

MIRVAC

ROL10 - Precinct 8 & 10, Everleigh

ENGINEERING SERVICES REPORT

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PLANS AND DOCUMENTS referred to in the PDA **DEVELOPMENT APPROVAL**

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1. INTRODUCTION

Premise was commissioned by Mirvac to prepare an Engineering Services Report for Precincts 8 & 10 of the Everleigh development. Everleigh is located at Teviot Road, Greenbank and is part of the Priority Development Area (PDA) with EDQ being the assessing authority.

The proposed development consists of Precinct 8 and Precinct 10. The breakdown of the two Precincts are as below;

- Precinct 8 consists of 286 residential lots, linear parks and roadways situated over an approximate residential area of 17.1ha, 44.4ha of parks and 2.7ha of WSUD and SPS areas. Precinct 8 will be split into four (4) residential, seven (7) park and one (1) sewage pump station sub-precincts to accommodate staged delivery. The precinct masterplan and sub-precinct split-up can be seen in the below Figure 1.1.
- Precinct 10 consists of 280 residential lots, linear parks and roadways situated over an over an approximate residential area of 18.1ha and 13ha of parks. To accommodate staged delivery, Precinct 10 will be split into five (5) residential and two (2) park sub-precincts. The Precinct 10 masterplan and sub-precinct split-up can be seen in the below Figure 1.1.

The Precinct 8 and Precinct 10 Masterplan Layouts, prepared by Urbis, can be seen in Appendix A.

This report addresses the engineering services that will be required to service the proposed development of Precinct 8 and Precinct 10, examining the development at an 'as if complete' conceptual level for Development Approval. This report should be read in conjunction with the reports provided by Urbis (Town Planning).





Figure 1.1: Precinct 8 and Precinct 10 layout & sub-precinct split

2. SITE CHARACTERISTICS

Precincts 8 and 10 have an approximate combined area of 43.83 ha and are located to the north of Future Precinct 6, Existing Precinct 9 and the school parcel. Precinct 10 adjoins the future development precinct 11 on its Western boundary and the existing Precinct 9 on its southern boundary.

The natural surface topography across Precinct 8 and 10 includes a depression running West to East, flanked by a ridge line on either side, with maximum grades of up to 7%.

An area of Precinct 8 and 10 has been altered by the Precinct 9 earthworks package that is being constructed under previous approvals. The Precinct 8 and 10 bulk earthworks operation will finalise the earthworks levels across the subject site.

A portion of the subject site area is situated over land which has previously had vegetation cleared due to borrow areas for the earthworks in Precinct 9. Vegetation clearing will be required over the balance of the subject site area to accommodate development.

The proposed site location in context with the Everleigh development can be seen in the figure below.





Figure 2.1: Site Location



3. DATA

Data for this report has been gathered from the following sources:

- Urbis Townplanners Lot layout
- Economic Development Queensland (EDQ) Greater Flagstone Priority Development Area plans and documents;
- Saunders Havill Group Detail Survey;
- Approved (EDQ) MWH Global Movement Network Infrastructure Master Plan;
- Approved (EDQ) MWH Global Sewer and Water Master Plan;
- Logan City Council Existing services location (where applicable and relevant) and Planning Scheme 2015 development information; and
- Dial Before You Dig.
- ATP Consulting Engineers 'Traffic Noise Impact Assessment, Everleigh Green Bank, RoL Application
- Stormwater technical letter 'RE: Everleigh Precinct 8 Stormwater Detention and Water Quality Analysis' prepared by Engeny



4. SERVICES FOR DEVELOPMENT

4.1 EARTHWORKS

Earthworks will be required to facilitate the construction of the roads, allotments and parks proposed within Precinct 8 and 10. The earthworks will consist of excavations, filling, permanent batters to existing surface level with maximum slope of 1 in 4 and batters between lots with a maximum slope of 1 in 2. Retaining walls will be constructed during civil works to provide level allotments. All retaining wall heights are less than or equal to 2.5m in height.

A preliminary 'as if complete' earthworks design has been carried out over the ROL10 area. While the target for the earthworks design was to minimise the cut and fill volumes associated with the earthworks operation along with targeting a cut to fill volume balance, there were several constraints that needed to be considered which influenced levels. These constraints included:

- Interface to natural surface levels and adjoining developed precincts
- Road Gradings
- Benching of allotments
- Relationship between benched allotments and retaining walls
- Coordination with landscape design in linear parks and pedestrian lanes
- Access and disability grades along footpaths
- Stormwater drainage outlet and channel levels

The preliminary earthworks design for the site has identified that the overall earthworks cut and fill volumes result in the requirement to source material from a location outside Precinct 8 and 10 to meet the fill material volume requirements. Additional material will be sourced from a borrow area in Precinct 6 to meet the requirements.

Vegetation clearing will be required to allow earthworks operations to commence. Additional clearing beyond the earthworks extent will be required to accommodate the recommendations of the Bushfire Hazard Assessment and Fire Management Plan.

The proposed earthworks design and extent can be seen on the Preliminary Earthworks Sketch Plans Provided in Appendix B.



4.2 EROSION & SEDIMENT CONTROL

Erosion and Sediment Control (ESC) measures will be required during all stages of development from site establishment to project completion. An Erosion and Sediment Control program will be designed and detailed during the detailed design phase.

4.3 ROADWORKS

Vehicle access to Precinct 10 will be gained via the northern leg of the Anderson Drive / Guroman Drive roundabout constructed in Precinct 9. The northern leg will be formed by Unnamed Road 073, a future neighbourhood connecter road. Precinct 8 will subsequently be accessed through Precinct 10 via Unnamed Road 073.

4.3.1 INTERNAL ROADS

The road layout within Precinct 9 has been developed in accordance with the road typologies nominated in the approved Movement Network Infrastructure Master Plan (MNIMP). The roads servicing the Precincts 8 & 10 include:

- Unnamed Road 073 Neighbourhood Connector 2; and
- All other roads Access Street, Typical and Park types.

A Road Hierarchy Plan showing the above road typologies located within the precincts can be seen in Appendix C.

All allotments can be accessed from the proposed internal road network via direct driveway access or the dedicated driveway access reserves provided. The proposed roads will be provided with concrete kerb and channel, 1.5m minimum width concrete footpaths or shared paths and minimum 4m wide verges which accommodate necessary service corridors as required by Logan City Council.

Internal Road Functional plans detailing the Precinct 8 & 10 internal road network can be seen in Appendix D.



4.4 NOISE ATTENUATION

A traffic noise impact assessment has been undertaken by ATP Consulting Engineers (ATP). ATP undertook traffic noise propagation modelling to consider the future traffic flows for a planning horizon of 2051. Based on the results of the traffic noise impact assessment for the ROL 10 (Precincts 8 and 10) of the Everleigh development, the following is concluded:

- Teviot Road does not affect the noise amenity at the allotments within ROL 10 (Precincts 8 and 10).
- Anderson Drive has limited noise impact on the allotments at ROL 10 with only Lot 4001, within
 Precinct 10, impacted by traffic noise. The traffic noise impact is limited to the upper floor of twostorey (high-set) house.
- In accordance with the noise control strategy for the Everleigh development, the upper floor of any
 two-storey house at Lot 4001 must be subject of design and construction in accordance with QDC
 MP4.4 or AS3671-1989 to ensure compliance with the internal noise criteria from AS/NZS 2107:2016.
 In addition, the outdoor living area of any house at Lot 4001 must be located along the façade which
 has no direct view to Anderson Drive.
- If the private open space of the house to be constructed at Lot 4001 is located along the protected northern façade (facing away from the road), or in a protected courtyard recessed into the side of the buildings, compliance with the traffic noise criterion will be achieved.
- All the other allotments with ROL 10 (Precincts 8 and 10) of Everleigh development are not affected by road traffic noise and the houses on these allotments do not require acoustic design to be facade.

ATP Engineers have stated within their Traffic Noise Impact Assessment Everleigh, Greenbank ROL10 Application report 'Provided the recommended planning and design noise control measures are implemented in the construction of Everleigh development ROL 10, road traffic noise will not impose any further constraints on the establishment of this stage of the development.'

Refer to ATP Consulting Engineers 'Traffic Noise Impact Assessment, Everleigh Green Bank, RoL Application' report attached as part of the application documentation for further information.

4.5 TRAFFIC

A Traffic Impact Assessment has been prepared which addresses the suitability of the proposed Precinct 8 and 10 site layout and road typologies, and determines traffic volumes in accordance with overall site data. The Traffic Impact Assessment provides confirmation of the above items with consideration to relevant guidelines, standards, and approved documents.

The Traffic Impact Assessment can be seen in Appendix E.



4.6 STORMWATER DRAINAGE

The proposed piped underground drainage, roofwater drainage and major storm overland flow for this site will be designed in accordance with EDQ Guideline 13, Logan City Council and QUDM stormwater design guidelines. It is proposed that a network of underground pipes and gully pits will be constructed to capture and convey stormwater collected from allotments and roadways towards a new Bio-Basin and Detention Basin at the North-Eastern Corner of Precinct 8 as well as via the existing main in Precinct 9.7 to the Bio-Basin and wetland South of the School Reserve. The existing Bio-basin has been sized to cater for the additional catchment areas from Precinct 8 and 10.

The major storm overland flows generated from the Precinct 8 and 10 catchments will be contained in the road reserves and are also conveyed towards existing precincts. Roadways in the existing Precincts 6 and 9 have been designed to accommodate these flows.

There are 2 defined overland flow paths in Precinct 8, a pedestrian link and that runs through the centre of the site and a pedestrian link/ driveway that is adjacent to and joins a flow path in Precinct 9.7, which has been designed to accommodate the additional overland flow.

Refer to the Preliminary Stormwater Drainage Plans provided in Appendix F for further details.

4.7 STORMWATER QUANTITY & QUALITY

The quantity management of Precinct 8 and 10 stormwater flows will be accommodated in a combined stormwater detention and treatment basin located to the north of Precinct 8. Stormwater quality management for the combined catchment will be treated through the use of a sediment pond and bioretention system.

Details on the proposed Stormwater Quantity and Quality treatments proposed for this precinct are provided within the stormwater technical letter 'RE: Everleigh Precinct 8 – Stormwater Detention and Water Quality Analysis' prepared by Engeny. This stormwater technical letter outlines the water quantity and quality analysis undertaken in support of the Reconfiguration of a Lot (ROL) submission for Precinct 8, 10 and a small portion of Precinct 11 of the Everleigh development.



4.8 SEWER RETICULATION

All proposed residential allotments within Precinct 8 and 10 will be provided with a sewer property service. Property services will be connected to a sewer reticulation pipe network located in the road verge. The sewer reticulation network will be designed and installed in accordance with SEQ D&C Code, Logan City Council requirements and Premise prepared whole of site sewer design master plan.

There are three (3) sewer catchments within the ROL area and are generally described below

- Catchment A Area serviced by gravity mains through Precinct 9 that drain to the south to the GB2 Regional pump station
- Catchment B Serviced by a gravity sewerage system draining to SPS C located in the Central Northern section of Precinct 8.
- Catchment C Area serviced by a gravity main (to be completed as part of these works) which is in future Precinct 6 and discharges into a constructed temporary sewage pump station located in future Precinct 6. This constructed temporary pump station then discharges by an existing rising main into the GB2 Regional pump station.

A summary of the Catchment demands is provided in the table 4.8.1 below and references the Premise Preliminary Sewer Catchment Plan is located in Appendix G

Table 4.8.1

Catchment	Unit	EP / Unit	Total EP
Catchment A			
Precinct 8	-	3 EP per Lot	O EP
Precinct 10	166 Lots	3 EP per Lot	498
Total	166 Lots	3 EP per Lot	498
Catchment B			
Precinct 8	288 Lots	3 EP per Lot	864
Precinct 10	101 Lots	3 EP per Lot	303
Future	58 Lots	3 EP per Lot	174
Total	447 Lots	3 EP per Lot	1,341
Catchment C			
Precinct 8	-	3 EP per Lot	0
Precinct 10	11 Lots	3 EP per Lot	33
Future*	-	3 EP per Lot	0
Total	11 Lots	3 EP per Lot	33
TOTAL OVERALL	624 Lots	3 EP per Lot	1,872

Note* - The future residentials have been included for the sizing of the SPS and downstream gravity main systems. These future lots will be completed as part of a future ROL approval.

CATCHMENT A

These catchment uses two previously planned gravity sewer main connections through Precinct 9. The locations of these connections are presented in the Preliminary Sewer Reticulation Plans in Appendix H. There is sufficient capacity within the downstream networks for this catchments demand.



CATCHMENT B

This catchment is serviced using a sewage pump station which then discharges into a constructed manhole in Precinct 9. The sizing of the sewage pump station is below

The demand on the SPS C is summarised in the table 4.8.2 below

Table 4.8.2

Category	Unit	EP / Unit	Total EP	Total ADWF	Total PWWF
Residential	447 Lots	3 EP per Lot	1,341	3.10 L/s	15.52 L/s

Note, A residential lot average day weather flow (ADWF) of 200L/EP/Day and peak wet weather flow (PWWF) of 1000L/EP/Day were adopted in accordance with the Logan Water Alliance Desired Standards of Service (DSS) April 2014

A summary of the wet well sizing is shown in the table below. The required operation storage of the wet well was calculated as 1.16m³ a wet well diameter of 2m was adopted. Using the preliminary sewer design Due to the incoming sewer invert level of 42.70m and the surface level of 48m the calculated depth of the wet well was 7.07m.

Table 4.8.3

Wet Well Details	Value
Capacity (PWWF) (L/s)	15.52
Operating Storage (m³)	1.16
Wet Well diameter (m)	2
Operating Depth (m)	0.37
Surface Level (m)	48.00
Incoming Invert Level (m)	42.70
Alarm RL (m)	42.55
Standby RL (m)	42.25
Pump TWL RL (m)	42.10
Pump BWL RL (m)	41.73
Floor Level RL (m)	41.33
Wet Well Depth (m)	7.07
Emergency Storage Time	4 hours at ADWF of 3.10L/s
Total Emergency Storage Volume Required (m³)	44.7
Emergency Storage in Wet Well (Above Alarm Level) (m³)	17.12
Additional Emergency Storage Required (m³)	27.58

A summary of the SRM sizing calculations is shown in the table 4.8.4 below. An DN180 PE100 DR11 pipe will have a suitable velocity of 0.94/s with a PWWF of 15.52L/s. The duty point of the pump station was calculated as 15.52 L/s at 17,8m. Preliminary design plans for the Sewage Pump Station and rising main are attached with the Preliminary Sewer Reticulation Plans in Appendix H.



Table 4.8.4

	Value
PWWF	15.52 L/s
Length of SRM	867.6
Pipe Type	PE100 DR11
Nominal Size	DN180
Internal Diameter (mm)	145
Area (m²)	0.017
Velocity (m/s)	0.94
C value	130
Friction Head (m)	6.10
Low point (Pump BWL) (m)	41.73
High point (m)	53.42
Static Head Requirement (m)	11.69
Total Pump Head (m)	17.79
Pump Duty Point	15.52 L/s at 17.79m

Note. The Option 2B alignment has been used for these calculations.

The detailed design submission for pumping infrastructure and the receiving system shall be accompanied by the Odour Impact Assessment Report. This Impact Assessment shall address the odour impacts at the air discharge of associated gravity mains at the SPS location, the operation of the SPS, at the rising main discharge point to the downstream gravity network, and gas release valve arrangements.

We have anticipated that the sewer rising main discharge manhole will be designed to meet the WSA 04 – 2005-2.1. On this basis the discharge manhole will be protected against corrosion using corrosion resistant materials and that an addition vent pole will not be required.

Three rising main alignment options were assessed to determine the preferred alignment for the development. These alignments are described below

Option1

- The alignment followed the northern park area before turning perpendicular into the development to the discharge point.
- This alignment kept the majority of the rising main away from the residential area.

Option2 (A&B)

- The Option 2 alignment takes a more direct route to the discharge point.
- This alignment does take the rising main through the residential area for all but a small section.
- The difference between Option 2A and Option 2B is the vertical grading.

The rising main alignments are included in the Premise Sketch MIR-1000-SKC65 attached in Appendix H



An assessment of the grading, construction phasing and overall costs was undertaken with the general comments for each alignment below Option 1

- a) A concern raised for this alignment was the high point along the alignment which required an air valve. This high point is required to prevent excessive depths.
- b) A scour valve is required for this alignment to go under a stormwater pipe
- c) There is a construction phasing constraint with the rising main alignment being through three precinct 8 sub-precincts. This will result in the rising main being constructed and then the finishing civil works occurring at a later stage.

Option 2A

- a) It has a reduced length as it is a more direct route to the discharge point
- b) There is a high point located in the park area which is the location for an air valve. This is due to the site contours and the vertical grading of the main to prevent clashes with a number of stormwater pipes.
- c) A scour valve is required for this alignment to go under a stormwater pipe

Option 2B

- a) Option 2B has the same horizontal alignment as option 2A however the vertical grading is amended.
- b) The vertical grading for the rising main has been lifted so that it goes above the stormwater infrastructure at approximate chainage 400. This vertical grading changes results in there not being a need for either an air or scour valve.
- c) The vertical grading of the sewer results in it being above the stormwater which does not conform with the SEQ code. With the use of the rising main PE material and being encased inside an RCP pipe assists in elevating the concerns of having a sewer above stormwater.

Verdict

While option 2B doesn't conform directly with the SEQ Code, it provides a lot of benefits over the other two options. The most significant benefit is the alignment not requiring either an air or scour valve. Further we have engaged with Logan Water and this alignment is preferred. It is recommended that Option 2B is progressed further into the detail design phase.

CATCHMENT C

The small demand from Catchment C will discharge via the constructed sewer gravity main along Anderson Road to this sewage pump stion.

The constructed sewer gravity main on Anderson Drive and the constructed Temporary sewage pump station have been completed under previous approvals. References to these approvals are

- Temporary sewage pump station, Approval Number DEV/2018/999/7 dated 21 April 2020
- Gravity sewer main in Anderson Drive, Approval Number DEV/2018/999/10 dated 15 December 2020

Copies of the approved drawings for both the constructed temporary sewage pump station and constructed gravity main are attached in Appendix I.



There is an additional capacity of 53 EP within the constructed temporary sewage pump station (SPS) provided to service the Everleigh School site. This additional capacity was to be used for other functions. The demand from Catchment C referred in Table 4.8.1 is 33 EPs which is within the remaining capacity of this temporary sewage pumpstation. Logan City Council is supportive of using the remaining capacity of this temporary sewage pumpstation to service residential lots. A copy of this support from Logan Water is attached in Appendix J.

The details described above sewer reticulation system are shown on the Preliminary Sewer Reticulation Plans in Appendix H.

4.9 WATER RETICULATION

All proposed allotments in Precinct 8 and 10 will be provided with a potable water service connection. A water reticulation pipe network will be provided in Precinct 8 and 10 to provide service connections to each allotment. The water reticulation network will be designed and installed in accordance with the SEQ D&C Code, Logan City Council requirements and the approved Water Supply Network Modelling Report prepared by Premise.

Precincts 8 and Precinct 10 will be serviced from the boosted Round Mountain Water Service Zone which is distributed via the existing 300mm diameter trunk water main located in Teviot Road adjoining the Everleigh site. Two (2) existing connections to the 300mm diameter main were installed with Precinct 1 and Precinct 9 respectively and currently services the Everleigh development.

The details described above are shown on the Preliminary Water Reticulation Plans in Appendix K.



4.10 ELECTRICITY, LIGHTING, TELECOMMUNICATIONS & GAS

Electrical, telecommunication, and gas services exist in previous precincts adjacent to the boundary of the proposed site, have enough capacity for the electrical demands that are proposed to be generated by Precinct 8 and 10.

Details of these will be confirmed during the operational works phase and will be designed in accordance with the relevant service provider requirements.

An electrical servicing statement prepared by Robin Russell has been provided in Appendix L.



5. **CONCLUSION**

Based on the information collected and preliminary investigations carried out it has been established that the proposed development can be adequately serviced.

All service and infrastructure layouts are generally in accordance with the relevant approved infrastructure master plans, EDQ requirements, and other relevant and appropriate design standards and guidelines.



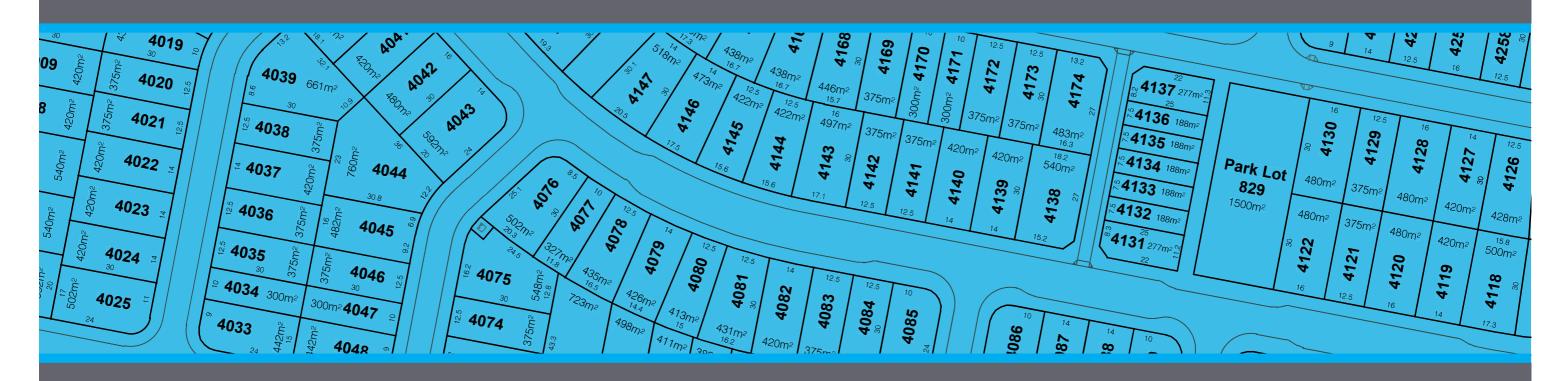
A.1 APPENDIX A – MASTERPLAN LAYOUT

Everleigh

ROL 10: RECONFIGURATION OF A LOT PLANS

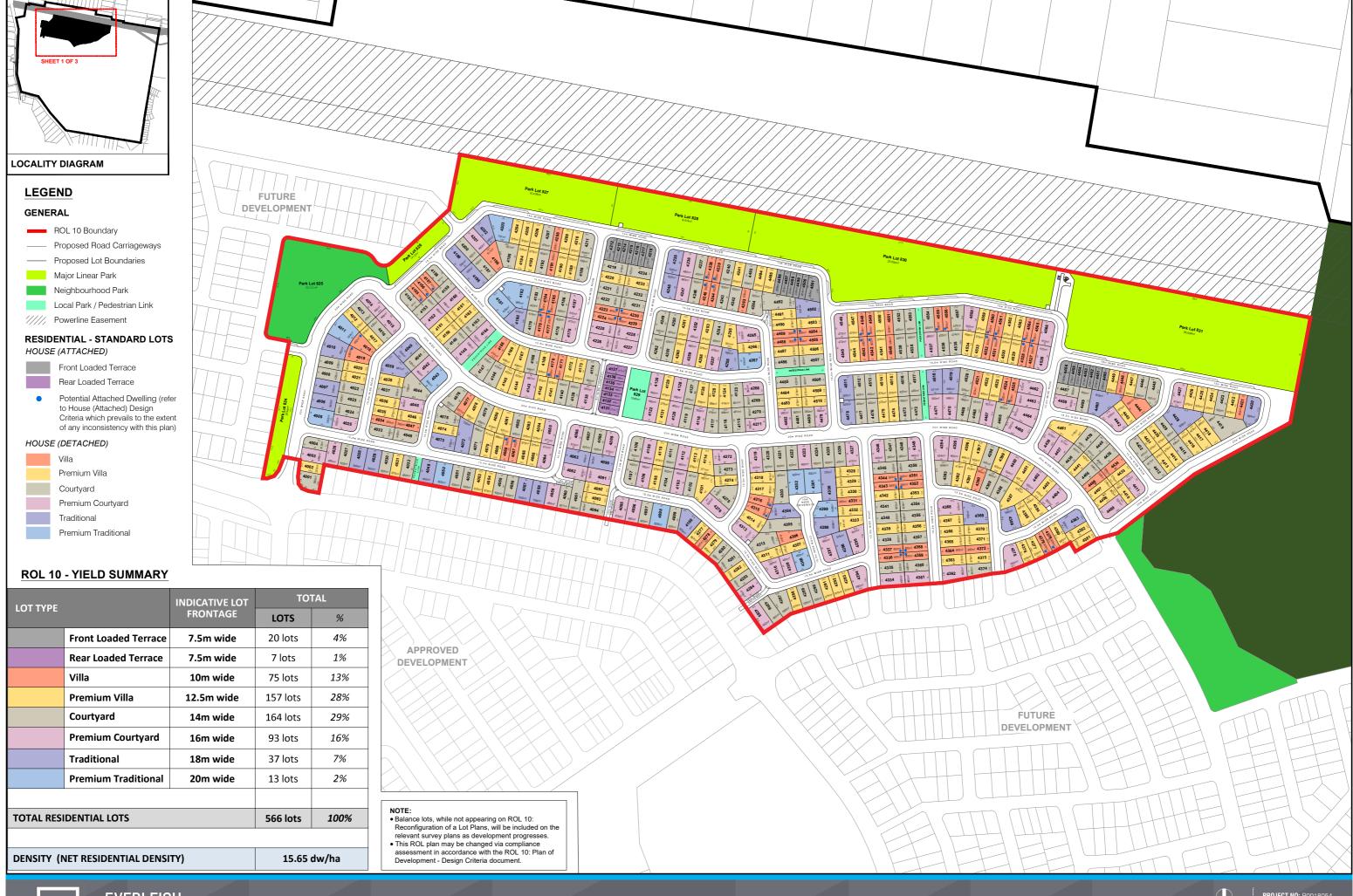
TEVIOT ROAD, EVERLEIGH

JULY 2022





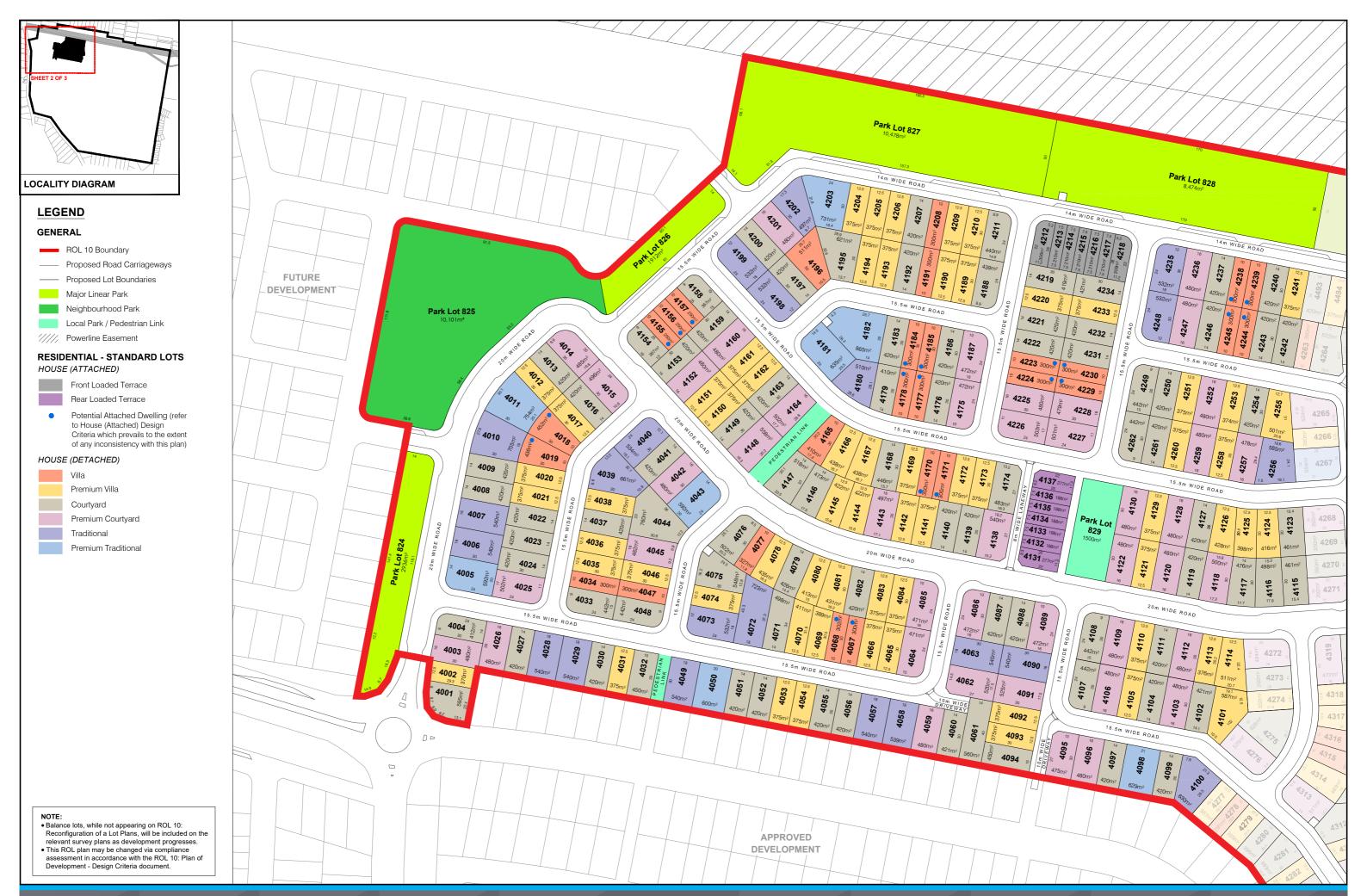




URBIS

EVERLEIGH

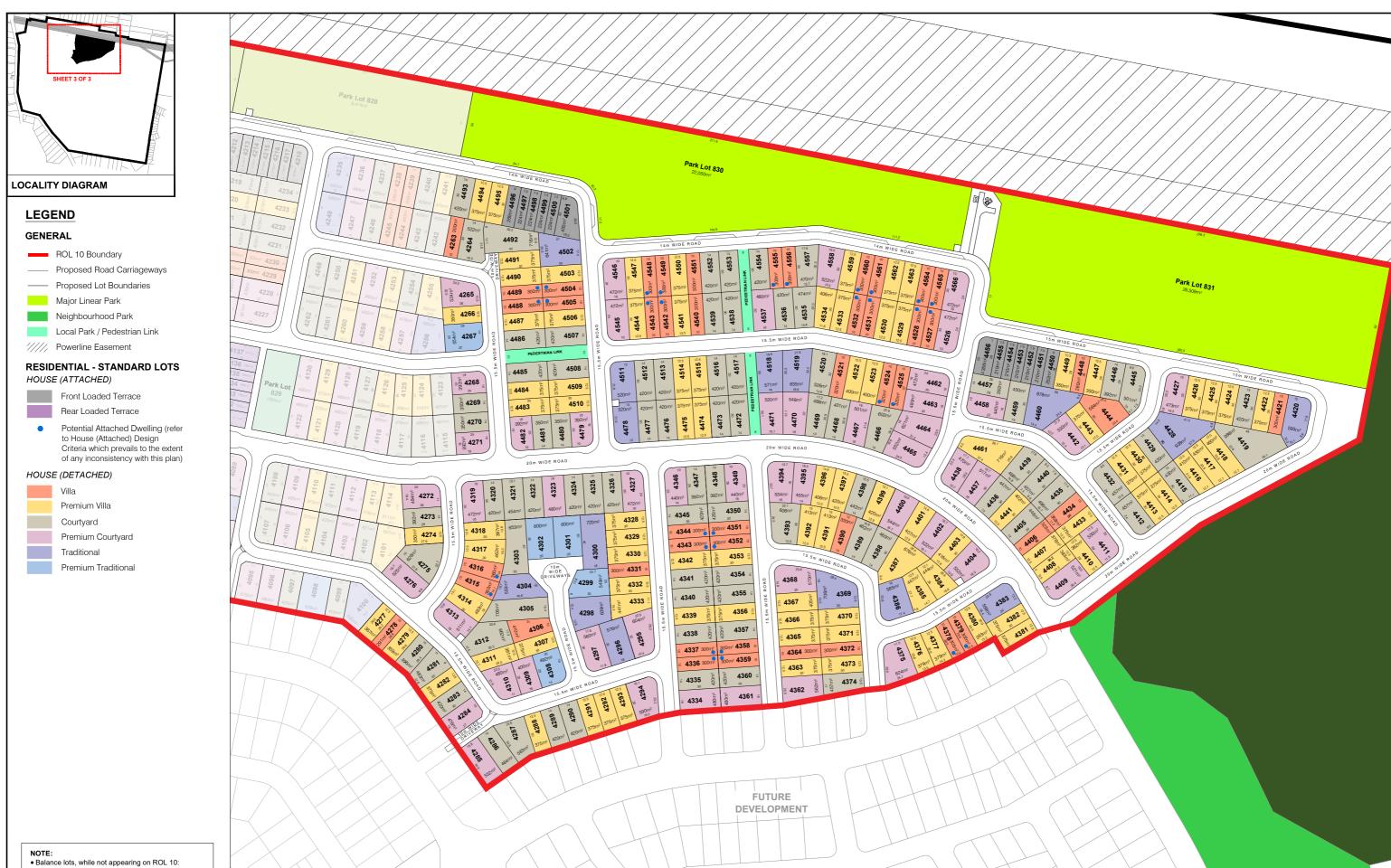
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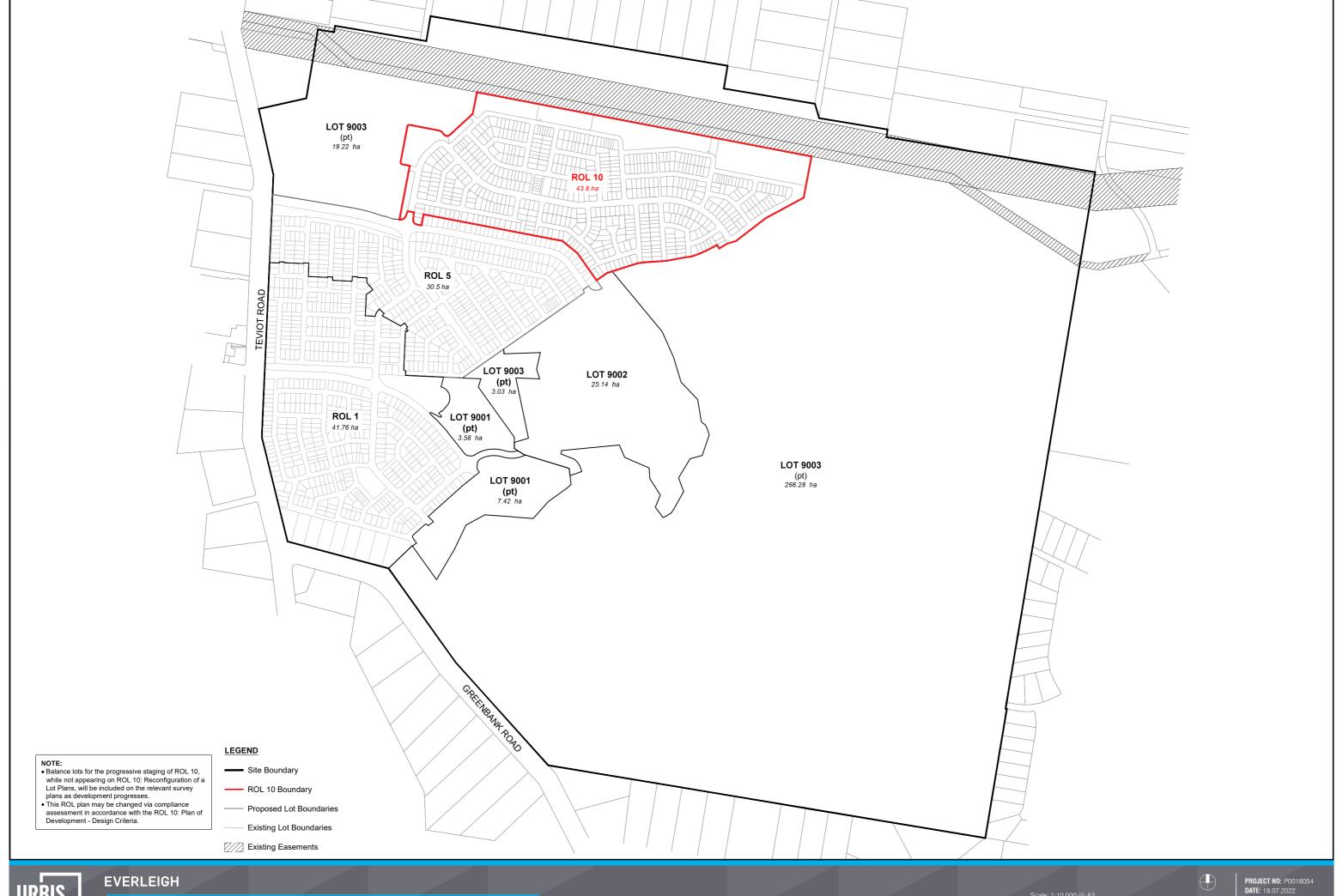
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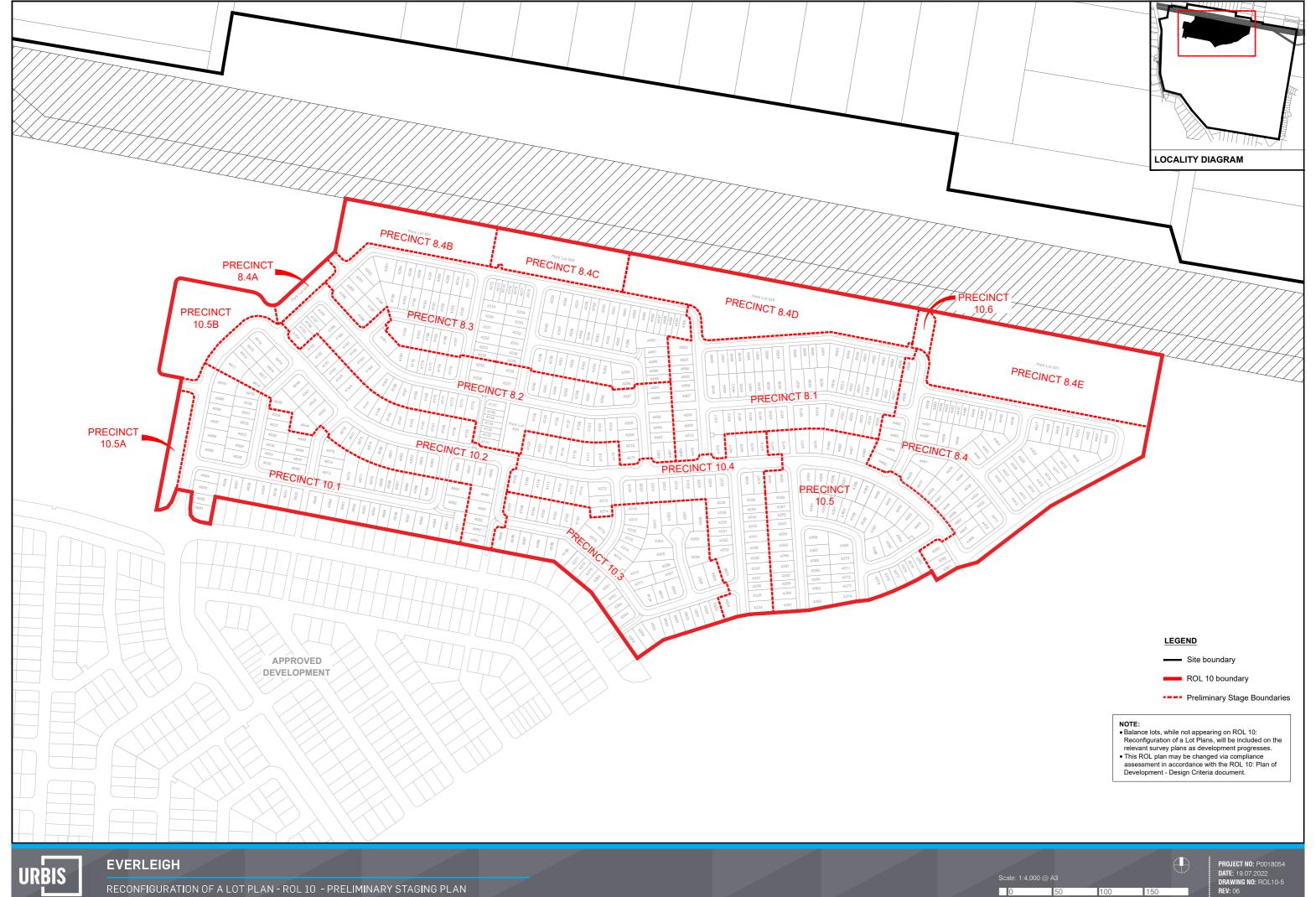
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- Reconfiguration of a Lot Plans, will be included on the relevant survey plans as development progresses.
- This ROL plan may be changed via compliance assessment in accordance with the ROL 10: Plan of Development - Design Criteria document

