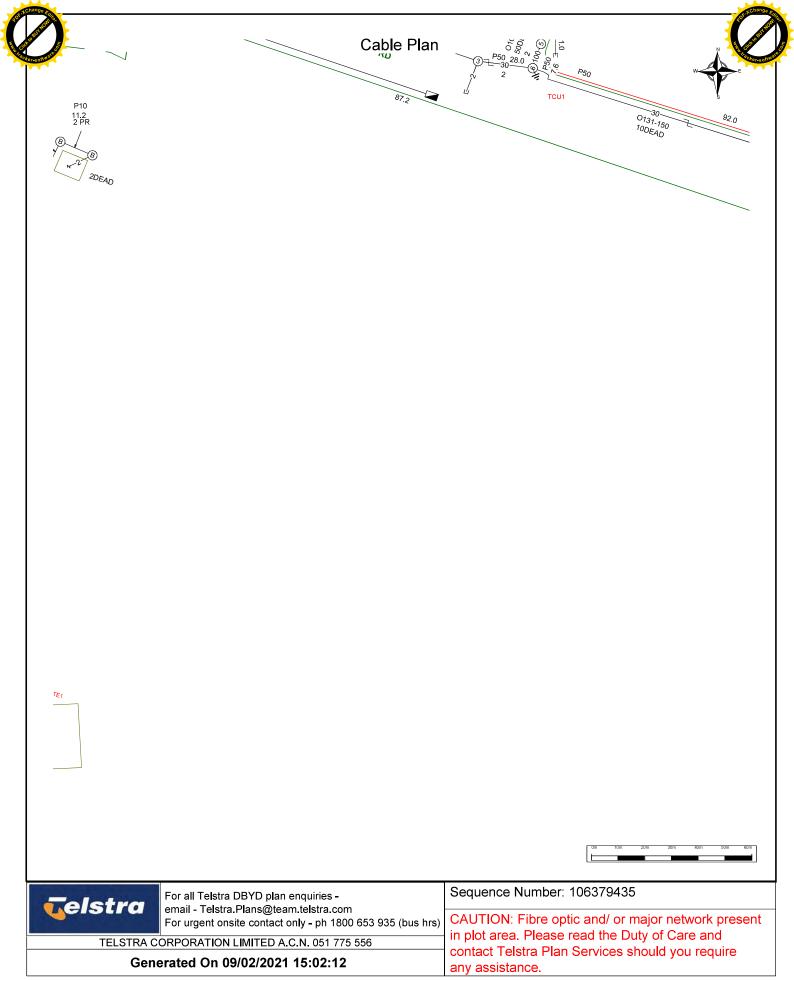




Enquiry No: 106379432 532 Beams Road Carseldine







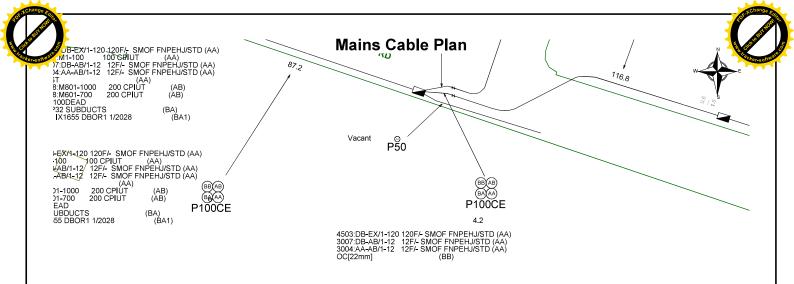
The above plan must be viewed in conjunction with the Mains Cable Plan on the following page

WARNING - Due to the nature of Telstra underground plant and the age of some cables and records, it is impossible to ascertain the precise location of all Telstra plant from Telstra's plans. The accuracy and/or completeness of the information supplied can not be guaranteed as property boundaries, depths and other natural landscape features may change over time, and accordingly the plans are indicative only. Telstra does not warrant or hold out that its plans are accurate and accepts no responsibility for any inaccuracy shown on the plans.

It is your responsibility to locate Telstra's underground plant by careful hand pot-holing prior to any excavation in the vicinity and to exercise due care during that excavation.

Please read and understand the information supplied in the duty of care statement attached with the Telstra plans. TELSTRA WILL SEEK COMPENSATION FOR LOSS CAUSED BY DAMAGE TO ITS PLANT.

Telstra plans and information supplied are valid for 60 days from the date of issue. If this timeframe has elapsed, please reapply for plans.



Telstra

For all Telstra DBYD plan enquiries - email - Telstra.Plans@team.telstra.com
For urgent onsite contact only - ph 1800 653 935 (bus hrs)

TELSTRA CORPORATION LIMITED A.C.N. 051 775 556

Generated On 09/02/2021 15:02:13

Sequence Number: 106379435

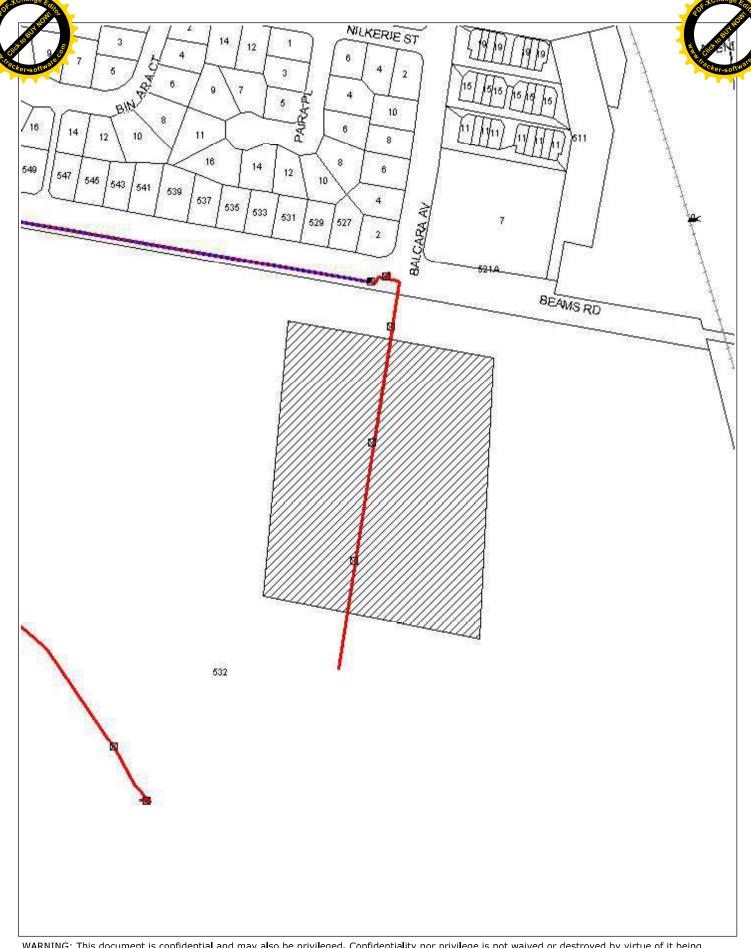
CAUTION: Fibre optic and/ or major network present in plot area. Please read the Duty of Care and contact Telstra Plan Services should you require any assistance.

WARNING - Due to the nature of Telstra underground plant and the age of some cables and records, it is impossible to ascertain the precise location of all Telstra plant from Telstra's plans. The accuracy and/or completeness of the information supplied can not be guaranteed as property boundaries, depths and other natural landscape features may change over time, and accordingly the plans are indicative only. Telstra does not warrant or hold out that its plans are accurate and accepts no responsibility for any inaccuracy shown on the plans.

It is your responsibility to locate Telstra's underground plant by careful hand pot-holing prior to any excavation in the vicinity and to exercise due care during that excavation.

Please read and understand the information supplied in the duty of care statement attached with the Telstra plans. TELSTRA WILL SEEK COMPENSATION FOR LOSS CAUSED BY DAMAGE TO ITS PLANT.

Telstra plans and information supplied are valid for 60 days from the date of issue. If this timeframe has elapsed, please reapply for plans.



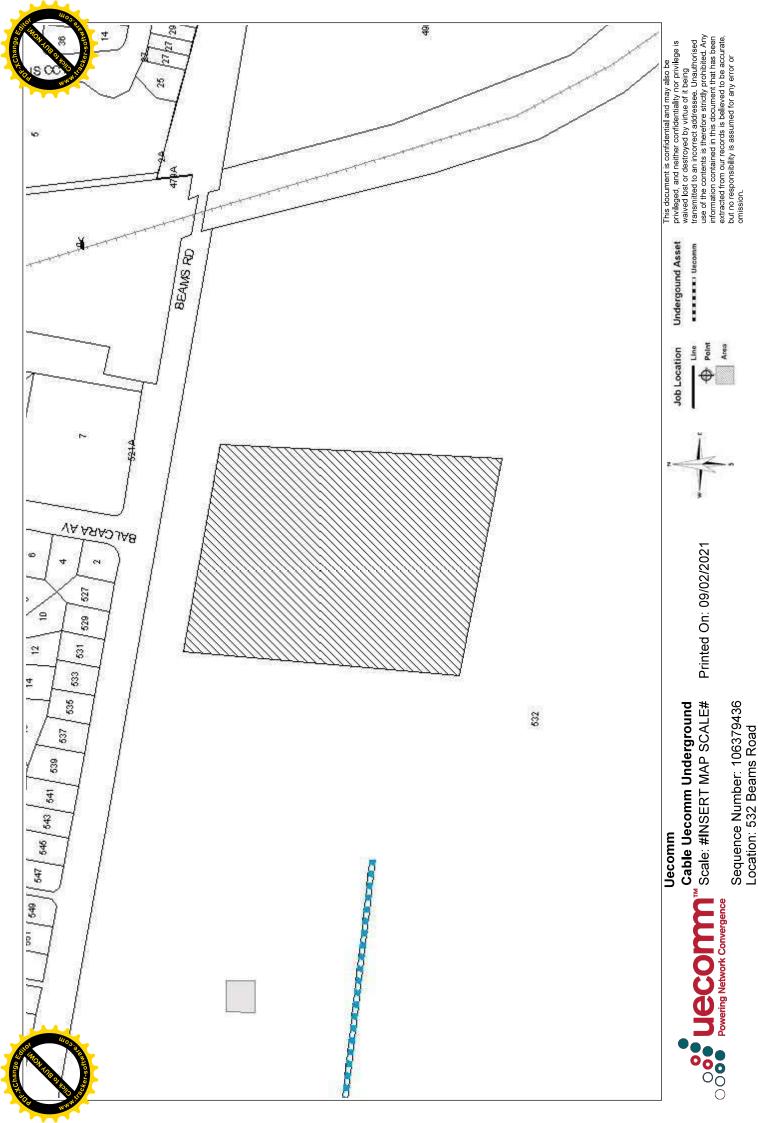
WARNING: This document is confidential and may also be privileged. Confidentiality nor privilege is not waived or destroyed by virtue of it being transmitted to an incorrect addressee. Unauthorised use of the contents is therefore strictly prohibited. Any information contained in this document that has been extracted from our records is believed to be accurate, but no responsibility is assumed for any error or omission. Optus Plans and information supplied are valid for 30 days from the date of issue. If this timeline has elapsed please raise a new enquiry.

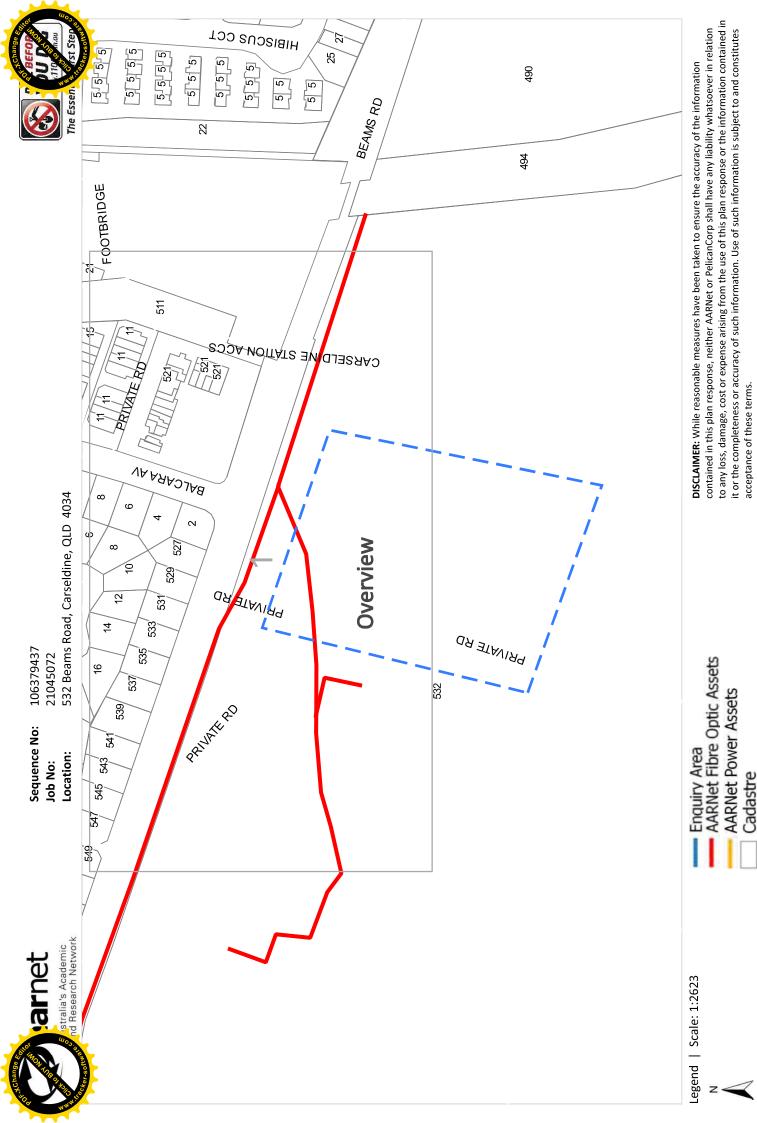
Sequence Number: 106379436



For all Optus DBYD plan enquiries – Email: Fibre,Locations@optus.net,au
For urgent onsite assistance contact 1800 505 777
Optus Limited ACN 052 833 208







Plans generated 09/02/2021 by Pelicancorp TicketAccess Software | www.pelicancorp.com

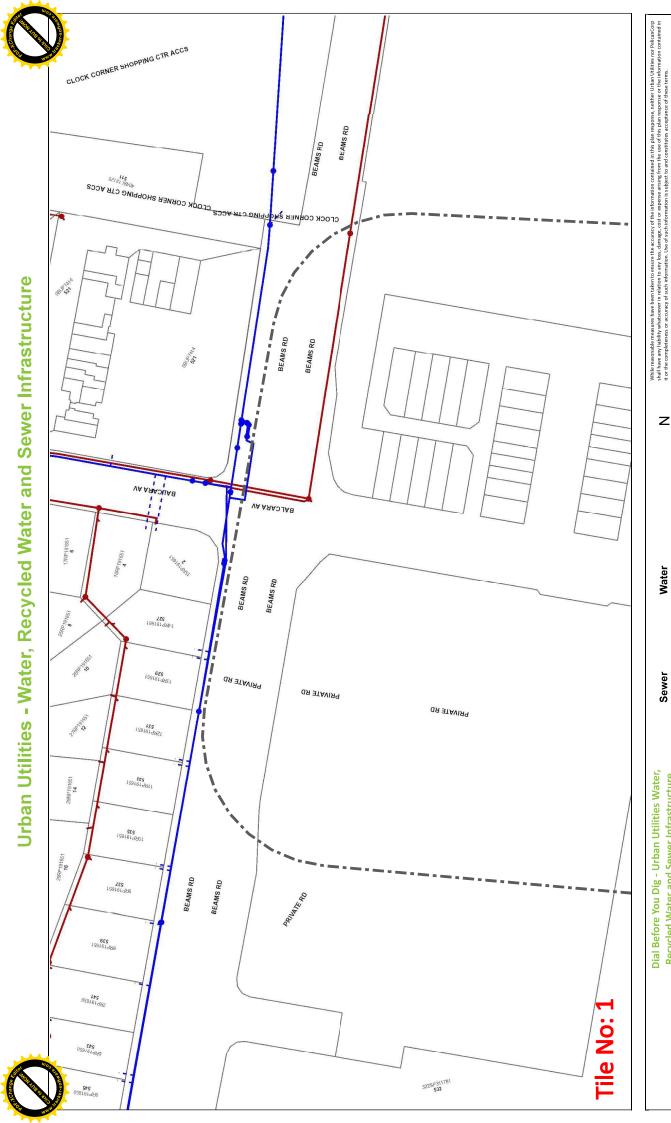


For further information, please call Urban Utilities on 13 26 57 (Bam-6pm weekdays). Faults and emergencies 13 23 E4 (24/7). ABN 86 673 835 011 Based on or contains data provided by the State of Queensland (Department of Natural Resources and Mines) (2020). In consideration of the State permitting the use of this days our acknowledge and agree that the State gives no warmyn melation to the data (including accuracy, liability in negligence) for any loss, the cost including consequents and anagel relating stora you so of the data. Data must not be used for direct marketing or be used in breach of the privary laws. © State of Queensian Department of Matural Resources and Mines (2020). The plans are indicative and approximate only and provided without warranties of any kind, express or implied including in relation to accuracy, completen correctness, currency or fitness for purpose. This plan should be used as guide only. Any dimensions should be confirmed on site by the relevant authority Map Scale 1:1781 - - - Water Service (Indicative only) Network Structures Major Infrastructure --- Network Pipelines Infrastructure Water Major Infrastructure Network Structures ---- Network Pipelines Infrastructure Sewer Produced By: Urban Utilities Dial Before You Dig - Urban Utilities Water, Recycled Water and Sewer Infrastructure Date DBYD Job to Commence: 10/02/2021 Date DBYD Map Produced: 09/02/2021 **DBYD Reference No: 106379439** Date DBYD Ref Received: 09/02/2021 This Map is valid for 30 days **Urban** Utilities

While reasonable measures have been taken to ensure the accuracy of the information contained in this plan response, neither tuthan Utilities nor PelicanCorp Shall have any limiting Watersener in relation to any loss, a manage, not are otherwise a respect in a measure as the information contained in a forther completeness or accuracy of such information. Use of such information is subject to and constitutes acceptance of these terms.

Urban Utilities takes no responsibility and accepts no liability for any loss, damage, costs or liability that may be Urban Utilities takes no responsibility and accepts no liability for any loss, damage, costs or liability that may be incurred by any person acting in reliance on the information provided on the plans.

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Plans generated [09 Feb 2021] by Pelicancorp TicketAccess Software | www.pelicancorp.com

This Map is valid for 30 days

For further information, please call Urban Utilities on 13 26 57 (8am-6pm weekdays). Faults and emergencies 13 23 64 (24/7).
ABN 86 673 835 011

Based on or contains data provided by the State of Queensland (Department of Natural Resources and Mines) (2020). In consideration of the State permitting the use of this days our acknowledge and agree that the State gives no warmyn melation to the data (including accuracy, liability in negligence) for any loss, the cost including consequents and anagel relating stora you so of the data. Data must not be used for direct marketing or be used in breach of the privary laws. © State of Queensian Department of Matural Resources and Mines (2020).

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This plan should be used as guide only. Any dime

Map Scale 1:1000

- - - Water Service (Indicative only)

Network Structures

Network Structures ---- Network Pipelines

Produced By: Urban Utilities

Date DBYD Job to Commence: 10/02/2021 Date DBYD Map Produced: 09/02/2021

Urban Utilities

 Major Infrastructure --- Network Pipelines

Major Infrastructure

Infrastructure

Recycled Water and Sewer Infrastructure

DBYD Reference No: 106379439 Date DBYD Ref Received: 09/02/2021

Infrastructure

The plans are indicative and approximate only and provided without warranties of any kind, express or implied including in relation correctness, currency or fitness for purpose.



Seq # 106379433 Job # 21045072

Provider: Brisbane City Council Telephone: 07 3403 8888



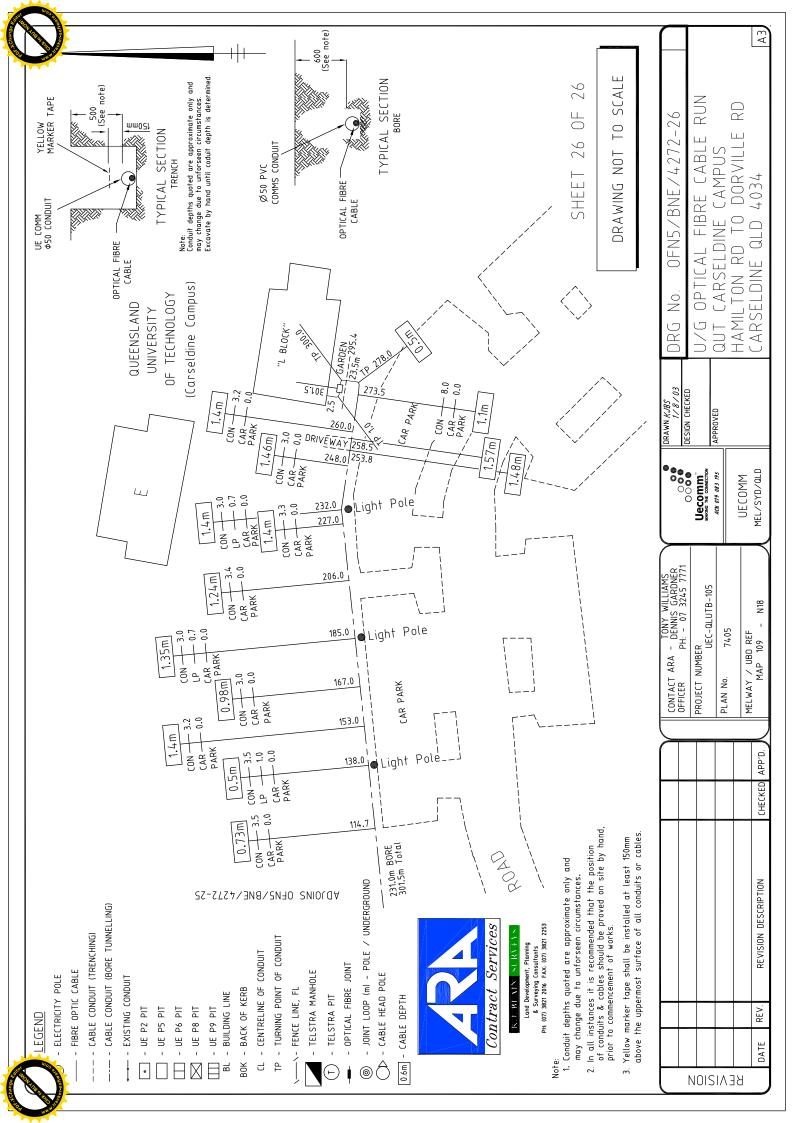


In an emergency contact Brisbane City Council on 07 3403 8888 Index Sheet

Scale 1:2,000

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Plans generated by SmarterWX™ Automate





Job No 21045072



Caller Details

Caller Id: 1411846 **Contact:** Mr Mark Shaw Phone: 0488 044 500 Company: KN Group Mobile: Not Supplied Fax: Not Supplied

Address: Email: mshaw@knpl.com.au Level 2/71 Grey Street

South Brisbane QLD 4101

Dig Site and Enquiry Details

WARNING: The map below only displays the location of the proposed dig site and does not display any asset owners' pipe or cables. The area highlighted has been used only to identify the participating asset owners, who will send information to you directly.



liser Reference Not Supplied Working on Behalf of: Private

Start Date: **End Date: Enquiry Date:** 17/02/2021 09/02/2021 10/02/2021

Address:

532 Beams Road Carseldine QLD 4034

Job Purpose: Onsite Activity: Excavation Manual Excavation **Location of Workplace:** Location in Road:

Both CarriageWay, Footpath, Nature Strip

Check the location of the dig site is correct. If not submit a new enquiry.

• If the scope of works change, or plan validity dates expire, resubmit your enquiry.

• Do NOT dig without plans. Safe excavation is your responsibility. If you do not understand the plans or how to proceed safely, please contact the relevant asset owners.

Notes/Description of Works:

Your Responsibilities and Duty of Care

- The lodgement of an enquiry does not authorise the project to commence. You must obtain all necessary information from any and all likely impacted asset owners prior to excavation.
- If plans are not received within 2 working days, contact the asset owners directly & quote their Sequence No.
- ALWAYS perform an onsite inspection for the presence of assets. Should you require an onsite location, contact the asset owners directly. Please remember, plans do not detail the exact location of assets.
- · Pothole to establish the exact location of all underground assets using a hand shovel, before using heavy machinery.
- Ensure you adhere to any State legislative requirements regarding Duty of Care and safe digging requirements.
- If you damage an underground asset you MUST advise the asset owner immediately.
- By using this service, you agree to Privacy Policy and the terms and disclaimers set out at www.1100.com.au
- For more information on safe excavation practices, visit www.1100.com.au

Asset Owner Details

The assets owners listed below have been requested to contact you with information about their asset locations within 2 working days. Additional time should be allowed for information issued by post. It is your responsibility to identify the presence of any underground assets in and around your proposed dig site. Please be aware, that not all asset owners are registered with the Dial Before You Dig service, so it is your responsibility to identify and contact any asset owners not listed here directly.