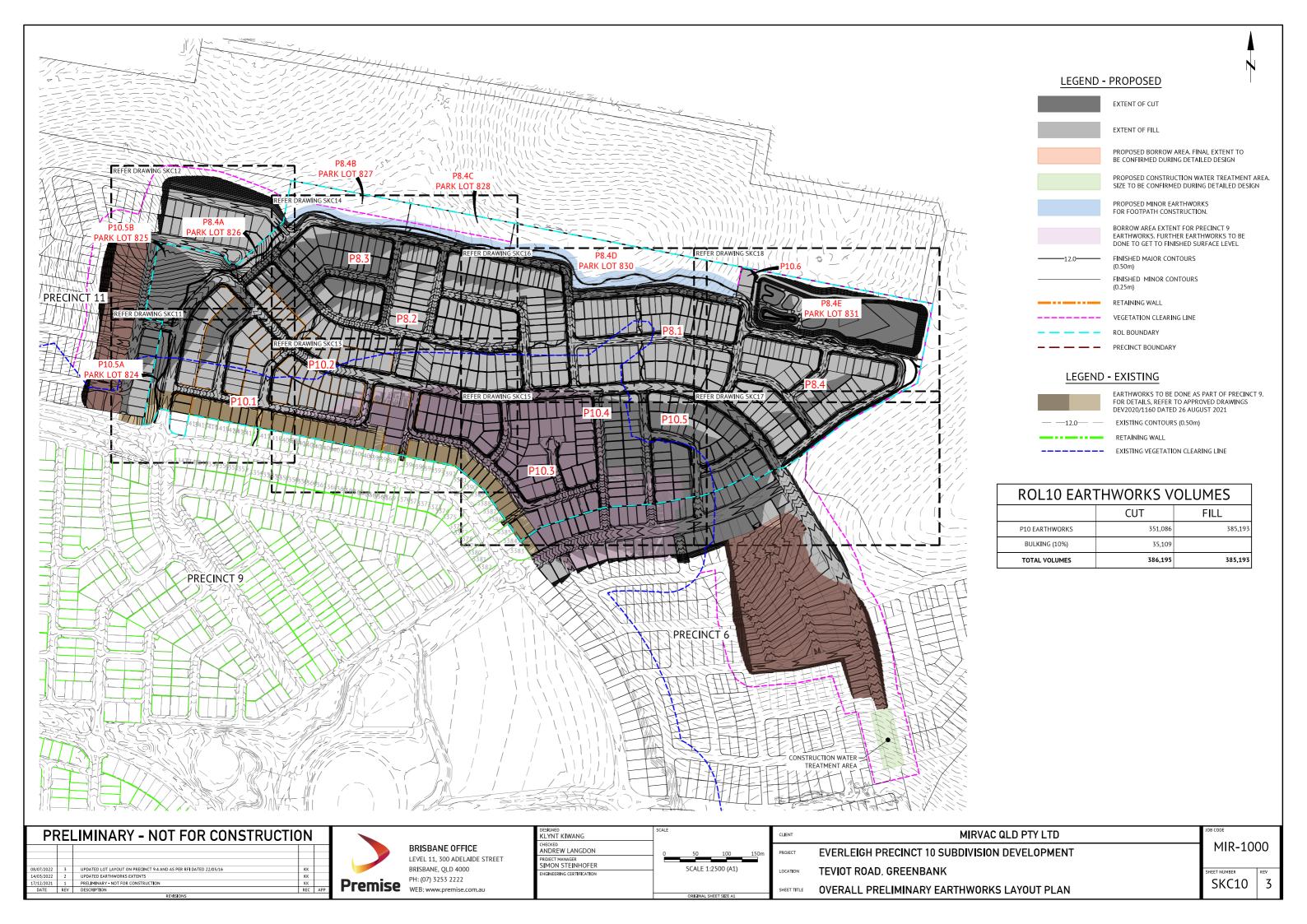
EVERLEIGH

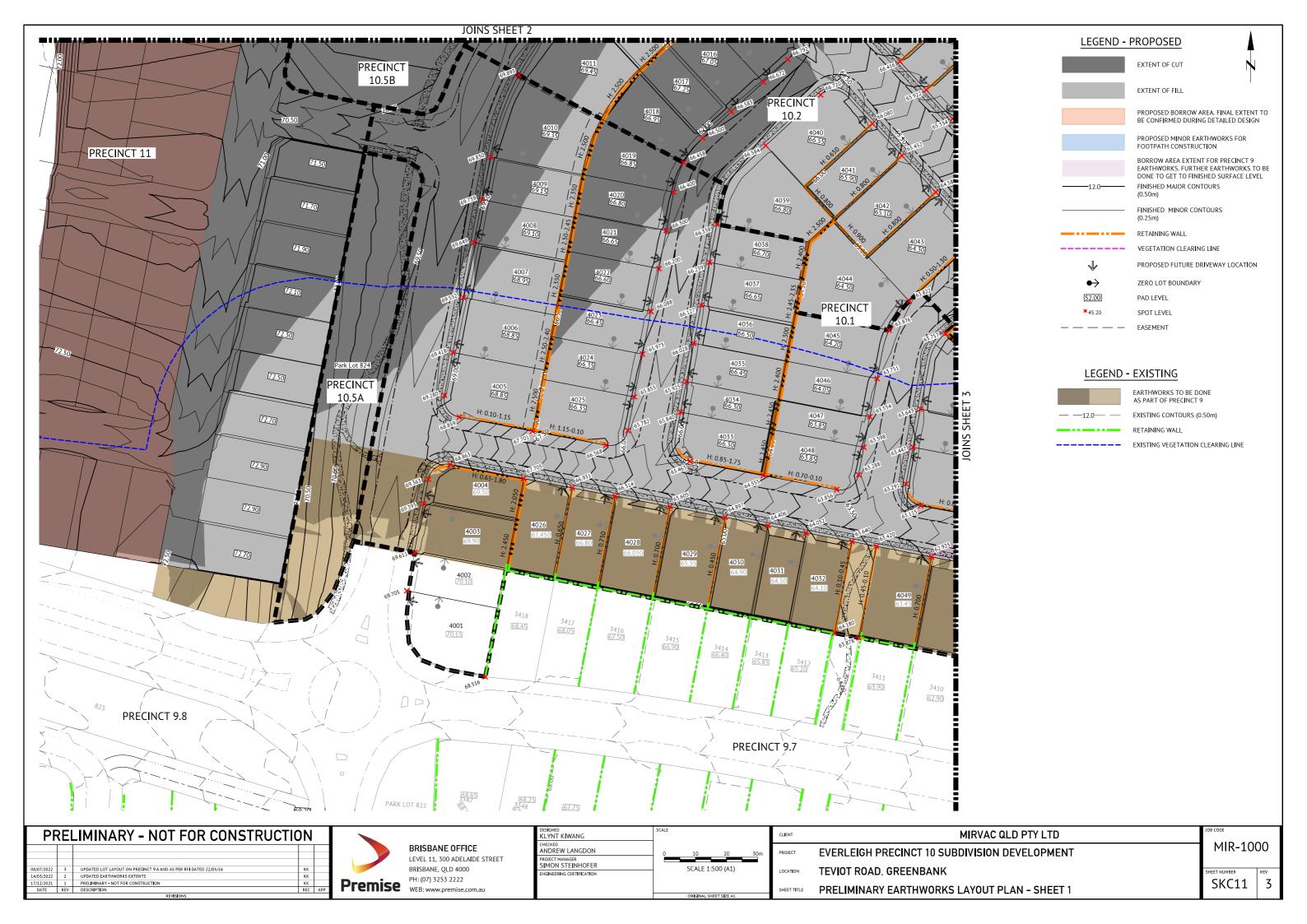


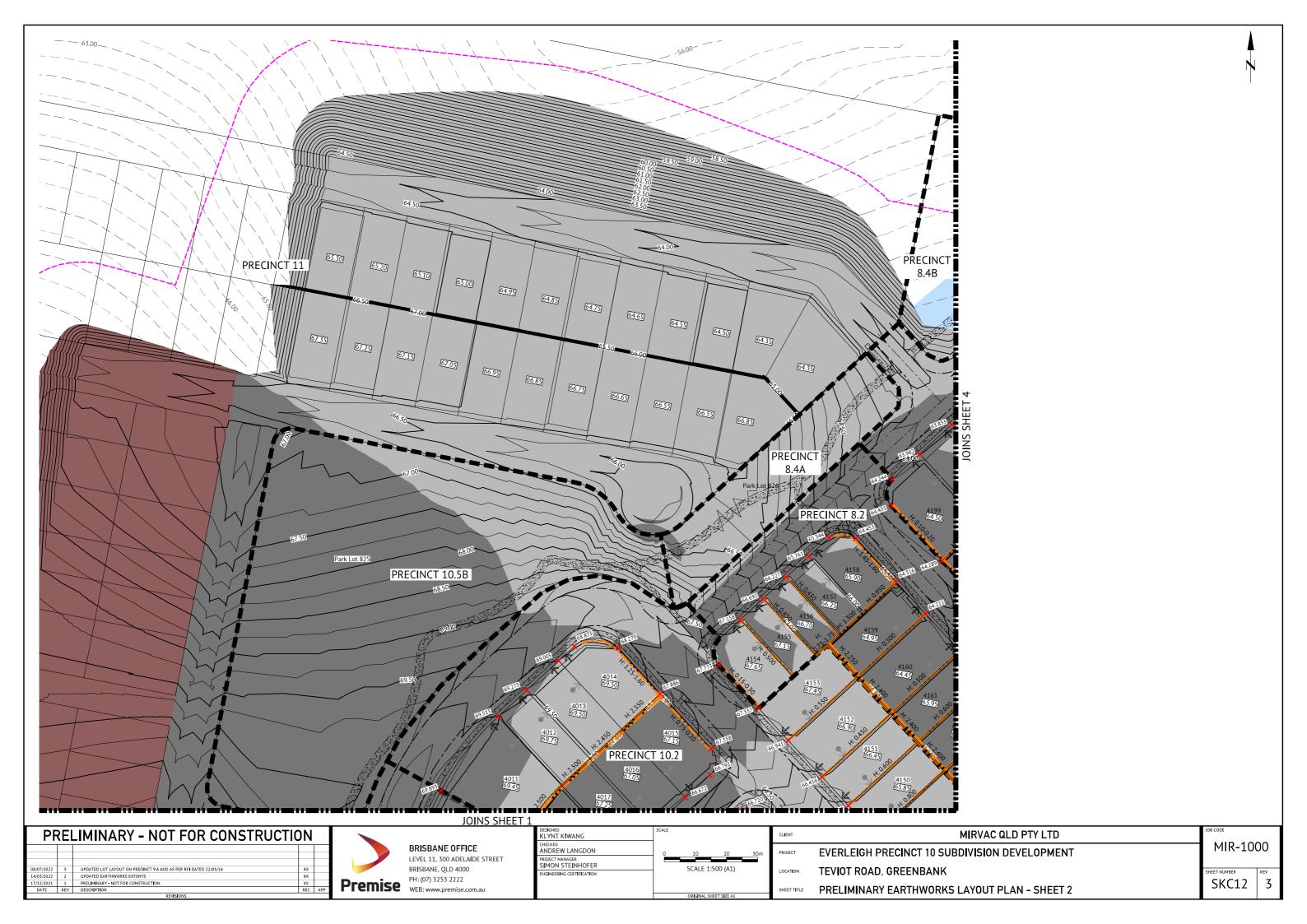


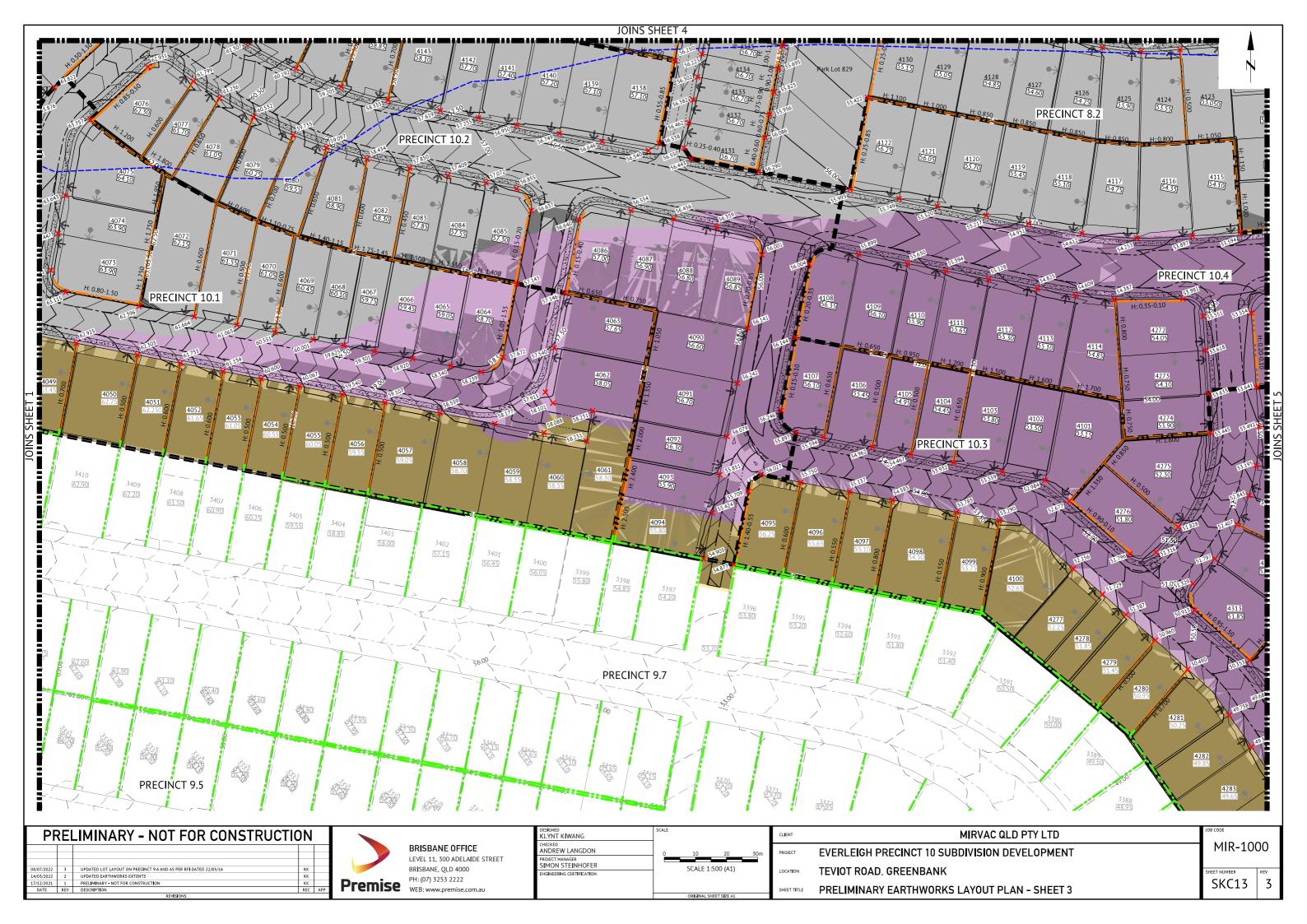


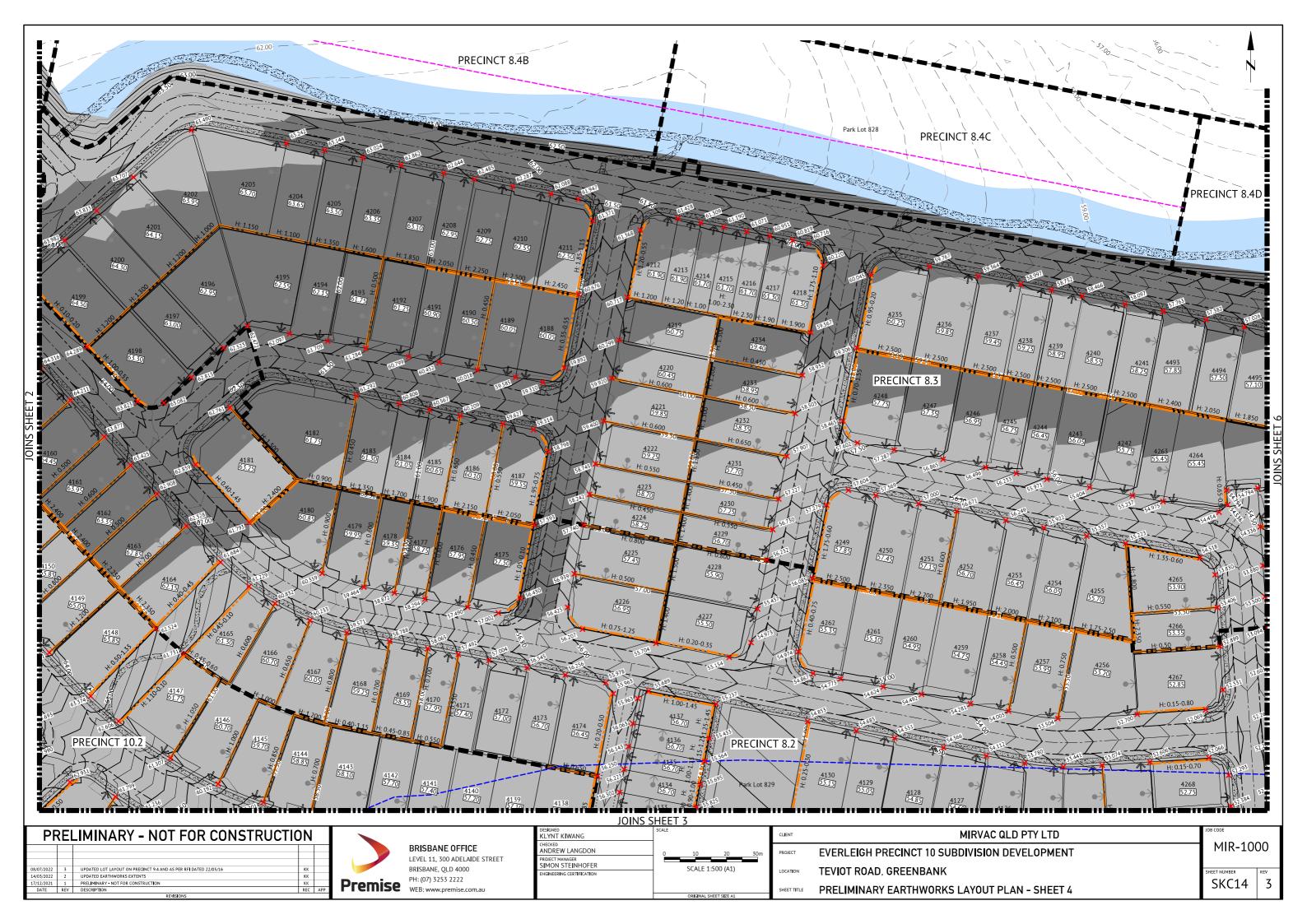
A.2 APPENDIX B – PRELIMINARY EARTHWORKS PLANS