** Asset owners highlighted by asterisks ** require that you visit their offices to collect plans.

Asset owners highlighted with a hash require that you call them to discuss your enquiry or to obtain plans.

Seq. No.	Authority Name	Phone	Status
106379437	AARNet Pty Ltd, Qld	1300275662	NOTIFIED
106379433	Brisbane City Council	0734038888	NOTIFIED
106379434	Energex, Electricity (Qld)	0736645400	NOTIFIED
106379438	NBN Co, Qld	1800626329	NOTIFIED
106379436	Optus and/or Uecomm, Qld	1800505777	NOTIFIED
106379432	Powerlink Qld	0738661313	NOTIFIED
106379435	Telstra QLD, South East	1800653935	NOTIFIED
106379431	TPG Telecom (QLD)	1800786306	NOTIFIED
106379439	Urban Utilities	132364	NOTIFIED

END OF UTILITIES LIST



APPENDIX E URBAN UTILITIES (UU)



Queensland Urban Utilities GPO Box 2765 BRISBANE QLD 4001 Phone: 07 3432 2200 or 13 26 57 www.urbanutilities.com.au/development-services

15th October 2018

Mal McCann Calibre Consulting (QLD) Pty Ltd PO Box 10349 Adelaide Street Brisbane QLD 4000

Via Email: BrisAdmin@calibreconsulting.co

Dear Applicant,

Queensland Urban Utilities Services Advice Notice

QUU Application Number: 18-SRV-36240
Applicant Name: Mal McCann

Calibre Consulting (QLD) Pty Ltd

Street Address: 532 Beams Road, Carseldine

Real Property Description: Lot 322 on SP172124

Proposed service connection/alteration/disconnection type:

Drinking water	Ø
Non-drinking water	
Wastewater	$\overline{\checkmark}$

Queensland Urban Utilities provides this Services Advice Notice in response to the request received in September 2018. In accordance with section 99BRAC(3) of the *South East Queensland Water (Distribution and Retail Restructuring) Act 2009,* this Services Advice Notice provides advice about the proposed connection having regard to the connections policy in the Queensland Urban Utilities Water Netserv Plan, the charges and conditions that may apply to the connection and other relevant matters about the connection. All terms used in this Services Advice Notice are defined by reference to the Queensland Urban Utilities Water Netserv Plan.

This Services Advice Notice does not constitute an application for connection, is not an approval to connect to the Queensland Urban Utilities network(s) and does not bind any future Queensland Urban Utilities' decision if the applicant applies for a connection.

Queensland Urban Utilities understands that the proposed development will consist of 178 residential dwellings. As per the request for a Service Advice Notice submitted, a material change of use/reconfiguration of a lot will be applied for as part of this development.

Based on your proposal and discussion with Queensland Urban Utilities officers, the following advice is provided:

Queensland Urban Utilities Services Advice

Infrastructure and Design

The project site is within the [name] Priority Development Area (PDA). Development applications for priority development areas are assessed by Economic Development Queensland (EDQ).

The infrastructure funding framework within each PDA is also typically prescribed and managed by EDQ under an Infrastructure Charges Offset Plan (ICOP). The developer should review the current ICOP and development scheme to understand the broader infrastructure obligations specific to this site.

Note: Developer Services needs to consult internally with Network Operations (as future owners of the assets) and Strategic Planning prior to EDQ finalising the proposed infrastructure layout.

Water

The subject site is located at Aspley Reservoir Gravity water pressure zone.

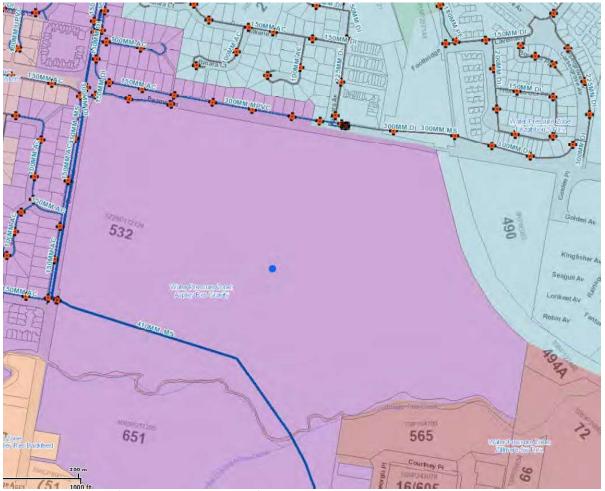


Figure 1: Existing Water infrastructure within the vicinity of the subject site

Calibre Consulting Engineers have proposed to connect the development to the QUU water network at 2 points, as indicated in Attachment 1:

- Point A: On the DN300 MPVC main in Beams Road
- Point B: On the DN150 AC main in Dorville Road

Queensland Urban Utilities does not object to the proposed water service arrangement. Please

note that:

- Connection point A shall be provided on the western side of gate valve RV436569, to ensure the property is contained within a singular pressure zone.
- Connection Point B shall be provided to the existing DN150 AC water main at the western verge of Dorville Road.

Wastewater

The subject site is currently serviced by connection to the existing DN300 VC trunk sewer at the near side of Beams Road.



Figure 1: Existing Wastewater infrastructure within the vicinity of the subject site

Calibre Consulting Engineers have proposed to connect the development to the existing DN825 concrete trunk sewer main traversing through the property, along the southern property boundary.

Queensland Urban Utilities does not object to the proposed water service arrangement. Please note that, connection shall be provided to a reticulation manhole in parallel to the existing manhole (MH37144) on the trunk main.

Note that the infrastructure required for the proposed development is to be provided in accordance with QUU requirements, including but not limited to the *SEQ Water Supply and Sewerage Design and Construction Code* (SEQ WS&S D&C Code, 2013), or current equivalent.

Network Demand and Capacity

Water

An assessment of the water supply available at the site, including computational hydraulic modelling of the network under peak demand and fire flow conditions, has been completed.

The analysis assumes a Peak Hour Demand of 4.8 L/s (corresponding to the details of the proposed development).

The assessment indicates that the existing water supply network at the vicinity of subject site has sufficient capacity to service the proposed development in accordance with the SEQ Water Supply and Sewerage Design and Construction Code, 2013 (SEQ WS&S D&C Code). The reticulated water supply network proposed within the development should be designed and sized in accordance with the SEQ Code Design Criteria.

Indicative flow and pressure advice for the two proposed connection points on existing DN300 MPVC main in Beams Road and DN150 asbestos cement main in Dorville Road is provided in Table 1, below.

Table 1: Indicative Flow and Pressure Advice

Table 1: Illalcative Flow and Flessare Advice							
Assumed Connection Main	Estimated RL Connection (m	Hydraulic Grade Line (m AHD)			Pressure (kPa) ¹		
, 155 u 110 u 100 110 110 110 110 110 110 110 110 11	AHD)	0 L/s 10 L/s 20 I			0 L/s	10 L/s	20 L/s
Point A – on DN300 MPVC main in Beams Road (constructed in 2015)	13.89	65.4	65.3	64.9	505	504	501
Point B – on DN150 AC main in Dorville Road (constructed in 1985)	22.18	65.4	65.2	64.8	424	422	418

Notes: ¹ Modelled pressure in supply main, relative to the estimated connection RL (m AHD).

Disclaimer

Information provided by Queensland Urban Utilities is based on hydraulic modelling ("Hydraulic Modelling Information"). Model results are for the anticipated performance. The Hydraulic Modelling Information has not been verified by field measurements and may be inaccurate due to field conditions.

As such, users relying on Hydraulic Modelling Information do so at their own risk and should make their own independent investigations to verify model outputs.

The Hydraulic Modelling Information does not state nor imply a guaranteed level of service. Designers are referred to Queensland Urban Utilities' Customer Charter and Customer Service Standards for facility hydraulic service considerations. Queensland Urban Utilities does not provide a service of minimum flows and pressures to private fire-fighting systems.

Due to changing operational circumstances, pressure and flows delivered to a service may vary. Designers are advised to make adequate provisions within the fire system installation for the pressure, flow and reliability requirements, for the life of the system.

A hydraulic assessment of the sewerage network servicing the site under peak wet weather flow conditions has been completed.

The analysis assumes a Peak Wet Weather Flow from the development of 6.0 L/s (corresponding to the details of the proposed development).

The assessment indicates that the localised gravity mains at the vicinity of the subject site have sufficient capacity to service the proposed development.

² Designers are required to adjust the Hydraulic Grade Line/Pressure model results for site/building RL differences and calculate the extra hydraulic losses from point of connection with the main.

³ Field performance of cast iron spun (or cement) lined mains can be variable. Field testing to ascertain actual pressure drops may be advisable.

⁴ Indicative flow and pressure results assume a background demand of 2/3 Peak Hour has been applied throughout the network.

Land and Easements

Sewer Main in Private Properties

Please refer to following link for easement requirements:

http://www.urbanutilities.com.au/development-services/our-services/building

Water Main in Private Properties

Please refer to table 5.2 and clause 5.4.4 of SEQ WS&S D&C Code for easement requirements.

Infrastructure Charges (as at 1 July 2018)

Infrastructure Charges will be levied in accordance with the Queensland Urban Utilities' Water Netserv Plan (Part A) Charges Schedule applicable at the time the water approval application is lodged.

Further information is available at the following website:

https://www.urbanutilities.com.au/development-services/help-and-advice/water-netserv-plan

Trade Waste

A Trade Waste Approval is not required for the proposed development based on the information supplied by the applicant.

Connection Application Process

A formal assessment as to whether your application qualifies as a Standard Connection, Minor Works Approval, or Major Works Approval will be resolved on application for a Water Approval. For the purposes of preliminary advice, and based on the information provided, it is expected that the following applications will be required to assess the ability to connect to Queensland Urban Utilities networks:

1. Network and/or Property Service Connection - Major Works

The Water Approval will require connection works to be undertaken. You will be able to choose which consultants and contractors to appoint to design and construct the works, including live works (in most cases) and then maintain the works for a specified period (usually 12 months) in accordance with the conditions stated in your Water Approval.

Please note that the information provided within this section is subject to the specific aspects of the development and water application.

Fees and Charges

Queensland Urban Utilities fees and charges are stated in the Queensland Urban Utilities' Water Netserv Plan (Part A) Charges Schedule. The fees and charges that are likely to be associated with these applications are outlined below:

1. Application Phase

Base Application Fee – Network (1-10 lots) \$609 (per application for each service) Fast-track application process (up to 10 lots only) \$2,436 (per application for each service) Technical Report Review Fee \$602 (per report)

2. Design, Construction and Maintenance Phases

Design Approval Fee (reticulation)

Property Service Connection Fee \$2,128 (per connection / disconnection / alteration) Network Connection Type A (1-10 lots) \$1,520 (per application for each service)

Re-checking Amended Plans Fee

Re-checking Amended Plans Fee \$602 per plan

Works Inspection Fee (reticulation)

Works Inspection Fee Type A \$365 (per inspection) Works Re-inspection Fee Type A \$547 (per inspection)

Notes:

- The customer may incur additional fees and charges during the approval and works phase, including but not limited to, fees levied by the RPEQ and construction contractor, fees associated with the provision of maintenance / uncompleted works bond(s), re-checking amended plans fees, re-inspection of works fees and infrastructure agreement preparation fees:
- 2. The above estimates are indicative only and are subject to review of the detailed application upon lodgement; and
- 3. Please refer to the QUU *Water Netserv Plan* for further details / clarifications on Fees and Charges.

Time Frames for Assessment

Connection Assessments (for applications other than Standard Connection)

To be completed within 20 business days of receipt of Properly Made Connection Application (including payment of the relevant assessment fee), or within a further 20 business days of receipt of requested information (unless extended by agreement).

Design Phase

Typically for an application classified as **major works**, the assessment of the design phase is to be completed within 20 business days of receipt of all designs.

This Services Advice Notice is current for a period of two (2) years from the date of issue. Should you wish to proceed with applying for a service connection please lodge your application via Queensland Urban Utilities Development Services Online Lodgement Portal at http://www.urbanutilities.com.au/development-services. Please include your Services Advice Notice reference number in your application.

Queensland Urban Utilities may, at its discretion, provide a reduced fee for a service connection application based on this Services Advice Notice if your application is received within 12 months of the date of issue and is substantially in accordance with the proposal upon which this advice was issued.

If you have any questions in relation to this Service Advice Notice, please do not hesitate to contact your account manager, Vindy Hapuarachchi on 07 3855 6251 or vindy.hapuarachchi@urbanutilities.com.au.

Alternatively, please email DCMTenquiries@urbanutilities.com.au.

Yours sincerely

Toby Turner Senior Engineer

Queensland Urban Utilities



Urban Utilities GPO Box 2765 BRISBANE QLD 4001 Phone: 07 3432 2200 or 13 26 57 www.urbanutilities.com.au/development-services

15th June 2020

Department of Housing & Public Works C/- Calibre Consulting (QLD) Pty Ltd PO Box 10349 Adelaide Street Brisbane QLD 4000

Via Email: BrisAdmin@calibreconsulting.co

Dear Applicant,

Urban Utilities Water Reticulation Analysis

UU Application Number: 20-SRV-46159

Applicant Name: Department of Housing & Public Works

C/- Calibre Consulting (QLD) Pty Ltd

Street Address: 532 Beams Road, Carseldine

Real Property Description: Lot 322 on SP172124

Proposed service connection/alteration/disconnection type:

Drinking water	Ø
Non-drinking water	
Wastewater	

Urban Utilities provides this Services Advice Notice in response to the request received on 02/06/2020. In accordance with section 99BRAC(3) of the *South East Queensland Water* (*Distribution and Retail Restructuring*) *Act 2009*, this Services Advice Notice provides advice about the proposed connection having regard to the connections policy in the Urban Utilities Water Netserv Plan, the charges and conditions that may apply to the connection and other relevant matters about the connection. All terms used in this Services Advice Notice are defined by reference to the Urban Utilities Water Netserv Plan.

This Services Advice Notice does not constitute an application for connection, is not an approval to connect to the Urban Utilities network(s) and does not bind any future Urban Utilities' decision if the applicant applies for a connection.

Urban Utilities understands that the proposed development will consist of 5 stages of residential development including a total of 601 residential multiple dwellings and 3 stages of non-residential development including 7,400 m² GFA. As per the request for a Service Advice Notice submitted, a material change of use/reconfiguration of a lot will be applied for as part of this development.

Based on your proposal and discussion with Urban Utilities officers, the following advice is provided:



Urban Utilities Services Advice

Background

Objective

Calibre Consulting Pty Ltd requested Urban Utilities to prepare a Water and Wastewater Network Analysis Report for the proposed mixed-use development at 532 Beams Road, Carseldine.

The proposed development is located at Brisbane City Council local government area. The site is bounded by Beams Road at north, Dorville Road at west, QR railway corridor at east and Cabbage Tree Creek at south. The proposed development consists of 5 stages of residential development including a total of 601 residential multiple dwellings and 3 stages of non-residential development including 7400 m² GFA.

This report includes a review of the necessary water and wastewater network configuration and summarises the modelling assessment undertaken for the proposed development.

Water Supply

The development site is located at the Aspley Reservoir Gravity Water Pressure Zone. A map of existing infrastructure is provided in Figure 1.

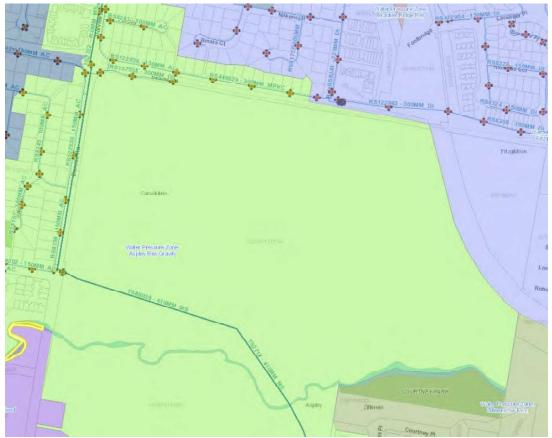


Figure 1 – Development site and surrounding water supply network

Multiple water mains (300mm MPVC /300mm DI/ 150mm AC) in Beams Road and a 150mm AC water main in Dorville Road are available at the vicinity of the site.

The applicant has proposed to service the development from the existing 300 MPVC main in Beams Road. The proposed water layout plan is provided in **Appendix 1**.

Wastewater:

A 825mm dia trunk sewer main at the western property boundary, a 225mm VC main in Dorville Road and 225mm/ 300mm VC mains in Beams Road are available at the vicinity of the subject site, as indicated in **Figure 2**.

As per the natural ground topography, the proposed development area drains towards the existing 825mm dia. trunk sewer main (Cabbage Tree Creek Main sewer) in S5 catchment.

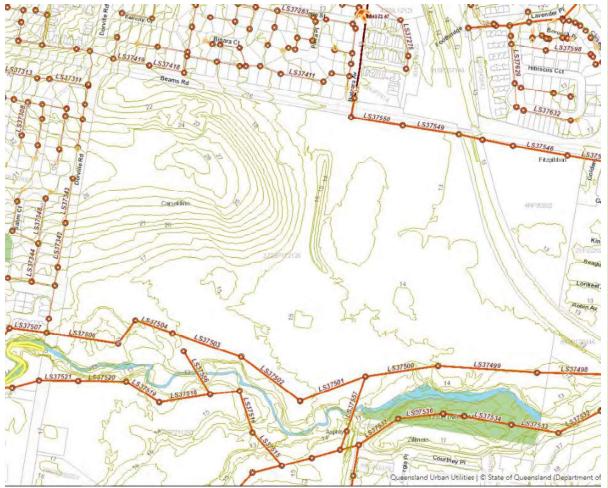


Figure 2 – Development site and surrounding Sewer network

The applicant has proposed to connect the development to the 825mm dia trunk sewer main at the western property boundary. The proposed wastewater layout plan is provided in **Appendix 1**.

Design Criteria

Development Yield

The proposed development has 601 Residential multiple dwellings and 7400 m2 GFA of Non-Residential space.

Equivalent Persons

The equivalent person (EP) rating of the development site was calculated based on development density factors outlined in Table A4.1, Brisbane City Planning Scheme Development Density of the SEQ WS&S D&C Code (Version 2.0 - February 2020).

The total EP in all stages of the development is calculated as 1,164.1 approximately. A summary of staging and EP calculation is provided below in **Table 1**.

Table 1: Summary of Staging and EP

Residential	Terrace	Apartments	Retirement	Total No: of dwellings	EP
Stage 1	79		150	229	435.1
Stage 2	45			45	85.5
Stage 3	57	100		157	298.3
Stage 4	20	142		162	307.8
Stage V		8		8	15.2
Sub Total	201 250 150 601				1141.9
Non-Residential		EP			
Stages 3, 4 & V		22.2			
Total		1164.1			

Water Demands

The water supply network Design Criteria (outlined in Table 4.1 of the SEQ WS&S D&C Code (Version 2.0 - February 2020) were used to determine the development's respective demands.

- Average Day Demand (AD): 230 L/EP/day
- Non-Revenue Water (NRW): 30 L/EP/day
- Peak Day Demand (PD): 2.0 x AD
- Peak Hour Demand (PH): 4.0 x AD

Based on above criteria, the water demand corresponding to the total EP (1164.1) is as follows:

- Average Day Demand (AD): 3.2 L/s
- Peak Day Demand (PD): 6.4 L/s
- Peak Hour Demand (PH): 12.8 L/s

Water Supply Network Firefighting Capacity

The SEQ Code Design Criteria requires provision of firefighting capacity of 25 L/s for greenfield low-density residential areas, 30 L/s for Commercial areas and 60 L/s for high density residential areas.

Considering this is a mixed-use development, 60 L/s firefighting demand was considered with a background demand of 2/3 of residential Peak Hour Demand (PH).

Sewerage Loading

The Sewerage network Design Criteria (outlined in Table 10 of the SEQ WS&S D&C Code (Version 2.0 - February 2020) were used to determine the development's respective sewerage loading.

- Average Dry Weather Flow (ADWF) = 210 L/EP/Day
- Peak Wet Weather Flow (PWWF) = 5 x ADWF

The sewerage loading corresponding to the total EP (1164.1) is as follows:

- Average Dry Weather Flow (ADWF) = 2.83 L/s
- Peak Wet Weather Flow (PWWF) = 14.2 L/s

Water Network Analysis

The existing and proposed water supply network performance was compared to the following guidelines from the SEQ WS&S D&C Code (Version 2.0 - February 2020)

- **Minimum pressure:** Under Peak Hour demands, the residual pressure in the water supply network servicing existing and proposed customers should not fall below 22 metres.
- Maximum pressure: A maximum service pressure of 55 metres is permitted.
- Maximum Velocity: 2.5 m/s
- Maximum Allowable Head loss: 5m/km (<=DN150), 3m/km (>DN150)
- **Firefighting capacity:** Under the identified fire flow event, with a background demand of two-thirds (2/3) Peak Hour, the minimum residual pressure at the flowing hydrant shall be 12 m, with a minimum pressure head of 6 m maintained through the water supply zone.

Existing network configuration

The proposed development site is located in the Aspley Reservoir Gravity Water Pressure Zone, which is serviced by Aspley Reservoir.

Reservoir details:

- Bottom water level (BWL): 63.09m AHD
- Top water level (TWL): 73.52m AHD

A 1060mm trunk main from Aspley Reservoir is supplying this area, branching off into a 910mm MSC trunk main in Pie Street, a 600mm MSC/ 410mm MS main in Kirby Road, which is supplying the 300mm MS main in Dorville Rd and 300mm DI/MPVC main in Beams Road.

Water Connection Points

The applicant has proposed to service the development from the existing 300 MPVC water main in Beams Road. Two connections from the development are proposed to this water main. As indicated in **Appendix 1**, Connection 1 is proposed at the boundary between 2 pressure zones (Aspley Res Gravity Pressure Zone and Bracken Ridge Reservoir pressure zone). Connection 2 is at the Aspley Res Gravity Pressure Zone (Refer to Figure 1). Since both connections must be at the same pressure zone, Connection 1 must be provided at the western side of Gate valve RV436569.

Water Main Sizing

The existing 300 MPVC water main in Beams Road has sufficient capacity to service the development.

Urban Utilities approved water main sizing is provided in **Appendix 1.** As indicated in Appendix 1, the 180mm diameter main should continue between Points A to B and B to C.

Note that the water infrastructure required for the proposed development is to be provided in accordance with Urban Utilities' requirements, including but not limited to the SEQ Water Supply and Sewerage Design and Construction Code (SEQ WS&S D&C Code - Version 2.0 - February 2020), or current equivalent.

Sewer Network Analysis

Capacity assessment

The existing 825mm Cabbage Tree Creek main sewer has sufficient capacity to service the development.

The pipe sizing provided in **Appendix 1** have sufficient capacity to service the development. Please

note that the minimum grades are required for all sewer mains within the development.

Note that the wastewater infrastructure required for the proposed development is to be provided in accordance with Urban Utilities' requirements, including but not limited to the SEQ Water Supply and Sewerage Design and Construction Code (SEQ WS&S D&C Code - Version 2.0 - February 2020), or current equivalent.

This Services Advice Notice is current for a period of two (2) years from the date of issue. Should you wish to proceed with applying for a service connection please lodge your application via Urban Utilities Development Services Online Lodgement Portal at http://www.urbanutilities.com.au/development-services. Please include your Services Advice Notice reference number in your application.