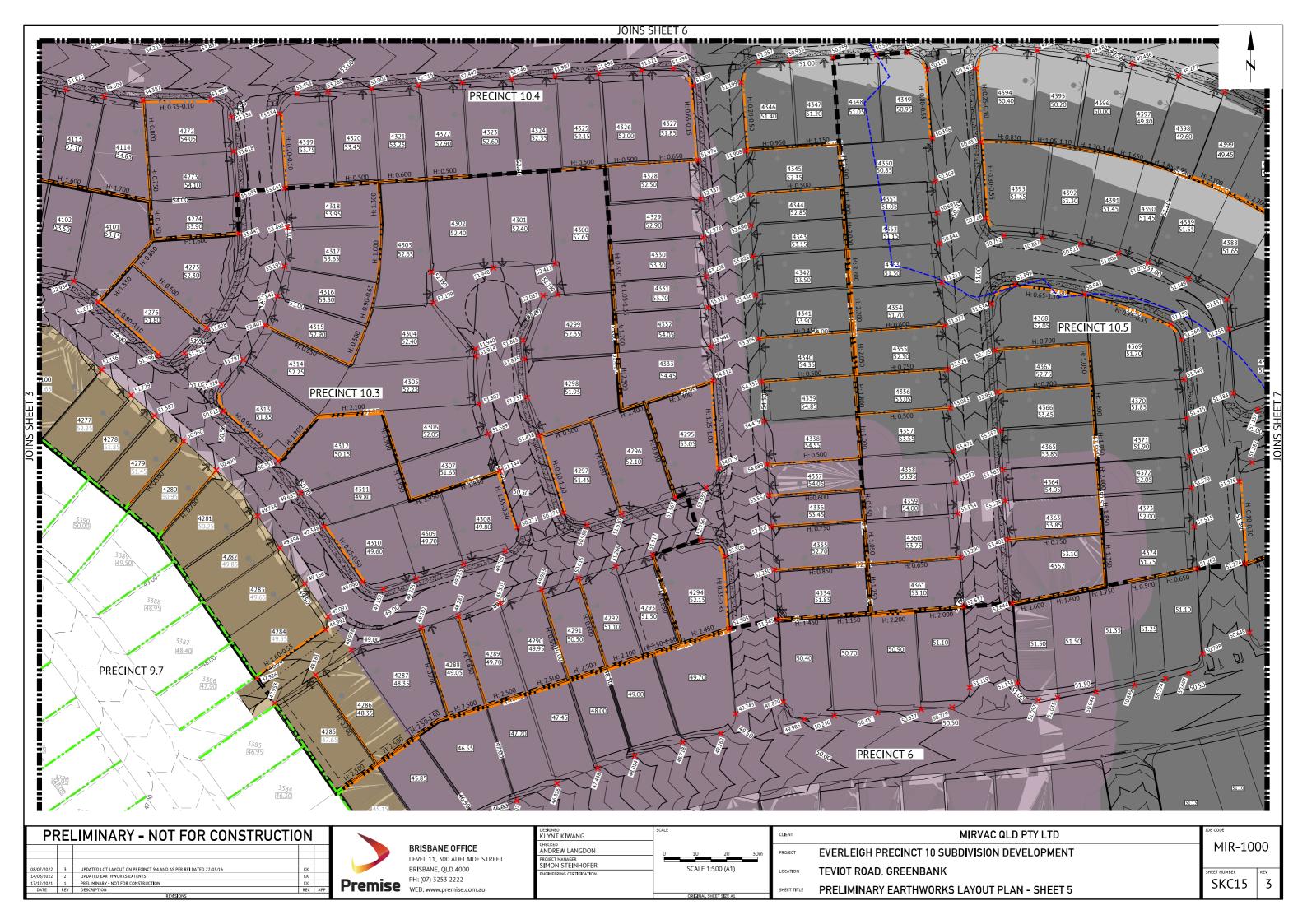


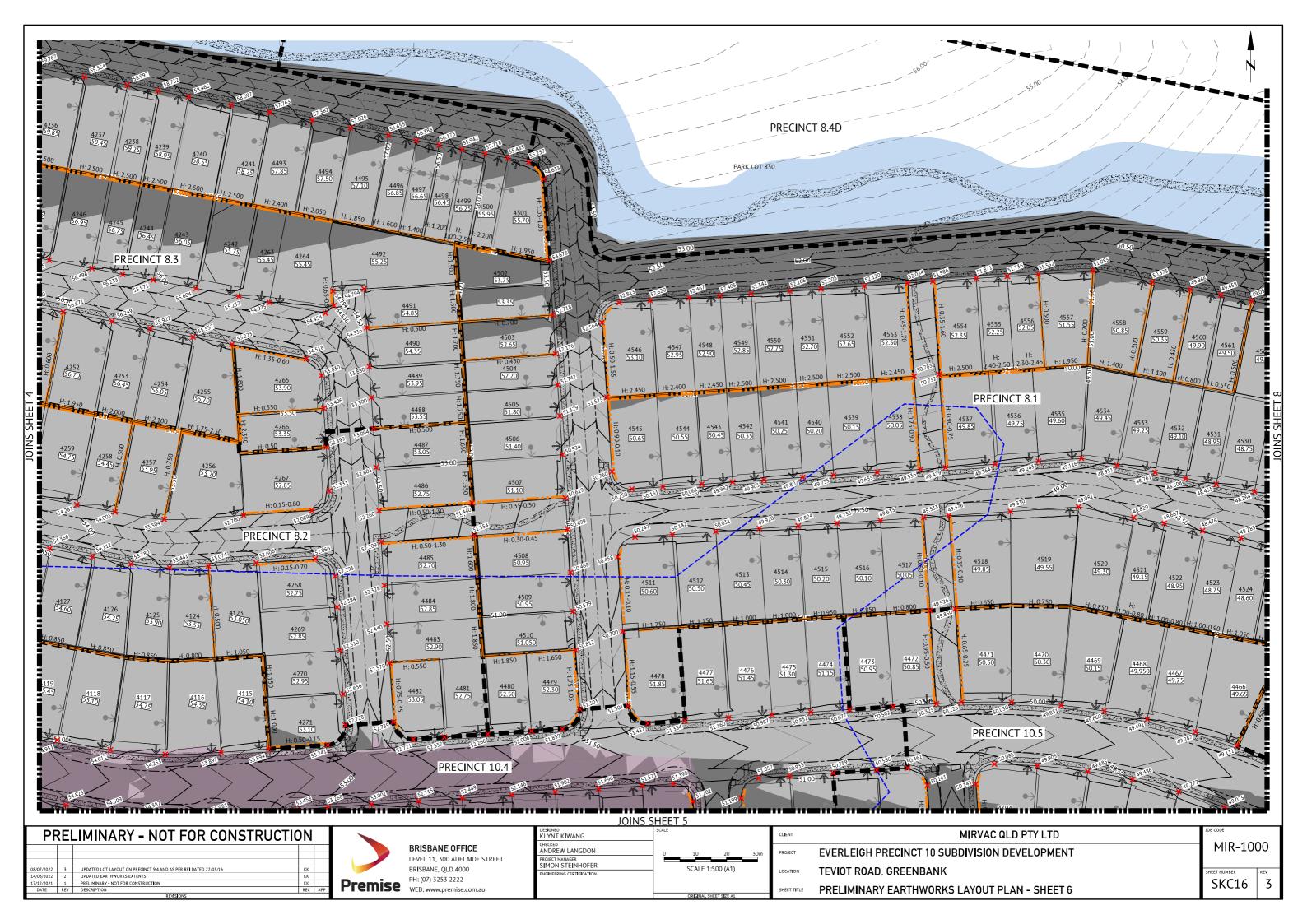


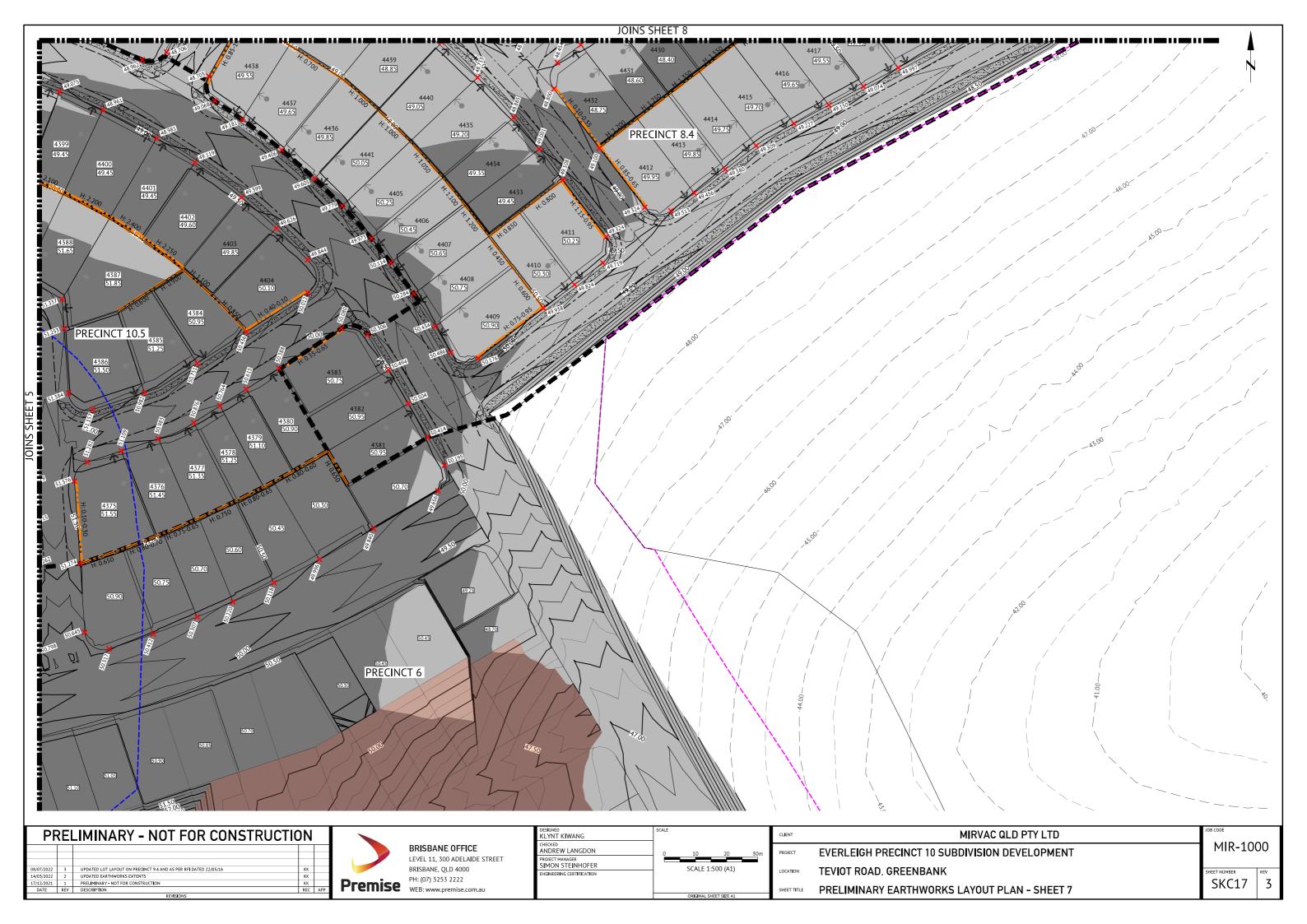


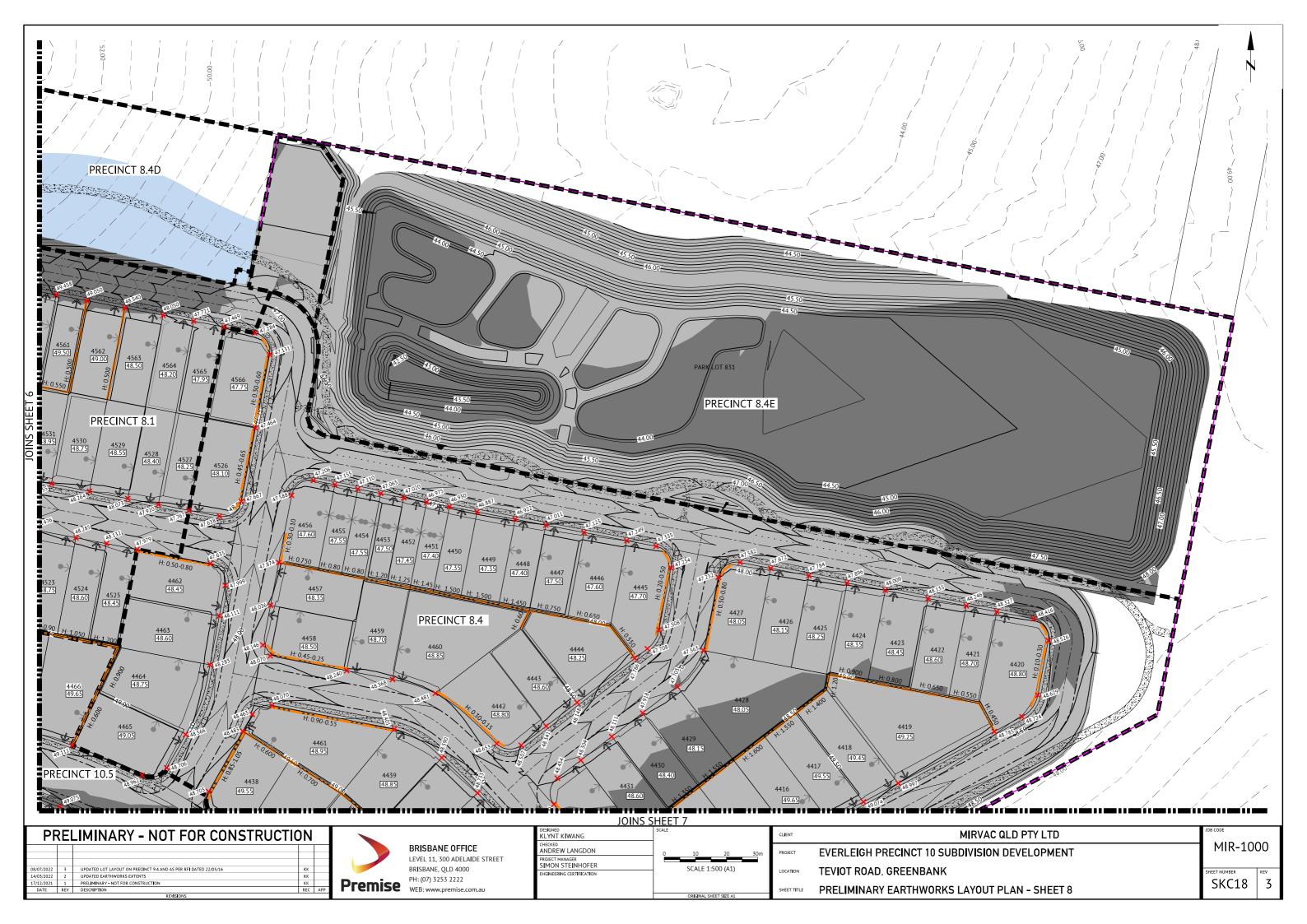






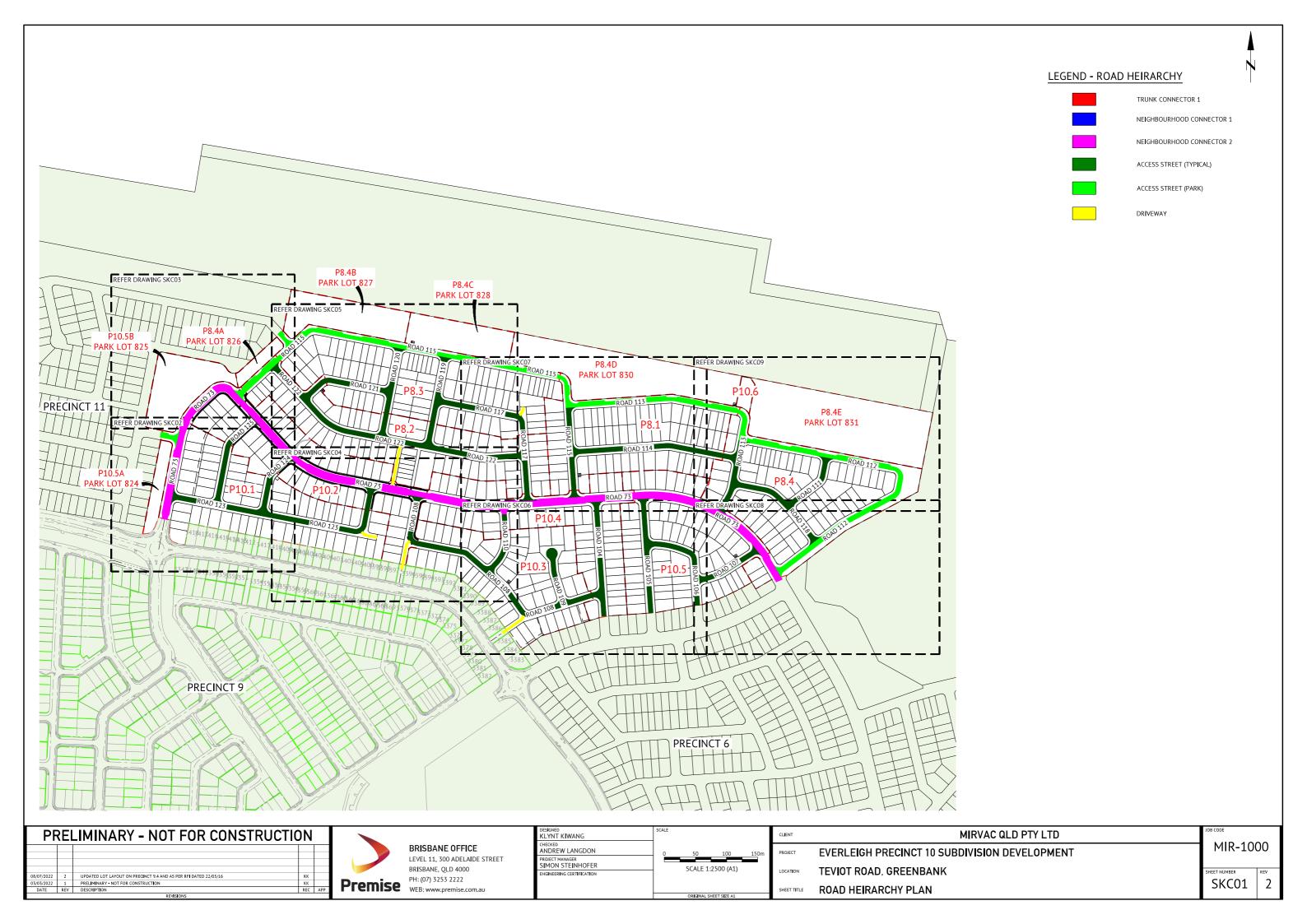






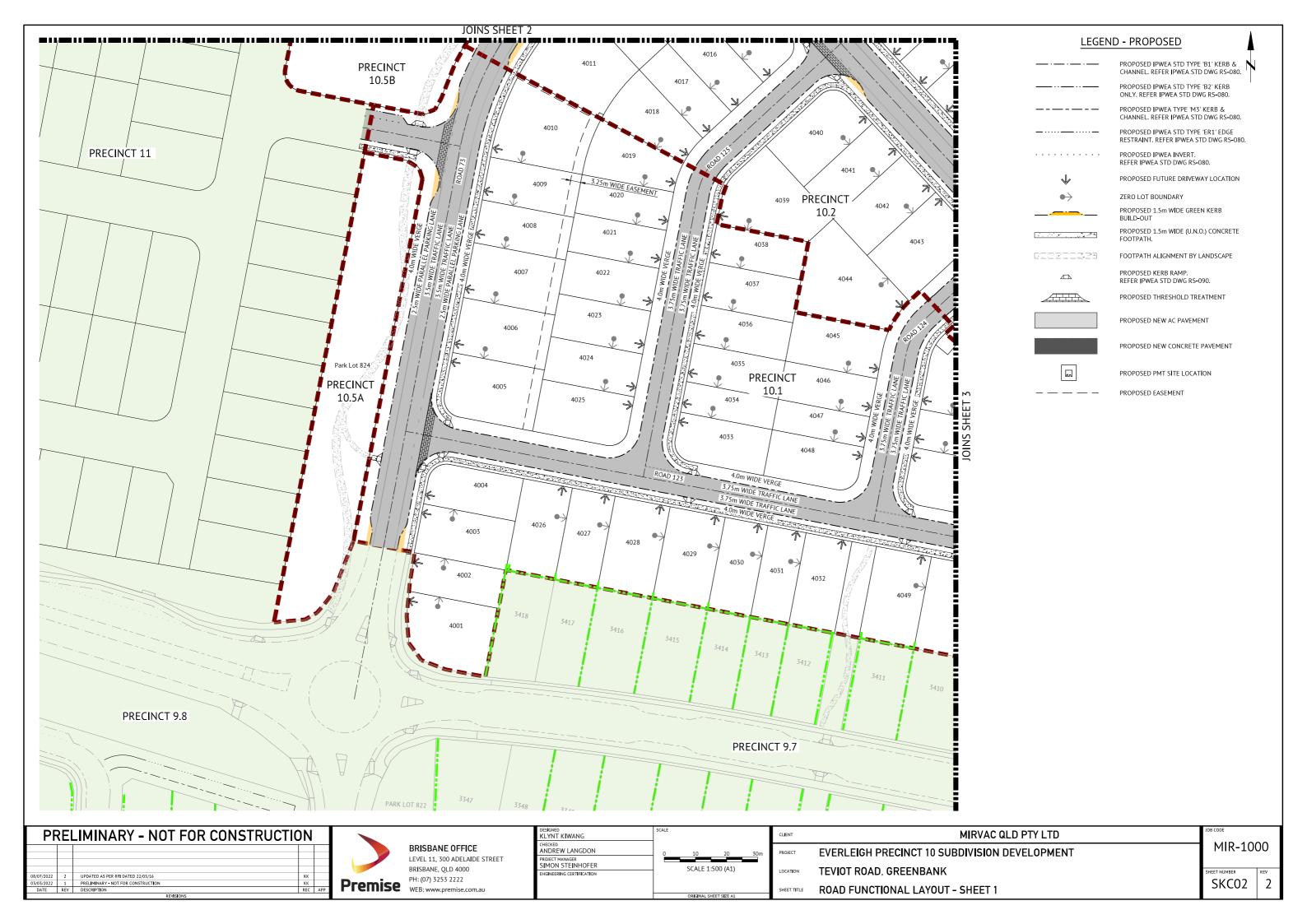


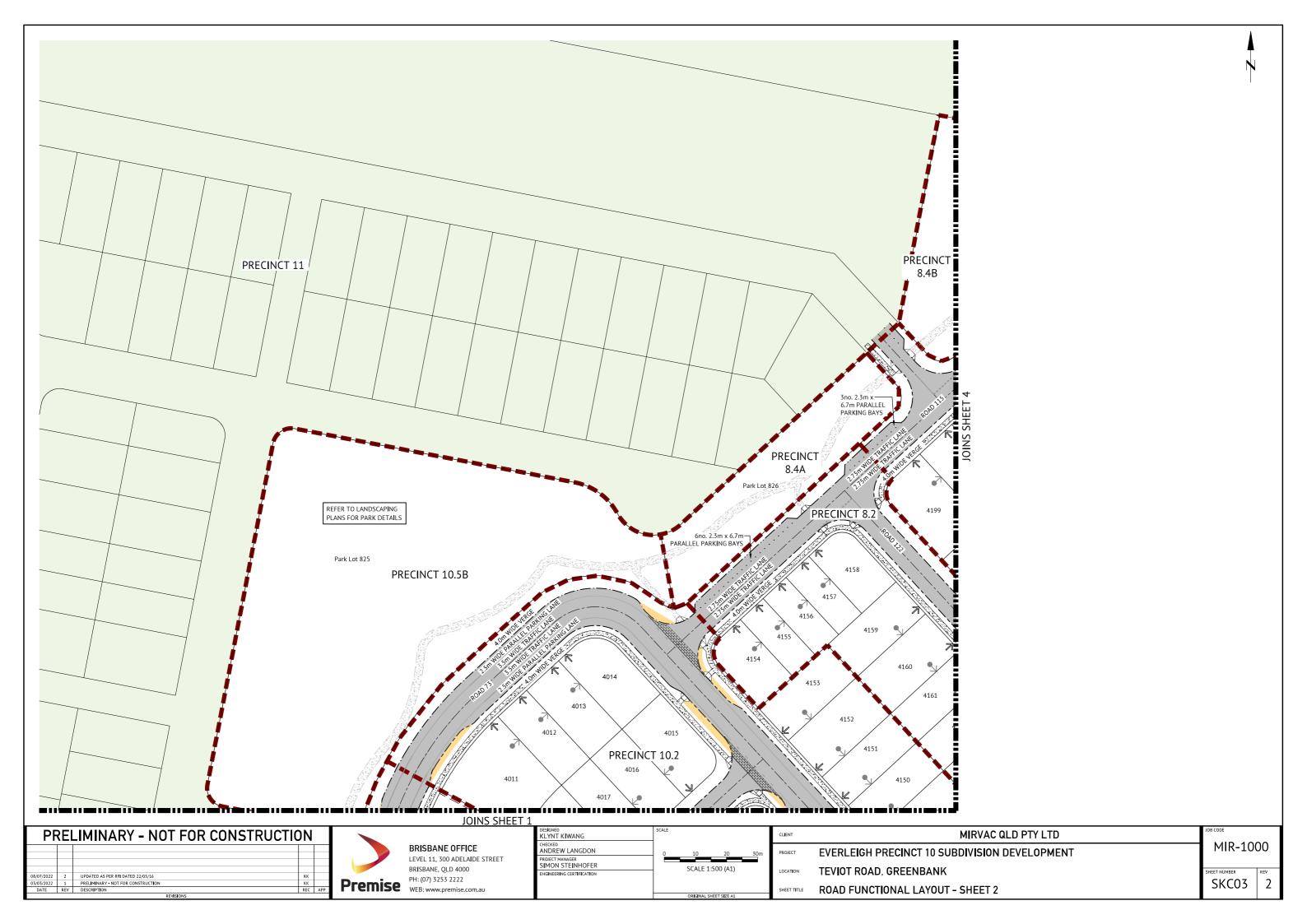
A.3 APPENDIX C – ROAD HEIRARCHY PLAN

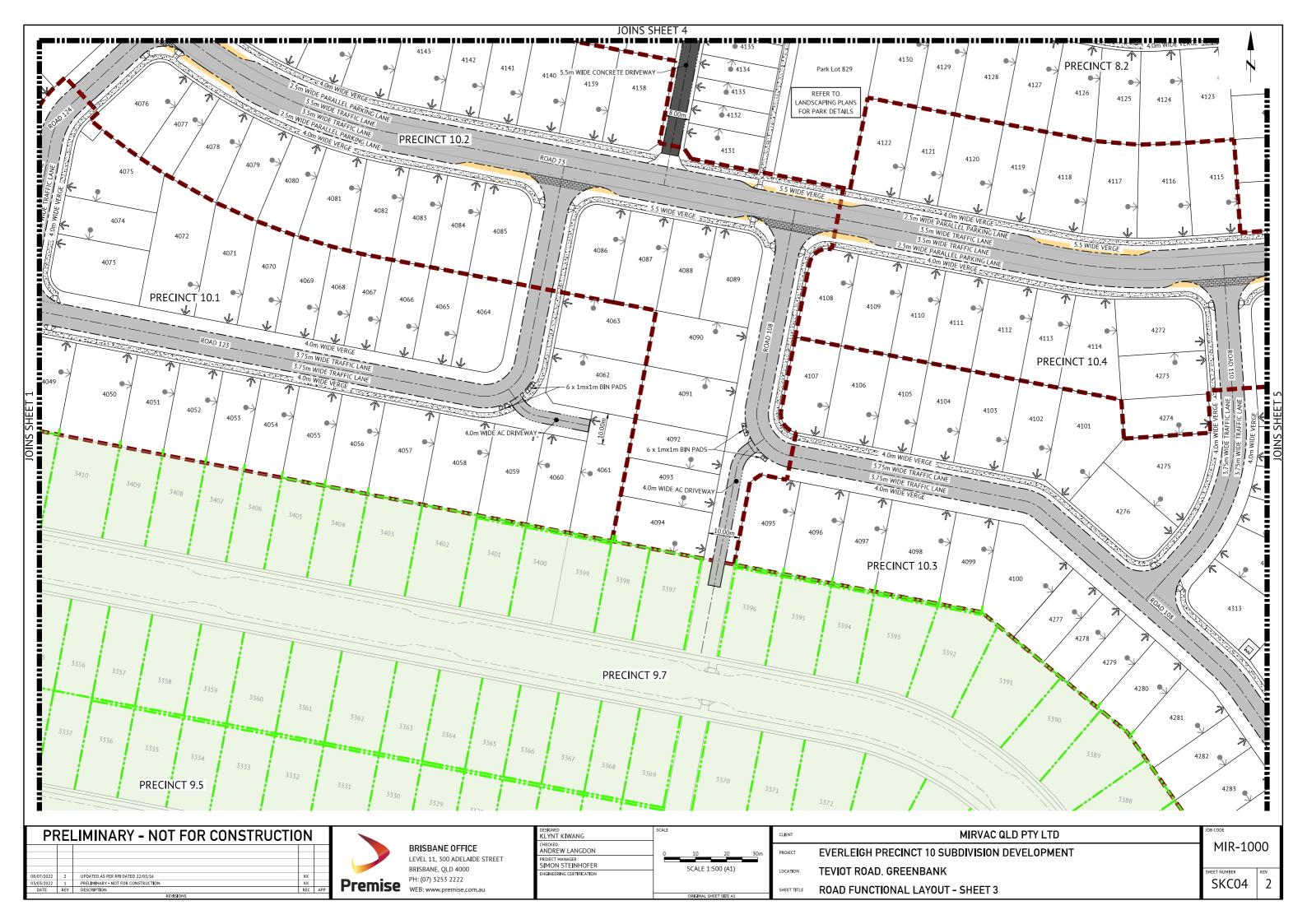


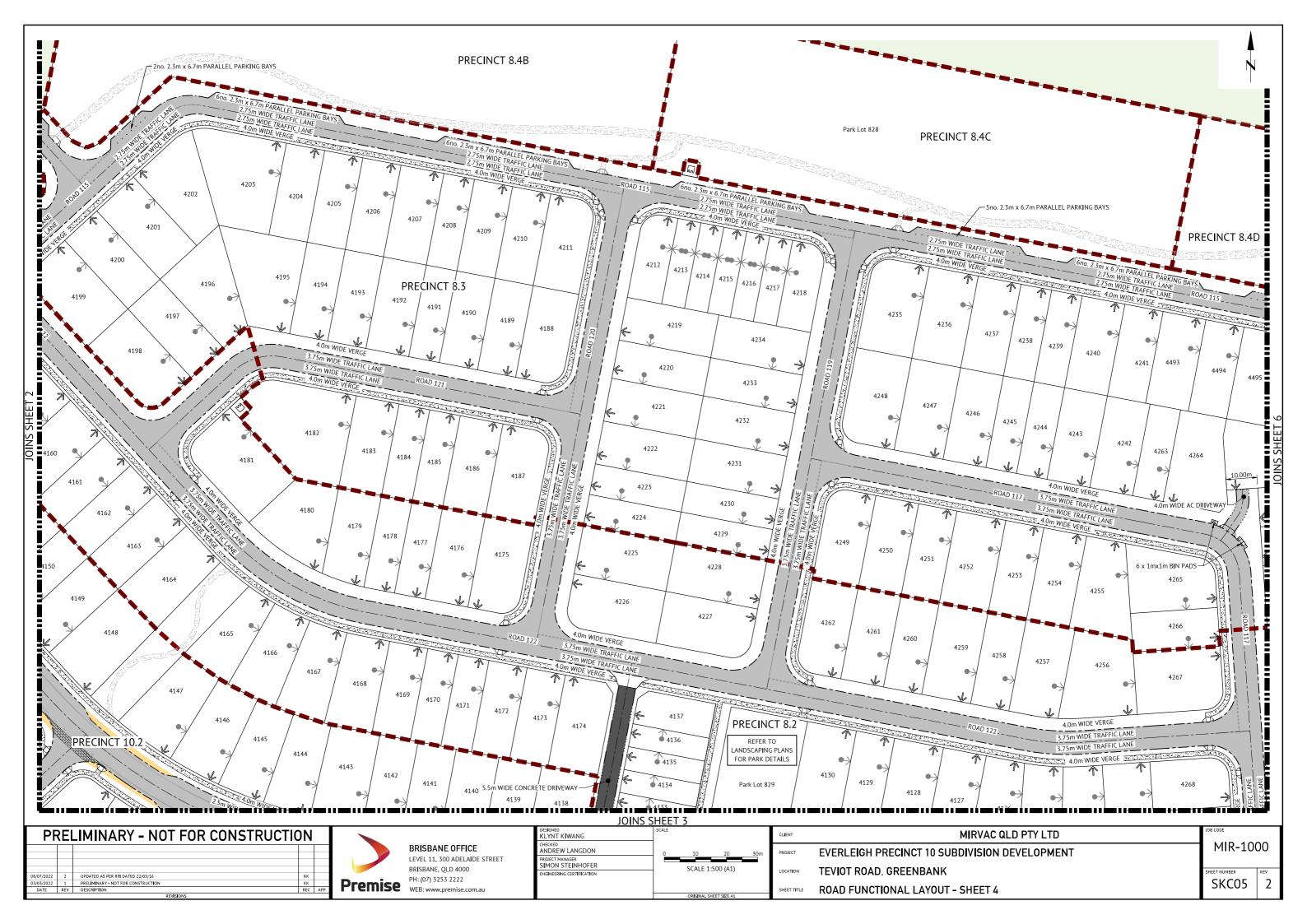


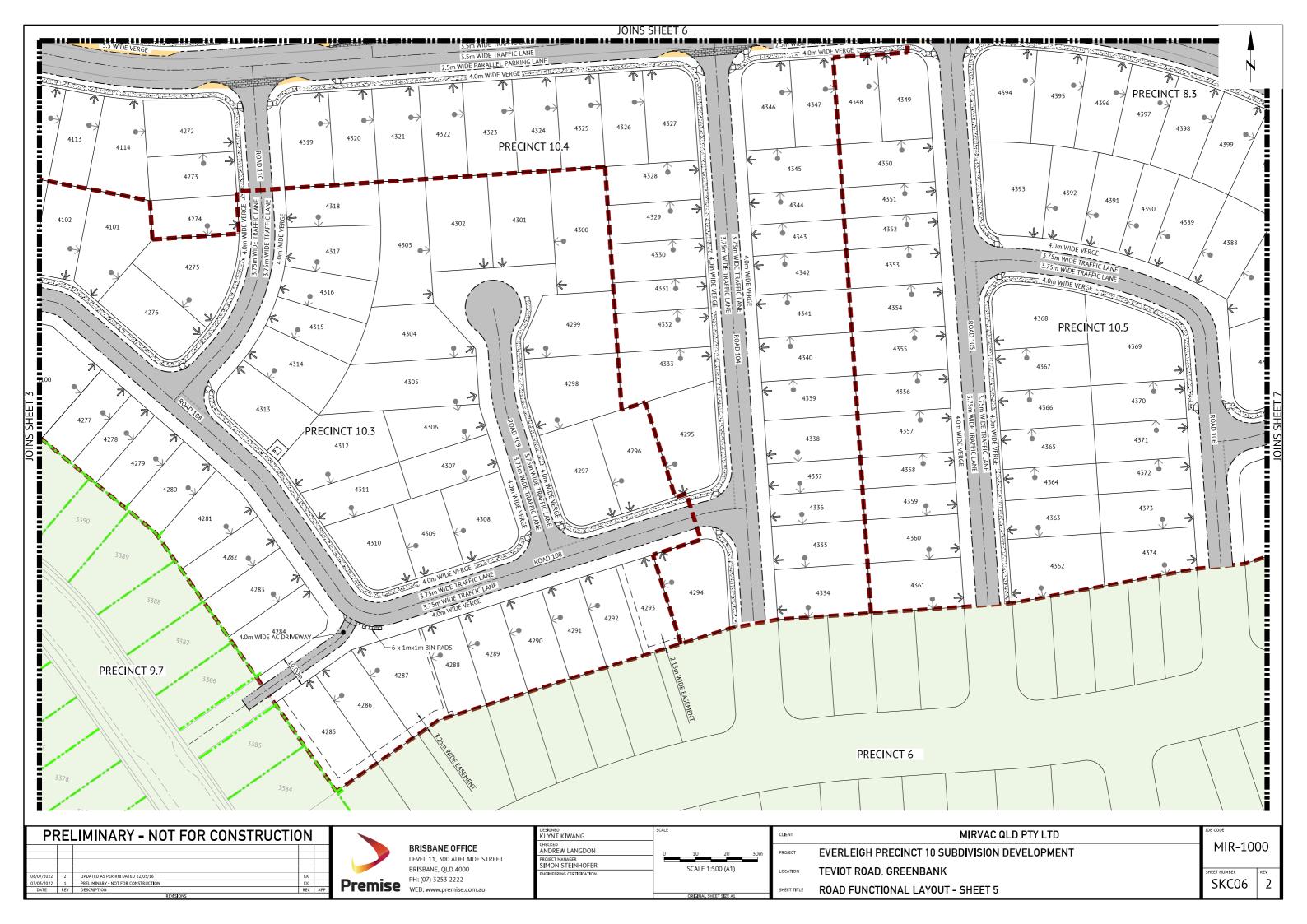
A.4 APPENDIX D – INTERNAL ROAD FUNCTIONAL PLANS

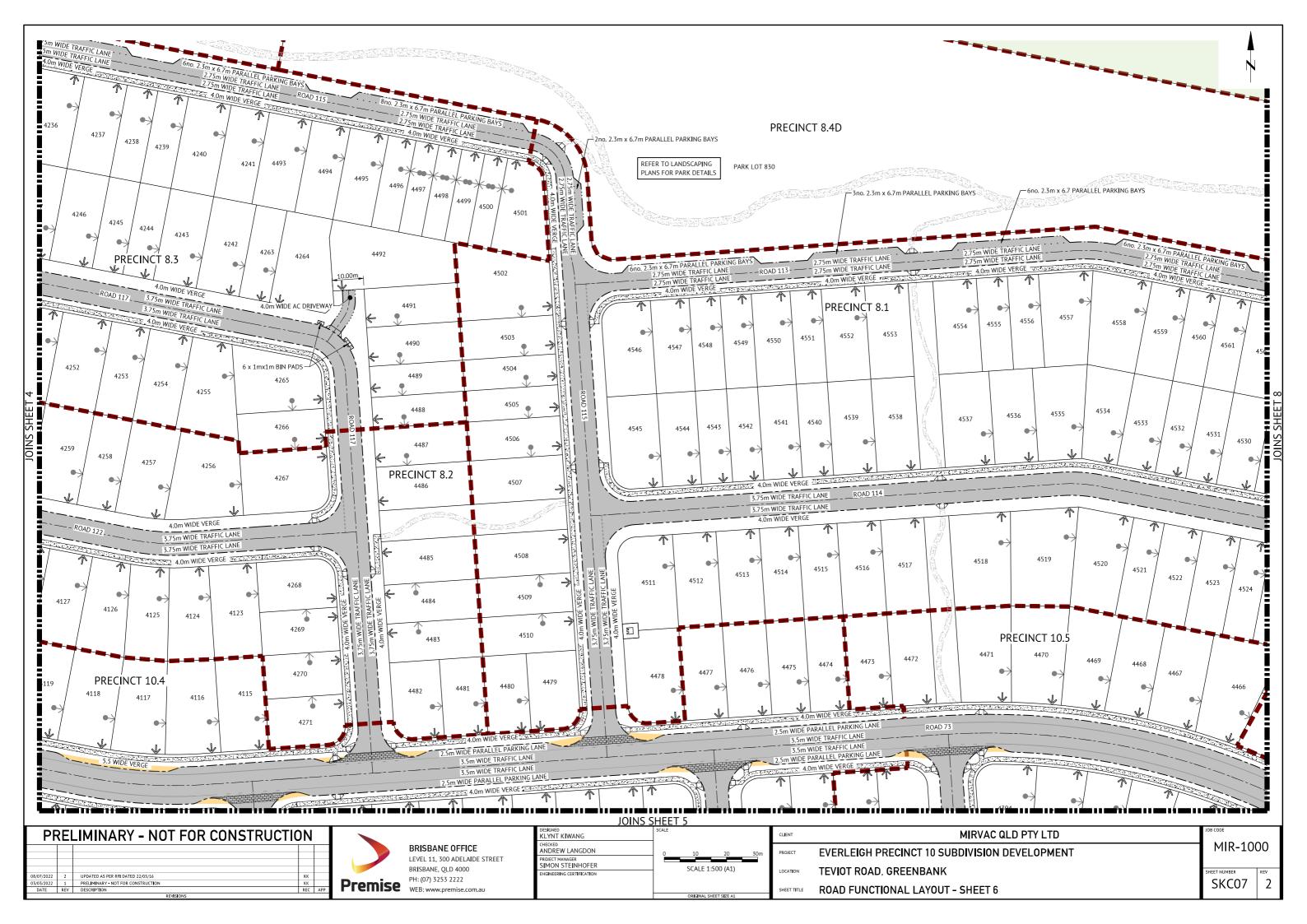


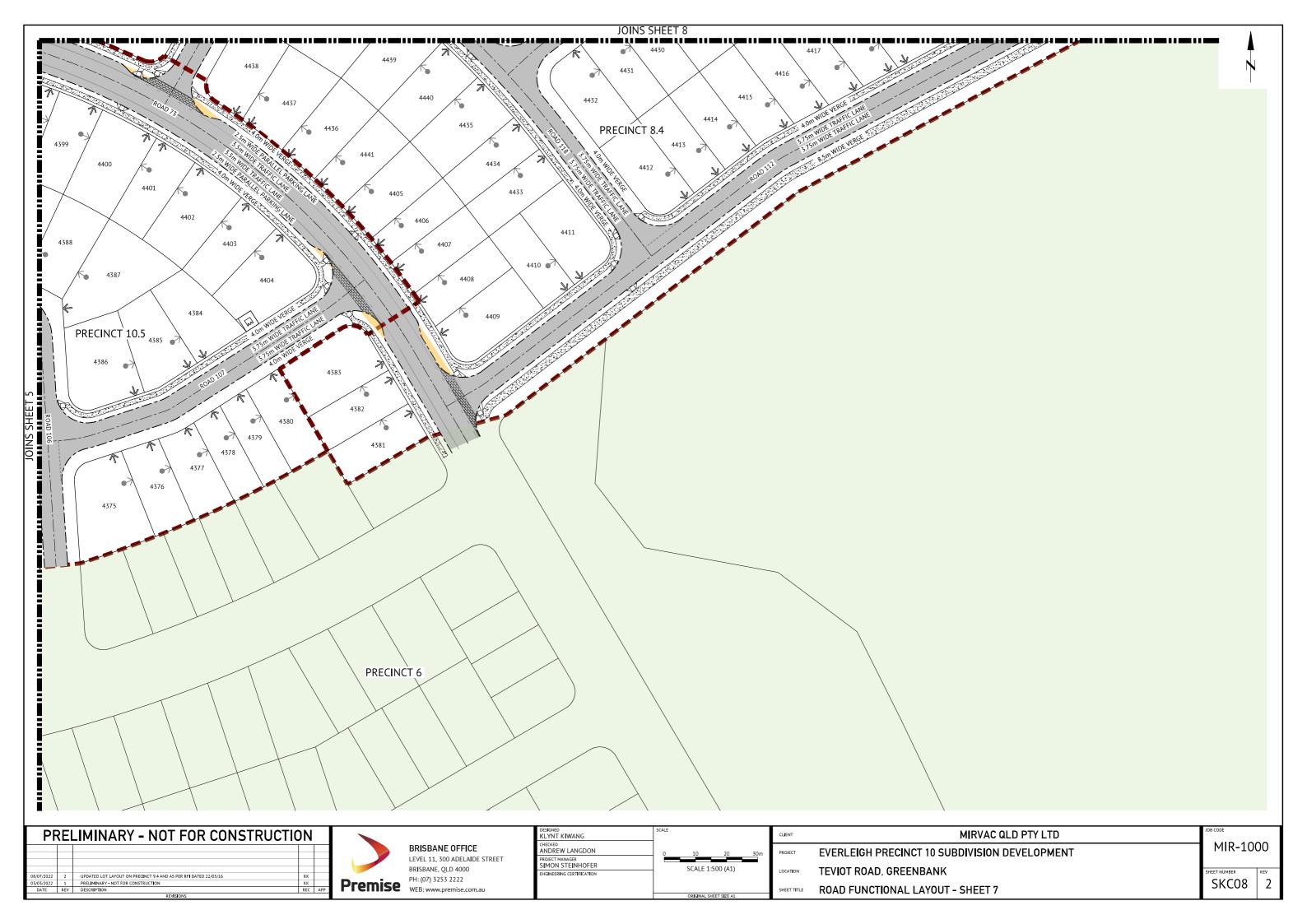


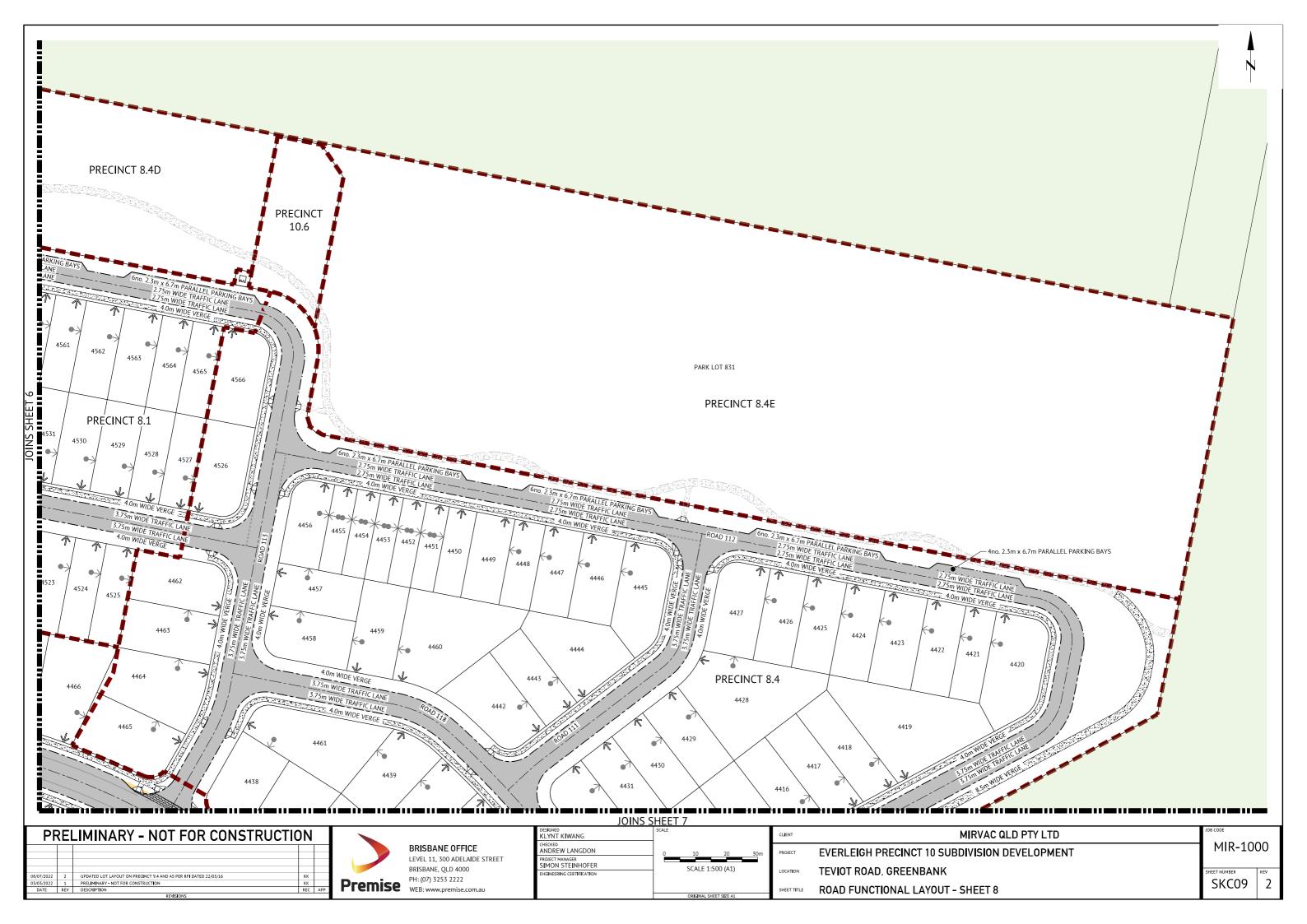


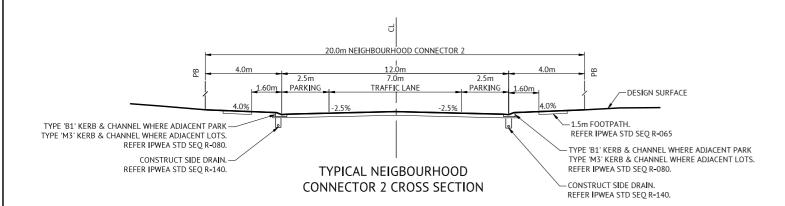


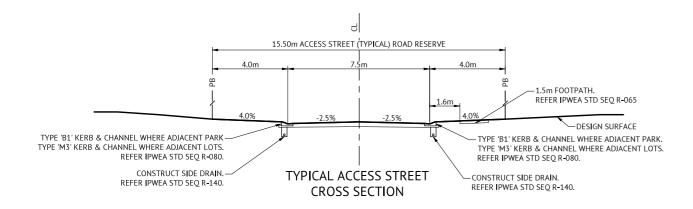


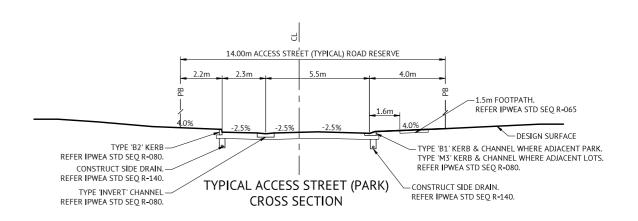


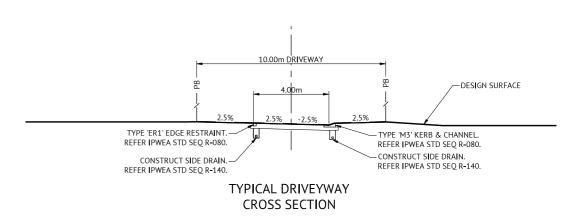


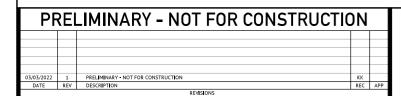




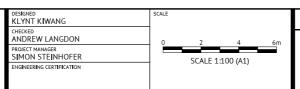












CLIENT	MIRVAC QLD PTY LTD	MIR-1000	
PROJECT	EVERLEIGH PRECINCT 10 SUBDIVISION DEVELOPMENT	MIR-100	JU
LOCATION	TEVIOT ROAD, GREENBANK	SHEET NUMBER	REV
SHEET TITLE	TYPICAL ROAD CROSS SECTIONS	SKC54	1



A.5 APPENDIX E – TRAFFIC IMPACT ASSESSMENT



MIRVAC

Everleigh Precincts 8 & 10

TRAFFIC IMPACT ASSESSMENT

Report No: MIR0800/R01

Rev: B

8 July 2022

MIRVAC EVERLEIGH PRECINCTS 8 & 10 TRAFFIC IMPACT ASSESSMENT



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MIRVAC EVERLEIGH PRECINCTS 8 & 10 TRAFFIC IMPACT ASSESSMENT

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APPENDIX E SIDRA OUTPUT – DESIGN YEAR (2036)

APPENDIX F TRAFFIC IMPACT ASSESSMENT CERTIFICATION



1. INTRODUCTION

Premise Australia Pty Ltd (Premise) has been engaged by Mirvac to undertake a Traffic Impact Assessment for precincts 8 & 10 of the Everleigh residential development in accordance with the Department of Transport and Main Roads' (TMR's) "Guide to Traffic Impact Assessment" (GTIA).

1.1 Background

The Everleigh development is an urban subdivision comprised of approximately 3,500 residential dwellings located on Teviot Road in Greenbank. The development is within the Greater Flagstone Priority Development Area (PDA) as defined by the Department of State Development, Infrastructure, Local Government and Planning and is therefore assessed by Economic Development Queensland (EDQ).

Precincts 8 & 10 are located on the north-east portion of the Everleigh site and contain 304 and 262 lots respectively. This report aims to quantify and assess the traffic impacts of the two (2) precincts as part of the Reconfiguring a Lot application for submission to EDQ.

1.2 Scope and Study Area

Figure 1 shows the assessment area which consists of Anderson Drive between its intersections with Teviot Road and Guroman Drive.

The construction period is scheduled to commence in 2023 and is expected to last four (4) years with:

- Precinct 10 planned for construction from 2023 to 2024; and
- Precinct 8 planned for construction from 2024 to 2026.

In accordance with the GTIA, the impact mitigation period for access intersections is 10 years after the opening of the final stage resulting in a design year of 2036. This is expected to coincide which the completion of the full Everleigh development.



Figure 1 - Impact assessment area MIDDLE ROAD STONEY CAMP ROAD FUTURE NEIGHBOURHOO D CENTRE (PRECINCT 13) LEANNE COURT PRECINCTS 8 & 10 SITE ANDERSON DRIVE PUBLANE GUROMAN DRIVE SCHOOL EVERLEIGH DRIVE NORY GREENBANK PARKWAY SHOPPING CENTRE SPORTS PARK ark Road Image: Queensland Globe



2. EXISTING CONDITIONS

2.1 Land Use and Zoning

The subject site is comprised of land on lots 9003 on SP324819 and 9004 on SP327213 and is currently undeveloped. The site is located within Everleigh Master Planned Community which is part of the Greater Flagstone PDA. The site is zoned for urban living in the Greater Flagstone PDA Development Scheme.

2.2 Adjacent Land Uses / Approval

Land surrounding the development site is generally zoned urban living in accordance with the Greater Flagstone PDA Development Scheme. The site is bounded by:

- Existing rural residential uses to the north;
- Nature reserves to the east;
- Precinct 9 and the future site of precinct 6 to the south; and
- The future site of precinct 11 to the west.

Figure 2 shows the land use zones outlined in the Logan City Plan for the area surrounding the PDA which consists primarily of rural residential uses.

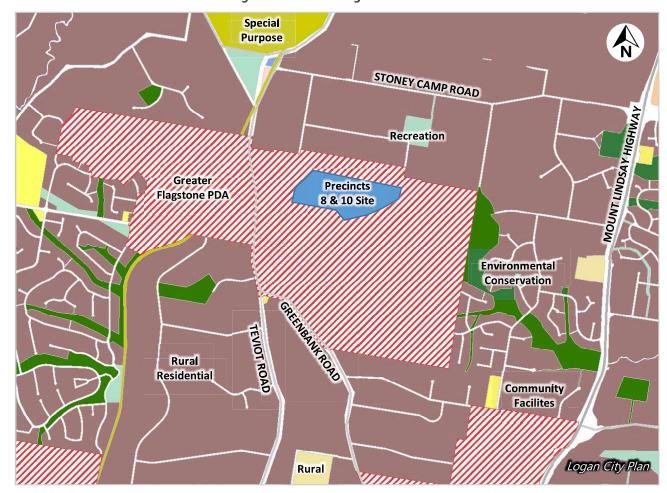


Figure 2 – Surrounding area land use



The primary land entitlements under the Everleigh Master Plan is standard residential lots with a minimum net residential density of 15 lots per hectare. Precincts 8 and 10 are being developed as standard residential lots. Approved non-residential land entitlements within the Everleigh Master Plan are shown by Figure 1 and consist of a Neighbourhood Centre and Community Health Centre to the west, and a State Primary School to the south.



2.3 Surrounding Road Network Details

The surrounding road network is shown by Figure 1.

2.3.1 ROAD LINKS

The existing road links applicable to this assessment include Teviot Road, Anderson Drive, Guroman Drive and Leanne Court.

2.3.1.1 Teviot Road

Teviot Road is an arterial road under the jurisdiction of Logan City Council (LCC). The road is generally aligned north-south between Middle Road to the north and Homestead Drive to the south. The cross-section features a two (2) lane undivided carriageway (one (1) lane each way) with marked traffic lanes as shown in Figure 3. Along the site frontage, a posted speed limit of 70km/h applies.

To support growth of the Greater Flagstone PDA, LCC is widening Teviot Road to four (4) lanes (two (2) lanes each way) between Middle Road and Greenbank Road. The upgrade includes intersection improvements and aims to deliver improved walking and cycling facilities. Within the Logan City Plan, Teviot Road is currently classified as a dual carriageway road in accordance with the proposed upgrade.



Figure 3 – Teviot Road cross-section



2.3.1.2 Anderson Drive

Anderson Drive is a future neighbourhood connector road being constructed as part of Everleigh. The road is aligned in a crescent shape connecting the development with Teviot Road to the west and Greenbank Road to the south.

The planned cross-section features a two (2) lane carriageway (one (1) lane each way) that is divided to the west of the Anderson Drive / Guroman Drive intersection and undivided to the east. Figure 4 shows an existing section of Anderson Drive that features the undivided carriageway.



Figure 4 – Anderson Drive cross-section fronting the school site



2.3.1.3 Guroman Drive

Guroman Drive is a neighbourhood connector road within Everleigh. The road is generally aligned north-south between the Anderson Drive / Guroman Drive roundabout to the north and Everleigh Drive to the south. The cross-section features a two (2) lane undivided carriageway (one (1) lane each way) with indented parking bays as shown by Figure 5. The default urban speed limit of 50km/h applies on Guroman Drive.



Figure 5 – Guroman Drive cross-section



2.3.1.4 Leanne Court

Leanne Court is classed as an urban access street under the jurisdiction of LCC. The court is approximately 350m in length and is generally aligned east-west between Teviot Road to the east and a dead-end to the west. Figure 7 shows the road cross-section which features an undivided two (2) way carriageway on an approximately 3.5m wide seal. The default urban speed limit of 50km/h applies on Leanne Court.



Figure 6 – Leanne Court cross-section



2.3.2 INTERSECTIONS

Intersections applicable to this assessment include:

- The Teviot Road / Anderson Drive crossroads; and
- The Anderson Drive / Guroman Drive roundabout.

2.3.2.1 Teviot Road / Anderson Drive Crossroads

Teviot Road and Leanne Court form a priority-controlled T-intersection on the local government road network. As part of the Teviot Road widening project, LCC is upgrading the intersection with Leanne Court to signal control as shown by Figure 7. The proposed layout features improved channelisation and pedestrian crossing facilities across three (3) intersection legs. In conjunction with the upgrade, Mirvac is constructing Anderson Drive to the east which will form the intersection's fourth leg.



Figure 7 – Teviot Road / Anderson Drive intersection functional layout plan



2.3.2.2 Anderson Drive / Guroman Drive Roundabout

Anderson Drive and Guroman Drive form a future roundabout controlled intersection on the local government road network. Figure 8 shows the functional layout plan for the intersection which is being constructed as part of Everleigh precinct 9. It features a 22m diameter central island and a single seven (7) metre wide circulating lane.

The plan indicates two (2) approach and two (2) departure lanes on the western leg of the roundabout, however, the final layout may be designed and constructed as one (1) approach and one (1) departure lane. The suitability of this option is addressed in "Everleigh Precinct 9 – Traffic Statement" (Precinct 9 Traffic Statement-revB) dated 11/05/2021 previously prepared by Premise.

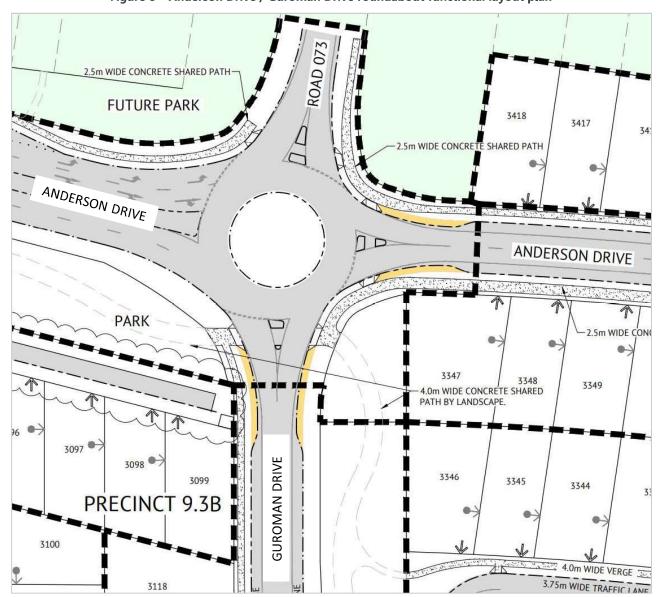


Figure 8 – Anderson Drive / Guroman Drive roundabout functional layout plan



2.4 Traffic Volumes

Premise previously developed a traffic model of Everleigh and the surrounding road network. The model is based on assumptions used in the AIMSUN model developed by MWH for the purpose of preparing "Movement Network Infrastructure Master Plan: Teviot Road, Greenbank" (MNIMP). The MNIMP was approved by EDQ on 9 August 2017 based on:

- 24-hour intersection traffic count data collected on Thursday 5 November 2015;
- Traffic generation rates and directional splits for land uses within Everleigh as agreed by MWH and Veitch Lister Consulting (VLC) on 25 January 2017;
- Growth rates of between 3% and 4%; and
- 25% discounting of trips produced by residential development within Everleigh to represent the community's self-containment.

Further to the above, the Premise traffic model is based on:

- The preferred hierarchy specified in the GTIA for daily traffic generation rates not specified by MWH;
 and
- An external trip distribution which was estimated based on the available information regarding the trip distribution in the MWH model.

While Premise has generally sort to keep the traffic model consistent with the MWH model, Premise has increased the number of trip generating zones within Everleigh from four (4) in the MWH model to 16 in the Premise model. EDQ acknowledges that this will provide a more refined traffic model and allow more realistic estimation of traffic on the network. In preparation for this report the Premise traffic model has been updated to reflect the latest forecasts of development yield and timing.

This assessment adopts volumes at the completion of precinct 9 as existing traffic volumes, this is expected to occur in 2023 (prior to construction commencing on precinct 10). 2023 morning and evening peak hour traffic volumes for the assessment area are shown in Figure 9 and Figure 10 respectively.

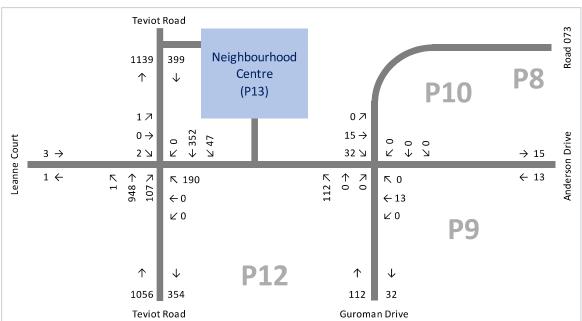


Figure 9 – Existing conditions (2023) morning peak hour traffic volumes



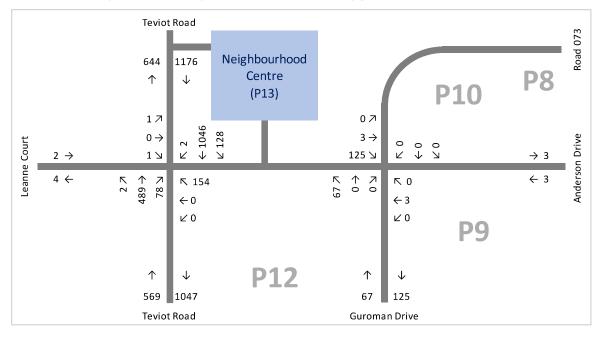


Figure 10 – Existing conditions (2023) evening peak hour traffic volumes

2.5 Intersection and Network Performance

Intersection (and access) performance has been assessed using SIDRA Intersection Version 9 (SIDRA). SIDRA is an advanced micro-analytical traffic tool for evaluation of intersections. SIDRA reports intersection performance in terms of a range of parameters including:

- **Demand Volumes (V):** The modelled number of vehicles arriving at the intersection during the assessment hour. Demand volumes are calculated by dividing the peak hour volume by the peak flow factor (PFF). SIDRA's default PFF of 95% has been adopted for all movements;
- **Degree of Saturation (DoS):** The ratio of the demand volume, V, to the theoretical capacity. An intersection is considered to be operating at its practical capacity when the DoS reaches 0.85 for a roundabout and 0.90 for traffic signals;
- Average Delay (D): The mean control delay including both queuing delay and geometric delay for all vehicles arriving during the assessment period including the delay experienced after the end of the flow period until the departure of the last vehicle arriving during the flow period. The GTIA specifies that average delays exceeding 42 seconds for any movement at a roundabout is a safety issue; and
- 95th Percentile Back of Queue Length (Q): The maximum backward extent of the queue relative to the stop line or give-way / yield line during a signal cycle or gap acceptance cycle below which 95% of all queue lengths fall. The 95th percentile back of queue length is generally accepted as the maximum queue length for design purposes.

SIDRA analysis assumes a heavy vehicle proportion of 5% for all vehicle movements.

2.5.1 TEVIOT ROAD / ANDERSON DRIVE PERFORMANCE

Intersection analysis has been undertaken at the Teviot Road / Anderson Drive intersection based on existing (2023) traffic volumes (refer Section 2.4). All analysis of the intersection adopts the site layout shown in Figure 11, the signal phase sequence shown in Figure 12 and a cycle time of 120 seconds.



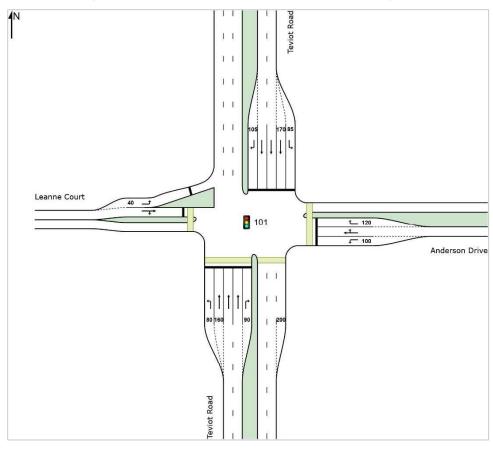
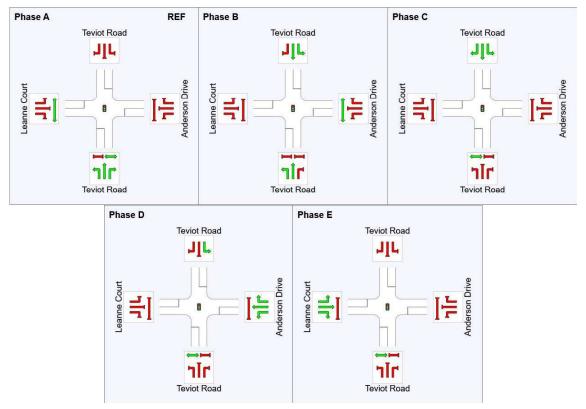


Figure 11 – Teviot Road / Anderson Drive SIDRA site layout

Figure 12 – Teviot Road / Anderson Drive SIDRA signal phase sequence





Appendix A shows SIDRA output results for intersection with key outputs from the SIDRA model provided in Table 1 and summarised below.

- The maximum DoS is 0.475, which is well below practical capacity;
- The maximum average delay to any movement is 65.8 seconds, which is expected under signal control; and
- The maximum queue length does not exceed 15.2 vehicles, which does not impact on neighbouring intersections.

Table 1 – SIDRA Output – Teviot Road / Anderson Drive, existing conditions (2023)

Movement		AM I	Peak		PM Peak					
	V (veh)	DoS	D (sec)	Q (veh)	V (veh)	DoS	D (sec)	Q (veh)		
South Appro	ach: Teviot I	Road								
Left	1	0.001	24.4	0.0	2	0.003	25.7	0.1		
Through	998	0.391	23.4	12.8	515	0.210	22.5	6.2		
Right	113	0.222	41.0	5.0	82	0.458	62.7	4.7		
East Approac	East Approach: Anderson Drive									
Left	1	0.002	41.2	0.0	1	0.003	44.4	0.0		
Through	1	0.224	38.5	4.7	1	0.202	40.8	3.9		
Right	200	0.224	44.2	4.7	162	0.202	46.4	3.9		
North Appro	North Approach: Teviot Road									
Left	49	0.053	20.7	1.4	135	0.107	11.7	2.5		
Through	371	0.302	42.7	6.1	1101	0.457	26.5	15.2		
Right	1	0.012	65.8	0.1	2	0.013	59.5	0.1		
West Approa	ach: Leanne	Court								
Left	1	0.012	65.8	0.1	1	0.012	65.8	0.1		
Through	1	0.035	60.8	0.2	1	0.023	60.5	0.1		
Right	2	0.035	66.5	0.2	1	0.023	66.2	0.1		



2.5.2 ANDERSON DRIVE / GUROMAN DRIVE PERFORMANCE

Appendix A shows the SIDRA output results for the Anderson Drive / Guroman Drive roundabout based on the proposed layout (refer Figure 8) and existing conditions (2023) traffic volumes. Key outputs from the SIDRA model are provided in Table 2 and summarised below:

- The maximum DoS is 0.083, which is well below practical capacity;
- The maximum average delay to any movement is 9.4 seconds, which is very low; and
- The maximum queue length does not exceed one (1) vehicle, which is short.

Table 2 - SIDRA Output - Anderson Drive / Guroman Drive, existing conditions (2023)

Movement		AM I	Peak		PM Peak					
	V (veh)	DoS	D (sec)	Q (veh)	V (veh)	DoS	D (sec)	Q (veh)		
South Appro	ach: Gurom	an Drive								
Left	118	0.081	3.9	0.4	71	0.047	3.8	0.2		
Through	1	0.081	4.0	0.4	1	0.047	4.0	0.2		
Right	1	0.081	8.9	0.4	1	0.047	8.9	0.2		
East Approac	East Approach: Anderson Drive									
Left	1	0.012	4.0	0.1	1	0.004	4.4	0.0		
Through	14	0.012	4.1	0.1	3	0.004	4.5	0.0		
Right	1	0.012	9.0	0.1	1	0.004	9.4	0.0		
North Appro	ach: Road 0	73								
Left	1	0.002	4.0	0.0	1	0.003	4.4	0.0		
Through	1	0.002	4.2	0.0	1	0.003	4.5	0.0		
Right	1	0.002	9.0	0.0	1	0.003	9.4	0.0		
West Approa	ach: Andersc	n Drive								
Left	1	0.032	3.8	0.1	1	0.083	3.8	0.4		
Through	16	0.032	4.0	0.1	3	0.083	4.0	0.4		
Right	34	0.032	8.8	0.1	132	0.083	8.8	0.4		

2.6 Road Safety Issues

Existing road safety issues in the study area were identified through crash rate analysis. The analysis was conducted for the existing Teviot Road / Leanne Court T-intersection based on crash data available on the Queensland Open Data Portal for crashes that occurred between 2005 and 2020. The information for each crash includes the crash type, location, year, number/type of vehicles involved, vehicle direction, conditions and contributing factors. There were a total of three (3) crashes recorded at the intersection for this period consisting of one (1) rear-end collision, one (1) entering roadway crash and one (1) off-path crash.

The rear-end collision (DCA 303) involved three (3) vehicles including one (1) vehicle turning right. The crash occurred in 2017 at 12:00PM in wet conditions and resulted hospitalisation.

The entering roadway crash (DCA 408) is a multi-vehicle crash that occurred between a vehicle travelling southbound on Teviot Road and a vehicle entering the roadway. The crash occurred in 2008 at 6:00PM in clear dry conditions and resulted in medical treatment.

The off-path crash (DCA 703) involved a single vehicle travelling southbound on Teviot Road that left the carriageway and collided with an object. The crash occurred in 2006 at 4:00PM in clear dry conditions and resulted in medical treatment.



2.7 Site Access

Currently, no direct access is provided to the site. At the completion of precinct 9, the site will be accessible via the northern leg of the Anderson Drive / Guroman Drive roundabout.

2.8 Public Transport

The subject site is not currently serviced by public transport. The closest bus stop pair is located on Teviot Road at its intersection with Pub Lane and serviced exclusively by school bus routes.

2.9 Active Transport

Footpaths and shared paths are provided along each road link within precinct 9 and in park land parallel to Guroman Drive and Anderson Drive to the west. Along the precinct 8 & 10 frontage, paths are provided on both sides of Anderson Drive and land is reserved for pedestrian links to adjacent access streets including three (3) to precincts 8 & 10.



3. PROPOSED DEVELOPMENT DETAILS

3.1 Development Site Plan

The proposed development is precincts 8 and 10 of Everleigh. The development site plan prepared by Urbis is shown in Figure 13. Precinct 10 features 280 residential lots. Precinct 8 features 286 residential lots.



Figure 13 – Development site plan

Pedestrian paths are expected to be provided on every road link. The development site plan indicates that eight (8) additional pedestrian links are to be provided including three (3) to Anderson Drive and five (3) internal to the site.

3.2 Operational Details

The construction period is scheduled to commence in 2023 and is expected to last (4) years with precinct 10 planned for construction from 2023 to 2024 and precinct 8 planned for construction from 2024 to 2026.

Based on the residential land uses the development is expected to have two (2) peak periods being:

- The morning commuter peak hour; and
- The evening commuter peak hour.



3.3 Proposed Access and Parking

Vehicle access to the development is proposed via the north leg of the Anderson Drive / Guroman Drive roundabout. The leg is formed by unnamed road 073, a neighbourhood connecter road which is generally aligned east-west between the roundabout to the west and a future connection to precinct 6 to the east. A total of four (4) future connections are proposed between precincts 8 and 6.

The ultimate internal roadway layout for Everleigh is attached in Appendix B and shows precincts 8 & 10 to consist of three (3) road cross sections as defined by the MNIMP, including:

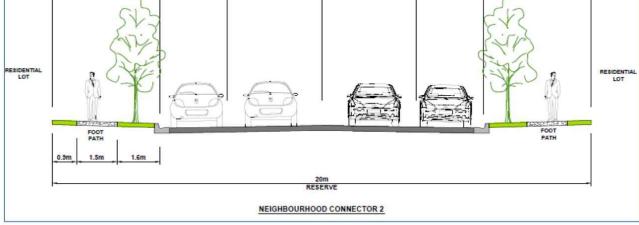
- Neighbourhood Connector 2;
- Access Street (Typical); and
- Access Street (Park).

3.3.1 NEIGHBOURHOOD CONNECTOR 2 CROSS-SECTION

Figure 14 shows the MNIMP approved neighbourhood connector 2 cross-section which will be provided by unnamed road 073. It features a total reserve width of 20m, two (2) 3.5m traffic lanes (one (1) lane each way), 2.5m wide parking lanes and 4m wide verges. Footpaths are provided on both sides of the neighbourhood connector 2 cross-section.

Lane Width Residential Vegetated Sound Median Lane 2 N/A 20m 3.5m 2.5m 4m N/A 50km/h Yes 4m VERGE 2.5m PARKING LANE 3.5m TRAFFIC LANE 3.5m TRAFFIC LANE 2.5m PARKING LANE

Figure 14 – Neighbourhood Connector 2 cross-section (source: MWH MNIMP)



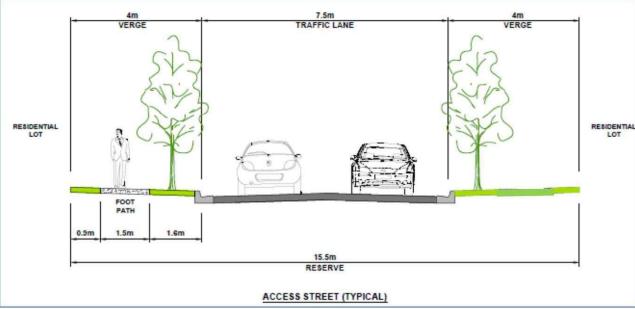


3.3.2 ACCESS STREET (TYPICAL) CROSS-SECTION

Figure 15 shows the MNIMP approved access street (typical) cross-section which features a total reserve width of 15.5m, two (2) 3.75m traffic lanes (one (1) lane each way) and 4m wide verges. A footpath is provided on one (1) side of the access street (typical) cross-section.

Figure 15 – Access Street (Typical) cross-section (source: MWH MNIMP)

			, ,,		`			
Traffic	Traffic Lane Width	Parking Lane	Median Width	Verge Width	Parking Lane Width	Total Reserve Width	Road	Residential Frontage
2	3.75	Kerbside	N/A	4m	N/A	15.5m	=<br 50km/h	Yes
	4m VERGE	547		7.5m TRAFFIC LANE		5.42	4m VERGE	





3.3.3 ACCESS STREET (PARK) CROSS-SECTION

Figure 16 shows the MNIMP approved access street (park) cross-section which features a total reserve width of 14m, two (2) 2.75m traffic lanes (one (1) lane each way) and a 2.3m wide parking lane adjacent to park land. A footpath is provided on one (1) side of the access street (park) cross-section.

Figure 16 – Access Street (Park) cross-section (source: MWH MNIMP)

Traffic Lanes	Traffic Lane Width	Median Width	Verge Width	Parking Lane Width	Total Reserve Width	Road	Residential Frontage
2	2.75m	N/A	2.2 – 4m	2.3	14.0m	= 50km/h</td <td>Yes</td>	Yes
	4m VERGE	583	5.5 TRAFFI		2.3m PARKING LA	NE VERGE	





4. DEVELOPMENT TRAFFIC

4.1 Traffic Generation

Peak hour development traffic generation is based on the model assumptions outlined in the MNIMP, being:

- 0.85 trips per dwelling; and
- 25% discounting for internal trips during the morning peak hour

The development consists of 566 residential lots and therefore is expected to generate 361 external trips during the morning peak hour and 481 trips during the evening peak hour. Table 3 outlines the expected peak hour generation for each precinct.

Precinct	Morning Peak Hour (Vehicles)	Evening Peak Hour (Vehicles)
8	182	243
10	179	238
Total	361	481

Table 3 – Development traffic generation

The residential trips are distributed between inbound and outbound consistent with the MNIMP model. This corresponds to 22% inbound and 78% outbound during the morning peak hour and 65% inbound and 35% outbound during the evening peak hour.

4.2 Trip Distribution

Development trips are distributed based on the MNIMP model and include:

- 10% of trips on Middle Road to the west;
- 15% of trips on Middle Road to the east;
- 10% of trips on Mount Lindsay Highway to the north via Stoney Camp Road;
- 5% of trips on Granger Road to the east via Stoney Camp Road;
- 40% of trips on Pub Lane to the west;
- 5% of trips on Crowson Lane to east via Greenbank Road;
- 5% of trips on Greenbank Road to the south via Greenbank Road; and
- 10% of trips on Teviot Road to the south.

Access to precincts 8 & 10 is limited to the to the north leg of the Anderson Drive / Guroman Drive roundabout until after the completion of precinct 6. Therefore, under the ultimate development case traffic is expected to redistribute between the roundabout access and future connections to the east via precinct 6. The development site plans show four (4) future connections to precinct 6 including three (3) access streets and one (1) neighbourhood connector.



4.3 Development Traffic Volumes on the Network

Development traffic volumes for the design morning and evening peak hours were estimated from the traffic generation determined in Section 4.1 and the trip distribution determined in Section 4.2. The resulting morning and evening peak hour volumes at the completion of precinct 10 (2024) are shown in Figure 17 and Figure 18 and volumes at the completion of precinct 8 (2026) are shown in Figure 19 and Figure 20. Morning and evening peak hour redistributed development traffic volumes under the ultimate development case are attached in Appendix C.

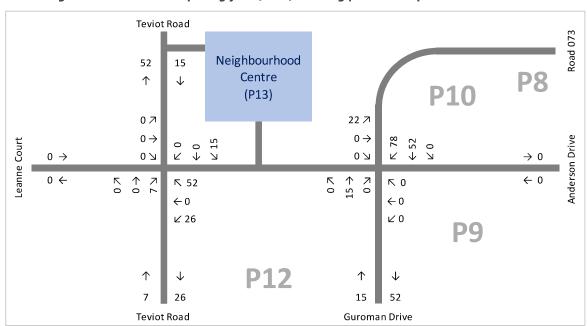


Figure 17 - Precinct 10 opening year (2024) morning peak development traffic volumes

Figure 18 - Precinct 10 opening year (2024) evening peak development traffic volumes

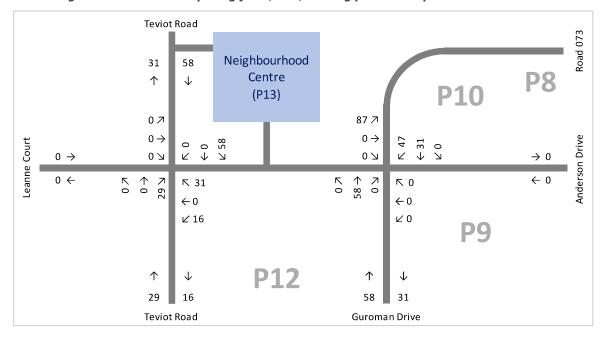




Figure 19 – Precinct 8 opening year (2026) morning peak development traffic volumes

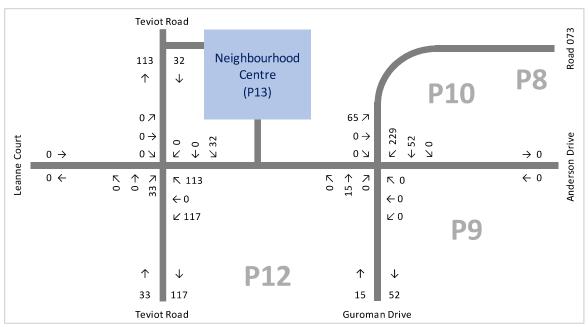
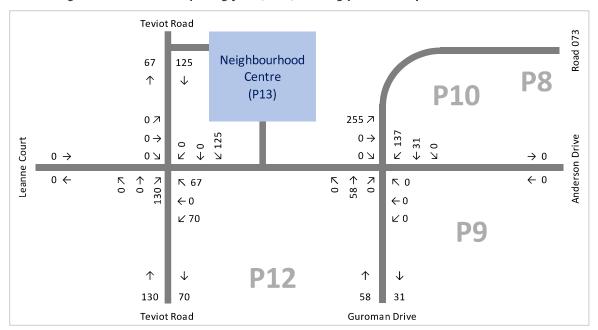


Figure 20 – Precinct 8 opening year (2026) evening peak development traffic volumes





5. IMPACT ASSESSMENT AND MITIGATION

5.1 With and Without Development Traffic Volumes

5.1.1 PRECINCT 10 OPENING YEAR (2024) TRAFFIC VOLUMES

'With development' traffic volumes at the completion of stage 10 (2024) were adopted from the Premise traffic model (refer Section 2.4) and are shown for the morning peak hour in Figure 21 and for the evening peak hour in Figure 22.

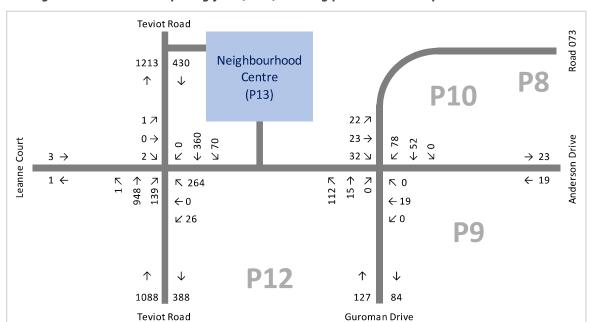
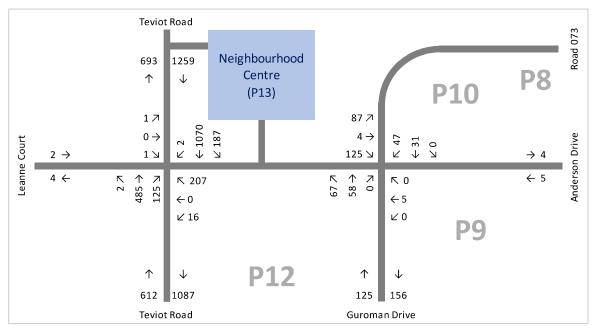


Figure 21 – Precinct 10 opening year (2024) morning peak 'with development' traffic volumes

Figure 22 – Precinct 10 opening year (2024) evening peak 'with development' traffic volumes





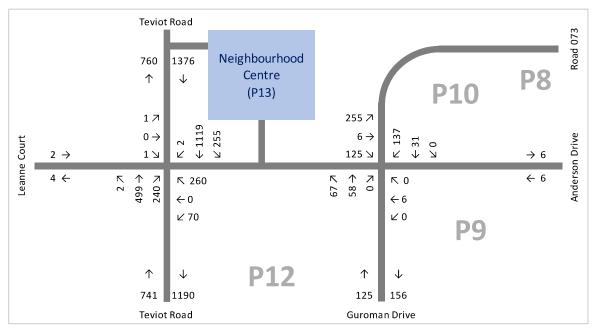
5.1.2 PRCINCT 8 OPENING YEAR (2026) TRAFFIC VOLUMES

'With development' traffic volumes at the completion of stage 8 (2026) were adopted from the Premise traffic model (refer Section 2.4) and are shown for the morning peak hour in Figure 23 and for the evening peak hour in Figure 24.

Teviot Road Road 073 Neighbourhood 1321 469 Centre (P13) 17 65 🗷 R 229 ←375 31 → $0 \rightarrow$ ←52 Anderson Drive 0 V 94 Leanne Court 2 🛚 32 🛭 $3 \rightarrow$ → 31 185 ₪ 112 A $15 \rightarrow$ **7** 0 ← 25 **∇** 0 **⊼** 343 ← 25 \leftarrow 0 ∠ 117 ∠ 0 P12 \uparrow \downarrow \uparrow \downarrow 1163 494 127 84 **Teviot Road** Guroman Drive

Figure 23 - Precinct 8 opening year (2026) morning peak 'with development' traffic volumes

Figure 24 - Precinct 8 opening year (2026) evening peak 'with development' traffic volumes





5.1.3 DESIGN YEAR (2036) TRAFFIC VOLUMES

Morning and evening peak 'with development' traffic volumes for the design year (2036) were adopted from the Premise traffic model (refer Section 2.4) and are attached in Appendix C.