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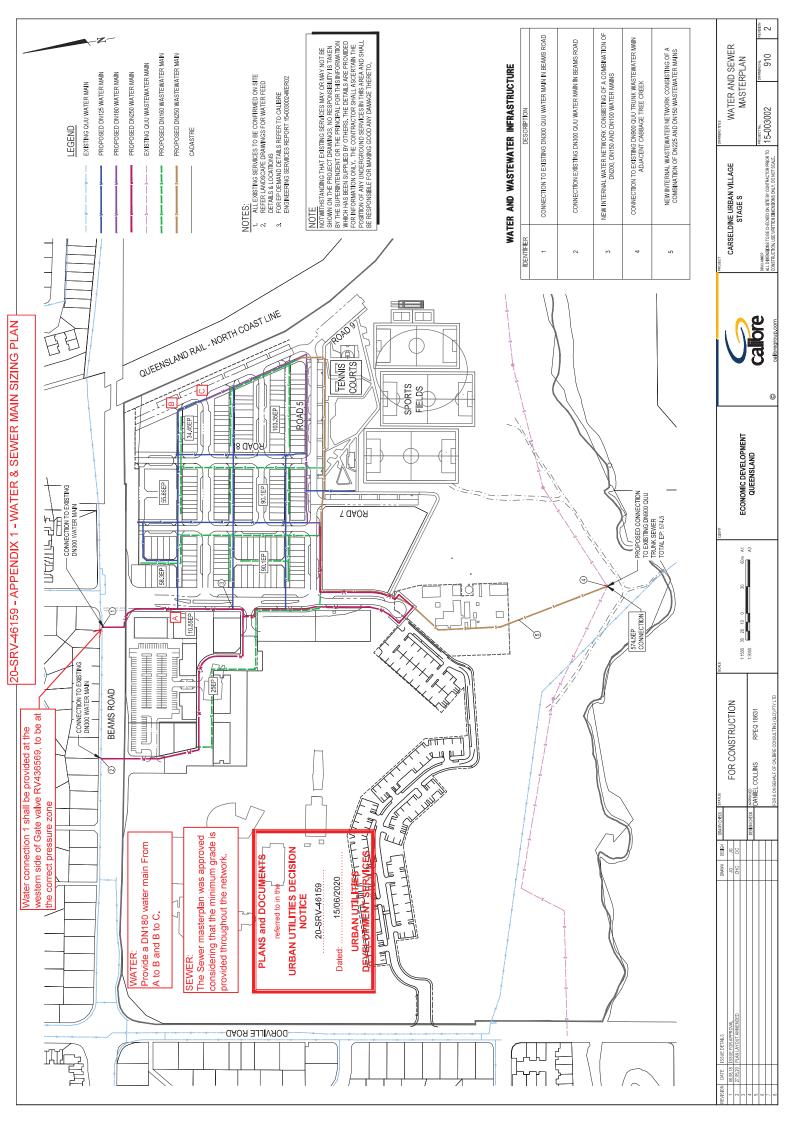
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Alternatively, please email DCMTenquiries@urbanutilities.com.au.

Yours sincerely

2

Sajid Imam SyedDevelopment Assessment Team Leader
Urban Utilities





APPENDIX F ASBESTOS REMEDIATION STRATEGY AND DISPERSIVE SOIL REPORT

CARSELDINE URBAN VILLAGE: STAGES 2 - 4 & V

Our Ref: GE20.025.L2

Date: 22nd December 2020

KN Group Pty Ltd

Via email: mark@kngroup.com.au

Attention: Mr. Mark Shaw

Dear Mark,

RE: TECHNICAL MEMORANDUM - ACID SULFATE SOIL (ASS) REVIEW FOR PROPOSED 'CARSELDINE URBAN VILLAGE STAGES 2 – 4 & V' DEVELOPMENT

Introduction & Background

Gallagher Environmental (GE) was commissioned by KN Group Pty Ltd to provide an acid sulfate soil (ASS) review of the proposed 'Carseldine Urban Village Stages 2 - 4 & V' development located at Beams Road, Carseldine.

Acid Sulfate Soil Mapping

According to the Department of Environment & Heritage Protection (DEHP) 'Special Acid Soil Maps', the proposed development area has negligible probability of ASS occurrence. The nearest indication of ASS is associated with two (2) tributaries located to the north-east of the development with 'low probability of ASS occurrence'.





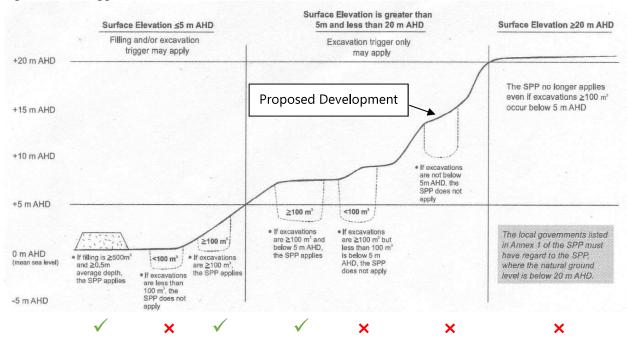


State Planning Policy (SPP)

The State Planning Policy (2017) and State Planning Policy (SPP) State Interest Guideline "Water Quality" – Policy 9 (2016) applies to all soil or sediment at or below 5m AHD (where the natural ground level is below 20m AHD), where the development would result in:

- The excavation of ≥100m³ of soil or sediment situated below 5m AHD; or
- Filling of land situated below 5m AHD that involves ≥500m³ of fill material with an average depth of ≥0.5m.

Figure 1: SPP Trigger Conditions (ASS)



Proposed Development

In accordance with design information supplied by KN Group, it is understood that the relevant proposed earthworks are summarised as follows:

- The majority of the proposed development area is essentially flat at approximately 13 14m AHD, with more elevated areas up to 26m AHD situated in the far western area of the proposed development.
- The proposed maximum (i.e. topographically lowest) invert level associated with the proposed earthworks is 11.0m AHD, within the proposed sewer.

Therefore, no soil material at or below 5m AHD will be intercepted during the proposed construction and therefore the SPP is not invoked for the development. Consequently, the proposed development is considered free of any ASS disturbance and shall not require an Acid Sulfate Soil Management Plan (ASSMP) in accordance with the State Planning Policy (SPP) (2017) and QASSIT Soil Management Guidelines (2014).





CARSELDINE URBAN VILLAGE: STAGE 1

For reference, acid sulfate soil (ASS) materials develop within former marine and estuarine sediments that were deposited as sea levels rose above the residual soil landscape during the Holocene Epoch (circa ~6500 years ago), and to a lesser extent, the Pleistocene Epoch (circa ~125,00 years ago). The relative sea levels during both these geological periods dictate the elevation (AHD) that ASS materials can generally be found: at or below 5m AHD, as adopted within the framework of the SPP, however more commonly below 2-3m AHD in coastal south-east Queensland.

We trust this is acceptable. Please feel free to contact me on 0438 724 929 or <u>glen@genviro.com.au</u> if you require further elaboration or wish to discuss anything further.

Yours faithfully,

Glen Gallagher BScApp(Env Sc)(Hons) MEIANZ CPESC

Principal Environmental Scientist | Gallagher Environmental

STANDARD LIMITATIONS

GurGallagher

This report has been prepared for the sole use of the client and the client's immediate representatives and agents. Third parties (excluding regulatory agencies assessing an application in relation to the purpose) shall not rely on this report. It is fundamental in the application of this report that the full report is read in its entirety and fully understood. Please contact Gallagher Environmental for additional explanation if any of the report content is not fully understood.

To the best of our knowledge, information contained in this report is accurate at the date of issue and in accordance with generally accepted consulting practice. The interpretation of scientific data, however, often involves both professional and subjective judgments including extrapolation of data. As such, interpretation is open to error. In addition, site conditions are subject to change in a limited time and there remains a risk that the site conditions will differ from these interpretations. Gallagher Environmental waives all responsibility for loss or damage where information provided by the Client (including third parties) used in the preparation of this report was inaccurate or in error. This report should be retained as a complete document and should not be copied in part, divided or altered in any way.





Dispersive Soil Management Plan (DSMP): Carseldine Urban Village: Stages 1- 4 & Stage V



Client: Economic Development Queensland C/- Calibre Group

Report No: GE20.025.R1

Date: 22nd April 2020



DOCUMENT CONTROL

Job No.

Document No: GE20.025.R1.doc

Title: Dispersive Soil Management Plan

(DSMP): Carseldine Urban Village Stages

1-4 & Stage V

Project Manager: Glen Gallagher

Qualifications: BScApp(EnvSc)(Hons) MEIANZ CPESC

GE20.025

Client: C/- Calibre Group

Client Contact: Mr. Daniel Collins

Synopsis: A detailed DSMP providing site-specific

management protocols for the construction phase of the development.

REVISION & CHECKING HISTORY

Telephone: +41 438 724 929

Email: glen@genviro.com.au

ABN 56 493 696 583

Revision Number	Date	Issued by	Signature
Original	22 April 2020	G Gallagher	GurGallagher

DISTRIBUTION

Gallagher

Environmental

59 Cremorne Rd KEDRON QLD 4031

Destination		Revision	
Destination	Original		
Calibre Group	1		
GE Database	1		

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This report is not a guarantee that the site conditions will behave in accordance with the interpretation set out herein, but rather our opinion as to the correct interpretations based on the results of desktop review, site investigations, in situ testing and/or laboratory testing in accordance with generally accepted consulting practice. To the best of our knowledge, information contained in this report is accurate at the date of issue. The interpretation of scientific data, however, often involves both professional and subjective judgments. As such, interpretation is open to error. In addition, site conditions are subject to change in a limited time and there remains a risk that the site conditions will differ from these interpretations. Gallagher Environmental waives all responsibility for loss or damage where information provided by the Client (including third parties) used in the preparation of this report was inaccurate or in error.

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APPENDIX A: BORELOGS

APPENDIX B: LABORATORY RESULTS





1. INTRODUCTION

1.1 DSMP Overview

Gallagher Environmental (GE) was commissioned C/- Calibre Group to prepare a Dispersive Soil Management Plan (DSMP) for the proposed 'Carseldine Urban Village – Stages 1 – 4 & Stage V' development located at Beams Road, Carseldine.

The purpose of the assessment is to define the overall soil dispersion risk of the site soils and to provide appropriate management principles where required in order to ensure that earthworks do not cause land degradation, and to mitigate effects on the built environment from soil dispersion as a consequence of soil disturbance.

The report is divided into sections describing: the physical characteristics of the site; a review of detailed laboratory results, an assessment of the soil dispersion potential, and where required, subsequent management strategies to be employed during the construction phase of the development.

1.2 Scope of Study

The scope of the study included:

- The logging, sampling and laboratory analysis of samples recovered from five (5) boreholes and additional grab samples for the purposes of soil dispersion hazard testing;
- · A detailed site inspection of the proposed development area by qualified GE staff;
- The detailed interpretation and analysis of the data obtained and comment on relevant recommendations.

Furthermore, the investigation, field and laboratory testing and interpretation were carried out in general accordance with the following documents and standards:

- 'Implementation Guideline No. 28 Dispersive Soils Management' (ICC, 2016);
- Best Practice Erosion & Sediment Control Books 1, 2 & 3 (IECA, 2008);
- Australian Soil & Land Survey Field Handbook (McDonald et. al., 1998);
- AS1289 Testing of Soils for Engineering Purposes; and
- Australian Soil Classification (Isbell, 2016).

1.3 Objectives

The specific objectives of the assessment were as follows:

- To undertake field survey and establish the soil types within the investigation area;
- To define the overall soil dispersion hazard of the site soils using desktop, field and laboratory analysis; and
- To provide specific strategies for the management of dispersive soils during the construction phase of the development and for inclusion with bulk earthwork/engineering and ESC plans, where required.

GE20.025.R1

Gallagher Environmental Soil Water Environment

DISPERSIVE SOIL MANAGEMENT PLAN (DSMP) CARSELDINE URBAN VILLAGE

1.4 DSMP Amendments

The DSMP is a flexible document that shall be modified in the event that site conditions change significantly from those considered within the DSMP and as site knowledge and site construction and engineering experience allows.

In the event that a monitoring program detects a notable failure to achieve the required DSMP objectives, the source of the failure shall be appropriately investigated, including engagement of a suitably-qualified professional (e.g. CPESC; RPEQ) where required, and the DSMP suitably modified to ensure incidents do not recur.



2. METHODOLOGY

A detailed field inspection was undertaken by a qualified Environmental Scientist on 7.04.20 and a total of five (5) boreholes drilled within the site area using solid flight hand auger equipment. Sampling from all examined profiles was undertaken within each major soil horizon (i.e. texture change) encountered and bore logging undertaken in accordance with the Australian Soil Classification (ASC, 2016). In addition, four (4) samples were taken from existing soil stockpiles on-site. The site plan detailing the sampling locations is provided in Drawing No. GE20.025.D1.

Laboratory analysis was subsequently undertaken on representative samples in order to define soil dispersion potential and soil electro-chemistry in accordance with the following Australian Standards:

- Emerson Class Number in accordance with AS1289 3.8.1; and
- pH and Electrical Conductivity (Raymont & Lyons, 2010).

Table 2.1 Testing Regime

Number of tests
5 profiles + 4 grab samples
14
14
14
2

Qualified GE staff undertook Emerson Class, pH and Electrical Conductivity testing on representative samples.

Two (2) representative samples were dispatched to ALS Laboratories, Stafford, Brisbane for the additional chemical analysis, including ESP. The laboratory certificates are contained in Appendix B.



3. SITE DESCRIPTION & PHYSICAL CHARACTERISTICS

3.1 General Overview

The site is located within the former QUT Carseldine Campus and contains several multi-storey buildings and sporting fields. The proposed residential and mixed-use development is approximately 11ha and shall include extensive cut to fill bulk earthworks, the construction of an internal road network and the installation of services (e.g. stormwater; sewer).

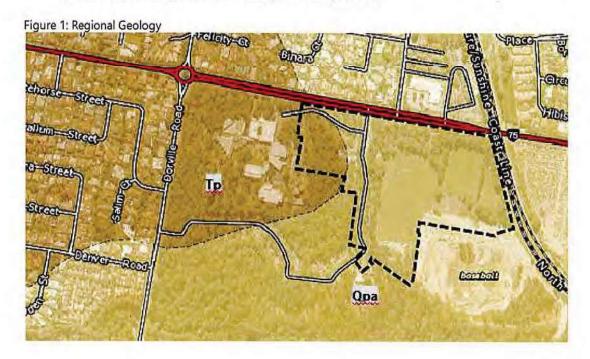
3.2 Slopes & Drainage

In accordance with the 'Australian Soil & Land Survey Field Handbook (1998)', the majority of the contains a flat to very gently inclined topography with slope magnitudes predominantly ranging between approximately 0% and 1%. However steeper slopes are located within the far western portion of the site, incusing slopes in the 5 – 15% range. The majority of the site grades towards the east and southeast of the development site.

3.3 Geology

Based on the Department of Mines 1:100,000 geological series maps, the site contains two (2) lithologies, detailed as follows and also displayed in Figure 1 below: :

- · Qpa -'Quaternary (Pleistocene) Alluvial Plains' consisting of ' clay, silt, sand, gravel'; and
- Tp -'Petrie Formation' that comprises 'mudstone, shale, sandstone, oilshale and minor pebble/cobble conglomerate' dating to Tertiary Period;





3.4 Detailed Site Inspection

A site inspection was undertaken by GE staff on 8.04.20 in order to examine the site soils and investigate any areas of active erosion, or evidence of dispersive soils. The site inspection of the general areas of the site revealed a stable, generally non-eroded land surface with intact topsoil cover and moderate to profuse grass surface cover (refer Plate 1 & 2).

Plate 1: Stable land surface of the general site areas (i.e. intact topsoil cover)



Plate 2: Stable land surface of the general site areas (i.e. intact topsoil cover)





3.5 Soil Profiles

According to the ASRIS soil database, the development area is situated in the Dermosol soil order, in accordance with the Australian Soil Classification (ASC, 2016). Based on the GE field and laboratory assessment, the site confirmed the presence of Dermosols. For reference purposes, the general soil dispersion likelihood of the various soil orders contained within the Australian Soil Classification (ASC, 2016) is shown in Table 3.1 below.

Table 3.1 General Soil Dispersion Risk of ASC Soil Orders

ASC Soil Order	Soil Horizon	General Soil Dispersion Likelihood
Sodosol	A (topsoil)	Low
3000501	B (subsoil)	Very High
Dermosol	A (topsoil)	Low
Definosof	B (subsoil)	Low - Moderate
Hydrosol	A (topsoil)	Low - Moderate
Hydrosor	B (subsoil)	Low - Moderate
Vertosol	A (topsoil)	Moderate
(sedimentary/alluvial)	B (subsoil)	Moderate - High
Vertosol	A (topsoil)	Very Low
(basalt)	B (subsoil)	Low
Kurosol	A (topsoil)	Very Low
Kulosol	B (subsoil)	Low - Moderate
Chromosol	A (topsoil)	Very Low
Cironosol	B (subsoil)	Low - Moderate
Kandosol / Tenosol	A (topsoil)	Very Low
/ Rudosol / Podosol	B (subsoil)	Low

A brief description of the characteristics of the identified soil orders are also given below and bore logs are included in Appendix A.

3.5.1 Dermosols

Dermosols are soils that do not exhibit a clear or abrupt textural B horizon and also exhibits a structure grade in the B2 horizon that is greater than weak. These soils were associated with all boreholes and were generally characterised by a sandy loam to sandy clay loam A1 horizon overlying a clay loam to light clay B2 horizon.



4. LABORATORY RESULTS

Laboratory results undertaken in order to define soil dispersion potential are shown in the following table and discussed in the following sections. The laboratory certificates are attached in Appendix B.

Table 4.1 Dispersion Hazard Test Results

Soil Type	Sample #	Emerson Class	рН	ECe (dS/m)	ESP (%)	Interpretation
	BH1 – 0.0m	7	5.6	0.3		Moderately Acidic ph
Α	BH2 - 0.0m	7	5.5	0.4	4.9	Non-saline
Horizon	BH3 – 0.0m	7	5.4	0.3		Non-sodic
(topsoil)	BH4 – 0.0m	7	5.6	0.5		Emerson Class: – Very Low Risk
	BH5 – 0.0m	7	5.9	0.7		Overall Very Low Dispersion Risk
	BH1 – 0.7m	5	5.7	0.5		
В	BH2 – 0.7m	6	5.9	0.5		Moderately Acidic ph
Horizon (subsoils)	BH3 – 0.8m	5	5.7	0.3	4.3	Non-saline
(30030113)	BH4 – 0.6m	5	5.7	0.3		Non-sodic
	BH5 – 0.5m	5	5.8	0.4		
	GS1	5	5.5	0.5		Emerson Class: Low Risk
Stockpiles	GS2	5	5.6	0.2		Overall
(subsoils)	GS2	6	5.9	0.4		Low Dispersion Risk
	GS4	5	5.6	0.3		





ABN 56 493 696 583 59 Cremorne Rd Kedron Qld 4031 glen@genviro.com.au

Contiduo

C/- Calibre Group

Gallagher Environmental Soil Water Environment

DISPERSIVE SOIL MANAGEMENT PLAN (DSMP) CARSELDINE URBAN VILLAGE

4.1 Discussion

4.1.1 Emerson Class Tests

An Emerson number of 1 indicates a strongly dispersive soil, an Emerson number of 2 indicates a high risk of significant soil dispersion; an Emerson number of 3 indicates a moderate risk of significant soil dispersion (but low risk of tunneling); whilst an Emerson number ranging between 4 and 8 indicates a soil with low to negligible dispersion tendencies.

Emerson Class testing undertaken on five (5) topsoil (i.e. A horizon) samples revealed Class 7 characteristics indicating a very low soil dispersion risk.

Emerson Class testing undertaken on nine (9) subsoil (i.e. B horizon) samples revealed Class 5– 6 characteristics indicating a low soil dispersion risk. These results are also not considered to exhibit any significant risk of sub-surface tunneling.

4.1.2 Soil pH

Soil pH is a secondary indicator in the estimation of soil dispersion hazard; where significantly alkaline pH values (e.g. pH >8.0) can indicate a higher risk of soil sodicity and subsequent soil dispersion. Conversely, strongly acidic samples (i.e. pH <5.5) can indicate high bio-available aluminum that can help counter-act soil dispersion tendencies of sodium ions in the soil.

The obtained topsoil (i.e. A horizon) pH values of 5.4 - 5.9 (median of 5.6) and subsoil pH values of 5.5 - 5.9 (median of 5.7) are indicative of generally moderately acidic pH levels which do not indicate any significant increase or decrease in relative soil dispersion risk.

4.1.3 Soil Salinity

Soil salinity reflects the relationship between landscape hydrology, geology, soil properties and vegetation. Soil salinity is also secondary indicator in the estimation of soil dispersion hazard.

Soils with mildly saline values (or relatively higher values to comparison soils) can sometimes indicate higher levels of sodium and therefore can indicate a higher risk of soil sodicity and subsequent soil dispersion.

Conversely, significantly high salinity levels have a mitigating effect on soil dispersion, as the actual soil dispersion risk is determined by the relative balance of sodium in relation to chloride levels within saline soils. Saline soils can often be sodic, but these soils will not show indicators of sodicity. The salts in the soil prevent dispersion of soil particles in high enough concentrations. If this salt level falls below the requirement for soil stability even a small amount of sodium can produce adverse effects. A combination of high sodium levels and low salt will produce extremely poor physical conditions in soils.

Soils that exhibit an EC_E <4 mS/cm are considered to be non-saline. The soil salinity classes are shown in Table 4.2 below.



Table 4.2: Salinity classes of soils (after Richards, 1954)

Class		EC _e (dS/m)	Comments
- In 2-1	None	<2	Salinity effects mostly negligible
Non-saline	Slight	2 – 4	Yields of very sensitive crops may be affected
	Moderate	4 – 8	Yields of many crops affected
Saline	Very 8 – 16	8-16	Only tolerant crops yield satisfactorily
Saline	High	>16	Only a few very tolerant crops yield satisfactorily

The calculated EC_e (saturated) values for the topsoil and subsoil materials ranged between 0.3-0.7 dS/m (median of 0.4 dS/m) indicating that these materials are non-saline and would not receive significant benefit from flocculation due to inherent salinity levels.

4.1,4 Soil Sodicity (ESP)

Soil Sodicity is a measure of exchangeable sodium in relation to other exchangeable cations. It is expressed as the Exchangeable Sodium Percentage (ESP). The common problems that may be encountered with sodic soils are synonymous with dispersive soils: lower hydraulic conductivity (i.e. water logging), higher susceptibility to tunnel erosion and severe gully erosion, poor aeration and reduction in plant-available water capacity and poor leaching (i.e. accumulation of salts).

The tendency for dispersion usually increases with increasing ESP. Sodic soil layers (ESP \geq 6) may disperse and strongly sodic soils (ESP \geq 15) usually do. The Australian sodicity classifications are provided in Table 4.3 below:

Table 4.3: Sodicity classes of soils

Sodicity Classification	ESP (%)
Non-sodic	≤6
Sodic	6 – 15
Strongly sodic	> 15
See a second see	

Source: DPI (1993)

The Exchangeable Sodium Percentage (ESP) of the representative topsoil and subsoil samples were 4.9% and 4.3% respectively, indicating non-sodic soils.



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DISPERSIVE SOIL MANAGEMENT PLAN (DSMP) CARSELDINE URBAN VILLAGE

4.2 Overall Soil Dispersion Risk

On the basis of the site inspection, investigated soil profiles and detailed laboratory results, it is considered that the soil dispersion risk and subsequent management requirements for the proposed development can be defined as follows:

4.2.1 Topsoil (0 – 150mm below natural NSL) – Very Low Risk

It is considered that the topsoil materials exhibit an overall very low soil dispersion risk and shall not require specific soil amelioration to mitigate soil dispersion risk during the construction phase.

However, all topsoil materials used in landscaping/stabilisation areas shall be suitably ameliorated where required (e.g. fertiliser) to promote optimum grass establishment. As per standard practice, all landscaping/stabilisation areas shall be monitored for suitable strike/cover to ensure compliance with the site ESCP requirements and on-maintenance requirements.

4.2.2 Subsoil (>150mm below natural NSL) – Low Risk

It is considered that the subsoil materials exhibit an overall *low* dispersion risk and are also not considered to exhibit a significant risk of sub-surface tunneling. Consequently, these materials shall not require specific soil amelioration (e.g. gypsum treatment) during the construction phase to mitigate soil dispersion risk.

As per standard practice, all disturbed subsoils shall require soil compaction to the project geotechnical requirements and all subsoils exposed during the construction phase shall be covered with hardstand or non-dispersive topsoil materials and appropriately revegetated in accordance with a Landscape Management Plan (or similar).