Annual Average Daily Traffic (AADT) volumes estimated for road links within the assessment area and precincts 8 & 10 are outlined in Table 4.

Road Link

Two-way AADT (vehicles per day)

Anderson Drive between Teviot Road and Guroman Drive

15,336vpd

Unnamed Road 073 north of Anderson Drive

2,890vpd

All other road links (precincts 8 & 10)

< 3,000vpd

Table 4 – Design year (2036) road link AADT

5.2 Road Safety Impact Assessment and Mitigation

The GTIA specifies the following two (2) stage process for assessment of road safety impacts:

- 1. Road Safety Risk Assessment to determine the change in risk profile associated with existing road safety issues as a result of the development; and
- Road Environment Safety Assessment to determine if changes to infrastructure require either a road safety audit by an accredited road safety auditor (RSA) or a road safety assessment by either an RSA or a registered professional engineer of Queensland (RPEQ).

5.2.1 ROAD SAFETY RISK ASSESSMENT

Existing road safety issues in the assessment area are identified in Section 2.6. The existing Teviot Road / Leanne Court intersection is being upgraded by LCC as part of Teviot Road upgrade (refer Section 2.3.2.1). The intersection upgrade is expected to minimise the risk of:

- Rear-end collisions by improving channelisation of turning movements;
- Entering roadway crashes by controlling conflicting traffic streams with signal control; and
- Off-path crashes by improving road alignment delineation with kerb and channel.

Therefore, all identified risks are considered to be mitigated by the development and no further mitigations are required to address existing safety issues.

5.2.2 ROAD ENVIRONMENT SAFETY ASSESSMENT

Road environment risk ratings calculated in accordance with the GTIA and design year (2036) AADT volumes include:

- Anderson Drive assessed as having a medium risk rating based on a speed limit of 50km/h and an AADT of more than 8,000vpd; and
- All other road links assessed as having low risk ratings based on speed limits of less than or equal to 50km/h and AADTs of less than 8,000vpd.



The proposed development is a Major Development as defined by the GTIA and therefore, any changes to the road environment on:

- Anderson Drive warrants a "road safety audit" by an accredited Road Safety Auditor (RSA) at the detailed design stage; and
- All other road links will not require a road safety audit but should be subject to a road safety assessment.

A road safety assessment may be conducted by either an accredited road safety auditor or a Registered Professional Engineer of Queensland (RPEQ). This requirement would be satisfied by safety reports prepared in accordance with Section 295 of the Work Health and Safety Regulation 2011 as part of the design process.

5.3 Access and Frontage Impact Assessment and Mitigation

5.3.1 INTERSECTION ANALYSIS

5.3.1.1 Precinct 8 Opening Year (2026)

Intersection analysis has been undertaken at the Teviot Road / Anderson Drive intersection based on the proposed layout (refer Figure 7) and precinct 8 opening year (2026) traffic volumes (refer Section 5.1.2). Appendix D shows the SIDRA output results for the intersection with key outputs from the SIDRA model provided in Table 5 and summarised below.

- The maximum DoS is 0.574, which is well below practical capacity;
- The maximum average delay to any movement is 66.5 seconds, which is expected under signal control; and
- The maximum queue length does not exceed 19 vehicles, which does not impact on neighbouring intersections.

Table 5 – SIDRA Output – Teviot Road / Anderson Drive, precinct 8 opening year (2026)

Movement		AM I	Peak		PM Peak					
	V (veh)	DoS	D (sec)	Q (veh)	V (veh)	DoS	D (sec)	Q (veh)		
South Appro	ach: Teviot I	Road								
Left	1	0.001	25.0	0.0	2	0.002	17.3	0.1		
Through	1028	0.411	24.3	13.5	525	0.164	13.1	4.8		
Right	195	0.395	43.8	9.3	253	0.564	48.3	13.0		
East Approac	ch: Andersor	n Drive								
Left	123	0.266	44.1	5.8	74	0.308	58.5	4.0		
Through	1	0.391	39.7	8.8	1	0.574	54.2	7.8		
Right	361	0.391	45.3	8.8	274	0.574	59.8	7.8		
North Appro	ach: Teviot I	Road								
Left	99	0.105	20.7	2.9	268	0.272	20.7	8.2		
Through	395	0.322	42.9	6.5	1178	0.567	32.9	18.3		
Right	1	0.012	65.8	0.1	2	0.023	66.2	0.1		
West Approa	West Approach: Leanne Co									
Left	1	0.012	65.8	0.1	1	0.012	65.8	0.1		
Through	1	0.035	60.8	0.2	1	0.023	60.5	0.1		
Right	2	0.035	66.5	0.2	1	0.023	66.2	0.1		



Appendix D shows the SIDRA output results for the Anderson Drive / Guroman Drive roundabout based on the proposed layout (refer Figure 8) and precinct 8 opening year (2026) traffic volumes (refer Section 5.1.2). Key outputs from the SIDRA model are provided in Table 6 and summarised below:

- The maximum DoS is 0.289, which is well below practical capacity;
- The maximum average delay to any movement is 10.4 seconds, which is low; and
- The maximum queue length does not exceed two (2) vehicles, which is short.

Table 6 - SIDRA Output - Anderson Drive / Guroman Drive, precinct 8 opening year (2026)

Movement		AM I	Peak			PM I	Peak	
	V (veh)	DoS	D (sec)	Q (veh)	V (veh)	DoS	D (sec)	Q (veh)
South Appro	ach: Gurom	an Drive						
Left	118	0.124	5.2	0.6	71	0.111	4.6	0.6
Through	16	0.124	5.3	0.6	61	0.111	4.7	0.6
Right	1	0.124	10.2	0.6	1	0.111	9.6	0.6
East Approac	ch: Andersor	n Drive						
Left	1	0.027	5.3	0.1	1	0.008	5.2	0.0
Through	26	0.027	5.5	0.1	6	0.008	5.3	0.0
Right	1	0.027	10.4	0.1	1	0.008	10.2	0.0
North Appro	ach: Road 0	73						
Left	1	0.215	4.2	1.2	1	0.147	4.5	0.8
Through	55	0.215	4.3	1.2	33	0.147	4.7	0.8
Right	241	0.215	9.2	1.2	144	0.147	9.6	0.8
West Approa	ach: Anderso	n Drive						
Left	68	0.091	3.9	0.5	268	0.289	4.2	1.8
Through	33	0.091	4.0	0.5	6	0.289	4.3	1.8
Right	34	0.091	8.9	0.5	132	0.289	9.2	1.8

5.3.1.2 Design Year Opening Year (2036)

Intersection analysis has been undertaken at the Teviot Road / Anderson Drive intersection based on the proposed layout (refer Figure 7) and design year (2036) traffic volumes (refer Section 5.1.3). Appendix E shows the SIDRA output results for the intersection with key outputs from the SIDRA model provided in Table 7 and summarised below.

- The maximum DoS is 0.819, which is below practical capacity;
- The maximum average delay to any movement is 66.5 seconds, which is expected under signal control;
- The maximum queue length does not exceed 31 vehicles, which does not impact on neighbouring intersections.



Table 7 - SIDRA Output - Teviot Road / Anderson Drive, design year (2036)

Movement		AM I	Peak		PM Peak					
	V (veh)	DoS	D (sec)	Q (veh)	V (veh)	DoS	D (sec)	Q (veh)		
South Appro	ach: Teviot I	Road								
Left	1	0.002	30.7	0.0	2	0.002	18.7	0.1		
Through	1395	0.678	34.2	23.1	738	0.240	15.3	7.4		
Right	213	0.593	53.3	11.5	324	0.804	57.7	19.3		
East Approac	ch: Andersor	n Drive								
Left	185	0.310	37.8	8.0	112	0.393	57.6	6.0		
Through	1	0.580	35.6	16.8	1	0.819	59.0	14.4		
Right	693	0.580	41.2	16.8	464	0.819	64.7	14.4		
North Appro	ach: Teviot I	Road								
Left	218	0.203	17.1	5.7	614	0.725	23.1	22.9		
Through	503	0.410	44.0	8.5	1555	0.803	39.3	30.8		
Right	1	0.012	65.8	0.1	2	0.023	66.2	0.1		
West Approa	ach: Leanne	Court								
Left	1	0.012	65.8	0.1	1	0.012	65.8	0.1		
Through	1	0.035	60.8	0.2	1	0.023	60.5	0.1		
Right	2	0.035	66.5	0.2	1	0.023	66.2	0.1		

Appendix E shows the SIDRA output results for the Anderson Drive / Guroman Drive roundabout based on the proposed layout (refer Figure 8) and precinct 8 opening year (2026) traffic volumes (refer Section 5.1.3). Key outputs from the SIDRA model are provided in Table 8 and summarised below:

- The maximum DoS is 0.612, which is below practical capacity;
- The maximum average delay to any movement is 13.3 seconds, which is low; and
- The maximum queue length does not exceed seven (7) vehicles, which will not impact on neighbouring intersections.

Table 8 – SIDRA Output – Anderson Drive / Guroman Drive, design year (2036)

Movement		AM I	Peak		PM Peak					
	V (veh)	DoS	D (sec)	Q (veh)	V (veh)	DoS	D (sec)	Q (veh)		
South Appro	ach: Gurom	an Drive								
Left	118	0.195	8.0	1.2	71	0.180	6.0	1.0		
Through	26	0.195	8.2	1.2	102	0.180	6.1	1.0		
Right	1	0.195	13.1	1.2	1	0.180	11.0	1.0		
East Approac	ch: Andersor	n Drive								
Left	1	0.485	5.6	3.6	1	0.295	5.4	1.8		
Through	547	0.485	5.7	3.6	308	0.295	5.5	1.8		
Right	2	0.485	10.6	3.6	11	0.295	10.4	1.8		
North Appro	ach: Road 0	73								
Left	9	0.194	5.1	1.1	5	0.179	8.3	1.1		
Through	92	0.194	5.3	1.1	55	0.179	8.4	1.1		
Right	115	0.194	10.2	1.1	68	0.179	13.3	1.1		
West Approa	West Approach: Anderson Drive									
Left	33	0.184	3.9	1.2	127	0.612	4.8	6.2		
Through	204	0.184	4.1	1.2	561	0.612	5.0	6.2		
Right	34	0.184	9.0	1.2	132	0.612	9.8	6.2		



5.3.2 ROAD FRONTAGE ASSESSMENT

As part of Everleigh, public transport facilities are proposed along Anderson Drive and Everleigh Drive including eight (8) indented bus stops pairs as shown in Appendix B. These bus stop pairs are expected to cater for future bus services along Anderson Drive.

The development proposed road cross-sections (refer Section 3.3) show that pedestrian paths will be provided on each road link or in adjacent park land. In addition, external links to Anderson Drive and its intersection with Guroman Drive are proposed to provide access to the surrounding path network and future indented bus bays.

The proposed public transport and active transport facilities are considered adequate to support the development.

5.4 Road Link Capacity Assessment

Capacity of road links was assessed based on the design year (2036) traffic volumes outlined in Section 5.1.3 and link characteristics outlined in Economic Development Queensland's (EDQ's) "PDA Guideline No.06 – Street and Movement Network".

Anderson Drive between Teviot Road and Guroman Drive is assessed as having a capacity of 7,500 – 18,000vpd based on a two-lane trunk connector cross-section. Anderson Drive is expected to carry 15,336vpd and therefore provides sufficient capacity.

Unnamed Road 073 is assessed as having a capacity of 3,000 – 7,499vpd based on a neighbourhood connector cross-section. Road 073 is expected to carry a maximum of 2,890vpd and therefore provides sufficient capacity.

All other road links being constructed as part of precincts 8 & 10 feature access street cross-sections and have a corresponding capacity of less than 3,000vpd. The road links are not expected to carry more than 3,000vpd and therefore provide sufficient capacity.

5.5 Intersection Spacing

Minimum intersection spacing along road links within precincts 8 & 10 was assessed based on design year (2036) road link AADT values outlined in Table 4 and intersection spacing requirements outlined in EDQ's "PDA Guideline No.06 – Street and Movement Network". It is noted that traffic volumes within the development site are not expected to increase beyond 2036 volumes.

All road links within the development site including unnamed road 073 are expected to experience AADT of less than 3,000vpd. In accordance with PDA Guideline No.06, based on an AADT of less than 3,000vpd the road links are classed as neighbourhood access streets and therefore have no minimum intersection spacing.



6. CONCLUSIONS AND RECOMMENDATIONS

6.1 Summary of Impacts and Mitigation Measures

Based on the preceding discussion this Traffic Impact Assessment makes the following conclusions:

- Risk items existing in the assessment area were identified through crash rates analysis of 16 years of historic crash data. A road safety risk assessment conducted in accordance with the GTIA concluded that the proposed upgrade of the Teviot Road / Anderson Drive will minimise the risk of all existing risk items. Therefore, no mitigation works are required to address existing road safety issues.
- A review of road environment safety assessment requirements outlined by the GTIA concluded that, changes to:
 - Anderson Drive warrants a "road safety audit" by an accredited Road Safety Auditor (RSA) at the detailed design stage; and
 - All other road links will not require a road safety audit but should be subject to a road safety assessment.

A road safety assessment may be conducted by either an accredited road safety auditor or a Registered Professional Engineer of Queensland (RPEQ). This requirement would be satisfied by safety reports prepared in accordance with Section 295 of the Work Health and Safety Regulation 2011 as part of the design process.

- Intersection analysis of the Teviot Road / Anderson Drive intersection and Anderson Drive / Guroman Drive roundabout was undertaken using SIDRA for precinct 8 opening year (2026) and design year (2036) traffic volumes. The analysis concluded that, both intersections will operate below capacity, experience acceptable delays and will not impact on neighbouring intersections.
- A road frontage assessment of proposed active transport and public transport facilities concluded that the facilities are adequate to support the development.
- A road link capacity assessment based on design year (2036) traffic volumes and link characteristics
 contained in Economic Development Queensland's "PDA Guideline No.06 Street and Movement
 Network" was undertaken. The assessment concluded that proposed cross-sections of all road links
 provide sufficient capacity to cater for anticipated traffic volumes.
- Minimum intersection spacing was determined in accordance with Economic Development Queensland's "PDA Guideline No.06 Street and Movement Network" for road links within precincts 8 & 10. Based on road link AADTs of less than 3,000vpd and the corresponding neighbourhood access street classification, the guideline doesn't require a minimum intersection spacing.

6.2 Certification Statement and Authorisation

This report was prepared by Alex Roberts under the direct supervision of Bradley Jones (RPEQ 19986).

The Traffic Impact Assessment Certification in accordance with the GTIA is attached in Appendix F.

APPENDIX A

SIDRA OUTPUT – EXISTING CONDITIONS

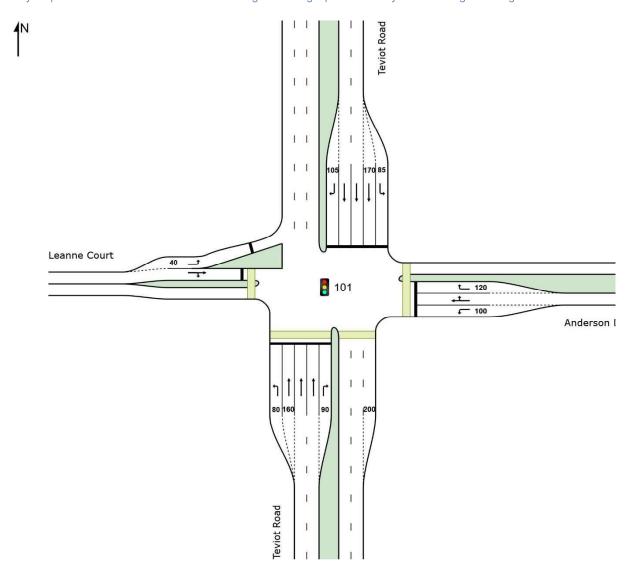
SITE LAYOUT

Site: 101 [AM Teviot / Anderson - Upgrade (Site Folder: Existing Conditions)]

Teviot Road / Anderson Drive Intersection Upgrade - 2023 Existing Traffic Volumes, Morning Peak Hour Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



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Organisation: PREMISE GROUP SERVICES PTY LTD | Licence: NETWORK / 1PC | Created: Tuesday, 22 February 2022 10:03:42 PM Project: C:\12dS\data\12dSynergy\MIR-0800 Greenbank - P8 ROL_13813\14. Engineering - Traffic\03. SIDRA\MIR-0800 SIDRA.sip9

PHASING SUMMARY

Site: 101 [AM Teviot / Anderson - Upgrade (Site Folder: Existing Conditions)]

Teviot Road / Anderson Drive Intersection Upgrade - 2023 Existing Traffic Volumes, Morning Peak Hour Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time)

Timings based on settings in the Site Phasing & Timing dialog

Phase Times determined by the program Phase Sequence: Phasing - Import Reference Phase: Phase A

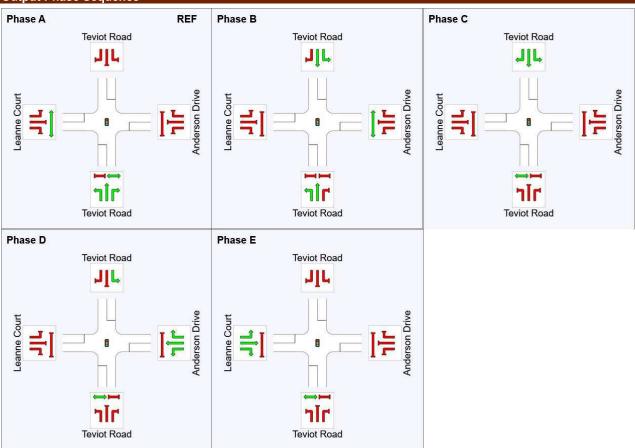
Input Phase Sequence: A, B, C, D, E Output Phase Sequence: A, B, C, D, E

Phase Timing Summary

Phase	Α	В	С	D	Е
Phase Change Time (sec)	0	40	60	72	108
Green Time (sec)	34	14	6	30	6
Phase Time (sec)	40	20	12	36	12
Phase Split	33%	17%	10%	30%	10%

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than 100%.

Output Phase Sequence



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Organisation: PREMISE GROUP SERVICES PTY LTD | Licence: NETWORK / 1PC | Processed: Friday, 18 February 2022 3:01:36 PM Project: C:\12dS\data\12dSynergy\MIR-0800 Greenbank - P8 ROL_13813\14. Engineering - Traffic\03. SIDRA\MIR-0800 SIDRA\sip9

Site: 101 [AM Teviot / Anderson - Upgrade (Site Folder: Existing Conditions)]

Teviot Road / Anderson Drive Intersection Upgrade - 2023 Existing Traffic Volumes, Morning Peak Hour Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time)

	Vehicle Movement Performance													
Mov	Turn	INPUT VO	LUMES	DEMAND I	FLOWS	Deg.	Aver.	Level of	95% BACK OF	QUEUE	Prop.	Effective	Aver. No.	Aver.
ID	Tuiti	[Total	HV]	[Total	HV]	Satn	Delay	Service	[Veh.	Dist]	Que	Stop Rate	Cycles	Speed
		veh/h	%	veh/h	%	v/c	sec		veh	m				km/h
South	: Tevio	ot Road												
1	L2	1	5.0	1	5.0	0.001	24.4	LOS C	0.0	0.2	0.56	0.60	0.56	41.9
2	T1	948	5.0	998	5.0	0.391	23.4	LOS C	12.8	93.8	0.71	0.62	0.71	43.4
3	R2	107	5.0	113	5.0	* 0.222	41.0	LOS D	5.0	36.7	0.81	0.76	0.81	35.5
Appro	ach	1056	5.0	1112	5.0	0.391	25.2	LOS C	12.8	93.8	0.72	0.63	0.72	42.4
East:	Anders	son Drive												
4	L2	1	5.0	1	5.0	0.002	41.2	LOS D	0.0	0.3	0.77	0.60	0.77	35.2
5	T1	1	5.0	1	5.0	* 0.224	38.5	LOS D	4.7	34.2	0.84	0.76	0.84	34.9
6	R2	190	5.0	200	5.0	0.224	44.2	LOS D	4.7	34.2	0.84	0.76	0.84	34.5
Appro	ach	192	5.0	202	5.0	0.224	44.1	LOS D	4.7	34.2	0.84	0.76	0.84	34.6
North	: Tevio	t Road												
7	L2	47	5.0	49	5.0	0.053	20.7	LOS C	1.4	10.3	0.52	0.68	0.52	43.7
8	T1	352	5.0	371	5.0	0.302	42.7	LOS D	6.1	44.5	0.88	0.71	0.88	35.3
9	R2	1	5.0	1	5.0	* 0.012	65.8	LOS E	0.1	0.4	0.97	0.59	0.97	28.5
Appro	ach	400	5.0	421	5.0	0.302	40.2	LOS D	6.1	44.5	0.84	0.71	0.84	36.1
West:	Leanr	ne Court												
10	L2	1	5.0	1	5.0	0.012	65.8	LOS E	0.1	0.4	0.97	0.59	0.97	28.7
11	T1	1	5.0	1	5.0	* 0.035	60.8	LOS E	0.2	1.3	0.97	0.62	0.97	29.3
12	R2	2	5.0	2	5.0	0.035	66.5	LOS E	0.2	1.3	0.97	0.62	0.97	29.0
Appro	ach	4	5.0	4	5.0	0.035	64.9	LOS E	0.2	1.3	0.97	0.61	0.97	29.0
All Ve	hicles	1652	5.0	1739	5.0	0.391	31.1	LOS C	12.8	93.8	0.76	0.67	0.76	39.6

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Critical Movement (Signal Timing)

			` •	• ,							
Pede	estrian Mo	vement l	Perforr	nance							
Mov ID	Crossing	I nput Vol.		Aver. Level of Delay Service	AVERAGE BACK [Ped	OF QUEUE Dist]		Effective Stop Rate	Travel Time	Travel Dist.	Aver. Speed
		ped/h	ped/h	sec	ped	m			sec	m	m/sec
Sout	h: Teviot Ro	oad									
P11	Stage 1	50	53	54.3 LOS E	0.2	0.2	0.95	0.95	221.6	217.5	0.98
P12	Stage 2	50	53	54.3 LOS E	0.2	0.2	0.95	0.95	216.5	210.9	0.97
East:	Anderson	Drive									
P2	Full	50	53	54.3 LOS E	0.2	0.2	0.95	0.95	221.3	217.2	0.98
West	:: Leanne C	Court									
P4	Full	50	53	54.3 LOS E	0.2	0.2	0.95	0.95	216.3	210.6	0.97
All P	edestrians	200	211	54.3 LOS E	0.2	0.2	0.95	0.95	218.9	214.1	0.98

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)

Pedestrian movement LOS values are based on average delay per pedestrian movement.

Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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PHASING SUMMARY

Site: 101 [PM Teviot / Anderson - Upgrade (Site Folder: Existing Conditions)]

Teviot Road / Anderson Drive Intersection Upgrade - 2023 Existing Traffic Volumes, Evening Peak Hour Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time)

Timings based on settings in the Site Phasing & Timing dialog

Phase Times determined by the program Phase Sequence: Phasing - Import Reference Phase: Phase A

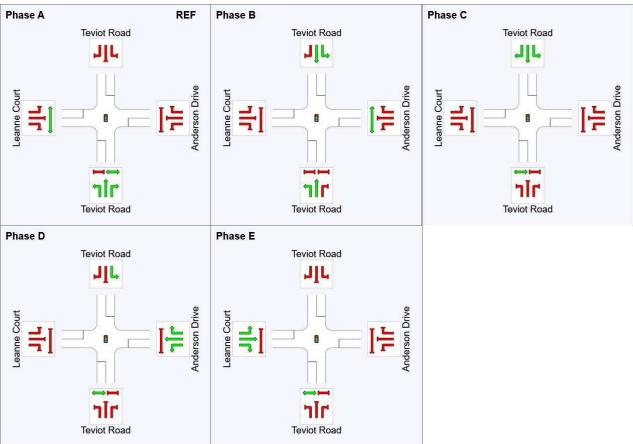
Input Phase Sequence: A, B, C, D, E Output Phase Sequence: A, B, C, D, E

Phase Timing Summary

Phase	Α	В	С	D	E
Phase Change Time (sec)	0	18	58	75	108
Green Time (sec)	12	34	11	27	6
Phase Time (sec)	18	40	17	33	12
Phase Split	15%	33%	14%	28%	10%

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than 100%.

Output Phase Sequence



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Site: 101 [PM Teviot / Anderson - Upgrade (Site Folder: Existing Conditions)]

Teviot Road / Anderson Drive Intersection Upgrade - 2023 Existing Traffic Volumes, Evening Peak Hour Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time)

	/ehicle Movement Performance													
Mov	Turn	INPUT V	DLUMES	DEMAND	FLOWS	Deg.	Aver.	Level of	95% BACK (OF QUEUE	Prop.	Effective	Aver. No.	Aver.
ID	Turri	[Total	HV]	[Total	HV]	Satn	Delay	Service	[Veh.	Dist]	Que	Stop Rate	Cycles 5	Speed
		veh/h	%	veh/h	%	v/c	sec		veh	m				km/h
South	: Tevi	ot Road												
1	L2	2	5.0	2	5.0	0.003	25.7	LOS C	0.1	0.5	0.58	0.61	0.58	41.3
2	T1	489	5.0	515	5.0	0.210	22.5	LOS C	6.2	45.0	0.66	0.55	0.66	43.8
3	R2	78	5.0	82	5.0	* 0.458	62.7	LOS E	4.7	34.4	0.99	0.77	0.99	29.3
Appro	ach	569	5.0	599	5.0	0.458	28.0	LOS C	6.2	45.0	0.71	0.58	0.71	41.0
East:	Ander	son Drive												
4	L2	1	5.0	1	5.0	0.003	44.4	LOS D	0.0	0.3	0.79	0.60	0.79	34.4
5	T1	1	5.0	1	5.0	* 0.202	40.8	LOS D	3.9	28.4	0.85	0.75	0.85	34.2
6	R2	154	5.0	162	5.0	0.202	46.4	LOS D	3.9	28.4	0.85	0.75	0.85	33.8
Appro	ach	156	5.0	164	5.0	0.202	46.4	LOS D	3.9	28.4	0.85	0.75	0.85	33.8
North:	Tevio	t Road												
7	L2	128	5.0	135	5.0	0.107	11.7	LOS B	2.5	18.2	0.34	0.66	0.34	49.0
8	T1	1046	5.0	1101	5.0	0.457	26.5	LOS C	15.2	110.8	0.76	0.67	0.76	42.0
9	R2	2	5.0	2	5.0	* 0.013	59.5	LOS E	0.1	8.0	0.93	0.62	0.93	30.0
Appro	ach	1176	5.0	1238	5.0	0.457	25.0	LOS C	15.2	110.8	0.72	0.66	0.72	42.6
West:	Leani	ne Court												
10	L2	1	5.0	1	5.0	0.012	65.8	LOS E	0.1	0.4	0.97	0.59	0.97	28.7
11	T1	1	5.0	1	5.0	* 0.023	60.5	LOS E	0.1	0.9	0.97	0.60	0.97	29.6
12	R2	1	5.0	1	5.0	0.023	66.2	LOS E	0.1	0.9	0.97	0.60	0.97	29.3
Appro	ach	3	5.0	3	5.0	0.023	64.2	LOS E	0.1	0.9	0.97	0.60	0.97	29.2
All Ve	hic l es	1904	5.0	2004	5.0	0.458	27.7	LOS C	15.2	110.8	0.73	0.65	0.73	41.2

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Critical Movement (Signal Timing)

			· ·								
Pede	estrian Mo	ovement F	Perforn	nance							
Mov ID	Crossing	Input Vol.		Aver. Level of Delay Service	AVERAGE BACK [Ped	OF QUEUE Dist]		Effective Stop Rate	Travel Time	Travel Dist.	Aver. Speed
		ped/h	ped/h	sec	ped	m			sec	m	m/sec
South	n: Teviot R	oad									
P11	Stage 1	50	53	54.3 LOS E	0.2	0.2	0.95	0.95	221.6	217.5	0.98
P12	Stage 2	50	53	54.3 LOS E	0.2	0.2	0.95	0.95	216.5	210.9	0.97
East:	Anderson	Drive									
P2	Full	50	53	54.3 LOS E	0.2	0.2	0.95	0.95	221.3	217.2	0.98
West	:: Leanne C	Court									
P4	Full	50	53	54.3 LOS E	0.2	0.2	0.95	0.95	216.3	210.6	0.97
All Pe	edestrians	200	211	54.3 LOS E	0.2	0.2	0.95	0.95	218.9	214.1	0.98

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)

Pedestrian movement LOS values are based on average delay per pedestrian movement.

Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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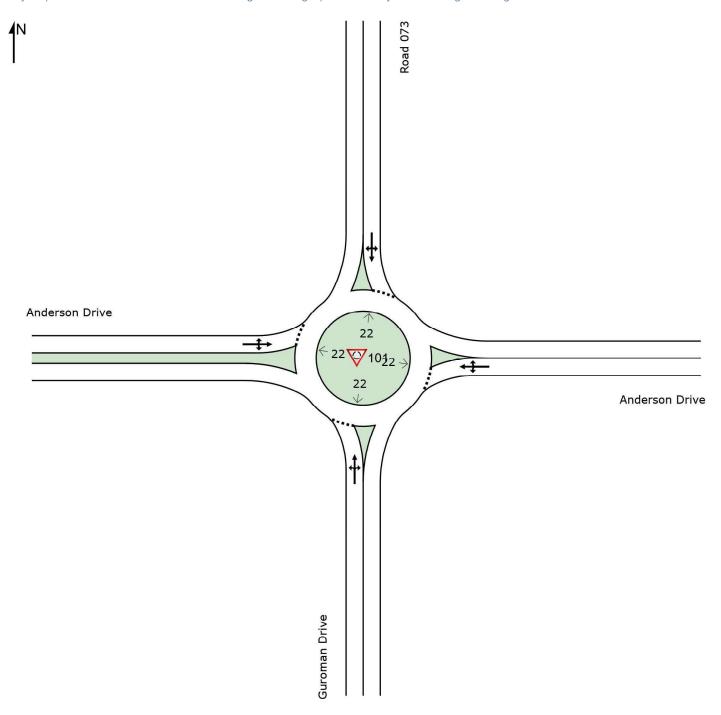
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SITE LAYOUT

Site: 101 [AM Anderson / Guroman (Site Folder: Existing Conditions)]

Anderson Drive / Guroman Drive Roundabout - 2023 Existing Traffic Volumes, Morning Peak Hour Site Category: (None) Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



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♥Site: 101 [AM Anderson / Guroman (Site Folder: Existing Conditions)]

Anderson Drive / Guroman Drive Roundabout - 2023 Existing Traffic Volumes, Morning Peak Hour

Site Category: (None)

Roundabout

Vehic	Vehicle Movement Performance													
Mov	Turn	INPUT VO	LUMES	DEMAND	FLOWS	Deg.	Aver.	Level of	95% BACK O	F QUEUE	Prop.	Effective	Aver. No.	Aver.
ID	Tulli	[Total	HV]	[Total	HV]	Satn	Delay	Service	[Veh.	Dist]	Que	Stop Rate	Cycles	Speed
		veh/h	%	veh/h	%	v/c	sec		veh	m				km/h
South	: Guroi	man Drive												
1	1 L2 112 5.0 118 5.0 0.081 3.9 LOS A 0.4 2.9 0.08 0.46 0.08													55.3
2	T1	1	5.0	1	5.0	0.081	4.0	LOS A	0.4	2.9	80.0	0.46	0.08	56.8
3	R2	1	5.0	1	5.0	0.081	8.9	LOS A	0.4	2.9	0.08	0.46	0.08	56.7
Appro	ach	114	5.0	120	5.0	0.081	3.9	LOS A	0.4	2.9	0.08	0.46	0.08	55.4
East:	Anders	on Drive												
4	L2	1	5.0	1	5.0	0.012	4.0	LOS A	0.1	0.4	0.13	0.40	0.13	54.8
5	T1	13	5.0	14	5.0	0.012	4.1	LOS A	0.1	0.4	0.13	0.40	0.13	56.2
6	R2	1	5.0	1	5.0	0.012	9.0	LOS A	0.1	0.4	0.13	0.40	0.13	56.1
Appro	ach	15	5.0	16	5.0	0.012	4.4	LOS A	0.1	0.4	0.13	0.40	0.13	56.1
North:	Road	073												
7	L2	1	5.0	1	5.0	0.002	4.0	LOS A	0.0	0.1	0.16	0.49	0.16	53.8
8	T1	1	5.0	1	5.0	0.002	4.2	LOS A	0.0	0.1	0.16	0.49	0.16	55.2
9	R2	1	5.0	1	5.0	0.002	9.0	LOS A	0.0	0.1	0.16	0.49	0.16	55.1
Appro	ach	3	5.0	3	5.0	0.002	5.7	LOS A	0.0	0.1	0.16	0.49	0.16	54.7
West:	Ander	son Drive												
10	L2	1	5.0	1	5.0	0.032	3.8	LOS A	0.1	1.1	0.03	0.59	0.03	53.0
11	T1	15	5.0	16	5.0	0.032	4.0	LOS A	0.1	1.1	0.03	0.59	0.03	54.3
12	R2	32	5.0	34	5.0	0.032	8.8	LOS A	0.1	1.1	0.03	0.59	0.03	54.3
Appro	ach	48	5.0	51	5.0	0.032	7.2	LOS A	0.1	1.1	0.03	0.59	0.03	54.3
All Ve	hicles	180	5.0	189	5.0	0.081	4.9	LOS A	0.4	2.9	0.07	0.49	0.07	55.1

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: SIDRA Roundabout LOS.

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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♥Site: 101 [PM Anderson / Guroman (Site Folder: Existing Conditions)]

Anderson Drive / Guroman Drive Roundabout - 2023 Existing Traffic Volumes, Evening Peak Hour

Site Category: (None)

Roundabout

Vehic	le Mo	vement Pe	erforma	nce										
Mov	Turn	INPUT VO	LUMES	DEMAND	FLOWS	Deg.	Aver.	Level of	95% BACK C	F QUEUE	Prop.	Effective	Aver. No.	Aver.
ID	Tulli	[Total	HV]	[Total	HV]	Satn	Delay	Service	[Veh.	Dist]	Que	Stop Rate	Cycles	Speed
		veh/h	%	veh/h	%	v/c	sec		veh	m				km/h
South	: Guro	man Drive												
1	L2	67	5.0	71	5.0	0.047	3.8	LOS A	0.2	1.7	0.04	0.46	0.04	55.4
2	T1	1	5.0	1	5.0	0.047	4.0	LOS A	0.2	1.7	0.04	0.46	0.04	56.9
3	R2	1	5.0	1	5.0	0.047	8.9	LOS A	0.2	1.7	0.04	0.46	0.04	56.9
Appro	ach	69	5.0	73	5.0	0.047	3.9	LOS A	0.2	1.7	0.04	0.46	0.04	55.5
East:	Anders	son Drive												
4	L2	1	5.0	1	5.0	0.004	4.4	LOS A	0.0	0.1	0.27	0.45	0.27	53.8
5	T1	3	5.0	3	5.0	0.004	4.5	LOS A	0.0	0.1	0.27	0.45	0.27	55.1
6	R2	1	5.0	1	5.0	0.004	9.4	LOS A	0.0	0.1	0.27	0.45	0.27	55.1
Appro	ach	5	5.0	5	5.0	0.004	5.5	LOS A	0.0	0.1	0.27	0.45	0.27	54.9
North:	Road	073												
7	L2	1	5.0	1	5.0	0.003	4.4	LOS A	0.0	0.1	0.27	0.49	0.27	53.4
8	T1	1	5.0	1	5.0	0.003	4.5	LOS A	0.0	0.1	0.27	0.49	0.27	54.8
9	R2	1	5.0	1	5.0	0.003	9.4	LOS A	0.0	0.1	0.27	0.49	0.27	54.7
Appro	ach	3	5.0	3	5.0	0.003	6.1	LOS A	0.0	0.1	0.27	0.49	0.27	54.3
West:	Ander	son Drive												
10	L2	1	5.0	1	5.0	0.083	3.8	LOS A	0.4	3.0	0.03	0.64	0.03	52.0
11	T1	3	5.0	3	5.0	0.083	4.0	LOS A	0.4	3.0	0.03	0.64	0.03	53.2
12	R2	125	5.0	132	5.0	0.083	8.8	LOS A	0.4	3.0	0.03	0.64	0.03	53.2
Appro	ach	129	5.0	136	5.0	0.083	8.7	LOS A	0.4	3.0	0.03	0.64	0.03	53.2
All Ve	hic l es	206	5.0	217	5.0	0.083	7.0	LOS A	0.4	3.0	0.04	0.57	0.04	54.0

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: SIDRA Roundabout LOS.

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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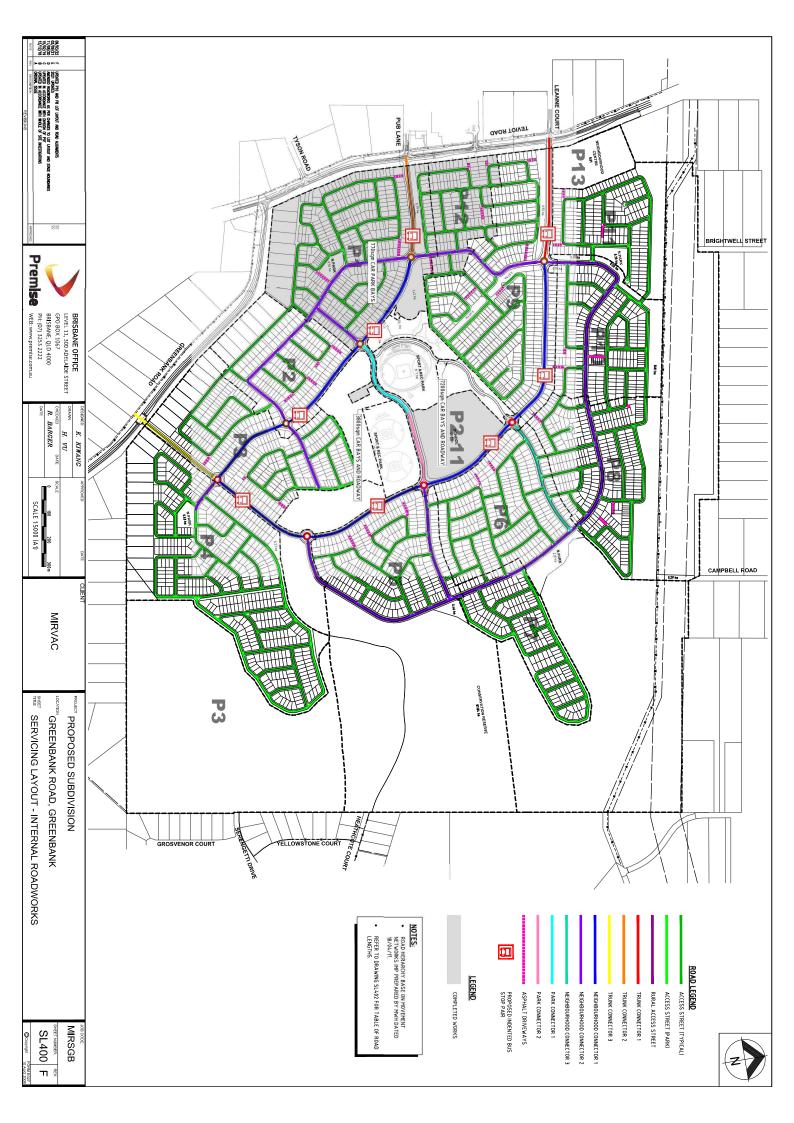
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APPENDIX B

EVERLEIGH INTERNAL ROAD LAYOUT

APPENDIX C

DESIGN YEAR (2036) TRAFFIC VOLUMES





APPENDIX D

SIDRA OUTPUT – PRECINCT 8 OPENING YEAR (2026)

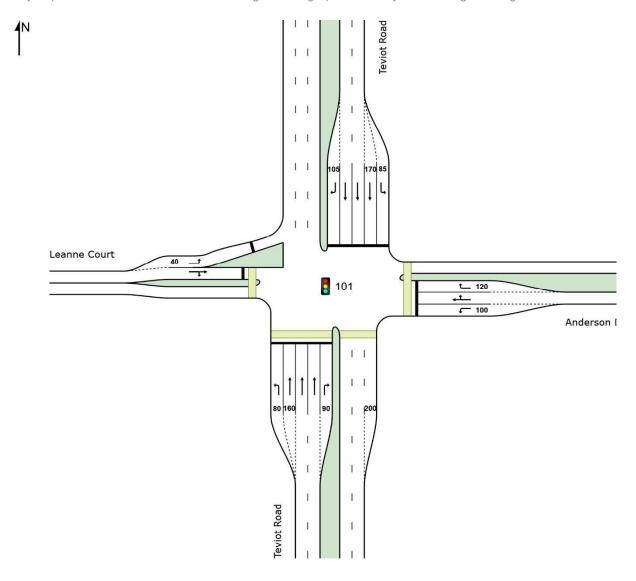
SITE LAYOUT

Site: 101 [AM Teviot / Anderson - Upgrade (Site Folder: 2026 Opening 8)]

Teviot Road / Anderson Drive Intersection Upgrade - 2026 Opening Year Traffic Volumes, Morning Peak Hour Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



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PHASING SUMMARY

Site: 101 [AM Teviot / Anderson - Upgrade (Site Folder: 2026 Opening 8)]

Teviot Road / Anderson Drive Intersection Upgrade - 2026 Opening Year Traffic Volumes, Morning Peak Hour Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time)

Timings based on settings in the Site Phasing & Timing dialog

Phase Times determined by the program Phase Sequence: Phasing - Import

Reference Phase: Phase A Input Phase Sequence: A, B, C, D, E

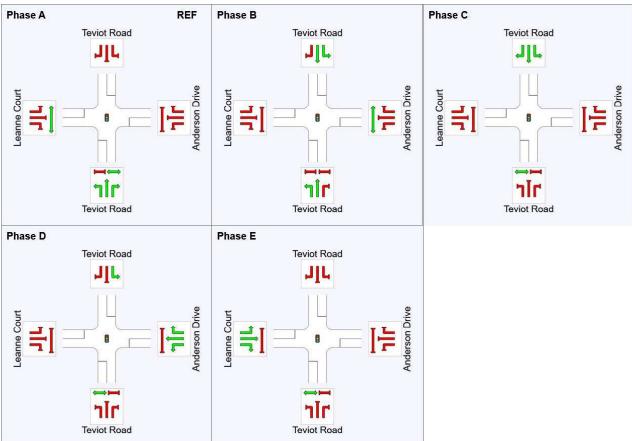
Input Phase Sequence: A, B, C, D, E Output Phase Sequence: A, B, C, D, E

Phase Timing Summary

Phase	Α	В	С	D	Е
Phase Change Time (sec)	0	39	59	71	108
Green Time (sec)	33	14	6	31	6
Phase Time (sec)	39	20	12	37	12
Phase Split	33%	17%	10%	31%	10%

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than 100%.

Output Phase Sequence



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Site: 101 [AM Teviot / Anderson - Upgrade (Site Folder: 2026 Opening 8)]

Teviot Road / Anderson Drive Intersection Upgrade - 2026 Opening Year Traffic Volumes, Morning Peak Hour Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time)

Vehi	cle Mo	vement	Perform	ance										
Mov ID	Turn	INP VOLU		DEMA FLOV		Deg. Satn		Level of Service	95% BA QUE		Prop. Que	Effective Stop Rate	Aver. No. Cyc l es	
		[Total	HV]	[Total	HV]	Oatii	Dolay	OCI VICC	[Veh.	Dist]	Que	Otop rtate	Cycles	Орсси
		veh/h	%	veh/h	%	v/c	sec		veh	m				km/h
South	า: Tevio	t Road												
1	L2	1	5.0	1	5.0	0.001	25.0	LOS C	0.0	0.2	0.57	0.60	0.57	41.6
2	T1	977	5.0	1028	5.0	0.411	24.3	LOS C	13.5	98.8	0.73	0.63	0.73	42.9
3	R2	185	5.0	195	5.0	* 0.395	43.8	LOS D	9.3	67.9	0.86	0.79	0.86	34.5
Appro	oach	1163	5.0	1224	5.0	0.411	27.4	LOS C	13.5	98.8	0.75	0.66	0.75	41.3
East:	Anders	on Drive												
4	L2	117	5.0	123	5.0	0.266	44.1	LOS D	5.8	42.0	0.84	0.77	0.84	34.3
5	T1	1	5.0	1	5.0	* 0.391	39.7	LOS D	8.8	64.1	0.87	0.79	0.87	34.5
6	R2	343	5.0	361	5.0	0.391	45.3	LOS D	8.8	64.1	0.87	0.79	0.87	34.2
Appro	oach	461	5.0	485	5.0	0.391	45.0	LOS D	8.8	64.1	0.86	0.79	0.86	34.2
North	: Teviot	Road												
7	L2	94	5.0	99	5.0	0.105	20.7	LOS C	2.9	20.8	0.53	0.70	0.53	43.8
8	T1	375	5.0	395	5.0	0.322	42.9	LOS D	6.5	47.6	0.89	0.72	0.89	35.2
9	R2	1	5.0	1	5.0	* 0.012	65.8	LOS E	0.1	0.4	0.97	0.59	0.97	28.5
Appro	oach	470	5.0	495	5.0	0.322	38.5	LOS D	6.5	47.6	0.82	0.71	0.82	36.6
West	: Leann	e Court												
10	L2	1	5.0	1	5.0	0.012	65.8	LOS E	0.1	0.4	0.97	0.59	0.97	28.7
11	T1	1	5.0	1	5.0	* 0.035	60.8	LOS E	0.2	1.3	0.97	0.62	0.97	29.3
12	R2	2	5.0	2	5.0	0.035	66.5	LOS E	0.2	1.3	0.97	0.62	0.97	29.0
Appro	oach	4	5.0	4	5.0	0.035	64.9	LOS E	0.2	1.3	0.97	0.61	0.97	29.0
All Ve	ehicles	2098	5.0	2208	5.0	0.411	33.8	LOS C	13.5	98.8	0.79	0.70	0.79	38.4

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

Pedestrian Mo	vemen	t Perfo	rmance							
Mov ID Crossing	Input Vol.	Dem. F l ow I	Aver. Level Of Delay Service		BACK OF EUE Dist 1	Prop. I Que	Effective Stop Rate	Trave l Time	Travel Dist.	Aver. Speed
	ped/h	ped/h	sec	ped	m			sec	m	m/sec
South: Teviot Ro	oad									
P11 Stage 1	50	53	54.3 LOS E	0.2	0.2	0.95	0.95	221.6	217.5	0.98
P12 Stage 2	50	53	54.3 LOS E	0.2	0.2	0.95	0.95	216.5	210.9	0.97
East: Anderson	Drive									
P2 Full	50	53	54.3 LOS E	0.2	0.2	0.95	0.95	221.3	217.2	0.98
West: Leanne C	ourt									
P4 Full	50	53	54.3 LOS E	0.2	0.2	0.95	0.95	216.3	210.6	0.97
All Pedestrians	200	211	54.3 LOS E	0.2	0.2	0.95	0.95	218.9	214.1	0.98

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)

Pedestrian movement LOS values are based on average delay per pedestrian movement.

Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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PHASING SUMMARY

Site: 101 [PM Teviot / Anderson - Upgrade (Site Folder: 2026 Opening 8)]

Teviot Road / Anderson Drive Intersection Upgrade - 2026 Opening Year Traffic Volumes, Evening Peak Hour Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time)

Timings based on settings in the Site Phasing & Timing dialog

Phase Times determined by the program Phase Sequence: Phasing - Import

Reference Phase: Phase A

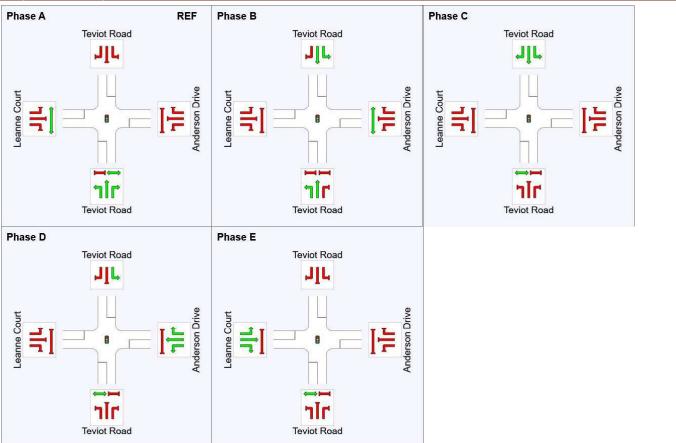
Input Phase Sequence: A, B, C, D, E Output Phase Sequence: A, B, C, D, E

Phase Timing Summary

Phase	Α	В	С	D	E
Phase Change Time (sec)	0	36	74	86	108
Green Time (sec)	30	32	6	16	6
Phase Time (sec)	36	38	12	22	12
Phase Split	30%	32%	10%	18%	10%

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than 100%.

Output Phase Sequence



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Site: 101 [PM Teviot / Anderson - Upgrade (Site Folder: 2026 Opening 8)]

Teviot Road / Anderson Drive Intersection Upgrade - 2026 Opening Year Traffic Volumes, Evening Peak Hour

Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time)

Vehi	cle Mo	vement	Perform	ance										
Mov ID	Turn	INP VOLU		DEMA FLOV		Deg. Satn		Level of Service		ACK OF EUE	Prop. Que	Effective Stop Rate	Aver. No. Cycles	
		[Total	HV]	[Total	HV]	Odin	Dolay	0011100	[Veh.	Dist]	Que	Otop Hate	- Cyolco	
		veh/h	%	veh/h	%	v/c	sec		veh	m				km/h
South	n: Tevio	t Road												
1	L2	2	5.0	2	5.0	0.002	17.3	LOS B	0.1	0.4	0.45	0.61	0.45	45.6
2	T1	499	5.0	525	5.0	0.164	13.1	LOS B	4.8	35.0	0.51	0.43	0.51	49.4
3	R2	240	5.0	253	5.0	* 0.564	48.3	LOS D	13.0	95.0	0.93	0.82	0.93	33.1
Appro	oach	741	5.0	780	5.0	0.564	24.5	LOS C	13.0	95.0	0.64	0.55	0.64	42.6
East:	Anders	on Drive												
4	L2	70	5.0	74	5.0	0.308	58.5	LOS E	4.0	29.2	0.94	0.76	0.94	30.4
5	T1	1	5.0	1	5.0	* 0.574	54.2	LOS D	7.8	56.8	0.99	0.80	0.99	30.4
6	R2	260	5.0	274	5.0	0.574	59.8	LOS E	7.8	56.8	0.99	0.80	0.99	30.1
Appro	oach	331	5.0	348	5.0	0.574	59.5	LOS E	7.8	56.8	0.98	0.79	0.98	30.2
North	: Teviot	Road												
7	L2	255	5.0	268	5.0	0.272	20.7	LOS C	8.2	59.7	0.57	0.74	0.57	43.8
8	T1	1119	5.0	1178	5.0	* 0.567	32.9	LOS C	18.3	133.5	0.86	0.75	0.86	39.1
9	R2	2	5.0	2	5.0	0.023	66.2	LOS E	0.1	0.9	0.97	0.61	0.97	28.4
Appro	oach	1376	5.0	1448	5.0	0.567	30.7	LOS C	18.3	133.5	0.80	0.74	0.80	39.9
West	: Leann	e Court												
10	L2	1	5.0	1	5.0	0.012	65.8	LOS E	0.1	0.4	0.97	0.59	0.97	28.7
11	T1	1	5.0	1	5.0	* 0.023	60.5	LOS E	0.1	0.9	0.97	0.60	0.97	29.6
12	R2	1	5.0	1	5.0	0.023	66.2	LOS E	0.1	0.9	0.97	0.60	0.97	29.3
Appro	oach	3	5.0	3	5.0	0.023	64.2	LOS E	0.1	0.9	0.97	0.60	0.97	29.2
All Ve	ehic l es	2451	5.0	2580	5.0	0.574	32.8	LOS C	18.3	133.5	0.78	0.69	0.78	38.9

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Critical Movement (Signal Timing)

т	Citilo	al Moveme	iii (Sigii	ai mining)							
Ped	estrian Mo	ovement F	erforn	nance							
Mo I D	v Crossing	Input Vol.		Aver. Level of Delay Service	AVERAGE BAC [Ped	K OF QUEUE Dist]	Prop. Que	Effective Stop Rate	Travel Time	Travel Dist.	Aver. Speed
		ped/h	ped/h	sec	ped	m			sec	m	m/sec
Sou	h: Teviot R	oad									
P11	Stage 1	50	53	54.3 LOS E	0.2	0.2	0.95	0.95	221.6	217.5	0.98
P12	Stage 2	50	53	54.3 LOS E	0.2	0.2	0.95	0.95	216.5	210.9	0.97
East	: Anderson	Drive									
P2	Full	50	53	54.3 LOS E	0.2	0.2	0.95	0.95	221.3	217.2	0.98
Wes	t: Leanne C	Court									
P4	Full	50	53	54.3 LOS E	0.2	0.2	0.95	0.95	216.3	210.6	0.97
All F	edestrians	200	211	54.3 LOS E	0.2	0.2	0.95	0.95	218.9	214.1	0.98

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)

Pedestrian movement LOS values are based on average delay per pedestrian movement.

Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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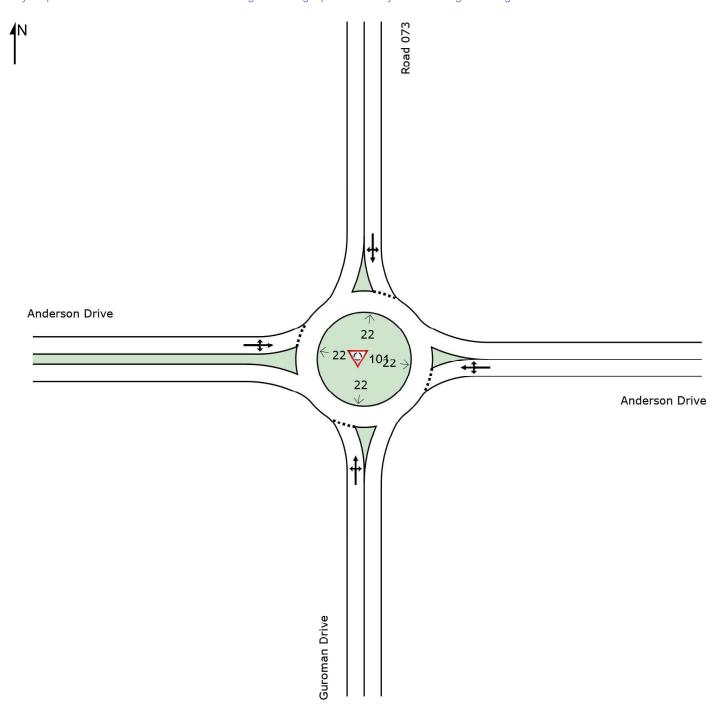
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SITE LAYOUT

♥Site: 101 [AM Anderson / Guroman (Site Folder: 2026 Opening 8)]

Anderson Drive / Guroman Drive Roundabout - 2026 Opening Year Traffic Volumes, Morning Peak Hour Site Category: (None) Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



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♥Site: 101 [AM Anderson / Guroman (Site Folder: 2026 Opening 8)]

Anderson Drive / Guroman Drive Roundabout - 2026 Opening Year Traffic Volumes, Morning Peak Hour

Site Category: (None)

Roundabout

Vehic	cle Mo	ovement P	erforma	ance										
Mov	Turn	INPUT VO	LUMES	DEMAND	FLOWS	Deg.	Aver.	Level of	95% BACK	OF QUEUE	Prop.	Effective	Aver. No.	Aver.
ID	Turn	[Total	HV]	[Total	HV]	Satn	Delay	Service	[Veh.	Dist]	Que	Stop Rate	Cycles	Speed
		veh/h	%	veh/h	%	v/c	sec		veh	m				km/h
South	: Gurd	oman Drive												
1	L2	112	5.0	118	5.0	0.124	5.2	LOS A	0.6	4.7	0.44	0.55	0.44	54.1
2	T1	15	5.0	16	5.0	0.124	5.3	LOS A	0.6	4.7	0.44	0.55	0.44	55.5
3	R2	1	5.0	1	5.0	0.124	10.2	LOS B	0.6	4.7	0.44	0.55	0.44	55.4
Appro	ach	128	5.0	135	5.0	0.124	5.3	LOS A	0.6	4.7	0.44	0.55	0.44	54.2
East:	Ander	son Drive												
4	L2	1	5.0	1	5.0	0.027	5.3	LOS A	0.1	1.0	0.45	0.50	0.45	53.4
5	T1	25	5.0	26	5.0	0.027	5.5	LOS A	0.1	1.0	0.45	0.50	0.45	54.7
6	R2	1	5.0	1	5.0	0.027	10.4	LOS B	0.1	1.0	0.45	0.50	0.45	54.7
Appro	ach	27	5.0	28	5.0	0.027	5.7	LOS A	0.1	1.0	0.45	0.50	0.45	54.7
North:	: Roac	d 073												
7	L2	1	5.0	1	5.0	0.215	4.2	LOS A	1.2	8.7	0.22	0.59	0.22	51.9
8	T1	52	5.0	55	5.0	0.215	4.3	LOS A	1.2	8.7	0.22	0.59	0.22	53.2
9	R2	229	5.0	241	5.0	0.215	9.2	LOS A	1.2	8.7	0.22	0.59	0.22	53.1
Appro	ach	282	5.0	297	5.0	0.215	8.3	LOS A	1.2	8.7	0.22	0.59	0.22	53.1
West:	Ande	rson Drive												
10	L2	65	5.0	68	5.0	0.091	3.9	LOS A	0.5	3.6	0.10	0.49	0.10	54.3
11	T1	31	5.0	33	5.0	0.091	4.0	LOS A	0.5	3.6	0.10	0.49	0.10	55.7
12	R2	32	5.0	34	5.0	0.091	8.9	LOS A	0.5	3.6	0.10	0.49	0.10	55.6
Appro	ach	128	5.0	135	5.0	0.091	5.2	LOS A	0.5	3.6	0.10	0.49	0.10	55.0
All Ve	hicles	565	5.0	595	5.0	0.215	6.8	LOS A	1.2	8.7	0.25	0.55	0.25	53.9

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: SIDRA Roundabout LOS.

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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♥Site: 101 [PM Anderson / Guroman (Site Folder: 2026 Opening 8)]

Anderson Drive / Guroman Drive Roundabout - 2026 Opening Year Traffic Volumes, Evening Peak Hour

Site Category: (None)

Roundabout

Vehic	cle Mo	ovement P	erforma	ance										
Mov	Turn	INPUT VO	LUMES	DEMAND	FLOWS	Deg.	Aver.	Level of	95% BACK	OF QUEUE	Prop.	Effective	Aver. No.	Aver.
ID	Turn	[Total	HV]	[Total	HV]	Satn	Delay	Service	[Veh.	Dist]	Que	Stop Rate	Cycles	Speed
		veh/h	%	veh/h	%	v/c	sec		veh	m				km/h
South	ı: Gurd	oman Drive												
1	L2	67	5.0	71	5.0	0.111	4.6	LOS A	0.6	4.3	0.33	0.47	0.33	54.2
2	T1	58	5.0	61	5.0	0.111	4.7	LOS A	0.6	4.3	0.33	0.47	0.33	55.7
3	R2	1	5.0	1	5.0	0.111	9.6	LOS A	0.6	4.3	0.33	0.47	0.33	55.6
Appro	ach	126	5.0	133	5.0	0.111	4.7	LOS A	0.6	4.3	0.33	0.47	0.33	54.9
East:	Ander	son Drive												
4	L2	1	5.0	1	5.0	0.008	5.2	LOS A	0.0	0.3	0.43	0.48	0.43	53.3
5	T1	6	5.0	6	5.0	0.008	5.3	LOS A	0.0	0.3	0.43	0.48	0.43	54.6
6	R2	1	5.0	1	5.0	0.008	10.2	LOS B	0.0	0.3	0.43	0.48	0.43	54.6
Appro	oach	8	5.0	8	5.0	0.008	5.9	LOS A	0.0	0.3	0.43	0.48	0.43	54.5
North	: Road	d 073												
7	L2	1	5.0	1	5.0	0.147	4.5	LOS A	8.0	5.7	0.32	0.60	0.32	51.6
8	T1	31	5.0	33	5.0	0.147	4.7	LOS A	8.0	5.7	0.32	0.60	0.32	52.9
9	R2	137	5.0	144	5.0	0.147	9.6	LOS A	8.0	5.7	0.32	0.60	0.32	52.8
Appro	oach	169	5.0	178	5.0	0.147	8.6	LOS A	8.0	5.7	0.32	0.60	0.32	52.8
West:	: Ande	rson Drive												
10	L2	255	5.0	268	5.0	0.289	4.2	LOS A	1.8	13.5	0.24	0.52	0.24	53.6
11	T1	6	5.0	6	5.0	0.289	4.3	LOS A	1.8	13.5	0.24	0.52	0.24	55.0
12	R2	125	5.0	132	5.0	0.289	9.2	LOS A	1.8	13.5	0.24	0.52	0.24	54.9
Appro	ach	386	5.0	406	5.0	0.289	5.8	LOS A	1.8	13.5	0.24	0.52	0.24	54.1
All Ve	hicles	689	5.0	725	5.0	0.289	6.3	LOS A	1.8	13.5	0.28	0.53	0.28	53.9

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: SIDRA Roundabout LOS.

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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APPENDIX E

SIDRA OUTPUT – DESIGN YEAR (2036)

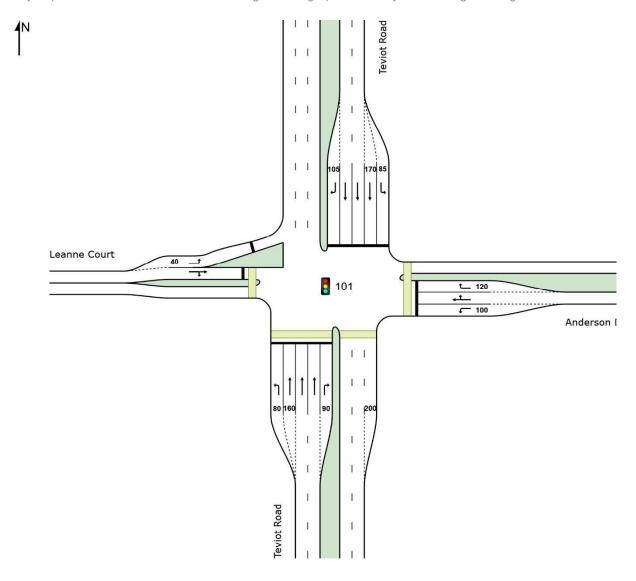
SITE LAYOUT

Site: 101 [AM Teviot / Anderson - Upgrade (Site Folder: 2036 Design Year)]

Teviot Road / Anderson Drive Intersection Upgrade - 2036 Design Year Traffic Volumes, Morning Peak Hour Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



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PHASING SUMMARY

Site: 101 [AM Teviot / Anderson - Upgrade (Site Folder: 2036 Design Year)]

Teviot Road / Anderson Drive Intersection Upgrade - 2036 Design Year Traffic Volumes, Morning Peak Hour Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time)

Timings based on settings in the Site Phasing & Timing dialog

Phase Times determined by the program Phase Sequence: Phasing - Import

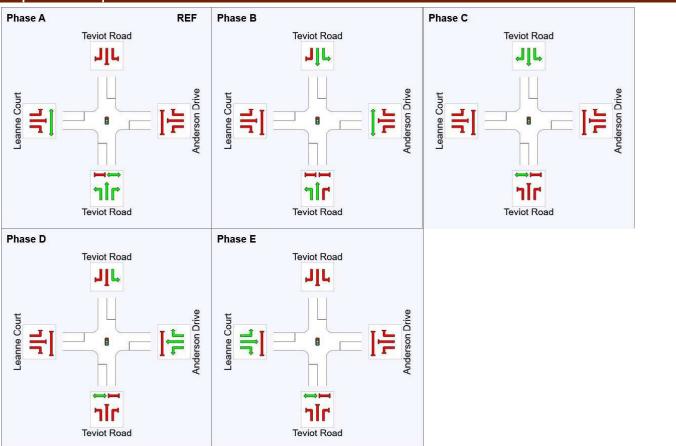
Reference Phase: Phase A Input Phase Sequence: A, B, C, D, E Output Phase Sequence: A, B, C, D, E

Phase Timing Summary

Phase	Α	В	С	D	Е
Phase Change Time (sec)	0	30	50	62	108
Green Time (sec)	24	14	6	40	6
Phase Time (sec)	30	20	12	46	12
Phase Split	25%	17%	10%	38%	10%

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than 100%.

Output Phase Sequence



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Site: 101 [AM Teviot / Anderson - Upgrade (Site Folder: 2036 Design Year)]

Teviot Road / Anderson Drive Intersection Upgrade - 2036 Design Year Traffic Volumes, Morning Peak Hour Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time)

Vehic	cle Mo	vement l	Perform	ance										
				DEMAND I	FLOWS	Deg.	Aver.	Level of	95% BACK OF	QUEUE	Prop.	Effective	Aver. No.	Aver.
ID	Turn	[Total	HV]	[Total	HV]	Satn	Delay		[Veh.	Dist]	Que	Stop Rate	Cycles	
		veh/h	%	veh/h	% -	v/c	sec		veh	m				km/h
South	ı: Tevio	t Road												
1	L2	1	5.0	1	5.0	0.002	30.7	LOS C	0.0	0.3	0.65	0.60	0.65	39.1
2	T1	1325	5.0	1395	5.0	0.678	34.2	LOS C	23.1	168.6	0.90	0.79	0.90	38.4
3	R2	202	5.0	213	5.0	* 0.593	53.3	LOS D	11.5	83.8	0.96	0.82	0.96	31.7
Appro	ach	1528	5.0	1608	5.0	0.678	36.8	LOS D	23.1	168.6	0.91	0.80	0.91	37.4
East:	Ander	son Drive												
4	L2	176	5.0	185	5.0	0.310	37.8	LOS D	8.0	58.6	0.79	0.78	0.79	36.4
5	T1	1	5.0	1	5.0	* 0.580	35.6	LOS D	16.8	122.5	0.88	0.83	0.88	35.9
6	R2	658	5.0	693	5.0	0.580	41.2	LOS D	16.8	122.5	0.88	0.83	0.88	35.5
Appro	ach	835	5.0	879	5.0	0.580	40.5	LOS D	16.8	122.5	0.86	0.82	0.86	35.7
North	: Tevio	t Road												
7	L2	207	5.0	218	5.0	0.203	17.1	LOS B	5.7	41.5	0.49	0.71	0.49	45.7
8	T1	478	5.0	503	5.0	0.410	44.0	LOS D	8.5	62.1	0.91	0.74	0.91	34.9
9	R2	1	5.0	1	5.0	* 0.012	65.8	LOS E	0.1	0.4	0.97	0.59	0.97	28.5
Appro	ach	686	5.0	722	5.0	0.410	35.9	LOS D	8.5	62.1	0.78	0.73	0.78	37.6
West:	Leanr	ne Court												
10	L2	1	5.0	1	5.0	0.012	65.8	LOS E	0.1	0.4	0.97	0.59	0.97	28.7
11	T1	1	5.0	1	5.0	* 0.035	60.8	LOS E	0.2	1.3	0.97	0.62	0.97	29.3
12	R2	2	5.0	2	5.0	0.035	66.5	LOS E	0.2	1.3	0.97	0.62	0.97	29.0
Appro	ach	4	5.0	4	5.0	0.035	64.9	LOS E	0.2	1.3	0.97	0.61	0.97	29.0
All Ve	hicles	3053	5.0	3214	5.0	0.678	37.6	LOS D	23.1	168.6	0.87	0.79	0.87	36.9

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Critical Movement (Signal Timing)

South: Teviot Road P11 Stage 1 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 221.6 217.5 0 P12 Stage 2 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 216.5 210.9 0 East: Anderson Drive P2 Full 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 221.3 217.2 0 West: Leanne Court P4 Full 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 216.3 210.6 0				, ,	٥,							
D Crossing Input Vol. Flow Delay Service Ped Dist Que Stop Rate Travel Time Travel Dist. Aver. Special Ped P	Ped	estrian Mo	vement l	Perforn	nance							
South: Teviot Road P11 Stage 1 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 221.6 217.5 0 P12 Stage 2 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 216.5 210.9 0 East: Anderson Drive P2 Full 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 221.3 217.2 0 West: Leanne Court P4 Full 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 216.3 210.6 0			Input Vol.						Effective Stop Rate	Travel Time	Travel Dist.	Aver. Speed
P11 Stage 1 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 221.6 217.5 0 P12 Stage 2 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 216.5 210.9 0 East: Anderson Drive P2 Full 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 221.3 217.2 0 West: Leanne Court P4 Full 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 216.3 210.6 0			ped/h	ped/h	sec	ped	m			sec	m	m/sec
P12 Stage 2 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 216.5 210.9 0 East: Anderson Drive P2 Full 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 221.3 217.2 0 West: Leanne Court P4 Full 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 216.3 210.6 0	Sout	h: Teviot Ro	oad									
East: Anderson Drive P2 Full 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 221.3 217.2 0 West: Leanne Court P4 Full 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 216.3 210.6 0	P11	Stage 1	50	53	54.3 LOS E	0.2	0.2	0.95	0.95	221.6	217.5	0.98
P2 Full 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 221.3 217.2 0 West: Leanne Court P4 Full 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 216.3 210.6 0	P12	Stage 2	50	53	54.3 LOS E	0.2	0.2	0.95	0.95	216.5	210.9	0.97
West: Leanne Court P4 Full 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 216.3 210.6 0	East	: Anderson	Drive									
P4 Full 50 53 54.3 LOS E 0.2 0.95 0.95 216.3 210.6 0	P2	Full	50	53	54.3 LOS E	0.2	0.2	0.95	0.95	221.3	217.2	0.98
	Wes	t: Leanne C	Court									
All Pedestrians 200 211 54.3 LOS E 0.2 0.95 0.95 218.9 214.1 0	P4	Full	50	53	54.3 LOS E	0.2	0.2	0.95	0.95	216.3	210.6	0.97
	All P	edestrians	200	211	54.3 LOS E	0.2	0.2	0.95	0.95	218.9	214.1	0.98

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)

Pedestrian movement LOS values are based on average delay per pedestrian movement.

Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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PHASING SUMMARY

Site: 101 [PM Teviot / Anderson - Upgrade (Site Folder: 2036 Design Year)]

Teviot Road / Anderson Drive Intersection Upgrade - 2036 Design Year Traffic Volumes, Evening Peak Hour Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time)

Timings based on settings in the Site Phasing & Timing dialog

Phase Times determined by the program

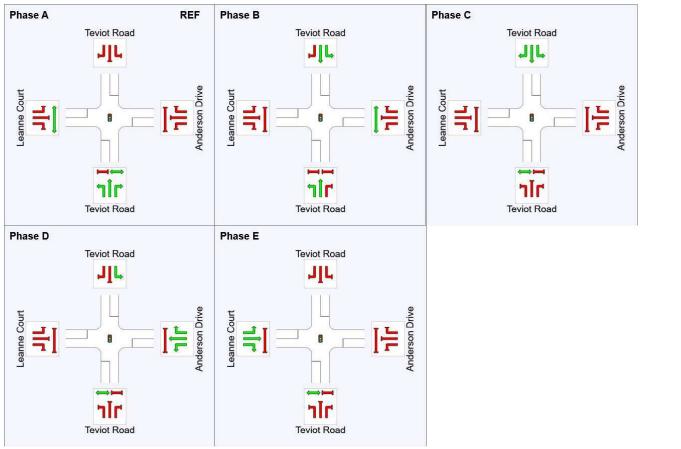
Phase Sequence: Phasing Reference Phase: Phase A Input Phase Sequence: A, B, C, D, E Output Phase Sequence: A, B, C, D, E

Phase Timing Summary

Phase	Α	В	С	D	Е
Phase Change Time (sec)	0	33	71	83	108
Green Time (sec)	27	32	6	19	6
Phase Time (sec)	33	38	12	25	12
Phase Split	28%	32%	10%	21%	10%

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than 100%.