5. DISPERSIVE SOIL MANAGEMENT PLAN

Responsibility	Civil Contractor; Developer
Operational Policy	 To mitigate the incidence of infrastructure damage and environmental harm resulting from tunnel and subsurface erosion. To ensure the appropriate management of water quality in order to avoid impacts on the downstream environment.
Performance Criteria	All areas of landscaping/rehabilitation shall attain suitable grass strike/cover to ensure compliance with the site ESCP requirements and on-maintenance requirements. All fill materials shall be suitably compacted to geotechnical requirements.
Implementation Strategy	Topsoil Materials 1. A high level of care shall be required during delineation of the site topsoil and subsoil materials in areas of subsoil dispersion risk and in order to ensure the soil texture of stripped topsoil materials in all areas is of suitable texture (i.e. clay content <35%).
	 Topsoil shall be stripped prior to bulk earthworks within the immediate construction stages and shall be stockpiled and shaped in a free draining condition to avoid long-term soil saturation. All topsoils materials used in landscaping/stabilisation shall be suitably ameliorated where required (e.g. fertiliser) to promote grass establishment. All landscaping/stabilisation areas shall be visually monitored for suitable strike/cover to ensure compliance with the site ESCP requirements and on-maintenance requirements.
	Subsoil Materials General
	 All exposed subsoil materials during earthwork activities shall be covered with hardstand or topsoil materials to a minimum depth of 150mm and appropriately revegetated in accordance with a Landscape Management Plan (or similar).
	 All excavated subsoil materials used for site fill shall be adequately compacted to an appropriate Geotechnical Specification – with a minimum 95% compaction requirement in accordance with AS3798 and subsequently verified to project-specific geotechnical requirements.
	Trench Excavations
	 All excavated and backfilled materials associated with service excavations shall be adequately compacted to an appropriate Geotechnical Specification – with a minimum 95% compaction requirement in accordance with AS3798 and subsequently verified to project-specific geotechnical requirements.



	Import Materials						
		erials (fill or topsoil) shall be propriately documented by	e verified non-dispersive soil y the supplier.				
	5. In the absence of the above, all import soil materials shall be tested and verified by a suitably qualified and experienced Environmental Consultant. It soil amelioration is required for import materials, an addendum DSMP Report shall be prepared by a suitably qualified and experienced Environmental Consultant.						
Monitoring	Topsoil Materials						
Requirements	undergo testing at the		regetation/rehabilitation sha es, with interpretation an nmental Consultant:				
	Material	Parameter	Validation Testing Frequency				
	Topsoil (A horizon)	Soil pH; Macro-nutrients (N, P, K, Ca, Mg, S)	One (1) composite sample per development phase				
Reporting Requirements	All soil test results shall Authorities upon request		Superintendent and Statutor				
Incident	Topsoil validation test re	sults not meeting the spec	ified criteria.				
Identification	Failure to adhere to the p	prescribed treatment methor	ods as stated above.				
	Evidence of sub-surface	tunnelling/erosion.					
Contingency Procedures	Review of control measu	res in consultation with En	vironmental Consultant.				
Troccaures	The re-application of top Consultant.	osoil ameliorants in consul	tation with the Environmenta				
	The use of modified sand	l blocks/barriers or shroud	s in trench excavations.				



6. DSMP CERTIFICATION

This DSMP assessment has been prepared by Glen Gallagher, Environmental (Soil & Water) Scientist and Certified Professional in Erosion & Sediment Control (CPESC) No. 8346.

Please feel free to contact Gallagher Environmental on 0438 724 929 or glen@genviro.com.au for any queries or if further elaboration is required.

Yours faithfully,

GurGallagher

Glen Gallagher BScApp(Env Sc)(Hons) MEIANZ CPESC

Principal | Gallagher Environmental



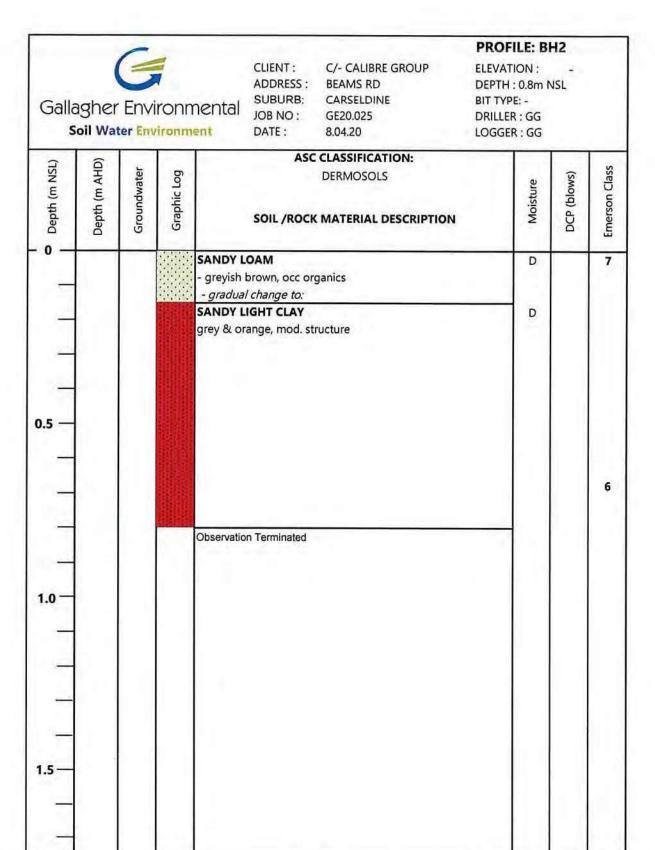
Gallagher Environmental Soil Water Environment

DISPERSIVE SOIL MANAGEMENT PLAN (DSMP) CARSELDINE URBAN VILLAGE

APPENDIX A: BORE LOGS



PROFILE: BH1 CLIENT: C/- CALIBRE GROUP **ELEVATION:** ADDRESS: BEAMS RD DEPTH: 0.8m NSL SUBURB: CARSELDINE BIT TYPE: -Gallagher Environmental JOB NO: GE20.025 DRILLER: GG **Soil Water Environment** DATE: 8.04.20 LOGGER: GG ASC CLASSIFICATION: Depth (m AHD) Depth (m NSL) **Emerson Class** Groundwater **DERMOSOLS** Graphic Log DCP (blows) Moisture SOIL /ROCK MATERIAL DESCRIPTION SANDY LOAM D 7 - greyish brown, occ organics - gradual change to: CLAY LOAM D grey & orange, mod. structure 0.5 5 Observation Terminated 1.0 1.5



PROFILE: BH3 CLIENT: C/- CALIBRE GROUP **ELEVATION:** ADDRESS: BEAMS RD DEPTH: 0.8m NSL SUBURB: CARSELDINE BIT TYPE: -Gallagher Environmental JOB NO: GE20.025 DRILLER: GG Soil Water Environment DATE: 8.04.20 LOGGER: GG ASC CLASSIFICATION: Depth (m NSL) Depth (m AHD) **Emerson Class** Groundwater Graphic Log **DERMOSOLS** DCP (blows) Moisture SOIL /ROCK MATERIAL DESCRIPTION LOAM 7 D - greyish brown, occ organics - gradual change to: **CLAY LOAM** D grey & orange, mod. structure 0.5 5 Observation Terminated 1.0 1.5



Gallagher Environmental

CLIENT:

C/- CALIBRE GROUP BEAMS RD

ADDRESS: SUBURB: JOB NO:

CARSELDINE GE20.025 8.04.20

PROFILE: BH4

ELEVATION: DEPTH: 0.7m NSL

BIT TYPE: -

DRILLER: GG LOGGER : GG

0 0			ASC CLASSIFICATION:			
Depth (m NSL)	Groundwater	Graphic Log	DERMOSOLS SOIL /ROCK MATERIAL DESCRIPTION	Moisture	DCP (blows)	Emerson Class
1.0			- greyish brown, occ organics - gradual change to: CLAY LOAM grey & red/orange, mod. structure Observation Terminated	D		5



Gallagher Environmental

Soil Water Environment

PROFI

CLIENT: C/- CALIBRE GROUP ADDRESS: BEAMS RD

SUBURB: CARSELDINE JOB NO: GE20.025

DATE: 8.04.20

PROFILE: BH5

BIT TYPE: -DRILLER : GG

DRILLER : GG LOGGER : GG

Depth (m NSL)	Depth (m AHD)	Groundwater	Graphic Log	ASC CLASSIFICATION: DERMOSOLS SOIL /ROCK MATERIAL DESCRIPTION	Moisture	DCP (blows)	Emerson Class
0.5				SANDY CLAY LOAM - greyish brown, occ organics - gradual change to: CLAY LOAM SANDY grey & red/orange, mod. structure	D D		7
-				Observation Terminated			
1.0							
-							
1.5							
_							

APPENDIX B: LABORATORY RESULTS





CLIENT:

C/- CALIBRE GROUP

ADDRESS:

BEAMS RD CARSELDINE

JOB NO : TEST DATE: GE20.025 10.04.20

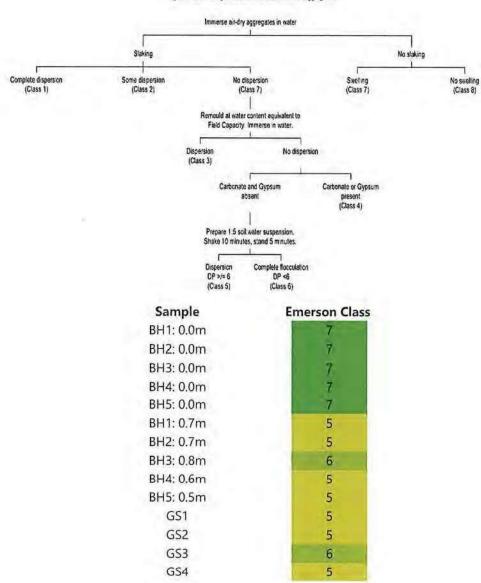
WATER:

DISTILLED

Emerson Class Test Certificate

(Method: AS1289 3.8.1)

Figure 1. Determining the Emerson Class Number of Aggregates





Gun Gallagher CPESC No. 8346



ADDRESS:

CLIENT: C/- CALIBRE GROUP

JOB NO:

BEAMS RD CARSELDINE GE20.025

TEST DATE: WATER:

10.04.20 DISTILLED

pH & Electrical Conductivity (EC) **Test Certificate**

(Soil Chemical Methods - Rayment & Lyons, 2010)

Sample	pH _{1:5}	EC _{1:5} (dS/m)	Texture Factor	Estimated Ece
BH1: 0.0m	5.6	0.02	14	0.3
BH2: 0.0m	5.5	0.03	14	0,4
BH3: 0.0m	5.4	0.02	14	0,3
BH4: 0.0m	5.6	0.04	14	0.5
BH5: 0.0m	5.9	0.05	14	0.7
BH1: 0.7m	5.7	0.05	9	0.5
BH2: 0.7m	5.9	0.06	8	0.5
BH3: 0.8m	5.7	0.03	9	0.3
BH4: 0.6m	5.7	0.03	9	0.3
BH5: 0.5m	5.8	0.04	9	0.4
GS1	5.5	0.05	9	0.5
GS2	5,6	0.02	8	0,2
GS3	5.9	0.04	9	0.4
GS4	5.6	0.03	9	6.0





CERTIFICATE OF ANALYSIS

Work Order : EB2009892

Client GALLAGHER ENVIRONMENTAL Laboratory Environmental Division Brisbane : MR GLEN GALLAGHER Contact Contact : Customer Services EB Address : 59 CREMORNE ROAD KEDRON

BRISBANE QUEENSLAND 4031 Telephone

Project : 20/025 CARSELDINE VILLAGE

Order number C-O-C number

Sampler GLEN GALLAGHER

Site Quote number EN/333 No. of samples received No. of samples analysed

Page : 1 of 3

2 Byth Street Stafford QLD Australia 4053 Address

Telephone : +61-7-3243 7222 Date Samples Received : 08-Apr-2020 15:40

Date Analysis Commenced : 14-Apr-2020 Issue Date : 20-Apr-2020 08:56





This report supersedes any previous report(s) with this reference. Results apply to the sample(s) as submitted. This document shall not be reproduced, except in full.

This Certificate of Analysis contains the following information:

General Comments
 Analytical Results

Additional information pertinent to this report will be found in the following separate attachments: Quality Control Report, QAQC Compliance Assessment to assist with Quality Review and Sample Receipt Notification.

Signatories
This document has been electronically signed by the authorized signatories below. Electronic signing is carried out in compliance with procedures specified in 21 CFR Part 11.

Signatories Position Accreditation Category

Brisbane Acid Sulphate Soils, Stafford, QLD Brisbane Acid Sulphate Coils, Ctafford, QLD Kim McCabe Senior Inorganic Chemist Satishkumar Trivedi Senior Acid Sulfate Seil Chemist

Page Work Order 2 of 3 EB2009892

GALLAGHER ENVIRONMENTAL 20/025 CARSELDINE VILLAGE Client Project



General Comments

The analytical procedures used by ALS have been developed from established internationally recognised procedures such as those published by the USEPA, APHA, AS and NEPM. In house developed procedures are fully validated and are often at the client request.

Where moisture determination has been performed, results are reported on a dry weight basis.

Where a reported less than (<) result is higher than the LOR, this may be due to primary sample extract/digestate dilution and/or insufficient sample for analysis.

Where the LOR of a reported result differs from standard LOR, this may be due to high moisture content, insufficient sample (reduced weight employed) or matrix interference.

When sampling time information is not provided by the client, sampling dates are shown without a time component. In these instances, the time component has been assumed by the laboratory for processing

Where a result is required to meet compliance limits the associated uncertainty must be considered. Refer to the ALS Contact for details.

Key: CAS Number = CAS registry number from database maintained by Chemical Abstracts Services. The Chemical Abstracts Service is a division of the American Chemical Society. LOR = Limit of reporting

- ^ = This result is computed from individual analyte detections at or above the level of reporting
- e = ALS is not NATA accredited for these tests.
 -- = Indicates an estimated value.
- ALS is not NATA accredited for the analysis of Exchangeable Aluminium and Exchange Acidity in soils when performed under ALS Method ED005.
- ALS is not NATA accredited for the analysis of Exchangeable Cations on Alkaline Soils when performed under ALS Method ED006.
- ED007 (Exchangeable Cations by ICP-AES): Unable to calculate Magnesium/Potassium Ratio for some samples as required Exchangeable Magnesium and/or Potassium results are less than the limit of reporting.
- ED007 and ED008: When Exchangeable AI is reported from these methods, it should be noted that Rayment & Lyons (2011) suggests Exchange Acidity by 1M KCI Method 15G1 (ED005) is a more suitable method for the determination of exchange acidity (II+ + Al3+).

Page Work Order Client Project

: 3 of 3 : EB2009892 : GALLAGHER ENVIRONMENTAL : 20/025 CARSELDINE VILLAGE



Analytical Results

Sub-Matrix: SOIL (Matrix: SOIL)		Cli	ent sample ID	BH2 0.0m	BH3 0.8m	-	4114	-
Client sampling date / ti			ing date / time	08-Apr-2020 00:00	08-Apr-2020 00:00		(3000)	-
Compound	CAS Number	LOR	Unit	EB2009892-001	EB2009892-002			-
Control of the Contro	2000 25 200 00 25			Result	Result		-	_
EA002: pH 1:5 (Soils)								
pH Value		0.1	pH Unit	5.4	5.7	-		
EA010: Conductivity (1:5)				The second second				
Electrical Conductivity @ 25°C		1	µS/cm	30	22			-
ED005: Exchange Acidity					LIVER LEADING TO SERVICE AND ADDRESS OF THE PARTY OF THE			
ø Exchange Acidity		0.1	meq/100g	0.4	1.0	_	-	-
e Exchangeable Aluminium		0.1	meq/100g	0.3	0.7	California Control	-	-
ED007: Exchangeable Cations								
Exchangeable Calcium	-	0.1	meq/100g	2.0	<0.1	-	****	-
Exchangeable Magnesium		0.1	meq/100g	1.5	2.1	- (444)	_	-
Exchangeable Potassium		0.1	meq/100g	0.2	<0.1	-		-
Exchangeable Sodium		0.1	meq/100g	0.2	0.3		-	-
Cation Exchange Capacity		0.1	meq/100g	4.4	7.6	-	-	-
Exchangeable Sodium Percent		0.1	76	4.9	4.3	E erte \		-
Calcium/Magnesium Ratio		0.1	(4)	1.3	<0.1			- 144
Magnesium/Potassium Ratio		0.1	(4)	6.6			-	



APPENDIX G GEO-TECHNICAL



EOTECHNICAL INVESTIGATION REPORT

ECONOMIC DEVELOPMENT QUEENSLAND

CARSELDINE URBAN VILLAGE, BEAMS ROAD, CARSELDINE – PHASE 2 SGS/17/E184B 29 MAY 2018





DOCUMENT CONTROL SHEET

SGS Australia Pty Ltd	Project No.	SGS/17/E184
ABN 44 000 964 278	Document No:	SGS.17.E184B.GI.R01
	Document Control Ref.	PF-AU-INDENG-AS-05 / Ver 1 / 01.03.18
	Title:	Geotechnical Report – Due Diligence
	Project Manager:	Robert Maxwell
Lawnton Office:	Author:	Christopher Kosiek
	Client:	Economic Development Queensland
PO Box 370 LAWNTON QLD 4501	Client Contact:	C/o: Calibre Consulting
Telephone: (07) 3481 9444 Email: au.ind.admin@sgs.com	Synopsis:	Phase 2 geotechnical investigation for proposed Urban Village off Beams Road, Carseldine.

REVISION AND CHECKING HISTORY

Revision Number	Date	Checked by	Issued by
0	29/05/2018	R Maxwell	C Kosiek

DISTRIBUTION

Destination	Revision				
	Original	-	-	-	
Client	pdf				
SGS File	1				
SGS Database	1				

LIMITATIONS

This report has been prepared for the sole use of the client and the client's immediate representatives and agents. It is fundamental in the application of this report that the report, including appendices, is read in its entirety and fully understood. Please contact SGS Australia Pty Ltd (Lawnton Office) for additional explanation if any of the report content is not fully understood.

This report is not a guarantee that the site ground conditions will behave in accordance with the interpretation set out herein, but rather our opinion as to the correct interpretations based on the results of site investigations, in situ testing and/or laboratory testing in accordance with generally accepted consulting practice. To the best of our knowledge, information contained in this report is accurate at the date of issue. The interpretation of scientific data, however, often involves both professional and subjective judgments. As such, interpretation is open to error. In addition, site conditions are subject to change in a limited time and there remains a risk that the site ground conditions will differ from these interpretations.

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SUMMARY

The following section provides a summary of the Phase 2 geotechnical investigation carried out for the proposed Urban Village development at 152-158 Beams Road, Carseldine. This summary must be read in conjunction with the report and appendices.

1.	Typical Soil Profiles	-	Topsoil varying in depth to 100mm overlying surface silty sands
		-	Overlying silty and sandy clays of stiff to hard consistency and medium dense to dense clayey sands.
		-	Uncontrolled fill associated with playing fields, tennis/basketball courts and fill bund adjacent to the central road.
2.	Rock	-	A deeply weathered sandstone profile associated with the Petrie Formation may be encountered during earthworks.
2.	Groundwater	-	No groundwater was encountered during the Phase 2 investigation
		-	Groundwater seepage was encountered in the Phase 1 investigation and may develop in the more permeable layers after rainfall or adjacent other sources of water ingress.
		-	Seepage may develop elsewhere, forming perched water in the more permeable layers or adjacent to other sources of moisture ingress.
4.	Reactivity	_	Natural profile Y₅ range 20mm to 50mm
			(Moderate to highly (M to H1) reactivity)
		-	Surface movements may increase by up to 60% post earthworks
5.	CBR values	-	CBR values ranged from 3.0% to 9%
6.	Site Issues/Problems	-	Numerous trees across site potentially creating abnormal moisture conditions and 'P' site classifications.
		-	Presence of uncontrolled fill in the vicinity of playing fields, tennis/basketball courts, mounds, roadway and ancillary structures/shelters observed at the time of the investigation.
		-	Near surface silty sands susceptible to moisture and loss of strength.

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LIS	ST OF APPENDICES					
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All appendices should be carefully read in conjunction with this report

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1 INTRODUCTION

This report presents the results and interpretations of the Phase 2 geotechnical investigation carried out by SGS Australia for the proposed Urban Village development off Beams Road, Carseldine.

The investigation was commissioned by Dan Collins of Calibre Consulting acting on behalf of Economic Development Queensland and was carried out in general accordance with the SGS proposal (SGS/17P/E184-Phase 2) dated 8 May 2018.

It is understood that the proposed project will comprise a multi-staged development including road construction, sporting fields, recreation areas, bioretention basins and future 3-5 storey commercial and residential buildings.

SGS Australia has previously undertaken the Phase 1 geotechnical investigation focusing on the proposed bioretention basins and sporting complex / recreation areas of the proposed development.

The aim of the Phase 2 investigation was to assess the remaining areas of the development with particular focus on proposed roadways and commercial/residential building areas. The Phase 2 geotechnical report is intended to provide supplementary information and should be read in conjunction with the Phase 1 report.

The scope in terms of number and position of boreholes was nominated by Calibre Consulting in correspondence dated 8 May 2018.

The investigation and interpretation of results was carried out in general accordance with the following reference materials:

- AS 1726 "Geotechnical Site Investigations"
- AS 1289 "Testing of Soils for Engineering Purposes"
- AS 2870 "Residential Slabs and Footings"
- AS 2159 "Piling Design and Installation"
- AS 3798 "Guidelines on earthworks for commercial and residential developments"

Relevant definitions and detailed site investigation procedures are provided in Appendix A.

2 INVESTIGATION PROCEDURE

The investigation was carried out on 14 May 2018 and comprised the following stages:

- a) Site investigation in accordance with AS 1726 "Geotechnical Site Investigations"
 - * Drilling of nine (9) boreholes to various target depths of 6.0m (borehole locations are shown on the site sketch in Appendix B).
 - * Soil classification by qualified and experienced technician.
 - * Sampling of representative soils for laboratory analysis.
 - * Dynamic cone penetrometer (DCP) testing adjacent each borehole in order to assess the relative density and strength consistency of the subsurface soils.
 - * Pocket penetrometer (PP) in undisturbed samples to estimate the undrained shear strength (Cu).
 - * Site and landform mapping by a suitably qualified Geotechnical Engineer.
- b) Laboratory testing in accordance with AS 1289 "Testing of Soils for Engineering Purposes" (where applicable)
 - * Shrink/swell index to allow ground surface movement predictions.
 - * Moisture/density relationship (standard compaction) and 4-day soaked CBR for preliminary pavement design.



INVESTIGATION RESULTS

3.1 SITE DESCRIPTION

The site is located within the former QUT Carseldine Campus, off Beams Road, Carseldine. The northern boundary of the site is bound by Beams Road, the western boundary by Dorville Road, the southern boundary by Cabbage Tree Creek and the eastern boundary by the Petrie Rail line.

Several existing multi storey buildings and car parks are located in the north western portion of the site and are currently occupied by the Queensland Department of Transport and Main Roads, with adjacent sporting grounds located in the lower eastern half of the site, open for public use.

The site topography typically falls from the north west at the corner of Beams and Dorville Roads towards the south east and generally levelling to the eastern sporting grounds. Bushland generally occupies the area along southern boundary and adjacent to Cabbage Tree Creek.

The site of the proposed urban village development shall be situated within the lower south eastern portion of the property in the location of the sporting grounds, as shown in Figure 1 below.



Figure 1 **Location Plan**

The majority of the site investigated during Phase 2 was occupied by two (2) playing grassed fields and a section of land occupied by a stormwater basin and internal roadways.

Surface drainage conditions across the site were reasonable with runoff controlled by a system of above and below ground stormwater drains. The stormwater basin adjacent the Beams Road entrance was bound by block retaining walls.

A large bund was observed adjacent to the western side of the sporting field (highlighted in orange above). The bund is approximately 2m in height and is assumed to be uncontrolled fill.

Tennis/netball/basketball courts with sealed surfaces were observed on the site. It is likely the courts were constructed by cut to fill earthworks and it is assumed all associated fill is uncontrolled.

Site photographs are provided in Appendix C of this report.

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3.2 REGIONAL GEOLOGY

The regional geology as described by the Department of Mines 1:100,000 Geological Series Map for Brisbane (Sheet 9543) is as follows:

Site Geological Areas:	Upper North Western Area (Cnr Beams/Dorville Rd)	Lower Eastern Area (Sporting Fields)
Geological Unit / Rock Name:	Tp – Petrie Formation	Qpa – Alluvial Plains
Age:	Tertiary Period	Quaternary (Pleistocene) Period
Lithology:	Mudstone, shale, sandstone, oilshale, minor pebble and cobble conglomerate	Sand, silt, clay, gravel.
Additional Features:	Ferrunginised mottled and kaolinized rocks; Deep weathering profile.	

3.3 SUBSURFACE PROFILE

The natural soil profiles encountered in the boreholes were generally consistent with the regional geology and typically comprised high plasticity, stiff (or stronger) silty clays overlying sandy clays and clayey sands to the borehole termination depth.

Placed topsoil (fill) was noted in the boreholes and deeper fill was encountered in boreholes BH02-B, BH06-B, and BH07-B. In the absence of any compaction control documentation, the fill is assumed to be uncontrolled. There is a high probability that additional uncontrolled fill will be present across the site associated with the sporting fields, mounds, roadway and ancillary structures observed at the time of the investigation.

Detailed soil profiles are provided in the Engineering Borehole Logs in Appendix C and a summary of the borehole data is provided in the following table.

Table 1 Summary of Soil Profiles

			Natural Ground								
B/hole No.	Topsoil (mm)	Fill (m)	Silty	CLAY	Clayey SAND						
		()	Stiff	Very Stiff	Medium Dense	Dense					
BH01-B	90	0.0 - 0.1	0.1 – 0.7	0.7 – 1.7		1.7 – 6.0					
BH02-B	90	0.0 – 1.8	1.8 – 3.1		3.1 – 6.0						
BH03-B	90	0.0 – 0.1		0.3 – 2.9	0.1 – 0.3 2.9 – 6.0						
BH04-B	100		0.1 – 1.6	1.6 – 2.2		2.2 - 6.0					
BH05-B	100		0.1 – 1.1			1.1 – 6.0					
BH06-B	90	0.0 - 0.5		0.5 - 2.7		2.7 - 6.0					
BH07-B	100	0.0 - 0.3	0.3 - 0.5	0.5 - 6.0							
BH08-B	85	0.0 - 0.1	0.1 – 0.5	0.5 - 6.0							
ВН09-В	90		1.1 – 4.1	0.3 – 1.1 4.1 – 6.0	0.1 – 0.3						

3.4 **GROUNDWATER**

Groundwater was not encountered in the boreholes at the time of the investigation however, seepage may develop forming perched water in the more permeable layers during/following extended wet weather periods or adjacent to other sources of moisture ingress (e.g. leaking services or irrigation systems).

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3.5 LABORATORY TEST RESULTS

Laboratory testing was carried out on selected samples taken from the site. Test reports are provided in Appendix D and results are summarised in the following table.

Table 2 Summary of Laboratory Geotechnical Test Results

P/holo No	Donth (m)		e/Density ip (Standard)	Soaked CBR	Shrink-Swell			
B/hole No.	Depth (m)	MDD OMC (t/m³) (%)		CBR (%)	Index			
BH01-B	0.2 - 1.0	1.75	17.6	7				
BH05-B	0.2 - 0.8	1.80	15.8	9				
BH09-B	0.3 - 1.0	1.69	19.2	3.0				
BH01-B	0.3				1.3			
BH05-B	0.5				0.9			
BH08-B	0.5				3.8			

Moisture/Density Relationship: MDD - Maximum Dry Density, OMC - Optimum Moisture Content

4 ENGINEERING CONSIDERATIONS

4.1 REACTIVITY AND INDICATIVE SITE CLASSIFICATION

The predicted surface movement (Ys) that could occur on this site has been assessed in accordance with the methodology provided in AS 2870 "Residential Slabs and Footings".

It is understood that ultimately, standard residential buildings as described in AS 2870 will be constructed on the site, post subdivision development. It is therefore assessed that AS 2870 methodology and derived parameters would apply to this site for the purpose of providing preliminary reactivity and indicative site classification details.

Reactivity testing was undertaken on three samples taken at various depths across the site. Shrink-Swell Index Values (Iss) ranged from 0.9 to 3.8. Based on limited testing, it appears that the dark grey coloured silty clays exhibited a higher shrink/swell index value.

Considering a natural (pre earthworks) 1.8m soil moisture change profile, the following would apply.

	Existing Profile	
	Mean Iss (mm)	Maximum Iss (mm)
Predicted Surface Movement	20 -30	45 - 55
Equivalent Reactivity	Moderate	High (H1)

Consideration must be given to the effect that cut to fill earthwork operations will have on the soil profiles. The following table provides surface movement predictions considering a full 1.8m controlled filled profile at various shrink/swell index values.

	1.8m Controlled Fill Profile									
	<u>lss= 1.0</u>	<u>lss= 2.0</u>	<u>Iss= 3.8</u>							
Predicted Surface Movement	20 – 30	40 — 50	70 – 80							
Equivalent Reactivity	Moderate	High (H1)	Extreme							

Based on the observed soil profiles at the borehole locations it would be expected that the majority of the sites would fall within the moderate to high classification range.

The above reactivity parameters not consider the potential effects of trees (if applicable) and site outcomes post earthworks (refer to Section 4.2).



4.2 EFFECTS OF VEGETATION

Trees can affect building foundation performance in reactive clay soils by removing soil moisture, which induces volume change (shrinkage) in the soil.

The effect of trees on a site classification (and subsequent footing design and performance) is assessed based on:

- the site soil reactivity;
- the distance between trees and the closest point to the dwelling; and
- the mature height of the trees.

The potential mature height of a particular tree species can vary with the condition of the tree, climate, soil types, drainage and other site-specific variables.

As part of the development civil design process careful consideration shall be given to the location and selection of any retained vegetation. Vegetation left in close proximity to proposed (or possible) building envelope locations may result in P site classifications at individual building application stage.

Any tree removal prior to building construction must also consider potential surface heave (rebound) associated with the re-establishment of soil moisture equilibrium conditions. This removal of trees will be pertinent across large portions of this development due to the presence of dense vegetation where it is expected that some thinning or complete removal will be required. Site classifiers and footing design engineers should consider the effects of this tree removal when assessing the individual allotments.

4.3 FOUNDATIONS

The type and depth of foundation system for the proposed structures will be dependent on the magnitude of structural loading, tolerance of the structures to movement (from both load induced settlement and shrink-swell movement) and the subsurface geotechnical conditions. The following table provides preliminary geotechnical strength parameters for both shallow (strip) and piled foundation alternatives.

Table 3 Preliminary Bearing Capacity Parameters

Matarial		Pad Fo	ootings	Strip Fo	ootings	Piled Fou	ındations
Material	Cu	qu	q _a	qu	q a	f _b	f _s
Uncontrolled Fill	1	NR	NR	NR	NR	NR	NC
Controlled Fill ⁽¹⁾	75	450	150	375	125	600	30
NATURAL Silty SAND / SILT(2)	-	NR	NR	NR	NR	NR	NC
NATURAL Stiff Silty/Sandy CLAY and Medium Dense Clayey SAND	50	300	100	250	80	400	20
NATURAL Very Stiff (or stronger) Silty/Sandy CLAY and Dense Clayey SAND	100	600	200	510	170	800	40

- (1) Based on the fill complying completely with the requirements in AS3798 and being placed under Level 1 conditions to 98% SDDR.
- (2) Silty Sand and Silt is not considered suitable founding material as it is subject to loss of strength when disturbed and/or moisture affected.

where:

Cu = Estimated undrained shear strength (kPa)

 $q_u = Ultimate base bearing pressure - high level strip footings (kPa)$

q_a = Allowable base bearing pressure (FOS = 3) – high level pad/strip footing (kPa)

f_b = Ultimate base bearing pressure – piles minimum 1.5m and 2.5 pile diameters deep (kPa)

 f_s = Ultimate shaft adhesion/friction (adhesion factor (α) = 0.4) (kPa)

NR = Not recommended for founding

NC = Not considered in shaft adhesion / friction



4.4 PAVEMENTS

The California Bearing Ratio (CBR) value represents the "strength" of the material when nominally compacted to 100% Standard Dry Density Ratio (SDDR) at the Optimum Moisture Content (OMC) and soaked for four (4) days. It should be noted that the CBR value is simply an index of strength at that particular density and moisture condition. The same material at a different density and moisture condition is likely to yield a lower or higher CBR value depending on the density and moisture circumstances existing at the time of testing. The modulus of subgrade reaction is derived from the CBR value based on published correlations.

Laboratory testing was carried out on representative material types sampled across the site. The CBR results ranged from 3.0 to 9. Due to the variability of results across the site, it is recommended the following assumed worst-case CBR value be used in preliminary pavement design.

Table 4 CBR and Modulus of Reactivity

Material Type	Soaked CBR Value (%)	Modulus of Subgrade Reaction k (kPa/mm)
(CH) Silty CLAY	3.0	27

Further soaked CBR testing will be required when bulk earthworks have been completed and the subgrade material has been exposed to determine final soil type boundaries representing the CBR values.

NOTES:

- Use of the above values (in preliminary design) assumes that the subgrade will be compacted uniformly to a minimum SDDR of 100% and that the pavement will be well drained during construction and in-service.
- The attached "CBR Standard Notes and Performance Warnings" (Appendix F) must be considered and implemented during the design and construction phases as appropriate.

4.5 EARTHWORKS

Reference should be made to the Phase 1 geotechnical report for earthworks procedures and recommendations. The following sections of this report should be read in conjunction with the previously issued report.

4.5.1 TOPSOIL DEPTHS

Topsoil depths within the boreholes ranged from 85mm to 100mm across the site. A nominal topsoil stripping depth of 90mm is considered applicable. It is expected deeper topsoil depths may be encountered in the gullies and low-lying areas.

4.5.2 UNSUITABLE MATERIAL

Uncontrolled fill was identified in the large bund, on the tennis/netball/basketball court platforms and in areas on the playing fields. Additional uncontrolled fill may be present on the site. Consequently, It is strongly recommended to have the Geotechnical Inspection and Testing Authority (GITA) onsite at the time of topsoil stripping to identify any uncontrolled fill and instruct on any necessary ground preparation works.

Furthermore, soft, moisture effected material and uncontrolled fill may be encountered in the existing stormwater basin adjacent to the existing Beams Road entrance. This area will require treatment (removal of unsuitable material and/or moisture conditioning) prior to filling.

All uncontrolled fill and temporary unsuitable material should be removed to a sound natural base and stockpiled to assess suitability for reuse as structural fill.



4.5.3 EXCAVATION CHARACTERISTICS

The soil encountered in the borehole should be readily excavated by small to medium sized plant.

No groundwater was encountered within the boreholes for Phase 2 however, the development of seepage may be possible in the more permeable layers as identified in the Phase 1 investigation. Allowance should be made for dewatering of excavations if applicable.

5 COMMENTS AND LIMITATIONS

The development and any associated infrastructure should be designed to accommodate for the ground conditions reported and which otherwise may be encountered during construction.

The geotechnical parameters given in this report should be considered as preliminary only and subject to confirming inspections, and potentially additional testing by an experienced geotechnical professional at the construction stage. SGS offer inspection services and it is recommended that the client and their agents and contractors avail themselves of these services.

The interpretation of geotechnical reports and the preferred or proposed engineering outcomes are often compromised by the non-continuity of geotechnical consultants on a project. In addition, there is an inherent potential for a conflict of interest and therefore increased potential for inappropriate administration of the geotechnical specification when the GITA is commissioned by the contractor.

For these reasons, it is strongly recommended that:

- SGS be commissioned as the Geotechnical Engineering Consultant and the GITA for all geotechnical related activities associated with this project; and
- 2. The Geotechnical Engineering Consultant and the GITA are commission independently of the contractor.

SGS cannot accept any responsibility for any interpretations and/or application of the contents of this report by any other Geotechnical Engineering Consultant or GITA.

SGS AUSTRALIA PTY LTD

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SGS.17.E184B- Phase 2 Report.docx

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APPENDIX A: NOTES RELATING TO THIS REPORT

GEOTECHNICAL INVESTIGATIONS





INTRODUCTION

The following notes are intended to complement the report and assist the reader in interpreting the report in regard to investigation procedures, definitions, terminology and limitations. Not all notes are necessarily relevant to this report.

The ground exhibits a variety of properties and characteristics which vary from place to place and can also change with time, weather patterns, changes in vegetation and human interaction. A geotechnical investigation puts into practice accepted methods and procedures to gather data relevant to the site and the proposed development. This report may contain such data obtained from drilling, excavation, inspection, sampling and testing. If so, the data are directly relevant to the ground at the place and time of the actual test sites. The client should be aware that in some cases soil conditions can change dramatically over short distances therefore conditions other than those represented in this report may occur on the site.

SITE INVESTIGATION PROCEDURES

a) Subsurface Investigations

Borehole/test locations are generally located to gain maximum coverage over the site giving consideration to contrasting topography. However, on occasions existing structures or other access restrictions do not permit ideal borehole locations.

Subsurface investigations may be carried out using one or more of the following methods:

- Test Pits: Test pits can be excavated by power equipment (backhoe, excavator etc) or in some cases by hand. Hand excavated test pits are usually limited to a maximum depth of about 1m.
- Hand Auger: Hand auger equipment is normally only used where drill rig access is unavailable. Hand auger refusal may occur on materials which could have otherwise been drilled if drill rig access was available.
- Drill Rig: Spiral Flight Auger: Spiral flight auger drilling is more economical and is usually adopted if ground conditions are suitable. Samples are returned to the surface by the flights or may otherwise be taken from the base of the borehole. Various drill bits may be attached to the auger during drilling. The depth of refusal of the different bit types can provide a useful indication of the strength of the material.
- Drill Rig Wash Drilling: Wash drilling is normally used below the water table when collapsing soils are encountered. Steel casing is pushed to support the collapsing soil and water is pumped through the drill rods to advance the borehole. The rods are withdrawn to allow sampling and testing at the base of the borehole.

b) Insitu Testing

- Dynamic Cone Penetrometer: The Dynamic Cone Penetrometer (DCP) test is carried out using a cone of 20mm diameter with a 30° tapered tip attached to steel rods of smaller diameter. The cone is driven by a 9kg hammer falling 510mm and results are recorded in blows per 100mm penetration. DCP test results can be used to estimate bearing capacity and insitu California Bearing Ratio. The test procedure is described in Australian Standard AS1289 6.3.2.
- Standard Penetration Test: The Standard Penetration Test (SPT) is carried out using a standard split steel tube sampler driven by a 63.5kg mass falling 760mm. Results are recorded in number of blows per 150mm penetration for a maximum depth of 450mm. The SPT "N" value is the sum of the blows for the 2nd and 3rd 150mm increments. The first 150mm is referred to as the seating penetration. In cases where the number of blows per 150mm exceeds 20, the result is recorded as 20/penetration (mm) and the 'N' value determined by linear interpolation. The SPT N value can be used to estimate allowable bearing pressure for foundations. The test procedure is detailed in Australian Standard AS1289 6.3.1.
- Pocket Penetrometer: The Pocket Penetrometer (PP) is used on undisturbed samples as a relatively simple and economical method of estimating the unconfined compressive strength of clay soils. The cohesive (undrained) shear strength (Cu) is generally taken as 0.5 of the PP value.

c) Sampling

The type and frequency of sampling and testing on a site is dependent on several issues including:

- number and depth of boreholes
- variability of soil types and conditions
- * type and magnitude of the development
- Undisturbed Samples: Undisturbed samples are taken by pushing a thin walled steel tube, 50mm diameter (U50) into cohesive soils. U50 samples are necessary for laboratory testing such as shrink-swell index, consolidation, shear strength etc.
- Disturbed Samples: Disturbed samples (D) are taken from drill augers, hand auger or open test pits. Disturbed samples are generally used for laboratory testing such as Atterberg Limits, Moisture Content, California Bearing Ratio, Particle Size Distribution etc.

d) Site Description

Underground Services: If underground services (sewer, stormwater etc) were observed during the site investigation, a record of the observation will usually be made on the site description notes included in this report. It should be noted however that our commission <u>does not</u> typically extend to locating underground services.

GEOTECHNICAL INVESTIGATIONS





As underground services can potentially affect a structure in the vicinity, it is important that any underground services are located and considered in the development of the site.

 Site Sketch: The site sketch is intended only as a general pictorial of relative locations of boreholes and site features. Any dimensions, slope directions, magnitudes, feature orientation, north point, etc are approximate and should be used as a guide only.

e) Soil and Rock Descriptions

Soil and rock descriptions contained in this report are in general accordance with Appendix A2 and A3 of AS1726 'Geotechnical Site Investigations". Details of the soil profiles provided in the Engineering Borehole Logs are based on visual descriptions of the soils and rock on site. Some soil descriptions may differ marginally from the format as described in AS1726, but this will in no way affect the results of this investigation.

- Controlled Fill: Controlled fill as described in this report refers to:
- (1) sand fill up to 0.8m deep and non-sand fill up to 0.4m deep which has been placed in layers not more than 150mm thick and compacted with mechanical compaction equipment.

or

(2) fill which has been supervised and tested and for which a statement has been provided certifying compliance with Table 5.1 of AS3798 "Guidelines on Earthworks for Residential and Commercial Developments". The statement of compliance can only be provided by the Geotechnical Testing Authority under a Level 1 commission as defined in Appendix B of AS3798

and

- (3) subject to the results of this investigation verifying the quality of the fill.
- Uncontrolled Fill:Uncontrolled fill is described as any fill
 not meeting the requirements of
 controlled fill as defined above.

SITE CLASSIFICATION

Site Classification as defined in AS2870 "Residential Slabs and Footings" is divided into various classes depending on the y_s (predicted surface movement) and other relevant ground conditions.

The classes are:

(

<u>CLASS</u>	<u>SOIL TYPE</u>	<u>ys (mm)</u>
Α	stable (sand or rock)	
S	slightly reactive clay	$0 < y_s \le 20$
M	moderately reactive clay	$20 < y_s \le 40$
H1	highly reactive clay	40 < y _s ≤ 60
H2	(very) highly reactive clay	$60 < y_s \le 75$
Ε	extremely reactive clay	y _s > 75
Р	problem	-

Problem Site: Problem sites include those which are filled, have soft and/or collapsing soils, have soils subject to erosion, subject to abnormal moisture conditions, have bearing pressure < 100kPa and any other sites which do not otherwise comply with class A, S, M, H or E requirements.

• Effect of Trees: Trees can have a significant drying effect resulting in abnormal moisture conditions of the soils in the vicinity of the tree(s). On reactive clay sites, this can have the effect of dramatically increasing the predicted surface movement (y_s) within the zone of influence of the tree(s). Past, present and future trees all potentially affect the site classification and subsequent footing and slab design. When it is known that large trees have been removed from a site, the site classifier or footing design engineer should be advised of the size, location and date of removal, so that appropriate consideration can be given to the footing design.

As recommended, and in accordance with AS2870, our preferred option for determination of Instability Index is by a combination of the shrink-swell index and identification of the soil profile. In some cases where shrink-swell index testing is not practicable, soil classification testing (Atterberg Limits and Particle Size Distribution) may have been used.

Values used in determination of the ys value were:

* soil profiles - refer borehole logs * shrinkage index - refer laboratory results

* extreme suction change - 1.2pF * depth of suction change - 1.5 to 2.3

* cracked zone - 0.5Hs (zero for reactive clay on controlled filled sites < 5 years old)

* α cracked zone - 1.0 * α uncracked zone - 2.0 - $\frac{z}{5}$

where z = depth from ground surface to the centroid of the layer under consideration.

Provision of y_s values and/or site classification is intended for use in residential applications only. Where this information has been provided in non-residential cases it is done so as supplementary information only and may not be suitable for application to AS2870 design principles.

EARTHWORKS

All earthworks should be carried out in strict accordance with the full requirements of Australian Standard AS 3798 "Guidelines on Earthworks for Commercial and Residential Developments". If local authority requirements apply to the earthworks and differ from AS 3798 the more stringent requirements should be adopted. Unless approved, the following materials are generally not suitable for use as structural filling:

- Organic Soils topsoils, severely root affected soils and peat
- Materials which may be contaminated with toxic substances through past site usages.
- Filling which contains wood, metal, plastic, boulders and other deleterious materials.
- Any other materials which have deleterious engineering properties.

GEOTECHNICAL INVESTIGATIONS





Any earthworks carried out after the site investigation will change the findings of the report. Particular care and consideration should be given to the site reactivity and classification which is likely to change with cutting and/or filling of the site.

On cut-and-fill sloping sites the fill shall be controlled and extend a minimum of 1m past the edge of any construction areas. Embankment slopes shall be protected from erosion and be not steeper than two horizontal to one vertical. The suitability of any such embankments shall be verified by an experienced geotechnical engineer prior to construction.

GROUNDWATER

Groundwater levels (where encountered) are provided on the borelog sheets.

Generally, groundwater or seepage tends to travel in the more permeable layers over less permeable materials (ie. along sand/clay interfaces, fill/natural interfaces, etc.) and in joints of rock.

Bulk earthworks (ie. cut/fill or fill operations) should not be carried out during wet periods and should be delayed sufficiently to ensure the moisture content of the materials approximates the optimum moisture content for compaction.

Should footing excavation commence during or following an extended wet period and where the soil profile comprises sandy soils or sandy soils overlying clays, the surface sands will tend to collapse during trench excavations requiring temporary shoring and the construction of a sump area from which groundwater can be pumped. Under no circumstances should softening of foundation soils be allowed to occur.

It is advised that a test pit be excavated to assess ground conditions prior to commencing trench excavations or earthworks if prevailing weather conditions are poor.

SITE MANAGEMENT

The short and long term serviceability of the development is largely dependent upon a responsible approach by the developer, builder and the owner/occupant towards drainage, landscaping and vegetation. The following basic requirements apply to most developments.

* Surface Drainage

Site preparations should include provision for slopes of no less than 1 vertical in 20 horizontal away from structures for a distance of at least 2m where possible. Spoon drains and catch drains should be constructed where necessary to direct surface drainage away from the structure.

* Landscaping

Landscaping should be planned to ensure excessive watering and/or water ponding areas do not occur. Landscaping areas should be considered in the design of site drainage systems.

Vegetation

To reduce (but not eliminate) the possibility of damage to structural elements, trees should be restricted to a distance of no closer than 1.5 times the mature height from the structure.

A more extensive discussion on site management is contained in the CSIRO document "Guides to Home Owners on Foundation Maintenance and Footing Performance" and its recommendations should be followed in full.

THE REPORT

This report was compiled in accordance with the relevant standards, sound geotechnical practices and general market requirements as appropriate.

Unless instructed otherwise, this investigation and report does not address the following issues:

- * Existing and/or proposed mining influence
- * Slope stability
- * Specific site drainage requirements and potential effects
- Contamination and/or hazardous materials on the site
- * Specific effects of post investigative works on the site
- * Existing underground services

The client should understand that whilst our investigation and report has been conducted within appropriate guidelines and with suitable diligence to accurately determine the ground conditions, on occasion, construction (earthworks/excavations) may indicate ground conditions differing from those shown in this report. Should this occur, SGS, should be advised immediately for further advice.

The work undertaken and reported is intended for the sole use of the client named on this report for the specific purpose of determining the parameters necessary for the design and construction of the development outlined. It may not contain sufficient information for other purposes. It is intended that this report will provide advice on geotechnical and related issues only and that SGS <u>will not</u> accept any responsibility for any structural design which does not fully consider and correctly apply the findings of this report.

It is important for the client to understand that long term serviceability of the structure will require all the findings of this report to be considered and undertaken. No responsibility will be accepted where these are not put into effect prior to commencement or in conjunction with construction as required.

Any bearing capacity parameters provided in the report must be considered as preliminary only and should be confirmed by an experienced geotechnical engineer during construction.

INSPECTIONS

SGS provides inspection services for any geotechnical issues in relation to this report. We encourage the client, their designers and contractors, to make use of this service to verify the findings of the report, particularly if there is any doubt regarding the ground conditions being encountered during construction.