Output Phase Sequence



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MOVEMENT SUMMARY

Site: 101 [PM Teviot / Anderson - Upgrade (Site Folder: 2036 Design Year)]

Teviot Road / Anderson Drive Intersection Upgrade - 2036 Design Year Traffic Volumes, Evening Peak Hour Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time)

Vehi	cle Mo	ovement F	Perform	ance										
Mov	Turn	INPUT VO	LUMES	DEMAND	FLOWS	Deg.	Aver.	Level of	95% BACK OF	QUEUE	Prop.	Effective	Aver. No.	Aver.
ID	Turri	[Total	HV]	[Total	HV]	Satn	Delay	Service	[Veh.	Dist]	Que	Stop Rate	Cycles :	Speed
		veh/h	%	veh/h	%	v/c	sec		veh	m				km/h
South	n: Tevi	ot Road												
1	L2	2	5.0	2	5.0	0.002	18.7	LOS B	0.1	0.4	0.47	0.61	0.47	44.8
2	T1	701	5.0	738	5.0	0.240	15.3	LOS B	7.4	54.3	0.56	0.48	0.56	48.0
3	R2	308	5.0	324	5.0	* 0.804	57.7	LOS E	19.3	140.9	1.00	0.91	1.12	30.5
Appro	oach	1011	5.0	1064	5.0	0.804	28.2	LOS C	19.3	140.9	0.70	0.61	0.73	40.8
East:	Ander	son Drive												
4	L2	106	5.0	112	5.0	0.393	57.6	LOS E	6.0	43.7	0.94	0.78	0.94	30.9
5	T1	1	5.0	1	5.0	* 0.819	59.0	LOS E	14.4	105.4	1.00	0.92	1.19	29.2
6	R2	441	5.0	464	5.0	0.819	64.7	LOS E	14.4	105.4	1.00	0.92	1.19	29.0
Appro	oach	548	5.0	577	5.0	0.819	63.3	LOS E	14.4	105.4	0.99	0.89	1.14	29.3
North	: Tevic	ot Road												
7	L2	583	5.0	614	5.0	0.735	23.1	LOS C	22.9	167.1	0.70	0.80	0.70	42.5
8	T1	1477	5.0	1555	5.0	* 0.803	39.3	LOS D	30.3	221.5	0.94	0.88	1.00	36.7
9	R2	2	5.0	2	5.0	0.023	66.2	LOS E	0.1	0.9	0.97	0.61	0.97	28.4
Appro	oach	2062	5.0	2171	5.0	0.803	34.7	LOS C	30.3	221.5	0.87	0.86	0.91	38.2
West	: Leani	ne Court												
10	L2	1	5.0	1	5.0	0.012	65.8	LOS E	0.1	0.4	0.97	0.59	0.97	28.7
11	T1	1	5.0	1	5.0	* 0.023	60.5	LOS E	0.1	0.9	0.97	0.60	0.97	29.6
12	R2	1	5.0	1	5.0	0.023	66.2	LOS E	0.1	0.9	0.97	0.60	0.97	29.3
Appro	oach	3	5.0	3	5.0	0.023	64.2	LOS E	0.1	0.9	0.97	0.60	0.97	29.2
All Ve	ehic l es	3624	5.0	3815	5.0	0.819	37.3	LOS D	30.3	221.5	0.84	0.79	0.90	37.1

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Critical Movement (Signal Timing)

South: Teviot Road P11 Stage 1 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 221.6 217.5 0 P12 Stage 2 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 216.5 210.9 0 East: Anderson Drive P2 Full 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 221.3 217.2 0 West: Leanne Court P4 Full 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 216.3 210.6 0				, ,	٥,							
D Crossing Input Vol. Flow Delay Service Ped Dist Que Stop Rate Travel Time Travel Dist. Aver. Special Ped P	Ped	estrian Mo	vement l	Perforn	nance							
South: Teviot Road P11 Stage 1 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 221.6 217.5 0 P12 Stage 2 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 216.5 210.9 0 East: Anderson Drive P2 Full 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 221.3 217.2 0 West: Leanne Court P4 Full 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 216.3 210.6 0			Input Vol.						Effective Stop Rate	Travel Time	Travel Dist.	Aver. Speed
P11 Stage 1 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 221.6 217.5 0 P12 Stage 2 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 216.5 210.9 0 East: Anderson Drive P2 Full 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 221.3 217.2 0 West: Leanne Court P4 Full 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 216.3 210.6 0			ped/h	ped/h	sec	ped	m			sec	m	m/sec
P12 Stage 2 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 216.5 210.9 0 East: Anderson Drive P2 Full 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 221.3 217.2 0 West: Leanne Court P4 Full 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 216.3 210.6 0	Sout	h: Teviot Ro	oad									
East: Anderson Drive P2 Full 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 221.3 217.2 0 West: Leanne Court P4 Full 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 216.3 210.6 0	P11	Stage 1	50	53	54.3 LOS E	0.2	0.2	0.95	0.95	221.6	217.5	0.98
P2 Full 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 221.3 217.2 0 West: Leanne Court P4 Full 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 216.3 210.6 0	P12	Stage 2	50	53	54.3 LOS E	0.2	0.2	0.95	0.95	216.5	210.9	0.97
West: Leanne Court P4 Full 50 53 54.3 LOS E 0.2 0.2 0.95 0.95 216.3 210.6 0	East	: Anderson	Drive									
P4 Full 50 53 54.3 LOS E 0.2 0.95 0.95 216.3 210.6 0	P2	Full	50	53	54.3 LOS E	0.2	0.2	0.95	0.95	221.3	217.2	0.98
	Wes	t: Leanne C	Court									
All Pedestrians 200 211 54.3 LOS E 0.2 0.95 0.95 218.9 214.1 0	P4	Full	50	53	54.3 LOS E	0.2	0.2	0.95	0.95	216.3	210.6	0.97
	All P	edestrians	200	211	54.3 LOS E	0.2	0.2	0.95	0.95	218.9	214.1	0.98

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)

Pedestrian movement LOS values are based on average delay per pedestrian movement.

Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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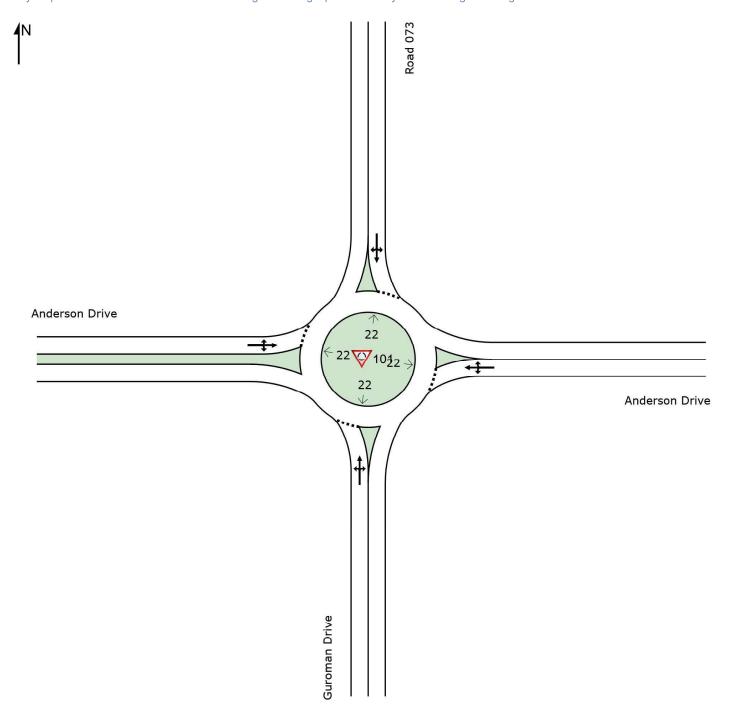
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SITE LAYOUT

♥Site: 101 [AM Anderson / Guroman (Site Folder: 2036 Design Year)]

Anderson Drive / Guroman Drive Roundabout - 2036 Design Year Traffic Volumes, Morning Peak Hour Site Category: (None) Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



MOVEMENT SUMMARY

♥Site: 101 [AM Anderson / Guroman (Site Folder: 2036 Design Year)]

Anderson Drive / Guroman Drive Roundabout - 2036 Design Year Traffic Volumes, Morning Peak Hour

Site Category: (None)

Roundabout

Vehic	ele Mo	vement P	erforma	ince										
Mov	Turn	INPUT VO	LUMES	DEMAND	FLOWS	Deg.	Aver.	Level of	95% BACK	OF QUEUE	Prop.	Effective	Aver. No.	Aver.
ID	Turn	[Total	HV]	[Total	HV]	Satn	Delay	Service	[Veh.	Dist]	Que	Stop Rate	Cycles	Speed
		veh/h	%	veh/h	%	v/c	sec		veh	m				km/h
South	: Guro	man Drive												
1	L2	112	5.0	118	5.0	0.195	8.0	LOS A	1.2	9.0	0.74	0.76	0.74	52.2
2	T1	25	5.0	26	5.0	0.195	8.2	LOS A	1.2	9.0	0.74	0.76	0.74	53.6
3	R2	1	5.0	1	5.0	0.195	13.1	LOS B	1.2	9.0	0.74	0.76	0.74	53.5
Appro	ach	138	5.0	145	5.0	0.195	8.1	LOS A	1.2	9.0	0.74	0.76	0.74	52.5
East:	Ander	son Drive												
4	L2	1	5.0	1	5.0	0.485	5.6	LOS A	3.6	26.6	0.58	0.58	0.58	52.9
5	T1	520	5.0	547	5.0	0.485	5.7	LOS A	3.6	26.6	0.58	0.58	0.58	54.2
6	R2	2	5.0	2	5.0	0.485	10.6	LOS B	3.6	26.6	0.58	0.58	0.58	54.1
Appro	ach	523	5.0	551	5.0	0.485	5.7	LOS A	3.6	26.6	0.58	0.58	0.58	54.2
North:	Road	073												
7	L2	9	5.0	9	5.0	0.194	5.1	LOS A	1.1	7.7	0.43	0.61	0.43	52.2
8	T1	87	5.0	92	5.0	0.194	5.3	LOS A	1.1	7.7	0.43	0.61	0.43	53.4
9	R2	109	5.0	115	5.0	0.194	10.2	LOS B	1.1	7.7	0.43	0.61	0.43	53.4
Appro	ach	205	5.0	216	5.0	0.194	7.9	LOS A	1.1	7.7	0.43	0.61	0.43	53.3
West:	Ande	rson Drive												
10	L2	31	5.0	33	5.0	0.184	3.9	LOS A	1.2	8.7	0.16	0.43	0.16	54.4
11	T1	194	5.0	204	5.0	0.184	4.1	LOS A	1.2	8.7	0.16	0.43	0.16	55.9
12	R2	32	5.0	34	5.0	0.184	9.0	LOS A	1.2	8.7	0.16	0.43	0.16	55.8
Appro	ach	257	5.0	271	5.0	0.184	4.7	LOS A	1.2	8.7	0.16	0.43	0.16	55.7
All Ve	hicles	1123	5.0	1182	5.0	0.485	6.2	LOS A	3.6	26.6	0.48	0.57	0.48	54.1

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: SIDRA Roundabout LOS.

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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MOVEMENT SUMMARY

♥Site: 101 [PM Anderson / Guroman (Site Folder: 2036 Design Year)]

Anderson Drive / Guroman Drive Roundabout - 2036 Design Year Traffic Volumes, Evening Peak Hour

Site Category: (None)

Roundabout

Vehic	cle Mo	vement P	erforma	ance										
Mov	Т	INPUT VO	LUMES	DEMAND	FLOWS	Deg.	Aver.	Level of	95% BACK	OF QUEUE	Prop.	Effective	Aver. No.	Aver.
ID	Turn	[Total	HV]	[Total	HV]	Satn	Delay	Service	[Veh.	Dist]	Que	Stop Rate	Cycles	Speed
		veh/h	%	veh/h	%	v/c	sec		veh	m				km/h
South	: Guro	man Drive												
1	L2	67	5.0	71	5.0	0.180	6.0	LOS A	1.0	7.6	0.56	0.61	0.56	53.3
2	T1	97	5.0	102	5.0	0.180	6.1	LOS A	1.0	7.6	0.56	0.61	0.56	54.6
3	R2	1	5.0	1	5.0	0.180	11.0	LOS B	1.0	7.6	0.56	0.61	0.56	54.5
Appro	ach	165	5.0	174	5.0	0.180	6.1	LOS A	1.0	7.6	0.56	0.61	0.56	54.0
East:	Ander	son Drive												
4	L2	1	5.0	1	5.0	0.295	5.4	LOS A	1.8	13.3	0.50	0.56	0.50	53.1
5	T1	293	5.0	308	5.0	0.295	5.5	LOS A	1.8	13.3	0.50	0.56	0.50	54.5
6	R2	10	5.0	11	5.0	0.295	10.4	LOS B	1.8	13.3	0.50	0.56	0.50	54.4
Appro	ach	304	5.0	320	5.0	0.295	5.7	LOS A	1.8	13.3	0.50	0.56	0.50	54.5
North	: Road	1 073												
7	L2	5	5.0	5	5.0	0.179	8.3	LOS A	1.1	8.3	0.75	0.79	0.75	50.4
8	T1	52	5.0	55	5.0	0.179	8.4	LOS A	1.1	8.3	0.75	0.79	0.75	51.6
9	R2	65	5.0	68	5.0	0.179	13.3	LOS B	1.1	8.3	0.75	0.79	0.75	51.5
Appro	ach	122	5.0	128	5.0	0.179	11.0	LOS B	1.1	8.3	0.75	0.79	0.75	51.5
West:	Ande	rson Drive												
10	L2	121	5.0	127	5.0	0.612	4.8	LOS A	6.2	44.9	0.51	0.51	0.51	52.9
11	T1	533	5.0	561	5.0	0.612	5.0	LOS A	6.2	44.9	0.51	0.51	0.51	54.2
12	R2	125	5.0	132	5.0	0.612	9.8	LOS A	6.2	44.9	0.51	0.51	0.51	54.2
Appro	ach	779	5.0	820	5.0	0.612	5.7	LOS A	6.2	44.9	0.51	0.51	0.51	54.0
All Ve	hicles	1370	5.0	1442	5.0	0.612	6.2	LOS A	6.2	44.9	0.54	0.56	0.54	53.9

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: SIDRA Roundabout LOS.

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

SIDRA INTERSECTION 9.0 | Copyright © 2000-2020 Akcelik and Associates Pty Ltd | sidrasolutions.com

Organisation: PREMISE GROUP SERVICES PTY LTD | Licence: NETWORK / 1PC | Processed: Friday, 4 March 2022 9:20:52 AM Project: C:\12dS\data\12dSynergy\MIR-0800 Greenbank - P8 ROL_13813\14. Engineering - Traffic\03. SIDRA\MIR-0800 SIDRA.sip9

APPENDIX F

TRAFFIC IMPACT ASSESSMENT CERTIFICATION



CERTIFICATION OF TRAFFIC IMPACT ASSESSMENT REPORT REGISTERED PROFESSIONAL ENGINEER OF QUEENSLAND FOR

Project Title	Everleigh Precinct 8 & 10: Traffic Impact Assessment
---------------	--

As a professional engineer registered by the Board of Professional Engineers of Queensland pursuant to the Professional Engineers Act 2002 as competent in my areas of nominated expertise, I understand and recognise:

- The significant role of engineering as a profession; and that
- The community has a legitimate expectation that my certification affixed to this engineering work can be trusted; and that
- I am responsible for ensuring its preparation has satisfied all necessary standards, conduct and contemporary practice.

As the responsible RPEQ, I certify:

- I am satisfied that all submitted components comprising this traffic impact assessment, listed in the following table, have been completed in accordance with the Guide to Traffic Impact Assessment published by the Queensland Department of Transport and Main Roads and using sound engineering principles; and
- ii) Where specialised areas of work have not been under my direct supervision, I have reviewed the outcomes of the work and consider the work and its outcomes as suitable for the purposes of this traffic impact assessment; and that
- iii) The outcomes of this traffic impact assessment are a true reflection of results of assessment; and that
- iv) I believe the strategies recommended for mitigating impacts by this traffic impact assessment, embrace contemporary practice initiatives and will deliver the desired outcomes.

Name	Bradley Jones
RPEQ No.	19986
RPEQ Competencies	Civil
Email	Bradley.Jones@premise.com.au
Postal Address	PO Box 1110, Townsville QLD 4810
Signature	Bladly Jan
Date	8/07/2022



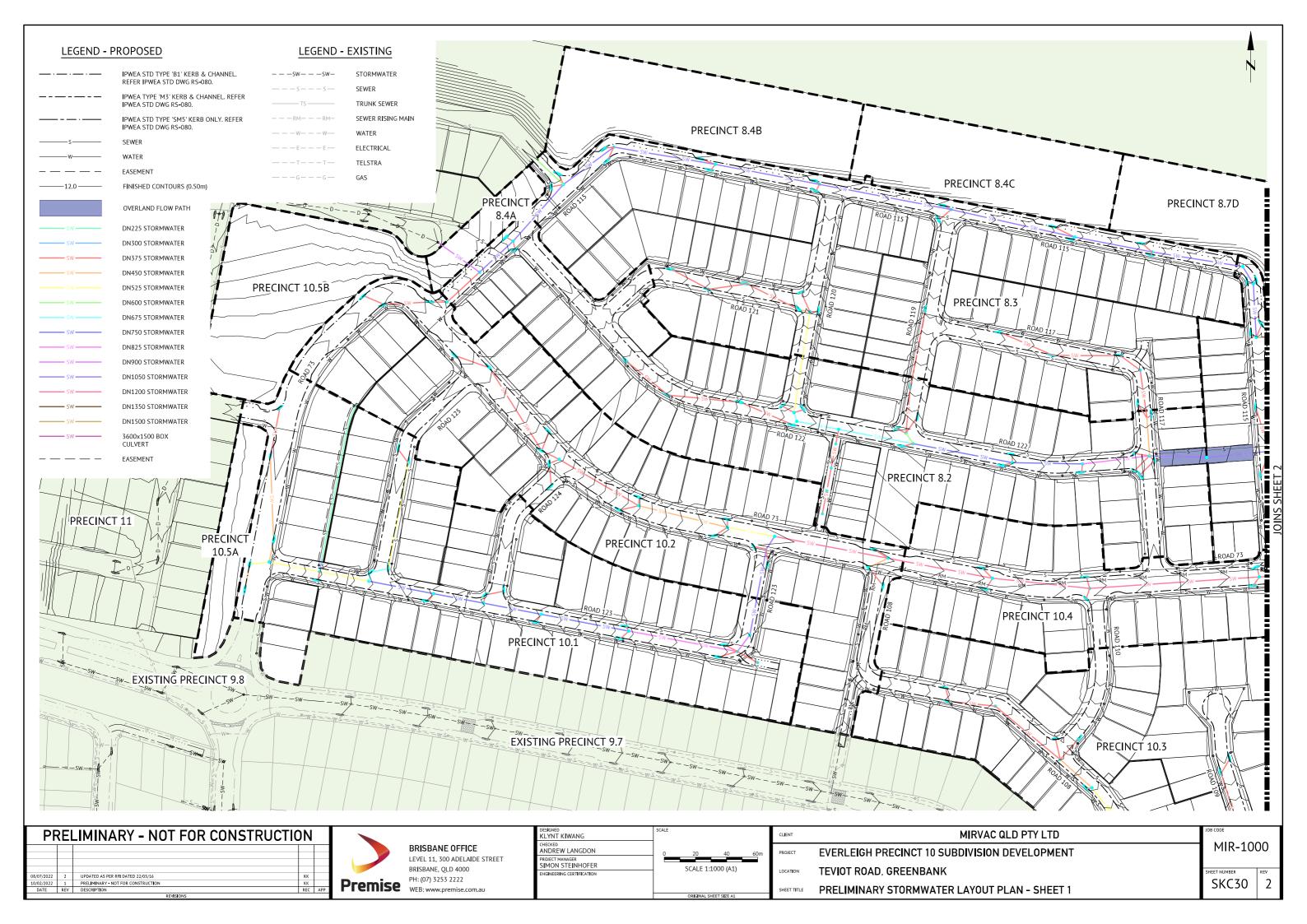
Traffic impact assessment components to which this certification applies	
1. Introduction	
Background	\boxtimes
Scope and study area	\boxtimes
Pre-lodgement meeting notes	
2. Existing Conditions	
Land use and zoning	\boxtimes
Adjacent land uses / approvals	\boxtimes
Surrounding road network details	\boxtimes
Traffic volumes	\boxtimes
Intersection and network performance	\boxtimes
Road safety issues	\boxtimes
Site access	\boxtimes
Public transport (if applicable)	\boxtimes
Active transport (if applicable)	\boxtimes
Parking (if applicable)	
Pavement (if applicable)	
Transport infrastructure (if applicable)	
3. Proposed Development Details	
Development site plan	
Operational details (including year of opening each stage and any relevant catchment / market analysis)	\boxtimes
Proposed access and parking	\boxtimes
4. Development Traffic	
Traffic generation (by development stage if relevant and considering light and heavy vehicle trips)	\boxtimes
Trip distribution	\boxtimes
Development traffic volumes on the network	\boxtimes
5. Impact Assessment and Mitigation	
With and without development traffic volumes	\boxtimes
Construction traffic impact assessment and mitigation (if applicable)	
Road safety impact assessment and mitigation	\boxtimes
Access and frontage impact assessment and mitigation	\boxtimes
Intersection delay impact assessment and mitigation	
Road link capacity assessment and mitigation	\boxtimes
Pavement impact assessment and mitigation	
Transport infrastructure impact assessment and mitigation	
Other impacts assessment relevant to the specific development type / location (if applicable) - Intersection Spacing	×
6. Conclusions and Recommendations	
Summary of impacts and mitigation measures proposed	\boxtimes
Certification statement and authorisation	\boxtimes

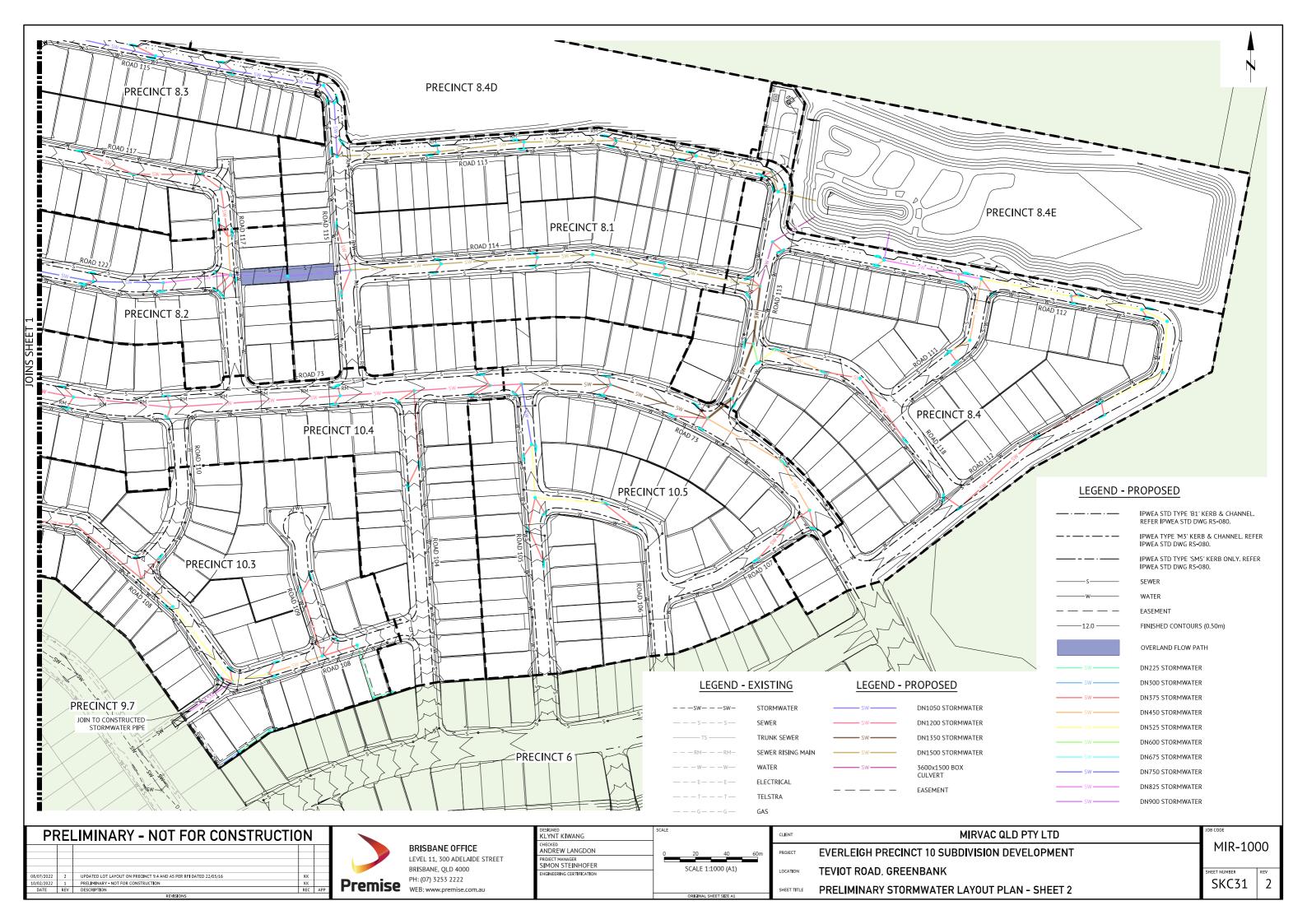






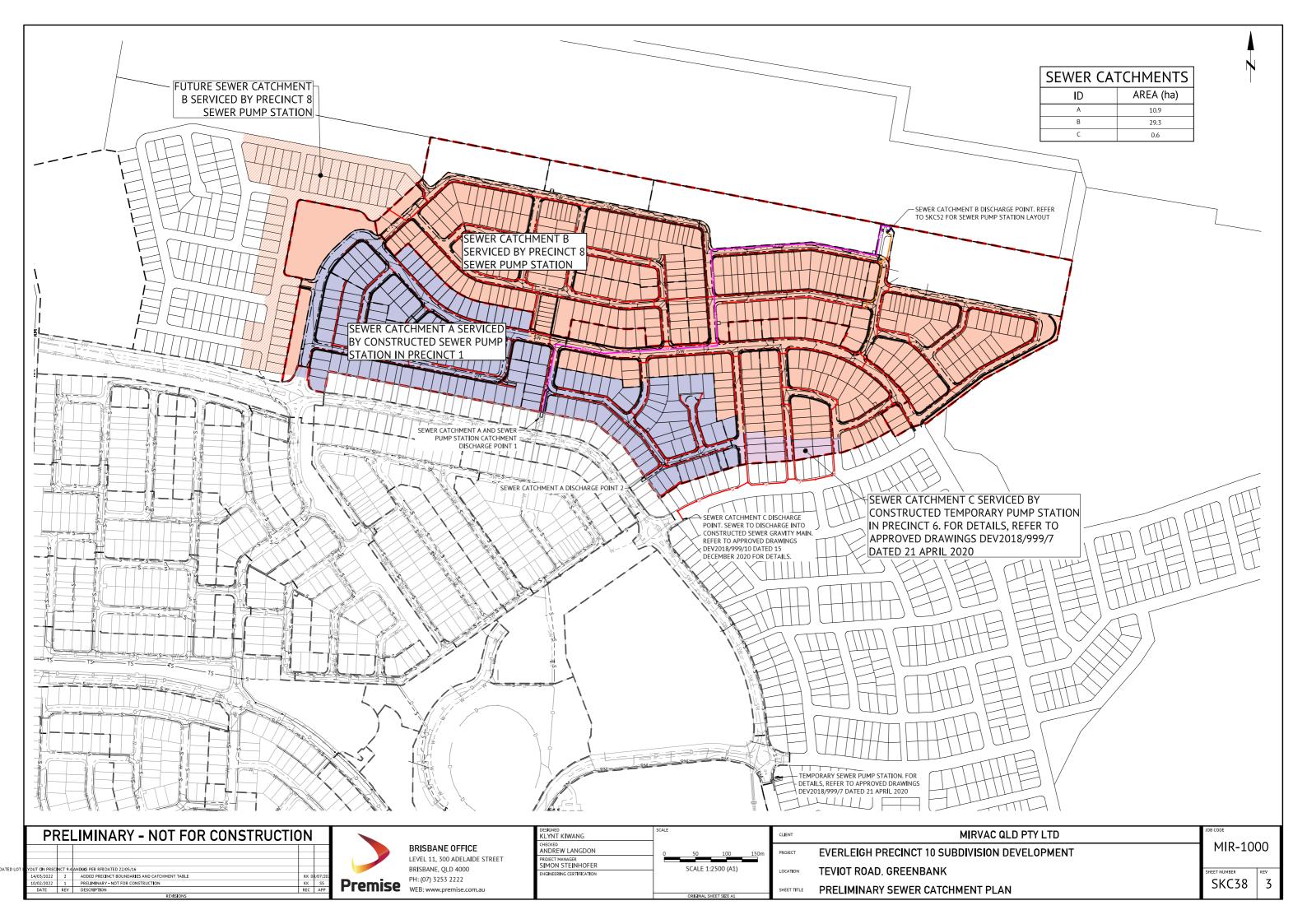
A.6 APPENDIX F – PRELIMINARY STORMWATER DRAINAGE PLANS





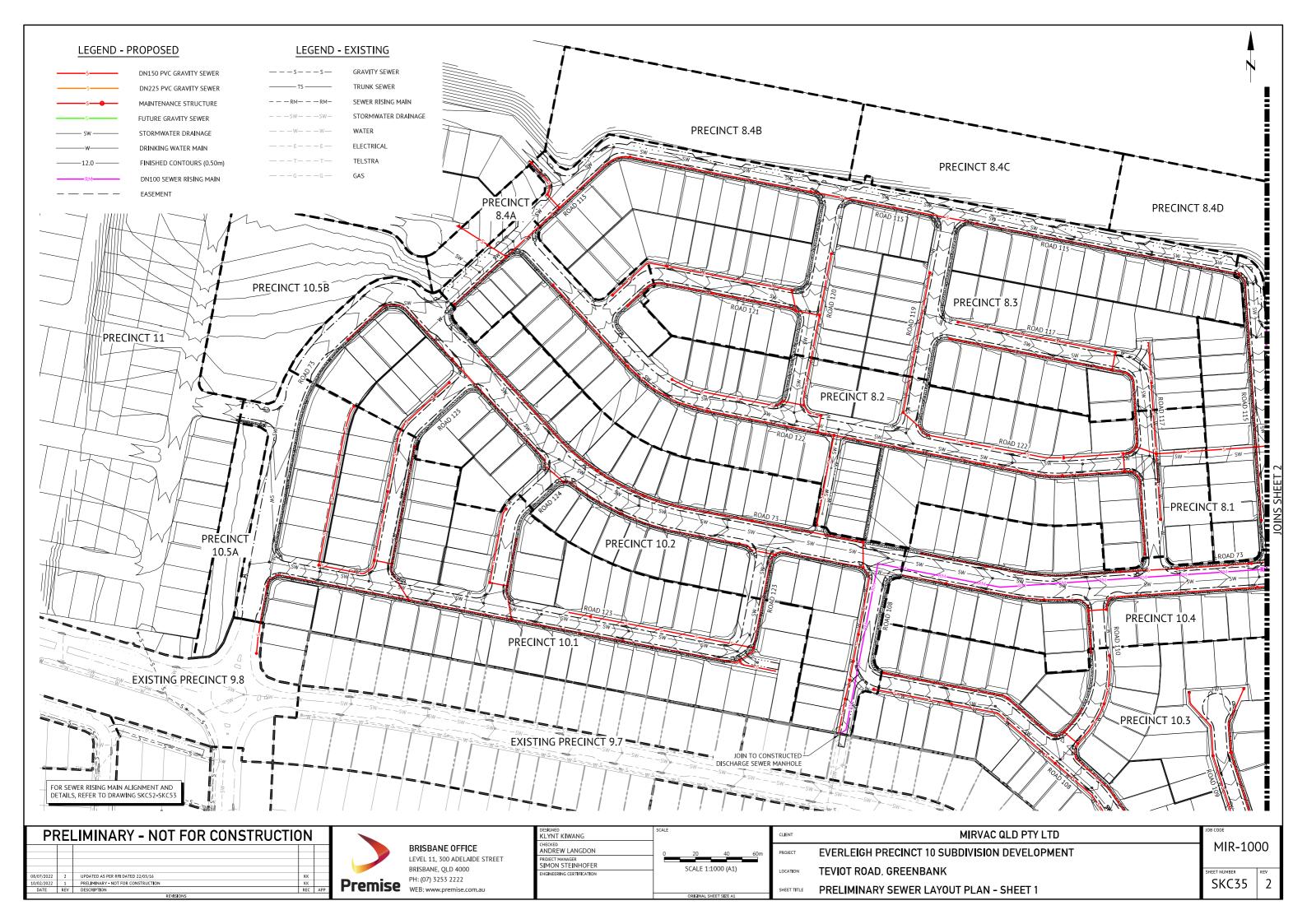


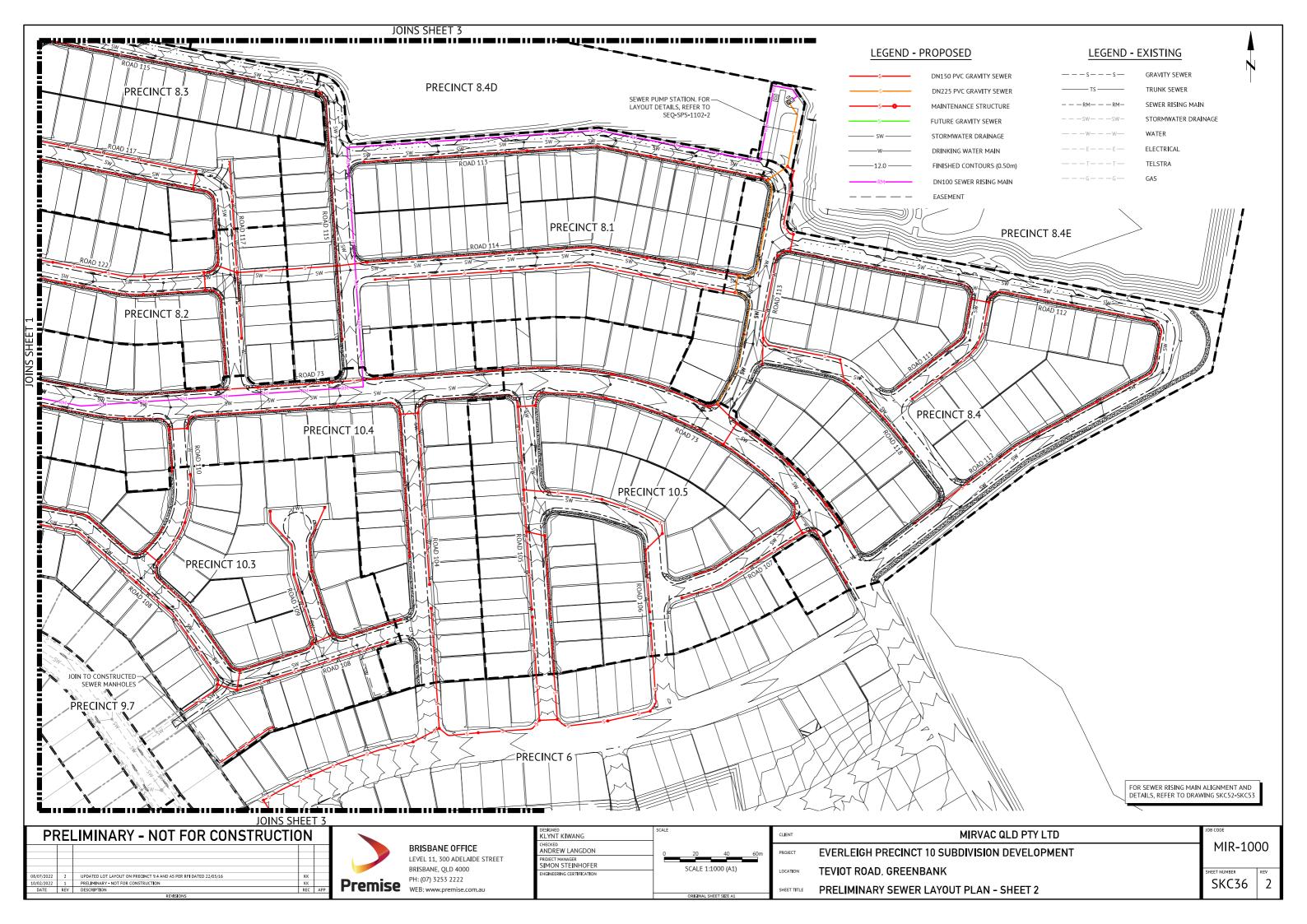
A.7 APPENDIX G – PRELIMINARY SEWER CATCHMENT PLAN