APPENDIX B: SITE PLAN - BOREHOLE LOCATIONS



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DRAWN

DATE 14.05.18

CLENT Economic Development QLD

Carseldine Village

Uncontrolled when printed



APPENDIX C: BOREHOLE RECORDS, SAMPLING AND INSITU TEST RESULTS



BOREHOLE LOG

BOREHOLE NO.: BH 01

SHEET: 1 OF 1

AUJNDLawnton@sgs.com

CLIENT: ECONOMIC DEVELOPMEN

ECONOMIC DEVELOPMENT QLDDATE COMMENCED: 14.5.2016

PROJECT: GEOTECHNICAL INVESTIGATION DATE COMPLETED: 14.5.2016
LOCATION: CARSELDINE VILLAGE, BEAMS RD, CARSELDINE LOGGED BY: J.SIPPEL

<u> </u>	ill C-	ntro	ctor	900	VI IC.	TRALIA		Poro Sizor 100mm	gle: -90°			East!-	a: F0	2626.00 Surface R.L. :		4
						i ralia						Eastin				
Di	ill Me	odel:		DTS	05			Drill Fluid: - Bearing:				Northi	ng: 69	74733.00 Datum: 56J		_
Method	Casing	□ DCP	RL (m)	Depth (m)	Geological Unit	Graphic Log	© Classification Symbol	Material Description FILL - Silty SAND, fine grained, dark grey, 90mm to	S liosad	S Condition	Consistency / Strength	Cementation / Weathering	Sample / Test	Field Records / Comments	Water	
		3 4 3 3 2 3 4		- -			CH	NATURAL - Silty CLAY, high plasticity, pale grey morange Silty CLAY, high plasticity, pale grey mottled orang	nottled i	N N	St		U ₅₀	PP=450kPa REC=210mm	- - -	
		5		1 - -											- - - -	
				_ 2 _ _			SC	Clayey SAND, fine to medium grained, yellow, orar	nge I	V	D		D		-	
SA/TC	Open Ho l e			3											-	
				4 5 6				Fad of DU 04 of Car								



LOCATION:

BOREHOLE LOG

BOREHOLE NO.: BH 02

LOGGED BY:

SHEET: 1 OF 1

J.SIPPEL

AUJNDLawnton@sgs.com

CLIENT: ECONOMIC DEVELOPMENT QLD

ECONOMIC DEVELOPMENT QLDDATE COMMENCED: 14.5.2016

PROJECT: GEOTECHNICAL INVESTIGATION DATE COMPLETED: 14.5.2016

CARSELDINE VILLAGE, BEAMS RD, CARSELDINE

_						TRALIA			Hole Angle: -9	no°			CD D1		
						i ralia		Bore Size: 100mm		7 U		Eastin	_		
	rill M	odel:		DTS	U5			Drill Fluid: -	Bearing:	Π	Π	North	i ng: 697	74818.00 Datum : 56J	
Method	Casing	DCP	RL (m)	Depth (m)	Geological Unit	Graphic Log	Classification Symbo l	Material Desc	cription	Moisture Condition	Consistency / Strength	Cementation / Weathering	Sample / Test	Fi el d Records / Comments	Water
		2 3 4 4 4 3 3					SM CH	FILL - Silty SAND, fine to mediu 90mm topsoil FILL - Silty CLAY, high plasticity medium sized gravel	,	M	L St		D		-
		4 6 8 9 8 6 7 7		<u>1</u>			SC	FILL - Clayey SAND, fine to coa with fine to medium sized grave	rse grained, brown, grey,	M	MD		D		-
		6 4 4 4 5 5 6		<u>2</u>			CH	NATURAL - Silty CLAY, high pl red, orange	asticity, dark grey mott l ed	M	VSt		U ₅₀	PP>600kPa REC=150mm	-
SA/TC	Open Hole			3 4			SC	Clayey SAND, fine to coarse gra	ained, orange, grey, yellow	М	MD				-
				5											
				- - - 6				Find of BH 02 at 6m							- - -



LOCATION:

BOREHOLE LOG

BOREHOLE NO.: BH 03

LOGGED BY:

SHEET: 1 OF 1

J.SIPPEL

Engineering and Environmental Consultants Ph 3481 9444 AU.IND.Lawnton@sgs.com

CLIENT: ECONOMIC

ECONOMIC DEVELOPMENT QLD DATE COMMENCED: **14.5.2016**

PROJECT: GEOTECHNICAL INVESTIGATION DATE COMPLETED: 14.5.2016

CARSELDINE VILLAGE, BEAMS RD, CARSELDINE

D	rill Co	ontra	ctor:	SGS	AUS	TRALIA		Bore Size: 100mm	Hole Angle: -9	00°		Eastin	ig: 50	2737.00	Surface R.L.:	
	rill Me	odel:		DTS	05			Drill Fluid: -	Bearing:			North	i ng : 69	74760.00	Datum: 56J	
Method	Casing	DCP	RL (m)	Depth (m)	Geological Unit	Graphic Log	Classification Symbo l	Material Desc	ription	Moisture Condition	Consistency / Strength	Cementation / Weathering	Sample / Test		Field Records / Comments	Water
SAITC	Open Hole	2 3 3 4 4 4 4 4 5 4 4] 1 - 2 3 4 5 6			SM SC CH	FILL - Silty SAND, fine to mediul 90mm topsoil NATURAL - Clayey SAND, fine orange Silty CLAY, high plasticity, pale syellow Sandy CLAY, medium plasticity, to medium grained Clayey SAND, fine to medium grange	to medium grained, grey, grey mottled orange,	M M	VSt VSt					



LOCATION:

BOREHOLE LOG

BOREHOLE NO.: BH 04

LOGGED BY:

SHEET: 1 OF 1

J.SIPPEL

AU.IND.Lawnton@sgs.com

CLIENT: ECONOMIC DEVELOPMENT QLD DATE COMMENCED: 14.5.2016

PROJECT: GEOTECHNICAL INVESTIGATION DATE COMPLETED: 14.5.2016

CARSELDINE VILLAGE, BEAMS RD, CARSELDINE

r	Dril	I Co	ntra	ctor:	SGS	AUS.	TRALIA		Bore Size: 100mm	Hole Angle: -	90°		Eastin	a: 50	02849.00 Surface R.L. :	
			odel:		DTS				Drill Fluid: -	Bearing:			Northi		974798.00 Datum : 56J	
H	Т	I	Juei.		ыз	03			Din Fluid	bearing.	I		NOTH	ng. oa	Datum. 303	
Mothod	00000	Casing		RL (m)	Depth (m)	Geological Unit	Graphic Log	Classification Symbol	Materia l Description		Moisture Condition	Consistency / Strength	Cementation / Weathering	Sample / Test	Field Records / Comments	Water
			1 2 2 3 4 4 5 4 5 6		- - 1			CH CH	NATURAL - Silty SAND, fine to medium (grey, 100mm topsoil Silty CLAY, high plasticity, grey mottled of the silty CLAY, medium plasticity, grey mottled of the silty CLAY, medium plasticity, grey mottled of the silty CLAY, medium plasticity, grey mottled of the silty can be silty of the silty	orange	M	VL St				-
					2			SC	Clayey SAND, fine to medium grained, gorange	grey mott l ed	M	D				- - - -
CE/ VO	2	Open Ho l e			3_											- - - -
					<u>4</u> -											- - - -
					5											- - - - -
					- 6				Ford of PILLON at Con							



PROJECT:

BOREHOLE LOG

BOREHOLE NO.: BH 05

SHEET: 1 OF 1

Engineering and Environmental Consultants Ph 3481 9444 AU.IND.Lawnton@sgs.com

CLIENT: **ECONOMIC DEVELOPMENT QLD** DATE COMMENCED: 14.5.2016

DATE COMPLETED: 14.5.2016

CARSELDINE VILLAGE, BEAMS RD, CARSELDINE LOCATION:

GEOTECHNICAL INVESTIGATION

LOGGED BY: J.SIPPEL

JOB NUMBER: SGS/17/E184B

CHECKED BY: C KOSIEK

Dr	ill Co	ontra	ctor:	SGS	AUS	TRALIA	\	Bore Size: 100mm	Hole Angle:	-90°		Eastir	ng: 50	2880.00 Surface R.L.:		_
Dr	ill Me	odel:		DTS	05			Drill Fluid: -	Bearing:			North	ing: 69	74869.00 Datum: 56J		
Method	Casing	1 DCP	RL (m)	Depth (m)	Geological Unit	Graphic Log	Glassification Symbol	Material Description	to medium	Moisture	Strength	Cementation / Weathering	Sample / Test	Field Records / Comments		
		2 3 2 3 3 4 4 5		- - - 1_			CH	NATURAL - Silty SAND, dark grey, fine grained, 100mm topsoil Silty CLAY, high plasticity, pale grey mo yellow	ittled orange,	M	St		D U ₅₀	PP>600kPa REC=200mm	- - -	
				-			SC	Clayey SAND, fine to medium grained, orange		D-M	D				-	
SA/TC	Open Hole			2 2 3 3 4 4			SC	Clayey SAND, fine to medium grained, orange and grey	red mottled	D	D					
				_ _ _ 6				End of BH 05 at 6m							- - -	



PROJECT:

BOREHOLE LOG

BOREHOLE NO.: BH 06

DATE COMMENCED: 15.5.2016

SHEET: 1 OF 1

15.5.2016

Engineering and Environmental Consultants Ph 3481 9444 AU.IND.Lawnton@sgs.com

CLIENT: **ECONOMIC DEVELOPMENT QLD**

GEOTECHNICAL INVESTIGATION DATE COMPLETED:

LOCATION: CARSELDINE VILLAGE, BEAMS RD, CARSELDINE LOGGED BY: J.SIPPEL

┍	rill C	ontra	ctor:	SGS	AUS	TRALIA	١	Bore Size: 100mm	Hole Angle:	-90°	0		Eastin	ig: 5	02848.00	Surface R.L.:	
L	rill M	odel:		DTS	05			Drill Fluid: -	Bearing:				Northi	ing: 6	974798.00	Datum: 56J	
Method	Casing	DCP	RL (m)	Depth (m)	Geological Unit	Graphic Log	Classification Symbo l	Material Descri	ption		Moisture Condition	Consistency / Strength	Cementation / Weathering	Sample / Test		Field Records / Comments	Water
SA/TC	Φ.	2 4 4 4 3 3 4 4 5		1 2 3 3 4 5 5 6			SM CH CH SM CH CH CH CH CH CH CH CH CH C	FILL - Silty SAND, fine to medium 90mm topsoil FILL - Silty CLAY, high plasticity, in NATURAL - Silty SAND, fine grain Silty CLAY, high plasticity, palle grorange Sandy CLAY, medium to high plastorange, fine to coarse grained sand clayey SAND, fine to coarse grain orange, red End of BH 06 at 6m	red, grey, brown ned, grey-brown rey mottled yellow, sticity, grey mottled		M M M	VSt VSt VSt					



BOREHOLE LOG

BOREHOLE NO.: BH 07

SHEET: 1 OF 1

Ph 3481 9444
ALLIND Lawnton@sgs.com

JOB NUMBER: SGS/17/E184B

CLIENT: **ECONOMIC DEVELOPMENT QLD**

DATE COMMENCED: 14.5.2016

PROJECT: **GEOTECHNICAL INVESTIGATION**

DATE COMPLETED: 14.5.2016

LOCATION: CARSELDINE VILLAGE, BEAMS RD, CARSELDINE

LOGGED BY: J.SIPPEL
CHECKED BY: C KOSIEK

_							E 104						CDD		C KUSIEI	`	
Dr	ill Co	ontra	ctor:	SGS	AUS	TRAL I A		Bore Size: 100mm	Hole Angle: -9	90°		Eastin	ig: 50	2744.00	Surface R.L.:		
Dr	ill Mo	odel:		DTS	05			Drill Fluid: -	Bearing:			Northi	ng: 69	74894.00	Datum: 56J		\blacksquare
Method	Casing	DCP	RL (m)	Depth (m)	Geological Unit	Graphic Log	Classification Symbol	Material Descrip		Moisture Condition	Consistency / Strength	Cementation / Weathering	Sample / Test		Field Records / Comments		Water
		3				XX	SM	FILL - Silty SAND, fine to medium 90mm topsoil	,	M	MD VSt						
		4		-		\ggg		FILL - Silty CLAY, high plasticity, g								-	1
		3		-			CH	NATURAL - Silty CLAY, high plas yellow, orange	ticity, grey mott l ed	М	St					_	1
		4		_			СН	Silty CLAY, high plasticity, pale gr orange	ey mottled yellow,	М	VSt					_	<u> </u>
		4						orange									
		5		-			l									_	
		4		1_												_	1
				_												_	
																_	
				-												_	1
				-			l									-	-
				2_													
				_			CH	Silty CLAY, high plasticity, pale pa orange	e grey mottled yellow,	М	VSt					_	1
				-				Grange								_	1
				_			l									_	
																_	
SA/TC	Hole			3													
SA	Open Ho l e			<u> </u>			l										1
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PROJECT:

BOREHOLE LOG

BOREHOLE NO.: BH 08

DATE COMMENCED: 14.5.2016

SHEET: 1 OF 1

Engineering and Environmental Consultants Ph 3481 9444 AU.IND.Lawnton@sgs.com

CLIENT: **ECONOMIC DEVELOPMENT QLD**

GEOTECHNICAL INVESTIGATION DATE COMPLETED: 14.5.2016

LOCATION: CARSELDINE VILLAGE BEAMS RD, CARSELDINE LOGGED BY: J.SIPPEL

Drill Model: DTS 05
PP-380-80kPa PP-3
SM FILL - Silty SAND, fine to medium grained, dark grey, M L M St NATURAL - Silty CLAY, high plasticity, grey motified red, orange M VSt Up PP-380kPa REC=150mm CH Silty CLAY, high plasticity, dark grey motified red, orange M VSt Up PP-380kPa REC=150mm CH Silty CLAY, high plasticity, parte grey motified orange and M VSt Up PP-380kPa REC=300mm PP-280-800kPa REC=300mm PP-280-800kPa REC=300mm
5



BOREHOLE LOG

BOREHOLE NO.: BH 09

SHEET: 1 OF 1

Ph 3481 9444
AU.IND.Lawnton@sgs.com

CLIENT: **ECONOMIC DEVELOPMENT QLD**

DATE COMMENCED: 14.5.2016

PROJECT: **GEOTECHNICAL INVESTIGATION**

DATE COMPLETED: 14.5.2016

LOCATION: CARSELDINE VILLAGE, BEAMS RD, CARSELDINE

LOGGED BY: J.SIPPEL

JOB	JOB NUMBER: SGS/17/E184B										CHECK	(ED B)	r: C KOSIEK	
Drill C	ontra	ctor:	SGS	AUS	TRAL I A		Bore Size: 100mm	Hole Angle: -9	90°		Eastin	ı g: 50	02500.00 Surface R.L.:	
Drill N	lodel:	: 	DTS	05			Drill Fluid: -	Bearing:	Г	1	Northi	ng: 69	74973.00 Datum: 56J	
Method	<u>а</u> 2	RL (m)	Depth (m)	Geological Unit	Graphic Log	© Classification Symbol	Material Descriptio NATURAL - Silty SAND, fine to medi		Moisture Condition	Consistency / Strength	Cementation / Weathering	Sample / Test	Field Records / Comments	Water
	3 4 4 5 5		-			SC GI	grey, 90mm topsoil Clayey SAND, fine to medium graine grey Sandy CLAY, medium plasticity, grey orange, red, fine to medium grained	d, brown, orange,	MD	M			PP>600kPa	-
	6 5 6 6		_ _ 1_									U ₅₀	REC=120mm	
			-			CH I	Silty CLAY, high plasticity, palle grey	mottled orange	St	M			PP=310kPa	-
			2_									U ₅₀	REC=350mm	
			-											-
SA/TC Open Ho l e			- 3_											-
SA			-											-
			-											-
			4			CH	Silty CLAY, high plasticity, palle grey	mottled yellow	VSt	М				_
			-									U ₅₀	PP=390kPa REC=400mm	-
			5											
			-											-
			-											1





SOIL CLASSIFICATION

CLASSIFICATION METHOD

The soils are classified based on Australian Standard AS 1726, Geotechnical Site Investigation Code and in accordance with the Unified Soil Classification (USC). Typically, the descriptions include classification group, soil name, grain size, plasticity, structure, colour, moisture, consistency, secondary components and other relevant information.

CLASSIFICATION GROUP

First and/or Second letter

Definition
Gravel
Sand
Silt
Clay
Organic
Peat

	Second Letter								
Letter	Definition								
Р	Poorly graded								
W	Well Graded								
Н	High Plasticity								
	Medium Plasticity								
L	Low Plasticity								

SOIL TYPES

	Major Divisions		Size (mm)
	Boulders		>200
	Cobbles		63 – 200
		coarse	19 – 63
l rec	Gravel	medium	6.7 – 19
Coarse		fine	2.36 – 6.7
		coarse	0.6 - 2.36
	Sand	medium	0.21 – 0.6
		fine	0.075 - 0.21
ا ہ	Silt		0.002 – 0.075
Fine Grained	Clay		<0.002
n S	Peat		N/A – Peat and other highly organic soils

COMPOSITE SOIL TYPES

Most natural soils are a mixture of basic soil types. The primary soil is described and modified by secondary constituents as follows:

Fine (Grained Soil	Coarse Grained Soil				
% Coarse grained	Modifier	% Fine grained	Modifier			
≤ 15	Omit or use 'trace'	≤ 5	Omit or use 'trace'			
15 - 30	Describe as 'with sand/grave l '	5 – 12	Describe as 'with clay/si l t'			
>30	Prefix soil as sandy/gravely	>12	Prefix soil as 'silty/clayey'			

COHESIVE SOIL DESCRIPTION Plasticity

Decementing Towns	Liquid Limit (%)						
Descriptive Terms	CLAY	SILT					
Low plasticity	≤ 35	≤ 50					
Medium plasticity	> 35 ≤ 50	N/A					
High plasticity	> 50	> 50					

Consistency

Term	Undrained Strength C _∪ (kPa)	Field Guide
Very Soft (VS)	≤ 12	Exudes between the fingers when squeezed in hand
Soft (S)	12 - 25	Can be moulded by light finger pressure
Firm (F)	25 – 50	Can be moulded by strong finger pressure
Stiff (St)	50 – 100	Cannot be moulded by fingers.
Very Stiff (VSt)	100 - 200	Can be indented by thumb nail.
Hard (H)	≥ 200	Can be indented with difficulty by thumb nail.

NON-COHESIVE SOIL DESCRIPTIONS

Particle size distribution

- Well graded a good representation of all particle sizes.
- Poorly graded an excess or deficiency of one or more intermediate particle sizes.
- Gap graded an absence of one or more intermediate particle sizes.
- Uniform essentially of one particle size.

Particle Shape

- Equidimensional particles may be described as rounded, sub-rounded, sub-angular, or angular.
- Two dimensional particles with third dimension small by comparison may be described as flaky or platy.
- One dimensional particles with the other two dimensions small by comparison may be described as elongated.

Consistency

TERM	DENSITY INDEX (%)	SPT N VALUE	DCP (Blows/100mm)
Very Loose (VL)	≤ 35	0 – 4	0 – 1
Loose (L)	15 – 35	4 – 10	1 – 3
Medium Dense (MD)	35 – 65	10 – 30	4 – 8
Dense (D)	65 – 85	30 – 50	9 – 15
Very Dense (VD)	> 85	> 50	> 15

MOISTURE CONDITION

Dry (D) Cohesive soils; hard, friable or powdery, well dry of plastic limit.

Granular soils; Cohesionless and free-running.

Moist (M) Soil feels cool, darkened in colour. Cohesive soils can be moulded.

Granular soils tend to cohere.

Wet (W) Soil feels cool, darkened in colour.

Cohesive soils usually weakened and free water form on hands

when handling.

Granular soils tend to cohere.

SOIL ORIGIN Weathered Soils

Residual Soil Soil developed on extremely weathered rock

Transported Soils

Aeolian Deposited by wind.

Alluvium Deposited by streams and rivers.

Colluvium Deposited on slopes (transported downslope by gravity).

Lacustrine Deposited by lakes.

Marine Deposited in ocean basins, beaches and estuarine (tidal

river

Fill

Controlled Fill Fill that has been placed under controlled conditions and certified by a Geotechnical Testing Authority

Uncontrolled Fill Fill that does not comply with controlled fill requirements

TYPICAL REPRESENTATION AND TERMS

YPICAL REPRESENTATION AND TERMS						
			USC	General Description		
GRAVEL	Clean Gravels		GW	Well graded gravels and gravel/sand mixtures		
	(Little or no Fines)	0.C	GP	Poorly graded gravels and gravel/sand mixtures		
	Gravel with Fines	9 <u>0</u> 0	GM	Silty Gravels, gravel/sand/silt mixtures		
			GC	Clayey Gravels, gravel/sand/clay mixtures		
	Clean Sands (Little or no Fines)		sw	Well graded sands, gravelly sands		
SANDS			SP	Poorly graded sands, gravelly/sand mixtures		
SANDS	Sands with Fines		SM	Silty sands		
			sc	Clayey Sands		
SILTS and CLAYS	Liquid Limit >50%		МН	High plasticity inorganic silts, silt mixtures		
			СН	High plasticity inorganic clays, clay mixtures		
		33	ОН	High plasticity organic clays and silts		
	Liquid Limit ≤ 35		ML	Low plasticity inorganic silts, silt mixtures		
			CL	Low plasticity inorganic clays, clay mixtures		
			OL	Low plasticity organic clays and silts		
HIGHLY ORGANIC		7 77 77	PT	Peat, Humus, Swamp Soils with high organics		
FILL				Fill		







SYMBOLS AND ABBREVIATIONS

Drilling methods

SA Solid Flight Auger HS Hollow Stem Auger WB Wash Boring

NMLC Triple tube rotary core drilling

HA Hand Auger

PHA Hydraulic powered hand auger CPT Cone Penetrometer Testing

Drilling Bits and Attachments

TC Tungsten Carbide bit

V V bit

RR Rock Roller (tricone)

BB Blade Bit

Excavation Attachments

GP General Purpose toothed bucket

Ba Batter Bucket TT Tiger Teeth

RB Hydraulic rock breaker

ST Single Tine

Sampling and Testing

SPT Standard Penetrometer Testing

N SPT Blow Count

DCP Dynamic Cone Penetrometer Testing

SV Shear Vane Test

U50 Undisturbed 50mm tube sample

D Disturbed Sample
W Water Sample
PP Pocket Penetrometer
Rec Length of sample recovered

R Refusal

RQD Rock Quality Designation

PL Point Load Test
A Point Load Test (axial)
D Point Load Test (diametral)
L Point Load Test (irregular Lump)

BH Borehole TP Test Pit

Water/Moisture

D Dry M Moist W Wet

First noted depth of water ground water inflow

Steady Water Level

Soil Properties

Cu Undrained Shear Strength

C' Effective Shear Stress

ou Angle of friction — Undrained

Angle of friction — Drained

Y Unit Weight Gs Specific Gravity

MC Moisture Content
LL Liquid Limit
PL Plastic Limit
PI Plasticity Index

WPI Weighted Plasticity Index LS Linear Shrinkage

PSD Particle Size Distribution

D_n n% of particles smaller than specified diameter

k Hydraulic Conductivity

 $\begin{array}{ll} M_{\nu} & \quad \text{Coefficient of Volume Compressibility} \\ C_{\alpha} & \quad \text{Coefficient of Secondary Compression} \end{array}$

C_c Compression Index C_v Coefficient of consolidation OCR Over Consolidation Ratio

e Void Ratio n Porosity

E Elastic Modulus

CBR California Bearing Ratio

UCS Unconfined Compressive Strength

Is(50) Point Load Strength Index

MDR Moisture Density Relationship

DD Dry Density WD Wet Density

MDD Maximum Dry Density
OMC Optimum Moisture Content

SDDR Standard (compactive effort) dry density ratio

DOS Degree of Saturation
APD Apparent Particle Density

Y_s Characteristic Surface Movement

Iss Shrink/Swell Index

H_s Depth of design soil suction changeH_t Maximum drying depth close to a tree

σ Total stressσ' Effective stressu Pore Water Pressure

Foundation Design

q_u Ultimate soil bearing capacity (shallow foundations)

qa Allowable soil bearing capacity (shallow foundations)

fs Ultimate shaft friction (piled foundations)

f_b Ultimate base bearing pressure (piled foundations) R_{dg} Ultimate geotechnical strength (Compression)

Rug Ultimate geotechnical strength (Compressi \$\phi_g\$ Ultimate geotechnical strength (Uplift) \$\phi_g\$ Geotechnical Strength Reduction Factor

Design characteristic strength of concrete

Standards and Specifications

AS Australian Standards

MRD Department of Transport and Main Roads

MRS Main Roads Specification

MRTS Main Roads Technical Specification ISO International Organization for

Standardization

Miscellaneous

CTB Cement treated base
RSS Reinforced soil structure
CFA Continuous flight auger

CH Chainage



APPENDIX D: LABORATORY TEST RESULTS



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SGS Australia Pty Ltd Lawnton Laboratory Unit 1/18 Leanne Crescent Lawnton QLD 4501 AUSTRALIA

Client: SGS Australia Pty Ltd (Engineering & Environmental 5105.426)

SGS/17/184B Project:

Beams Road, Carseldine Location:

SGS Job Number: 18-55-376

Lab: **Lawnton Laboratory** Client Job No:

Order No. Tested Date:

18-LT-1403 Sample No:

Sample ID:

BH09 (300 - 1000)

24/05/2018

CALIFORNIA BEARING RATIO

AS1289.6.1.1 (Soaked)

(CH) CLAY - Brown Sample Description:

16/05/2018 Date Sampled: Moisture Content Method: AS1289.2.1.1

Sampling Method: AS1289.1.2.1 cl 6.5.3 in-situ power auger Compactive Effort Used: AS1289.5.1.1 Standard Compaction

Test Type: SOAKED Retained on 19.0mm (%): 0 Retained Material Excluded: Yes

	RESULT	RATIO (%)
TARGET RESULTS		
Moisture Content (%):	19.2	100.0
Dry Density (t/m3):	1.69	100.0
PLACEMENT RESULTS		
Moisture Content (%):	19.7	102.5
Dry Density (t/m3):	1.68	99.0
AFTER SOAKING RESULTS		
Moisture Content (%):	22.4	116.5
Dry Density (t/m3):	1.64	97.0
AFTER PENETRATION RESULTS		
Moisture Content of Top (%):	22.9	119.5

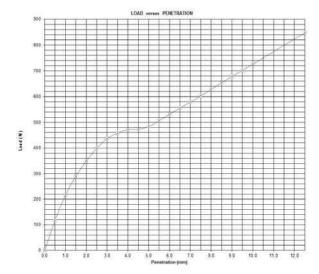
SOAKING DETAILS

Soaking Period (days): 4 Surcharge Applied (kg): 4.5 Swell (%): 2.0

CBR RESULTS

Correction Applied (mm): 0.0 CBR bearing ratio @ 2.5mm (%): 3.0 CBR bearing ratio @ 5.0mm (%): 2.5

CBR VALUE (%): 3.0 @ 2.5mm Penetration





(Dave Gregson) Date: 28/05/2018



Accreditation No.: 2418

Accredited for compliance with ISO/IEC 17025 - Testing

Client Address: 1/18 Leanne Crescent Lawnton Qld 4501

Site No.: 4984 Cert No.: 18-LT-1403-S500_auto Form No.RP-AU-INDCMT-TE-S500_AUTO V5.0

Page 1 of 1



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Client Job No:

Order No:

SGS Australia Pty Ltd Lawnton Laboratory Unit 1/18 Leanne Crescent Lawnton QLD 4501 AUSTRALIA

17/05/2018

Client: SGS Australia Pty Ltd (Engineering & Environmental 5105.426)

Project: SGS/17/184B

Location: Beams Road, Carseldine Tested Date:

 SGS Job Number:
 18-55-376
 Sample No:
 18-LT-1404

 Lab:
 Lawnton Laboratory
 Sample ID:
 BH01 0.3

Shrink-Swell Index

AS 1289.7.1.1 Undisturbed

Sample Data

Sample Type: U50
Depth (m): 0.3
Borehole Number: 1

Sample Description: (CI) Sandy CLAY, Brown mottled Grey

SWELL TEST

Initial Moisture Content (%):

Final Moisture Content (%):

19.0

Total Swell (%):

0.99

SHRINKAGE TEST

Moisture Content (%):

Shrinkage (%):

1.8

SHRINK - SWELL

INDEX (Iss):

Estimated Inert Inclusions (%):

Extent of Crumbling:

Nil

Extent of Cracking:

Nil

Note: Sampled by SGS Australia Pty Ltd according to AS1289.1.3.1 (3.1.3.2)

Authorised

Signatory: (Stephen Bird) Date: 28/05/2018

Site No.: 4984 Cert No.: 18-LT-1404-Z300 Form No.RP-AU-INDCMT-TE-Z300 V10.0

Client Address: 1/18 Leanne Crescent Lawnton Qld 4501



SGS Job Number:

TEST CERTIFICATE

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SGS Australia Pty Ltd Lawnton Laboratory Unit 1/18 Leanne Crescent Lawnton QLD 4501 AUSTRALIA

Client: SGS Australia Pty Ltd (Engineering & Environmental 5105.426)

Project: SGS/17/184B

Location: Beams Road, Carseldine

Lab: Lawnton Laboratory

18-55-376

Client Job No:

Order No: Tested Date:

Sample No: Sample ID: 17/05/2018 18-LT-1405 BH05 0.5

Shrink-Swell Index

AS 1289.7.1.1 Undisturbed

Sample Data

Sample Type: U50
Depth (m): 0.5
Borehole Number: 5

Sample Description: (CI) Sandy CLAY, Brown mottled Grey, Yellow, Red

SWELL TEST

Initial Moisture Content (%):

Final Moisture Content (%):

Total Swell (%):

18.3

20.2

0.17

SHRINKAGE TEST

Moisture Content (%): 18.6 Shrinkage (%): 1.5

SHRINK - SWELL

INDEX (Iss):

Estimated Inert Inclusions (%):

Extent of Crumbling:

Nil

Extent of Cracking:

Low

Note: Sampled by SGS Australia Pty Ltd according to AS1289.1.3.1 (3.1.3.2)

Authorised

Signatory: (Stephen Bird) Date: 28/05/2018

Site No.: 4984 Cert No.: 18-LT-1405-Z300 Form No.RP-AU-INDCMT-TE-Z300 V10.0

Client Address: 1/18 Leanne Crescent Lawnton Qld 4501



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SGS Australia Pty Ltd Lawnton Laboratory Unit 1/18 Leanne Crescent Lawnton QLD 4501 AUSTRALIA

Client: SGS Australia Pty Ltd (Engineering & Environmental 5105,426) Client Job No:

Project: SGS/17/184B Order No:
Location: Beams Road, Carseldine Tested Date:

 Location:
 Beams Road, Carseldine
 Tested Date:
 17/05/2018

 SGS Job Number:
 18-55-376
 Sample No:
 18-LT-1406

 Lab:
 Lawnton Laboratory
 Sample ID:
 BH08 0.5

Shrink-Swell Index

AS 1289.7.1.1 Undisturbed

Sample Data

Sample Type: U50
Depth (m): 0.5
Borehole Number: 8

Sample Description: (CH) CLAY, Brown mottled red, yellow

SWELL TEST

 Initial Moisture Content (%):
 28.2

 Final Moisture Content (%):
 31.2

 Total Swell (%):
 0.78

SHRINKAGE TEST

Moisture Content (%): 28.5 Shrinkage (%): 6.5

SHRINK - SWELL

INDEX (Iss): 3.8

Estimated Inert Inclusions (%): 5

Extent of Crumbling: Nil

Extent of Cracking: Low

Note: Sampled by SGS Australia Pty Ltd according to AS1289.1.3.1 (3.1.3.2)

Authorised

Signatory: (Stephen Bird) Date: 28/05/2018

Site No.: 4984 Cert No.: 18-LT-1406-Z300 Form No.RP-AU-INDCMT-TE-Z300 V10.0

Client Address: 1/18 Leanne Crescent Lawnton Qld 4501



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SGS Australia Pty Ltd Lawnton Laboratory
Unit 1/18 Leanne Crescent
Lawnton QLD 4501
AUSTRALIA

Client: SGS Australia Pty Ltd (Engineering & Environmental 5105.426)

SGS/17/184B Project:

Beams Road, Carseldine Location:

SGS Job Number: 18-55-376

Lab: **Lawnton Laboratory** Client Job No:

Order No. Tested Date:

Sample No: 18-LT-1401

Sample ID:

BH01 (200 - 1000)

24/05/2018

CALIFORNIA BEARING RATIO

AS1289.6.1.1 (Soaked)

(CI-CH) Sandy CLAY - Brown Sample Description:

14/05/2018 Date Sampled: Moisture Content Method: AS1289.2.1.1

Sampling Method: AS1289.1.2.1 cl 6.5.3 in-situ power auger Compactive Effort Used: AS1289.5.1.1 Standard Compaction

Test Type: SOAKED Retained on 19.0mm (%): Retained Material Excluded: Yes

	RESULT	RATIO (%)
TARGET RESULTS		
Moisture Content (%):	17.6	100.0
Dry Density (t/m3):	1.75	100.0
PLACEMENT RESULTS		
Moisture Content (%):	17.3	98.0
Dry Density (t/m3):	1.76	100.0
AFTER SOAKING RESULTS		
Moisture Content (%):	18.9	107.5
Dry Density (t/m3):	1.74	99.5
AFTER PENETRATION RESULTS		
Moisture Content of Top (%):	19.7	112.0
SOAKING DETAILS		

SOAKING DETAILS

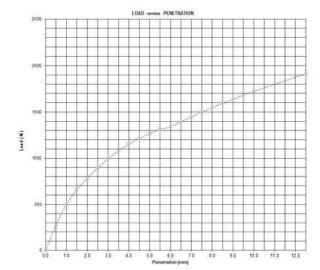
Soaking Period (days): 4 Surcharge Applied (kg): 4.5 Swell (%): 1.0

CBR RESULTS

Correction Applied (mm): 0.0 CBR bearing ratio @ 2.5mm (%): 7 CBR bearing ratio @ 5.0mm (%): 6

CBR VALUE (%):

@ 2.5mm Penetration



Signatory:



(Dave Gregson)



Accreditation No.: 2418

Accredited for compliance with ISO/IEC 17025 - Testing

Client Address: 1/18 Leanne Crescent Lawnton Qld 4501

Site No.: 4984 Cert No.: 18-LT-1401-S500_auto Form No.RP-AU-INDCMT-TE-S500_AUTO V5.0

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Date: 28/05/2018



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SGS Australia Pty Ltd Lawnton Laboratory Unit 1/18 Leanne Crescent Lawnton QLD 4501 AUSTRALIA

Client: SGS Australia Pty Ltd (Engineering & Environmental 5105.426)

Project: SGS/17/184B

Location: Beams Road, Carseldine

SGS Job Number: 18-55-376
Lab: Lawnton Laboratory

Client Job No:

Order No: Tested Date:

Sample No: 18-LT-1402 Sample ID: BH05 (200 - 800)

24/05/2018

CALIFORNIA BEARING RATIO

AS1289.6.1.1 (Soaked)

Sample Description: (CI) Sandy CLAY - Brown

Date Sampled: 16/05/2018
Moisture Content Method: AS1289.2.1.1

Sampling Method: AS1289.1.2.1 cl 6.5.3 in-situ power auger Compactive Effort Used: AS1289.5.1.1 Standard Compaction

Test Type: SOAKED
Retained on 19.0mm (%): 0
Retained Material Excluded: Yes

	RESULT	RATIO (%)
TARGET RESULTS		
Moisture Content (%):	15.8	100.0
Dry Density (t/m3):	1.80	100.0
PLACEMENT RESULTS		
Moisture Content (%):	15.8	100.0
Dry Density (t/m3):	1.79	99.5
AFTER SOAKING RESULTS		
Moisture Content (%):	18.1	114.5
Dry Density (t/m3): AFTER PENETRATION RESULTS	1.78	99.0

18.5

SOAKING DETAILS

Moisture Content of Top (%):

Soaking Period (days): 4
Surcharge Applied (kg): 4.5
Swell (%): 1.0

CBR RESULTS

 Correction Applied (mm):
 0.2

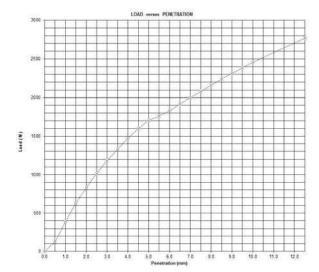
 CBR bearing ratio @ 2.5mm (%):
 8

 CBR bearing ratio @ 5.0mm (%):
 9

CBR VALUE (%):

@5.0mm Penetration

117.5



Authorised Signatory:



(Dave Gregson)



Accreditation No.: 2418

Accredited for compliance with ISO/IEC 17025 - Testing

Client Address: 1/18 Leanne Crescent Lawnton Qld 4501

Site No.: 4984 Cert No.: 18-LT-1402-S500_auto Form No.RP-AU-INDCMT-TE-S500_AUTO V5.0

Page 1 of 1

Date: 28/05/2018



APPENDIX E: SITE PHOTOGRAPHS







Photos taken facing west over playing fields with uncontrolled fill batter in background





Photos taken facing north-east overlooking existing stormwater basin and Beams Road entrance





Photos facing north-east overlooking lower playing field and basketball courts



APPENDIX F: EARTHWORKS NOTES

REF: PF-AU-INDENG-RM-005 / Rev 1 / 30.5.2017



PROJECT: LEVEL 1 EARTHWORKS CONTROL

These instructions apply to this project unless otherwise addressed in the job specifications or subsequently by the superintendent.

(A) PRIOR TO FILLING

- (1) Topsoil and organic matter must be stripped to the nominated depth from the proposed cut and fill areas.
- (2) The superintendent or GTA should be notified if the required stripping exceeds the nominated depth.
- (3) Any existing (uncontrolled) fill must be either removed or investigated, approved and documented.
- (4) The stripped natural surface (fill foundation) must be inspected, proof rolled and approved.
- (5) Any unsound areas are subject to supplementary site instructions (in general, the fill foundation is subject to the same compaction requirements as the fill). The practice of "bridging" over soft, unstable and wet fill foundation is generally not acceptable.

(B) FILLING

- (6) If necessary, the fill material must be moisture conditioned as required.
 - a) Too wet dry fill to within a moisture range that the specified density can be achieved and the fill area is not deflecting (surface heaving) under construction traffic to the detriment of the fill in general.
 - b) Too dry moisten the fill to within a moisture range that the specified density can be achieved.
 - c) The fill should be mixed to ensure reasonably uniform distribution of the moisture.
- (7) Remove excessive vegetation (sticks, stumps, etc.) as required.
- (8) Place fill in layers generally not exceeding 200mm thick and compact to specification (larger or more efficient compaction equipment may enable the placement of thicker fill layers).
- (9) The fill must be tested at the rate of:
 - a) Minimum of one (1) test every 2nd layer (each 400mm lift)
 - b) Minimum of one (1) test/500m³ of fill large scale project
 - c) Minimum of one (1) test/200m³ of fill small scale project

or as directed by the GTA or superintendent

- (10) Areas represented by a failed test must be reworked and retested and a positive result obtained prior to placing additional fill.
- (11) Where fill abuts against sloping ground, benches should be cut in the ground generally to a depth of 200mm to 300mm.
- (12) Fill should be placed in near horizontal layers of uniform thickness deposited systematically across the fill area.
- (13) If topsoil is stockpiled adjacent to the fill area, care should be taken to ensure that structural fill does not encroach into the stockpile area.
- (14) The maximum particle size of rocks within the layer after compaction should not exceed two-thirds of the compacted layer thickness.
- (15) Equipment and haul roads should be selected to avoid the overloading (and development of surface heaving) of the fill areas.
- (16) If the filling programme is interrupted (eg. by rainfall periods), the interrupted surface must be inspected and assessed prior to placing additional fill (i.e. in accordance with "(A)".



PROJECT: LEVEL 1 EARTHWORKS CONTROL

These notes apply to this project unless otherwise instructed by the project superintendent.

(A) TEST PROCEDURES

Test procedures to be used on the site will be selected from the following:

- AS1289 5.1.1 Dry Density/Moisture Content Relationship (Standard Compaction)
- AS1289 5.2.1 Dry Density/Moisture Content Relationship (Modified Compaction)
- AS1289 5.3.1 Determination of the Field Density of a Soil (Sand Replacement)
- AS1289 5.4.1 Dry Density Ratio, Moisture Variation and Moisture Ratio
- AS1289 5.5.1 Determination of the Minimum and Maximum Dry Density of a Cohesionless Material
- AS1289 5.6.1 Density Index for a Cohesionless Material
- AS1289 5.7.1 Hilf Density Ratio and Moisture Variation
- AS1289 5.8.1 Determination of the Field Density of a Soil (Nuclear Gauge)

(B) CONTRACTORS RESPONSIBILITIES

Construction/Compaction Equipment

Careful consideration should be given to the selection of compaction equipment and the proportion of compaction equipment to incoming fill quantities. The plant should be capable of compacting all of the fill area including its edges, batters, irregular surfaces and junctions with the natural ground.

Construction Equipment Operators

It is the responsibility of the contractor to ensure that operators are adequately trained in the basic standard practices and requirements of earthwork construction (eg. rolling patterns, benching, appropriate layer thicknesses, etc.).

Notification of Filling

The Geotechnical Testing Authority relies on the Contractor, Constructor or Superintendent to advise when the filling operation will commence, or re-commence following delay periods. Level 1 certification <u>cannot</u> be given for fill placed without the knowledge of the Geotechnical Testing Authority.

Specification Compliance

Regardless of the role of the Geotechnical Testing Authority, the contractor is responsible for complying with all aspects of the specification including the quality, placement methods and compaction of the fill.

(C) UNSUITABLE MATERIALS

In relation to structural filling, unsuitable materials may be termed either "unsuitable" or "temporary unsuitable".

1) Unsuitable

Unless otherwise approved by the superintendent, the following materials are not suitable for forming any part of structural filling. At the direction of the superintendent, unsuitable materials should either be removed to spoil or used in non-structural areas (eg. park areas, footpaths, etc.).

- organic soils topsoils, severely root affected soils and peat
- materials which may be contaminated with toxic substances through past site usages
- filling which contains wood, metal, plastic, boulders and other deleterious materials
- any other materials which have deleterious engineering properties

2) Temporary Unsuitable

"Temporary unsuitable" refers to materials which are deemed unsuitable for use as structural fill in the present condition but may be rectified for subsequent use by some form of treatment.

Typical examples of temporary unsuitable materials and appropriate treatments are shown below:

Temporary Unsuitable Material

Material too wet

Excessive oversize

Excessive organics (sticks/stumps)

Possible Remedial Treatment
Spread and Dry
Screen/remove oversize
Remove sticks/stumps



(D) REACTIVE CLAYS

Soil reactivity is a term which refers to the volume change (shrinking and swelling) of clay soils undergoing moisture change. Reactive clay soils swell when wetted up and shrink when dried out. This characteristic is measured in the laboratory and used extensively for residential site classification and footing design. The following issues should be considered.

- 1) The site classification of a lot is not only affected by filling of the lot but also by the reactivity characteristics of the soils used to fill the lot.
- 2) Clay soils placed in a new environment (fill) will, over a period, adjust to equilibrium conditions (moisture and density). Clay soils which are over dried and over compacted (beyond equilibrium conditions) may result in a fill area with a high swell potential.

A Modified Compaction specification will often necessitate the drying of clay soils well beyond the equilibrium conditions to meet the specification requirements. In temperate climates, the Standard Compaction Optimum Moisture Content is more likely to approximate the equilibrium moisture content (AS 3798 - 2007 Clause 5.3).

(E) SANDY SOILS (SILTY SANDS AND CLAYEY SANDS)

Sandy soils are generally prone to loss of strength and stability (heaving under load) as the moisture content approaches the standard optimum moisture content. The condition generally worsens as the moisture content increases above the optimum moisture content. This condition can develop and be evident on fill areas that may otherwise comply with the density requirement. As a general rule, the moisture content should be maintained approximately 1% to 3% dry of the optimum moisture content (standard compaction).

(F) TOPSOILING

Spreading of topsoil in excessive quantities over controlled fill may reduce the likelihood of a site being re-classified from a 'P' site. As a general rule, topsoil depth should be restricted to about 100mm in proposed building areas.

(G) COMPACTION STANDARDS

Unless otherwise notified, the compaction standard specified by the local authority will be adopted as the density acceptance/rejection criteria.

(H) CONTROLLED FILL ACCEPTANCE/REJECTION CRITERIA

Any combination of the following issues may influence an acceptance/rejection instruction on a section of fill presented for testing.

- density testing
- load testing deflection/surface heaving
- quality of fill organics/deleterious materials
- consistency of compaction

(I) EXCLUSIONS

Unless specifically requested Level 1 compaction control does not address the following issues:

- slope stability
- reactive soils
- soft natural soils and/or pre-existing (uncontrolled) fill on the site outside of the nominated controlled fill area
- soils which may be contaminated with toxic substances
- backfill to service trenches, subsequent to the controlled fill commission or when not included in the controlled fill commission
- site drainage
- topsoil placed subsequent to completion of controlled filling
- where the filling exceeds 5m, advice from a geotechnical professional should be sought



APPENDIX G: STANDARD CBR NOTES AND PERFORMANCE WARNINGS

 Project No.
 SGS/17/E184B
 29 May 2018

 Revision
 0
 Page G



SAMPLING

At the time of sampling, earthworks had not been carried out and the proposed subgrade had not been exposed.

As the subgrade was not exposed, and could not be viewed at the time of sampling, some of the samples may not be representative of predominant or worst case soil types.

Soil type boundaries (representing the soaked CBR samples) should be established when bulk earthworks is completed and the proposed subgrade is exposed.

Sampling frequency/location was in accordance with the instruction received from our client.

Unless otherwise instructed, samples are generally recovered from the zone of extreme pavement thickness, i.e. 00 - 500mm below design subgrade level.

TESTING

Testing was carried out in accordance with A.S. 1289 "Methods of Testing Soils for Engineering Purposes", A.S. 1289 6.1.1.

The test specimen was nominally placed at the Optimum Moisture Content and to the expected required density of the subgrade.

In accordance with the test procedure, the test specimen was soaked for a period of four (4) days with a surcharge mass of <u>4.5kg</u>. This surcharge mass is approximately equivalent to the pressure applied by a 2.0 T/m³ insitu density pavement thickness of <u>150mm</u> (Refer to A.S. 1289 6.1.1, Figure 7 for full minimum pavement thickness requirements).

The minimum pavement thickness should be at least equivalent to the pavement thickness represented by the surcharge mass, refer to AS1289.6.1.1, Figure 7 for full minimum pavement thickness requirements

Test method A.S. 1289 6.1.1 allows for any +19.0mm material to be replaced in the test portion by -19.0mm + 4.75mm material. Unless otherwise instructed by our client, +19.0mm material will be excluded from the test portion.

PERFORMANCE WARNINGS

Sandy Soils (Sands, Silty Sands and Clayey Sands)

Sandy soils are generally prone to loss of strength, reduced insitu C.B.R. and stability (heaving under load) as the moisture content approaches the standard compaction optimum moisture content. The condition generally worsens proportionally with increasing moisture content (above the optimum moisture content).

The C.B.R. value obtained on the laboratory test specimen is only representative of the material at the nominated density and moisture content.

Serviceable drainage, both surface and sub-surface (side drains) and uniform conforming density is critical to the sound performance of sandy subgrades. Provided that this is achieved, the subgrade insitu C.B.R. value should approximate the laboratory C.B.R. value for the representative soil types.

Seepage zones are common in sandy soils, particularly following rainfall periods. Wet sandy soils and seepage within the depth zone affected by loading (eg. by construction traffic) can be highly detrimental to the trafficability, workability and performance on subgrades and road pavements.

The permeability of <u>compacted</u> Silty and Clayey Sand subgrades is generally low, ensuring good serviceability provided that the sub-surface drainage is adequate.

Clayey Soils (Clays, Sandy Clays and Silty Clays)

Clay soils generally have very low permeability and as a result, construction and performance problems associated with wet weather are usually confined to the exposed surface of the subgrade. However, workability problems can occur in poorly drained areas or after prolonged wet periods.

The C.B.R. value obtained on the laboratory test specimen is generally representative of the material in "the worst case", after four (4) days of continuous soaking. Most clay soils are reactive, to varying extents and swell when exposed to water. As a general rule, increasing swell is proportional to the decreasing C.B.R. value on most clay soils. Dry "baked out" clay subgrades can produce insitu C.B.R. values far in excess of the laboratory Soaked C.B.R. value.

Excessive drying and compaction of clay subgrades can be detrimental to the long term performance to some pavements. Upon wetting up to the "equilibrium moisture" some clay subgrades can swell resulting in deformation and weakening to the pavement.

CONSTRUCTION

Care should be taken when backfilling services (sewer/stormwater etc.) in the pavement area to ensure that materials in the top 500mm of backfill is not of lesser C.B.R. than the C.B.R. representing that section of pavement.

Should additional earthworks of any kind be carried out after the soil boundaries have been established, the boundaries may become invalid and should be re-confirmed.



APPENDIX H FILLING AND EXCAVATION CODE



FILLING & EXCAVATION CODE

PERFORMANCE CRITERIA AND ACCEPTABLE SOLUTIONS

PERFORMANCE CRITERIA	ACCEPTABLE SOLUTIONS	SOLUTIONS ¹	COMMENTS	COUNCIL USE ONLY
P01 Development for filling or excavation minimises visual impacts from retaining walls	A01 Development ensures that the total height of any cut and fill, whether or not retained, does not exceed:	A/S	S01 A terraced retaining wall in accordance with Brisbane City Council guidelines is proposed to	
and earthworks.	 a. 2.5m in a zone in the Industry zones category; b. 1m in all other zones, or if adjoining a sensitive zone. 		address the 5.0m level difference to the adjoining property.	
P02	A02.1		502.1	
Development of a retaining wall proposed as	Development of a retaining structure, including footings,	6	The terraced retaining wall shall be designed with	
result of filling or excavation:	æ		1m high vert : 1m horizontal terraces in	
a. Is designed and constitucted to be intitle burbose:	 a. is whomy contained within the site, b. if the total height to be retained is greater than 1m. 		accoluance with council guidelines. The Till horizontal sections will incorporate low	
b. Does not impact adversely on significant	then:		maintenance planting.	
vegetation;	i. the retaining wall at the property boundary			
c. Is capable of easy maintenance	is no greater than 1m above the ground			
comply with the Building Beaulation and	II. all lul tilel tellacilig ilolii tile IIII liigli boundary rataining wall is 1 vartical unit:1			
embankment gradients will need to comply	boundary retaining wan is 1 vertical unit.1 horizontal unit;			
with the Building Regulation . Note—	iii. the distance between each successive			
Guidance on the protection of native	retaining wall (back of lower wall to face of			
vegetation is included in the <u>Biodiversity</u> areas planning scheme policy.	higher wall) is no less than 1m horizontally to incorporate planting areas			
	A02.2		502.2	
	Development of a retaining wall over 1m in height protects significant vegetation on the site and on	٩Z	The FFMP addresses the consideration of significant vegetation. Retaining walls will be	
	adjoining land and is designed and constructed in		designed and constructed in accordance with the	
	accordance with the structures standards in the Infrastructure design planning scheme policy and certified		structures standards in the infrastructure design planning scheme policies and certified by a RPEO.	
	by a Registered Professional Engineer Queensland.			

Solution: 9 = Acceptable Solution
A/S = Alternative Solution
N/A= Not Applicable to this Proposal



PERFORMANCE CRITERIA	ACCEPTABLE SOLUTIONS	SOLUTIONS ¹	COMMENTS	COUNCIL USE ONLY
	A02.3 Development provides a retaining wall finish that presents to adjoining land that is maintenance free if the setback is less than 750mm from the boundary.	6	So2.3 Retaining walls will have a finish that presents to adjoining land that is maintenance free and accessible from the development.	
	A02.4 Development for filling only uses clean fill that does not include any construction rubble or debris.	ō	S02.4 Clean fill will be used for any on site filling.	
Po3 Development ensures that a rock anchor is designed and constructed to be fit for purpose	Ao3 Development ensures that a rock anchor: a. is constructed in accordance with the standards in the <u>Infrastructure design planning scheme policy</u> : b. where it extends beyond the property boundary, is supported by a letter of consent from the adjoining land and building owner	Ō	Soa Currently no rock anchors are proposed.	
P04 Development protects all services and public utilities.	A04 Development protects services and public utilities and ensures that any alteration or relocation of services or public utilities meets the standard design specifications of the responsible service authorities.	5	\$04 The alteration or relocation of services and public utilities will be in accordance with the service authority requirements.	
Pos Development provides surface and sub- surface drainage to prevent water seepage, concentration of run-off or ponding of stormwater on adjacent land.	A05 Development ensures all flows and subsoil drainage are directed to a lawful point of discharge of a surface water diversion drain, including to the top or toe of a retaining wall in accordance with the stormwater drainage section of the Infrastructure design planning scheme policy.	6	All drainage will be directed to the lawful point of discharge in accordance with the stormwater drainage section of the Infrastructure design planning scheme policy. Refer to Stormwater Management Plan prepared by Design Flow for the stormwater strategy	



PERFORMANCE CRITERIA	ACCEPTABLE SOLUTIONS	SOLUTIONS ¹	COMMENTS	COUNCIL USE ONLY
P06	A06		908	
Development ensures that the design and	No acceptable outcome is prescribed.	A/S	The Phase 2 vegetated catch drain works are	
construction of all open drainage works is			proposed as part of this DA. The design allows for	
undertaken in accordance with natural			major flows to be conveyed to a legal point of	
channel design principles, being the			discharge. The vegetated profile is to council	
development of a stormwater conveyance			requirements.	
system for major flows, by using a vegetated				
open channel or drain that approximates the				
features and functions of a natural waterway				
to enhance or improve riparian values of those				
stormwater conveyance systems.				
Editor's note—Guidance on natural channel				
design principles can be found in the Council's				
publicationNatural channel design guidelines.				
P07	A07.1		507.1	
Development for <u>filling or excavation</u> :	Development for filling or excavation provides water	6	Proposed filling or excavation complies with the	
a. does not degrade water quality or	quality treatment that complies with the Stormwater		Stormwater Management Code and the	
adversely affect environmental values in	drainage section of the Infrastructure design planning		Infrastructure Design Planning Scheme Policy.	
receiving waters;	scheme policy.			
b. ensures site sediment and erosion	A07.2		507.2	
control standards are best practice.	Development provides erosion and sediment control	6	Proposed filling or excavation complies with the	
	standards that are in accordance with the stormwater		Sediment Control Standards within Council's	
	drainage section of the <u>Infrastructure design planning</u>		Infrastructure Design Planning Scheme Policy.	
	<u>scheme policy</u> .		Refer to Stormwater Management plan prepared	
			by Design Flow for the stormwater strategy	



PERFORMANCE CRITERIA	ACCEPTABLE SOLUTIONS	SOLUTIONS ¹	COMMENTS	COUNCIL USE ONLY
P08	A08.1		508.1	
Development for filling or excavation is	Development ensures that no dust emissions extend	6	Construction and demolition works will occur	
conducted such that adverse impacts at a	beyond the boundary of the site, including dust from		during work times in accordance with the	
sensitive use due to noise and dust are	construction vehicles entering and leaving the site.		relevant planning scheme policies and	
prevented or minimised.			guidelines. A Construction Management Plan	
Note—A noise and dust impact management			will be provided by the contractor prior to	
plan prepared in accordance with the			commencement of site works.	
Management plans planning scheme policy	A08.2		808.2	
can assist in demonstrating achievement of this	Development for filling or excavation activity only	6	Filling or excavation activities will be	
performance outcome.	occurs between the hours of 6:30am and 6:30pm		undertaken between the hours of 6:30am and	
	Monday to Saturday, excluding public holidays.		6:30pm Monday to Saturday, excluding public holidays or as agreed by Brisbane City Council.	
P09	A09		608	
Development ensures that vibration generated	Development involving filling or excavation does not	6	Filling or excavation will be undertaken using	
by the <u>filling or excavation</u> operation does not	cause a ground-borne vibration beyond the boundary of		methods which do not cause a ground-borne	
exceed the vibration criteria in Table 9.4.3.3.D,	the site.		vibration beyond the boundary of the site.	
<u>Table 9.4.3.3.E, Table 9.4.3.3.F</u> and <u>Table</u>				
9.4.3.3.G.				
Note—A noise management report prepared in				
accordance with the Noise impact assessment				
planning scheme policy can assist in				
demonstrating achievement of this				
performance outcome.				
P010	A010		S010	
Development ensures that heavy trucks hauling	Development ensures that heavy trucks hauling	6	Haulage of material will be undertaken with	
material to and from the site do not affect the	material to and from the site:		consideration to the local environment with	
amenity of established areas and limits			appropriate mitigation measures implemented	
environmental nuisance impact on adjacent land.	b. use a major road to access the site;c. only use a minor road for the shortest-most- direct		to prevent nuisance.	
			The routes used for transportation of	
	nuisance if there is no major road alternative.		earthworks will be approved with EDQ DA/TS	
			and Council prior to commencement of	
			construction.	



PERFORMANCE CRITERIA	ACCEPTABLE SOLUTIONS	SOLUTIONS ¹	COMMENTS	COUNCIL USE ONLY
P011 Development for filling or excavation protects the environment and community health and wellbeing from exposure to contaminated land and contaminated material.	A011 Development does not involve: a. excavation on land previously occupied by a notifiable activity or on land listed on the Environmental Management Register or the Contaminated Land Register; b. filling with material containing a contaminant.	NA	S011 The site is not on the Environmental Management Register or Contaminated Land Register.	
P012 Development provides for: a. landscaping for water conservation purposes; b. water sensitive urban design measures	A012.1 Development provides landscaping which is designed using the standards in the Landscape design guidelines for water conservation planning scheme policy.	6	S012.1 See Saunders Havill Group Landscape Design and response to Landscape Code.	
which are employed within the landscape design to maximise stormwater use and to reduce any adverse impacts on the landscape; c. stormwater harvesting to be maximised and any adverse impacts of stormwater	A012.2 Development ensures that the design and requirements for irrigation are in compliance with the standards in Landscape design guidelines for water conservation planning scheme policy.	6	S012.2 There is no irrigation proposed for the development.	
minimised.	A012.3 Development provides areas of pavement, turf and mulched garden beds which are drained. Note—This may be achieved through the provision and/or treatment of swales, spoon drains, field gullies, subsurface drainage and stormwater connections.	O)	S012.3 Areas of pavement, turf and mulched garden beds are drained through the provision of stormwater connections.	



PERFORMANCE CRITERIA	ACCEPTABLE SOLUTIONS	SOLUTIONS ¹	COMMENTS	COUNCIL USE ONLY
Pota Development provides roads, pavement, edging and landscaping which: a. are designed and constructed in accordance with the road hierarchy; b. provide for safe travel for pedestrians, cyclists and vehicles; c. provide access to properties for all modes; d. provide utilities; e. provide utilities; e. provide high levels of aesthetics and amenity, improved liveability and future growth; f. provide for the amelioration of noise and other pollution; g. provide a high-quality streetscape; h. provide a low-maintenance asset with a minimal whole-of-life cost. Note—This can be demonstrated in an engineering report prepared and certified by a Registered Professional Engineer Queensland in accordance with the Infrastructure design planning scheme policy.	A01 Development provides roads and associated pavement, edging and landscaping which are designed and constructed in compliance with the road corridor design standards in the Infrastructure design planning scheme policy.	ത	The development will provide roads and associated pavement, edging and landscaping designed in accordance with the Infrastructure Design Planning Scheme Policy.	
Po2 Development provides road pavement surfaces which: a. are well designed and constructed; b. durable enough to carry the wheel loads of the intended types and numbers of travelling and parked vehicles; c. (ensures the safe passage of vehicles, pedestrians and cyclists, the discharge of stormwater run-off and the preservation of all-weather access; d. allows for reasonable travel comfort.	A02 Development provides road pavement surfaces which are designed and constructed in compliance with the road corridor design standards in the Infrastructure design planning scheme policy.	ത	S02 The development will provide road pavement surfaces which are designed and constructed in compliance with the Infrastructure Design Planning Scheme.	

9 = Acceptable Solution A/S = Alternative Solution N/A= Not Applicable to this Proposal

Solution:

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COLINCILLISE ONLY	COUNCIL USE ONLY		
STUBMINGO	Soa The development will provide road pavement edges in accordance with the Infrastructure Design Planning Scheme. Any damage to road verge during site construction activities, including damage to the kerb and channel, will be rectified to its existing condition.	Where provided, verges will be designed and constructed in accordance with the Infrastructure Design Planning Scheme Policy. Safe pedestrian access and sufficient area for public utility services provided. Verges will be maintainable by Council.	S05 If provided, lane or laneway will be designed in accordance with the Infrastructure Design Planning Scheme Policy.
COLLITIONES	SOLUTIONS:	o	o
ACCEPTABLE COLLITIONS	A03 A03 Development provides pavement edges which are designed and constructed in compliance with the road corridor design standards in the Infrastructure design planning scheme policy.	A04 Development provides verges which are designed and constructed in compliance with the road corridor design and streetscape locality advice standards in the Infrastructure design planning scheme policy.	A05 Development provides a lane or laneway identified in a neighbourhood plan which is embellished in compliance with the streetscape locality advice standards in the Infrastructure design planning scheme policy.
DEDECOMANCE COTTED!A	PERFORMANCE CRITERIA P03 Development provides a pavement edge which is designed and constructed to: a. control vehicle movements by delineating the carriageway for all users; b. provide for people with disabilities by allowing safe passage of wheelchairs and other mobility aids.	Po4 Development provides verges which are designed and constructed to: a. provide safe access for pedestrians clear of obstructions and access areas for vehicles onto properties; b. provide a sufficient area for public utility c. services; d. be maintainable by the Council.	Pos Development provides a lane or laneway identified in a neighbourhood plan which: a. allows equitable access for all modes; b. is safe and secure; (c) has 24-hour access; c. is a low-speed shared zone environment; d. has a high-quality streetscape.



PERFORMANCE CRITERIA	ACCEPTABLE SOLUTIONS	SOLUTIONS ¹	COMMENTS	COUNCIL USE ONLY
Pobe Development of an existing premises provides at the frontage to the site, if not already provided, the following infrastructure to an appropriate urban standard: a. an effective, high-quality paved roadway; b. an effective, high-quality roadway kerb and channel; c. safe, high-quality vehicle crossings over channels and verges; d. safe, accessible, high-quality verges compatible and integrated with the surrounding environment; e. safe vehicle access to the site that enables ingress and egress in a forward gear; f. provision of and required alterations to public utilities; g. effective drainage; h. appropriate conduits to facilitate the provision of required street-lighting systems and traffic signals.	Development of an existing premises provides at the frontage of the site, if not already existing, the following infrastructure to the standard that would have applied if the development involved new premises as stated in the road corridor design standards in the infrastructure design planning scheme policy: a. concrete kerb and channel; b. forming and grading to verges; c. crossings over channels and verges; (d) a constructed bikeway; d. a constructed verge or reconstruction of any damaged verge; e. construction of the carriageway; f. payment of costs for required alterations to public utility mains, services or installations; g. construction of and required alterations to public utility mains, h. services or installations; i. drainage works; j. installation of electrical conduits.		All surrounding roads are currently in good condition. Any damage to the Beams Rd carriageway and verges due to the installation of the proposed water main crossing will be rectified at the developer's expense. High-quality verges proposed which integrate with existing environment. Safe vehicular access proposed.	
Po7 Development provides both cycle and walking routes which: a. are located, designed and constructed to their network classification (where applicable); b. provide safe and attractive travel routes for pedestrians and cyclists for commuter and recreational purposes; c. provide safe and comfortable access to properties for pedestrians and cyclists; d. incorporate water sensitive urban design into stormwater drainage; (e) provide for utilities; f. provide for a high level of aesthetics and amenity, improved liveability and future growth;	A07 Development provides cycle and walking routes which are located, designed and constructed in compliance with the road corridor design and off- road pathway design standards in the Infrastructure design planning scheme policy.	ര	S07 Existing cycle and walking routes are to be maintained on road and verge.	

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 g. are a low-maintenance asset with a minimal whole-of-life cost; 			
h. minimise the clearing of significant native			
vegetation.			
Note—This can be demonstrated in an			
engineering report prepared and certified by a			
Registered Professional Engineer Queensland			
in accordance with the Infrastructure design			
planning scheme policy.			
P08	A08.1		508.1
Development provides refuse and recycling	Development provides refuse and recycling collection 9	•	Refuse and recycling collection and storage has
collection, separation and storage facilities that	and storage facilities in accordance with the Refuse		been demonstrated within the Cardno Traffic
are located and managed so that adverse	planning scheme policy.		assessment.
impacts on building occupants, neighbouring			
properties and the public realm are minimised.	A08.2		508.2
	Development ensures that refuse and recycling	•	Refuse and recycling collection and storage has
	collection and storage location and design do not have		been demonstrated within the Cardno Traffic
	any adverse impact including odour, noise or visual		assessment.
	impacts on the amenity of land uses within or adjoining		
	the development.		
	Note—Refer to the <u>Refuse planning scheme policy</u> for further midance		
	ימונות פתומות.		
P09	A09.1		809.1
Development ensures that:	Development ensures that the reticulated water and	•	The development has allocations for sewer and
a. land used for an urban purpose is serviced	sewerage distribution system for all services is in place		water networks to service the development
adequately with regard to water supply	before the first use is commenced.		yield in accordance with UU requirements.
and waste disposal, h (the water supply meets the stated	409.2		509.3
	Development provides the lot with reticulated water 9	•	Refer to S09.1.
and fire-fighting purposes.	supply and sewerage to a standard acceptable to the		
	מוזנו וסמנסו ובנמובו.		



PERFORMANCE CRITERIA	ACCEPTABLE SOLUTIONS	SOLUTIONS ¹	COMMENTS	COUNCIL USE ONLY
Dovelopment provides public utilities and street lighting which are the best current or Alternative technology and facilitate accessibility, easy maintenance, minimal whole-of-life costs, and minimal adverse environmental impacts.	A010.1 Development provides public utilities and street lighting which are located and aligned to: a. avoid significant native vegetation and areas Identified within the Biodiversity areas overlay map; b. minimise earthworks; c. avoid crossing waterways, waterway corridors and wetlands or if a crossing is unavoidable, tunnel- boring techniques are used to minimise disturbance, and a disturbed area is reinstated and restored on completion of the work. Note—Guidance on the restoration of habitat is included in the Biodiversity areas planning scheme policy.	ത	Provision of public utilities and street lighting Provision of public utilities and street lighting will be determined at detailed design stage and incorporated as required.	
	A010.2 Development provides compatible public utility services and street-lighting services which are co-located in common trenching for underground services.	o	S010.2 Determined at detailed design stage and incorporated as required. Common public utility trenching will be implemented where practicable.	
	A010.2 Development provides public utilities and street lighting which are designed and constructed in compliance with the public utilities standards in the Infrastructure design planning scheme policy.	6	S010.3 Provision of public utilities and street lighting will be determined at detailed design stage and incorporated as required. They will be designed and constructed in compliance with the prescribed standards.	



PERFORMANCE CRITERIA	ACCEPTABLE SOLUTIONS	SOLUTIONS1	COMMENTS	COUNCIL USE ONLY
P011 Development ensures that land used for urban purposes is serviced adequately with telecommunications and energy supply.	A011 Development provides land with the following services to the standards of the approved supplier: a. electricity; b. telecommunications services; c. gas service where practicable.	თ	Electrical and telecommunication services are available to service the site. Electrical and telecommunication servicial and telecommunication servicing will be provided in Accordance with Council requirements and agreements with the relevant service providers. Detailed design will be undertaken during the Operational Works stage.	
P012 Development ensures that major public projects promote the provision of affordable, high-bandwidth telecommunications services throughout the city.	Development provides conduits which are provided in all major Council and government works projects to enable the future provision of fibre optic cabling, if: a. the additional expense is unlikely to be prohibitive; or b. further major work is unlikely or disruption would be a major concern, such as where there is a limited capacity road; or c. there is a clear gap in the telecommunications network; or d. there is a clear gap in the bandwidth available to the area. Editor's note—An accurate, digital 'as built' three-dimensional location plan is to be supplied for all infrastructure provided in a road.	თ	The proposed development will be designed to provide for future telecommunications services and providers, in accordance with the relevant Building Codes and Australian Standards.	
Po13 Development provides public art identified in a neighbourhood plan or park concept plan which: a. is provided commensurate with the status and scale of the proposed development; b. is sited and designed: i. as an integrated part of the project design; ii. as conceptually relevant to the context of ii. to reflect and respond to the cultural values of the community; iv. to promote local character in a planned and informed manner.	A013 Development provides public art identified in a neighbourhood plan or <u>park concept plan</u> which is sited and designed in compliance with the public art standards in the <u>Infrastructure design planning scheme policy.</u>	NA	S013 No public art is proposed with these subdivision works.	

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PERFORMANCE CRITERIA	ACCEPTABLE SOLUTIONS	SOLUTIONS1	COMIMENTS	COUNCIL USE ONLY
P014 Development provides signage of buildings and spaces which promote legibility to help users find their way.	A014 Development provides public signage: a. at public transport interchanges and stops, key destinations, public spaces, pedestrian linkages and b. at entries to centre developments; c. which details the location of the key destinations, public spaces and pedestrian linkages in the vicinity, the services available within the development and where they are located. Editor's note—Signage is to be in accordance with Local Law Number 1 (Control of Advertisements Local Law).	O	Signage requirements to be addressed at detailed design stage.	
P015 Development that provides community facilities which form part of the development is functional, safe, low maintenance, and fit for purpose.	A015 Development that provides community facilities which form part of the development is designed in compliance with the community facilities standards in the Infrastructure design planning scheme policy.	NA	S015 No community facilities to be provided at development.	
Pol6 Development provides public toilets which: a. are required as part of a community facility or park; b. are located, designed and constructed to be: i. safe; ii. durable; iii. resistant to vandalism; iv. able to service expected demand; v. fit for purpose.	A016 Development that provides public toilets is designed and constructed in compliance with the public toilets standards in the Infrastructure design planning scheme policy.	6	S016 No public toilets are proposed.	



PERFORMANCE CRITERIA	ACCEPTABLE SOLUTIONS	SOLUTIONS1	COMMENTS	COUNCIL USE ONLY
Po17 Development provides bridges, tunnels, elevated structures and water access structures that are designed and constructed using proven methods, materials and technology to provide for: a. safe movement of intended users; b. an attractive appearance appropriate to the general surroundings and any adjacent structures; c. functionality and easy maintenance; d. minimal whole-of-life cost; e. longevity; f. current and future services. Note—All bridges and elevated and associated elements must be designed and certified by a Registered Professional Engineer Queensland in accordance with the Infrastructure design planning scheme policy.	tunnels, elevated structures and water access structures is designed and constructed in compliance with the standards in the Infrastructure design planning scheme policy.	NA	No bridges, tunnels, elevated structures and water access structures are proposed.	
Po18 Development provides culverts which are designed and constructed using proven methods, materials and technology to provide for: a. safety; b. an attractive appearance appropriate to the general surroundings; c. functionality and easy maintenance; d. minimal whole-of-life cost; e. longevity; f. future widening; g. current and future services; h. minimal adverse impacts, such as increase in water levels or flow velocities, and significant change of flood patterns. Note—All culverts and associated elements are to be designed and certified by a Registered Professional Engineer Queensland in accordance with the applicable design standards	A018 Development that provides culverts is designed and constructed in compliance with the structures standards in the Infrastructure design planning scheme policy.	۸A	No culverts are proposed.	

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DEDECIDAMANCE CRITERIA	ACCEDIARIE COLLITIONS	COLLITIONS	COMMENTS	COLINCILLISE ONLY
P019	A019		8019	
Development provides batters, retaining walls, and seawalls and river walls which are designed and constructed using proven methods, materials and technology to provide for: a. safety; b. an attractive appearance appropriate to the surrounding area; c. easy maintenance; d. minimal whole-of-life cost; (e) longevity; e. minimal water seepage. Note—All retaining walls and associated elements are to be designed and certified by a Registered Professional Engineer Queensland in accordance with the applicable design standards. If for development with a gross floor area greater than 1,000m2	Development that provides batters, retaining walls, seawalls and river walls is designed and constructed in compliance with the structures standards in the Infrastructure design planning scheme policy.	O	Batters and retaining walls will be suitably designed and certified geo-technical engineer by an design approved structural RPEQ at the detailed design stage.	
Development ensures that construction is managed so that use of public spaces and movement on pedestrian, cyclist and other traffic routes is not unreasonably disrupted and existing landscaping is adequately protected from short- and long-term impacts. Note—The preparation of a construction management plan can assist in demonstrating achievement of this performance outcome. Note—The Transport, access, parking and servicing planning scheme policy provides advice on the management of vehicle parking and deliveries during construction.	Development ensures that during construction: a. the ongoing use of adjoining and surrounding parks and public spaces, such as malls and outdoor dining, is not compromised; b. adjoining and surrounding landscaping is protected from damage; c. safe, legible, efficient and sufficient pedestrian, cyclist and vehicular accessibility and connectivity to the wider network are maintained.	O)	Construction operations will be managed in accordance with the relevant planning scheme policies and guidelines. A Construction Management Plan will be provided by the contractor prior to commencement of site works.	

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	ACCEDIABLE COLLITIONS	POINCITI I CO		
FORMANCE CRITERIA	ACCEPTABLE COLLITIONS	COLLITIONIC4		
	ACCEPTABLE SOLUTIONS	SOLUTIONS	COMMENTS	COUNCIL USE ONLY
_	A021.1		5021.1	
olition	Development ensures that demolition and	6	Construction and demolition works will occur	
	construction:		during work times in accordance with the	
	a. only occur between 6:30am and 6:30pm		relevant planning scheme policies and guidelines.	
a sensitive use, due to noise and dust, including dust from	Monday to Saturday, excluding public		A Construction Management Plan will be	
construction vehicles entering and leaving the site.	holidays;		provided prior to commencement of site works.	
	b. do not occur over periods greater than 6			
Note—A noise and dust impact management plan	months.			
prepared in accordance with the Management plans	A021.2		S021.2	
strating	Development including construction and	6	Appropriate dust suppression will be provided for	
achievement of this performance outcome.	demolition does not release dust emissions		the duration of construction and demolition	
)q	beyond the boundary of the site.		works in accordance with the relevant planning	
			scheme policies and guidelines. A Construction	
			Management Plan will be provided prior to	
			commencement of site works.	
V	A021.3		\$021.3	
	Development construction and demolition	6	Asbestos is not expected to exist on the site. If	
p	does not involve asbestos- containing		found to occur it will be removed in accordance	
<u>u</u>	materials.		with the appropriate handling and removal	
			procedures prior to demolition works	
			commencing.	
P022 A0	A022		5022	
Development ensures that:	Development ensures that the nature and	6	Construction operations are not expected to	
a. construction and demolition do not result in damage sc	scale of construction and demolition do not		result in vibration levels that can damage	
to surrounding property as a result of vibration;	generate noticeable levels of vibration		surrounding properties. Vibration from site	
b. vibration levels achieve the vibration criteria in Table			works will be managed in accordance with the	
9.4.4.3.B, Table 9.4.4.3.C, Table 9.4.4.3.D and Table			relevant planning scheme policies and guidelines.	
<u>9.4.4.3.E.</u>			A Construction Management Plan will be	
Note—A vibration impact assessment report prepared in			provided prior to commencement of site works.	
accordance with the Noise impact assessment planning				
this norformance + this normal training achievement of				
uns periorniance				

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