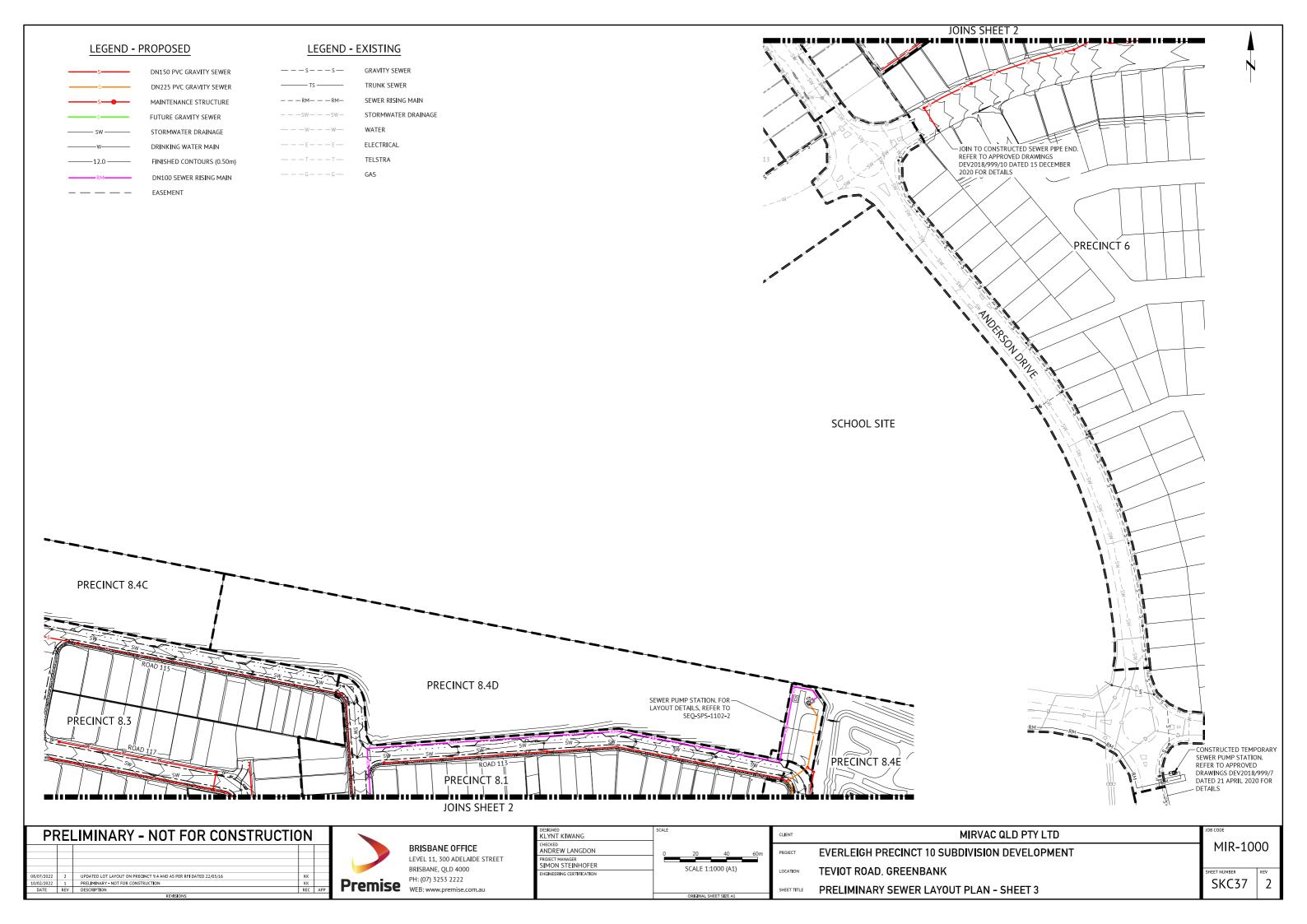


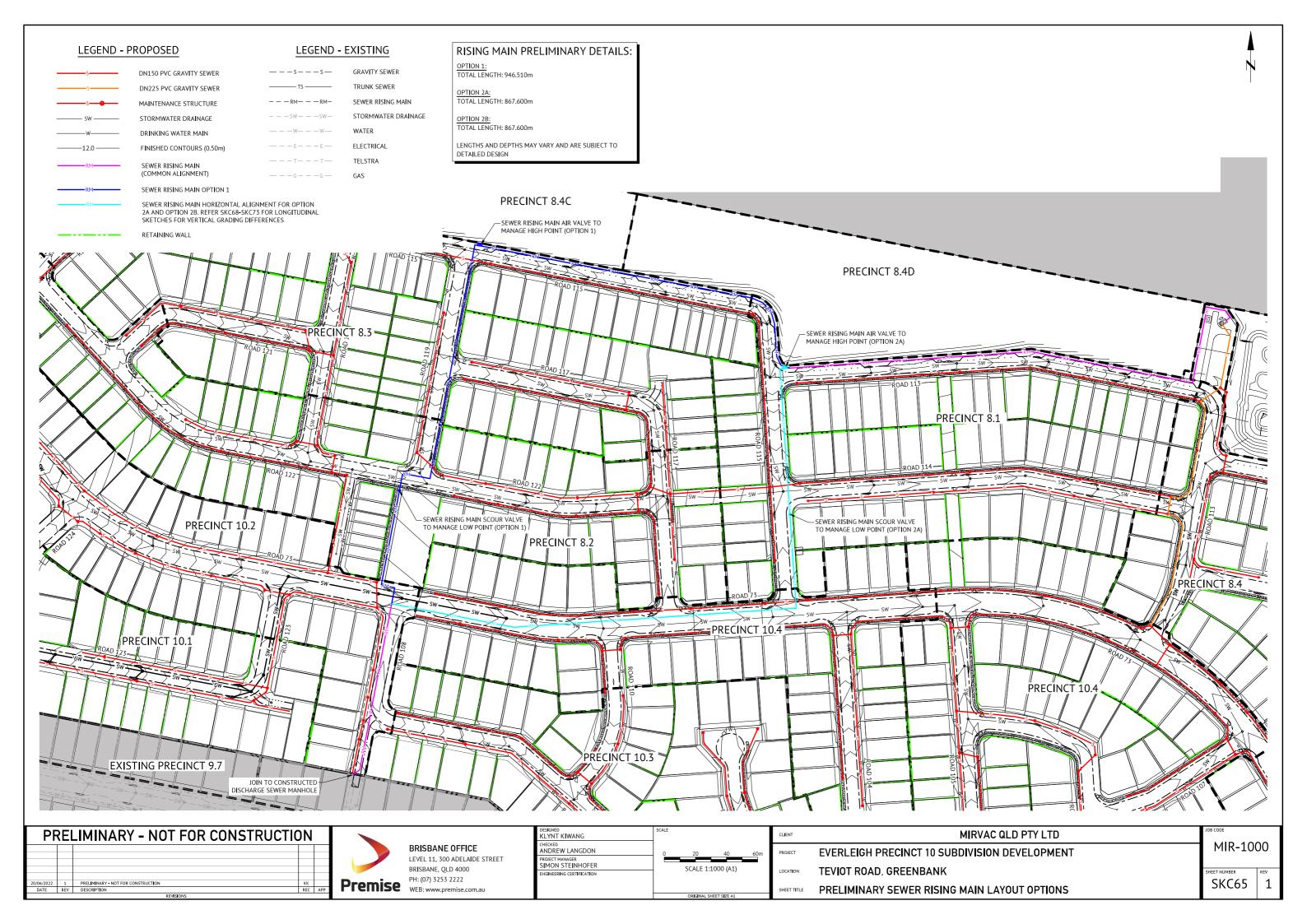


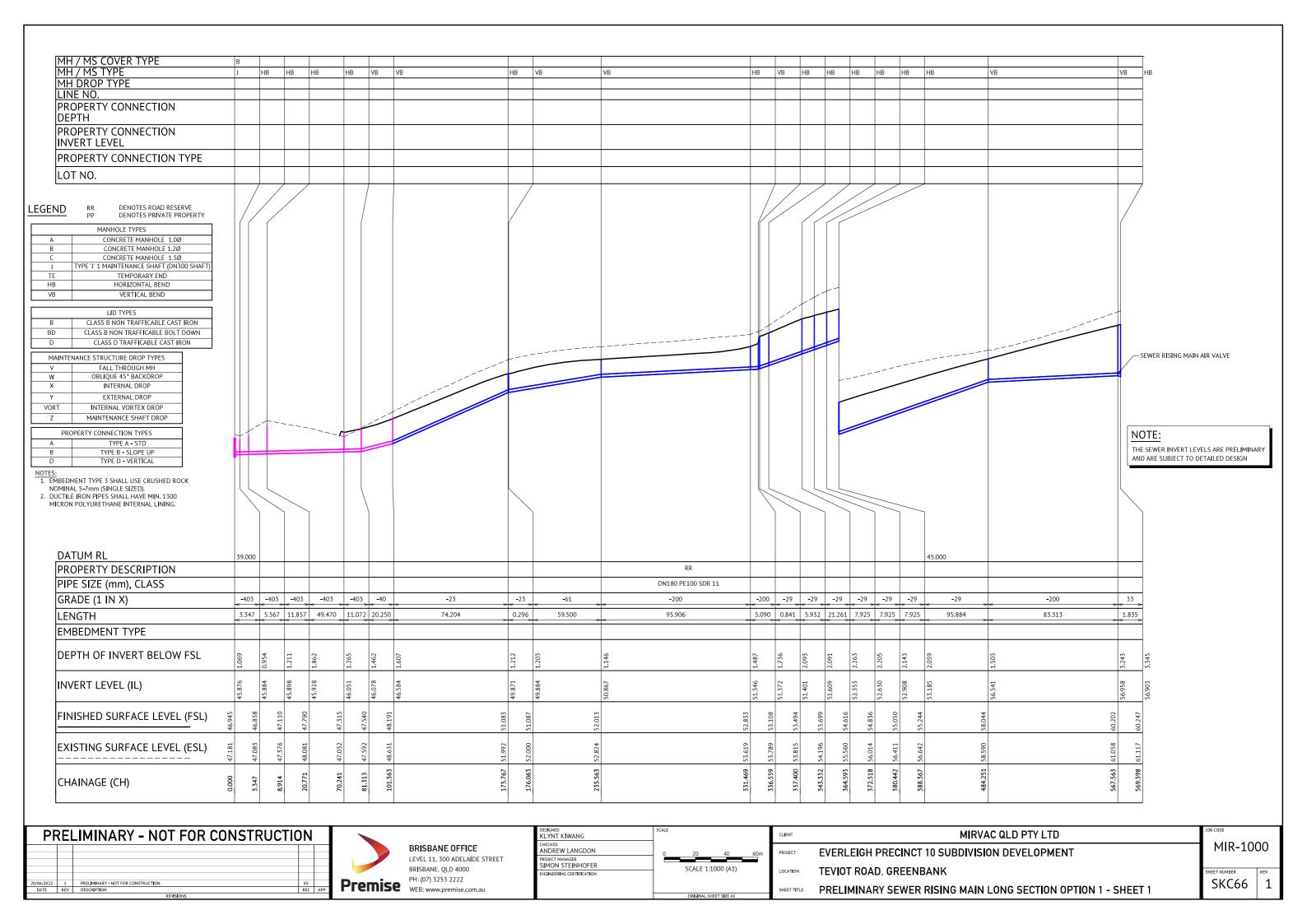
A.8 APPENDIX H – PRELIMINARY SEWER RETICULATION PLANS

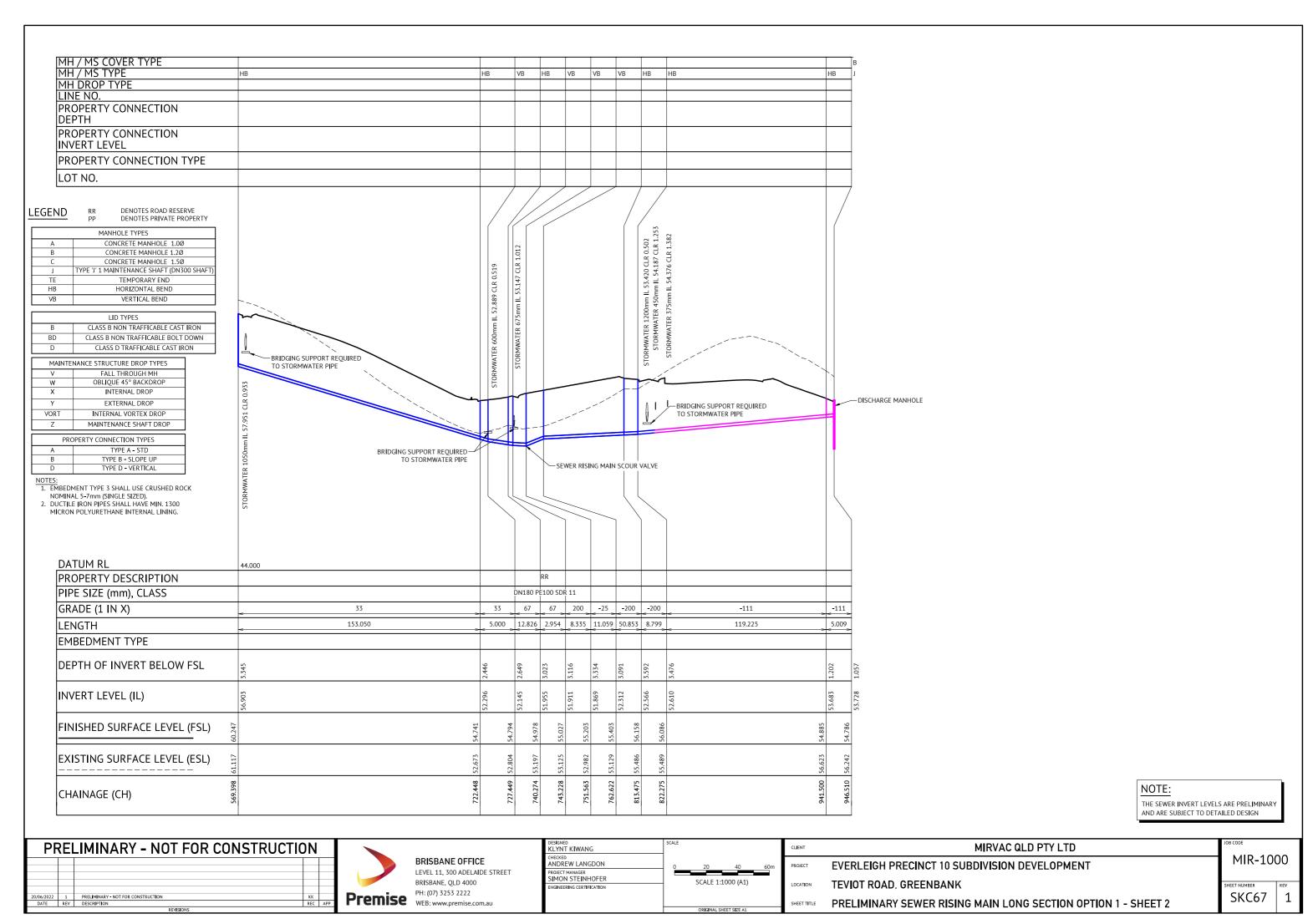


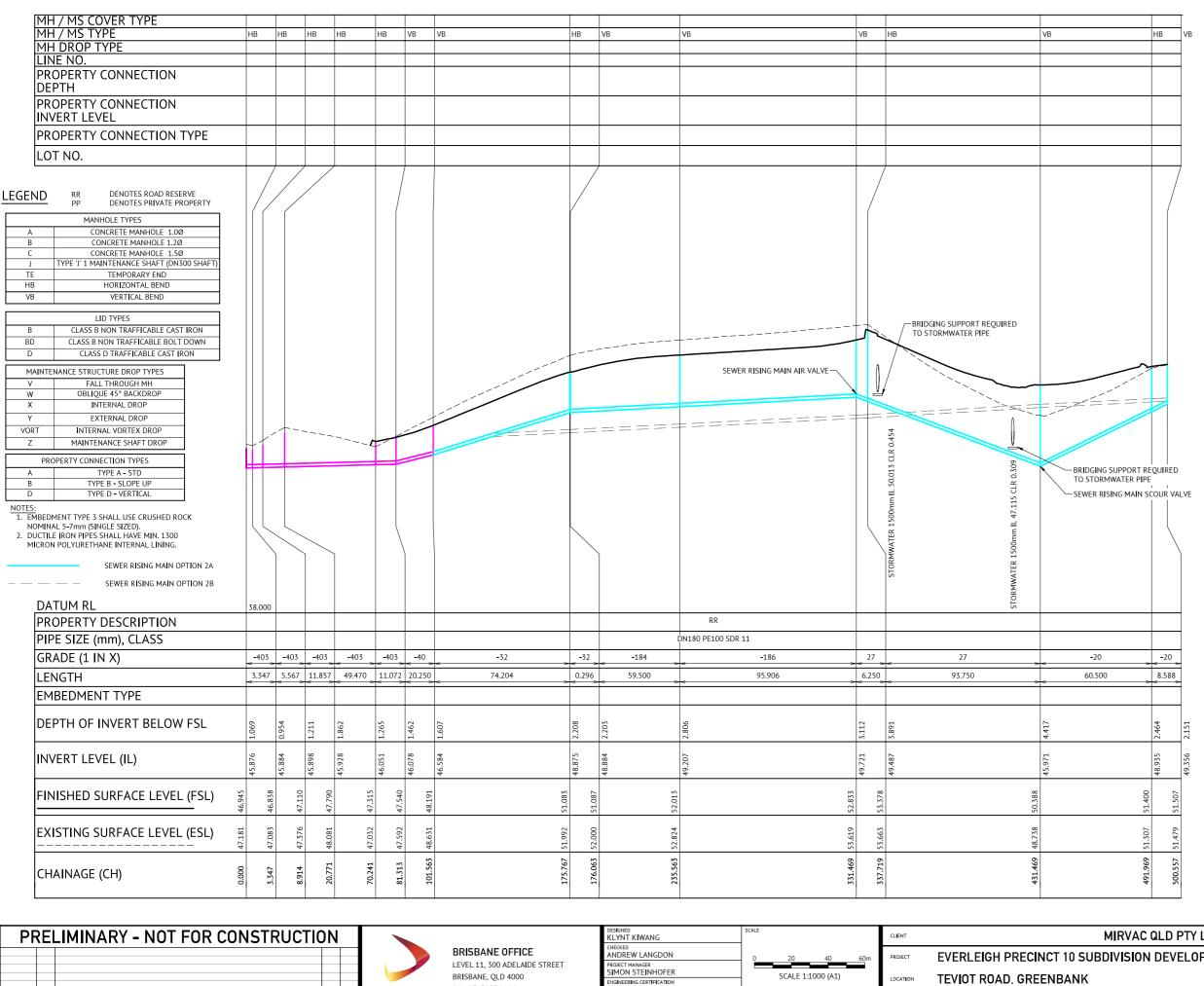












NOTE:

THE SEWER INVERT LEVELS ARE PRELIMINARY AND ARE SUBJECT TO DETAILED DESIGN.

REFER TO SKETCHES SKC72-SKC73 FOR OPTION 2B LEVELS.

PRELIMINARY - NOT FOR CONSTRUCTION

Premise PH: (U/) 3233 2222 WEB: www.premise.com.au

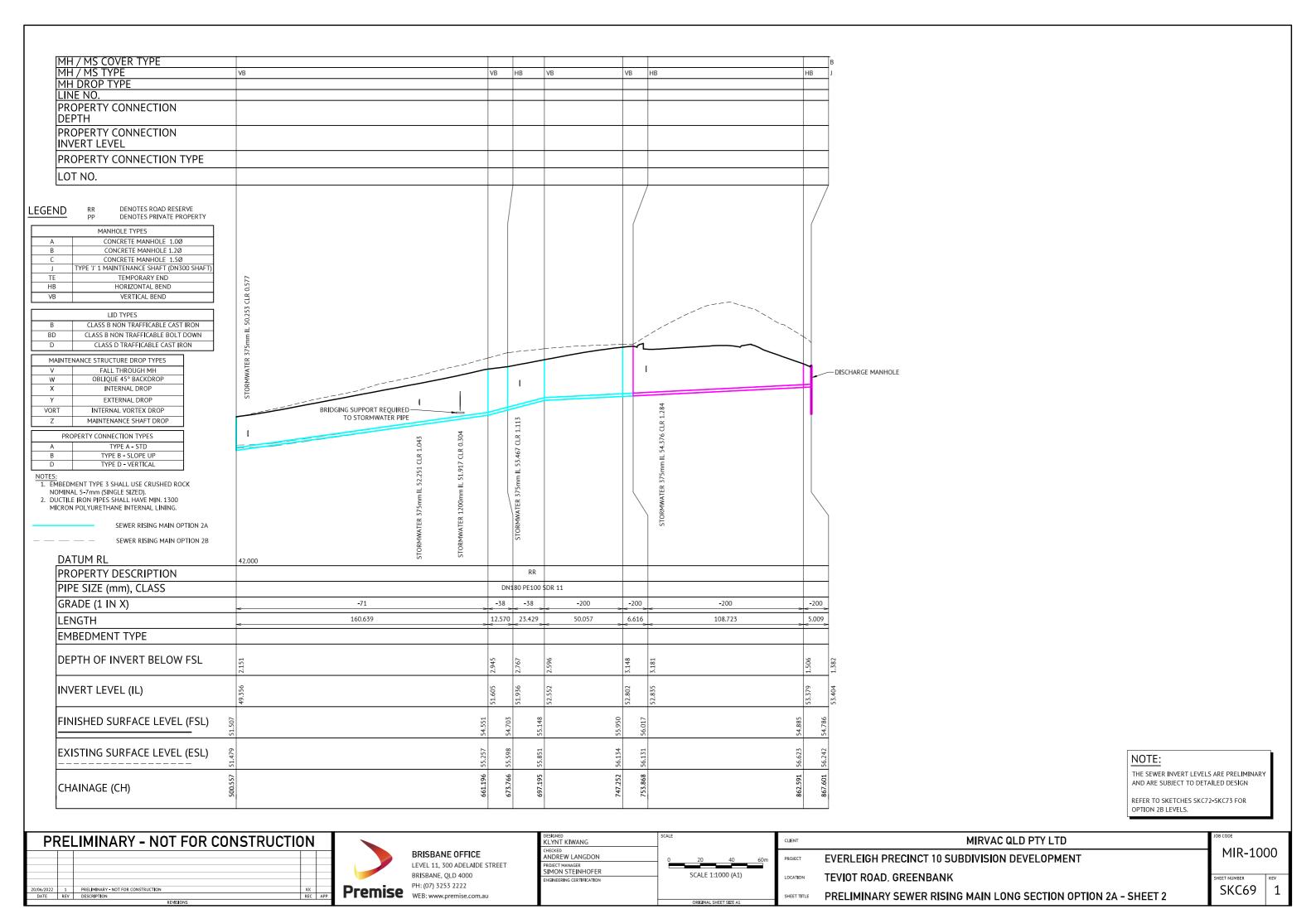
BRISBANE OFFICE LEVEL 11, 300 ADELAIDE STREET BRISBANE, QLD 4000 PH: (07) 3253 2222

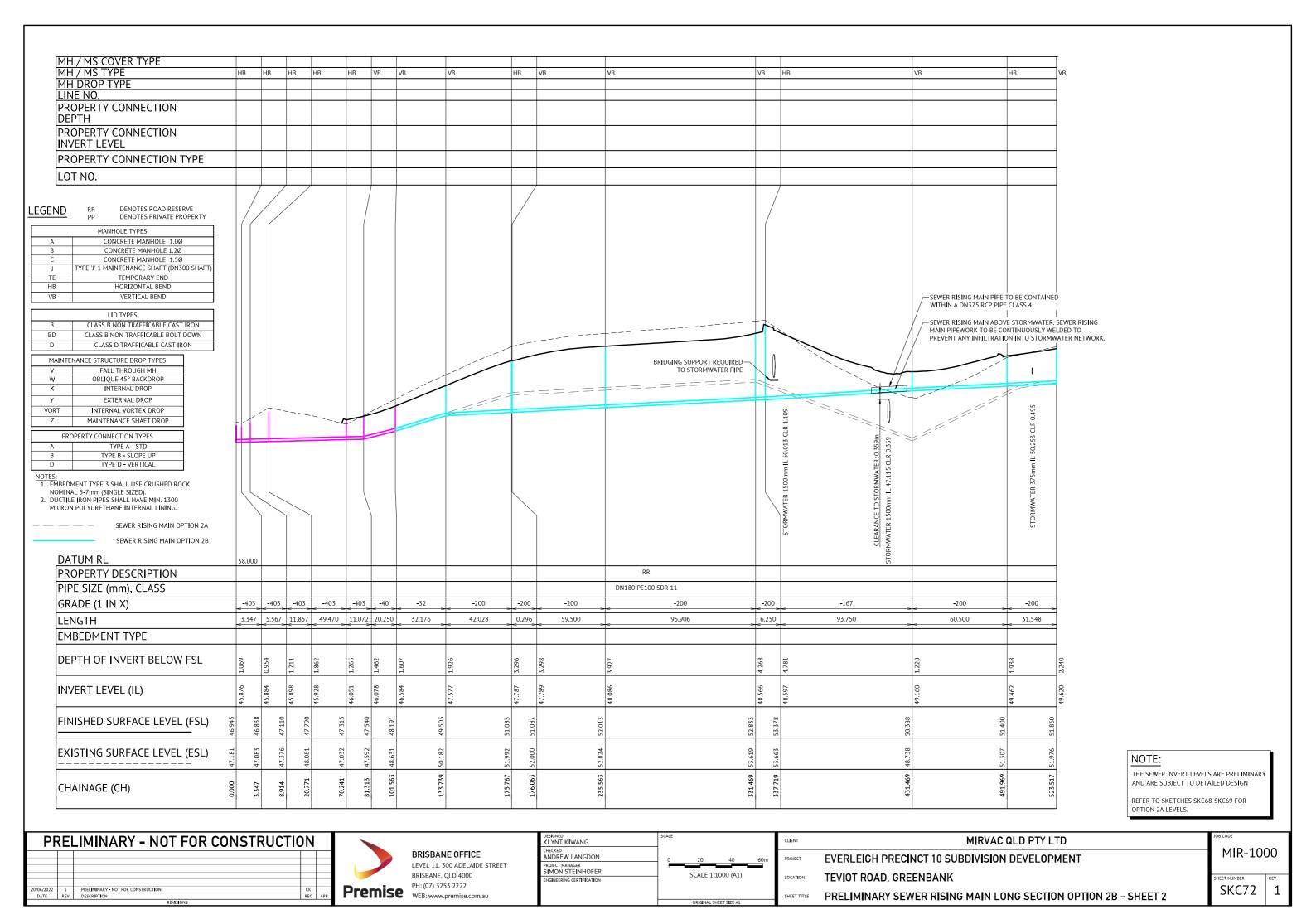
NED NT K I WANG	SCALE
REW LANGDON	0 20 40 60m
CT MANAGER DN STEINHOFER EERING CERTIFICATION	SCALE 1:1000 (A1)
	ORIGINAL SHEET SIZE A1

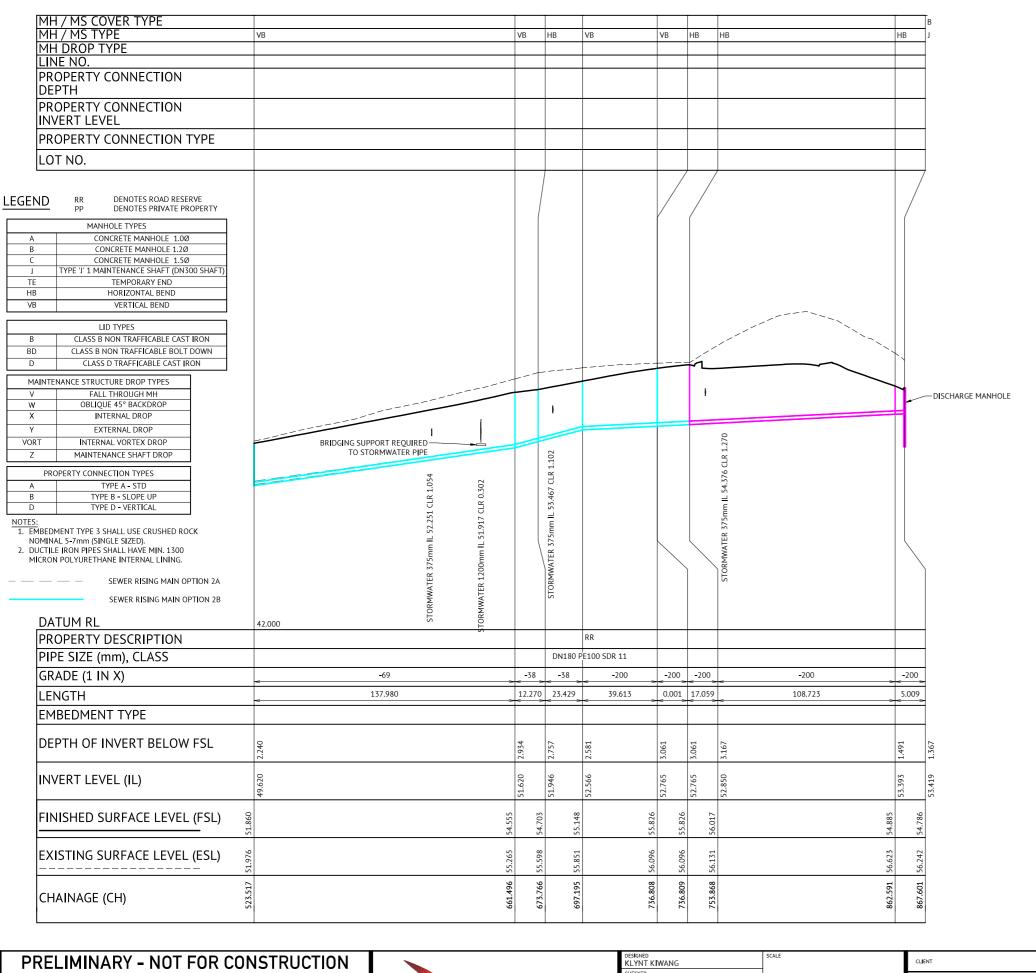
CLIENT	MIRVAC QLD PTY LTD
PROJECT	EVERLEIGH PRECINCT 10 SUBDIVISION DEVELOPMENT
LOCATION	TEVIOT ROAD, GREENBANK
SHEET TITLE	PRELIMINARY SEWER RISING MAIN LONG SECTION OPTION 2A - SHEET 1

MIR-1000

SKC68







NOTE:

THE SEWER INVERT LEVELS ARE PRELIMINARY AND ARE SUBJECT TO DETAILED DESIGN

REFER TO SKETCHES SKC68-SKC69 FOR OPTION 2A LEVELS.

PF	PRELIMINARY - NOT FOR CONSTRUCTION							
20/06/2022	1	PRELIMINARY - NOT FOR CONSTRUCTION	KK					
DATE	REV	DESCRIPTION	REC	APF				

Premise

BRISBANE OFFICE LEVEL 11, 300 ADELAIDE STREET BRISBANE, QLD 4000 PH: (07) 3253 2222 WEB: www.premise.com.au

gned YNT K IW ANG	SCALE			
CKED DREW LANGDON	0	20	40	60m
IECT MANAGER	1 =			
ION STEINHOFER		SCALE 1:1	IOOO (A1)	
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		OBIGINAL SE	IEET SIZE A1	

CLIENT	MIRVAC QLD PTY LTD
PROJECT	EVERLEIGH PRECINCT 10 SUBDIVISION DEVELOPMENT
LOCATION	TEVIOT ROAD, GREENBANK
SHEET TITLE	PRELIMINARY SEWER RISING MAIN LONG SECTION OPTION 2B - SHEET 2

MIR-1000

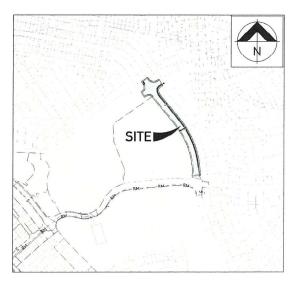
SKC73



A.9 APPENDIX I – Constructed Temporary SPS and Anderson Drive Gravity Main Approvals

EVERLEIGH SCHOOL SITE PACKAGE 3 - ANDERSON DRIVE TEVIOT ROAD, GREENBANK FOR MIRVAC

SEWERAGE RETICULATION



LOCALITY PLAN

REAL PROPERTY DESCRIPTION

	SHEET LIST TABLE
SHEET NO.	SHEET TITLE
C500	SEWERAGE RETICULATION LOCALITY PLAN & NOTES
C501	SEWERAGE RETICULATION LAYOUT PLAN
C502	SEWERAGE RETICULATION LONG SECTIONS - SHEET 1 OF 2
C503	SEWERAGE RETICULATION LONG SECTIONS - SHEET 2 OF 2
C504	SEWERAGE RETICULATION NOTES AND DETAILS

GENERAL NOTES

- ALL WORK AND MATERIALS SHALL BE IN ACCORDANCE WITH CURRENT SOUTH EAST QUEENSLAND SEWERAGE CODE SPECIFICATIONS AND
- LINI ESS SPECIFIED OTHERWISE ALL MATERIALS AND WORK SHALL COMPLY
- THE CONSTRUCTION OF THE SEWERAGE WORK SHOWN ON THIS DRAWING SHALL BE SUPERVISED BY AN ENGINEER WHO HAS RPEQ REGISTRATION. SEWERAGE WORKS NOT COMPLYING WITH THIS REQUIREMENT WILL NOT BE PERMITTED TO CONNECT INTO THE SEQ SERVICE PROVIDER SEWERAGE SYSTEM
- ALL WORK ASSOCIATED WITH LIVE SEWERS OR MAINTENANCE HOLES SHALL BE CARRIED OUT BY THE CONTRACTOR UNDER LOGAN WATER SUPERVISION AT THE DEVELOPER'S COST.
- ALL PIPES AND MATERIALS SHALL COMPLY WITH THE REQUIREMENTS OF THE "ACCEPTED PRODUCTS AND MATERIALS" LIST.
- EACH ALLOTMENT SHALL BE SERVED BY A DN100 PROPERTY CONNECTION. FOR ALLOTMENTS OTHER THAN SINGLE RESIDENTIAL, A DN150 PROPERTY CONNECTION SHALL BE PROVIDED
- PROPERTY CONNECTIONS SHALL BE LOCATED WITHIN THE PROPERTY AS SHOWN IN THE DRAWINGS
- PROPERTY CONNECTION BRANCHES SHALL EXTEND INTO THE PROPERTY A MINIMUM OF 300mm AND A MAXIMUM OF 750mm
- WHERE PIPES ARE LAID IN FILL, THE FILLING SHALL BE CARRIED OUT IN LAYERS NOT EXCEEDING 300mm (LOOSE) IN DEPTH AND SHALL BE COMPACTED UNTIL THE COMPACTION IS NOT LESS THAN 95% OF THE MATERIALS MAXIMUM COMPACTION WHEN TESTED IN ACCORDANCE WITH A.S. 1289 (MODIFIED COMPACTION). TESTING SHALL BE CARRIED OUT AFTER EACH ALTERNATE LAYER IN ALL SUCH CASES APPROVAL OF CONSTRUCTED SEWERS WILL NOT BE ISSUED BY THE SEQ SERVICE PROVIDER UNLESS CERTIFICATES ARE PRODUCED CERTIFYING THAT THE REQUIRED
- 10. WHERE SEWERS HAVE A GRADE OF 1 IN 20 OR STEEPER BUI KHEADS SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE SEQ SEWER CODE.
- 11. THE CONTRACTOR SHALL VERIFY THE LOCATION AND DEPTH OF EXISTING SERVICES WITH RELEVANT AUTHORITIES BEFORE COMMENCING WORKS.
- 12. SEWERS SHALL BE DISUSED /ABANDONED IN ACCORDANCE WITH PROCEDURES SET OUT IN THE SEQ SEWER CODE.
- 13 RENCH MARK AND LEVELS TO AHD
- REFER TO BULK EARTHWORKS DRAWINGS FOR FINISHED SURFACE LEVELS. ALL SEWER CONSTRUCTION WORK UNDERTAKEN BY THE CONTRACTOR SHALL COMPLY WITH THE REQUIREMENTS OF THE QUEENSLAND WORK HEALTH AND SAFETY ACT. FOR INFORMATION PHONE: 1300 369 915
- THE CONTRACTOR IS RESPONSIBLE FOR OBTAINING ALL NECESSARY PERMITS TO ALLOW CONSTRUCTION OF THE SEWER SYSTEM.
- 17. THE CONTRACTOR IS RESPONSIBLE FOR EXCAVATION AND SAFE SHORING TO ALLOW SEWER MAINTENANCE SECTION TO CARRY OUT LIVE SEWER
- 18. CONSTRUCT TRENCHES TO SEQ-SEW-1200-2, WITH EMBEDMENT TYPE 3 SUPPORT MINIMUM TO SEQ-SEW-1201-1, AND ROAD CROSSINGS TO SEO-SEW-1205-1 AND LCC STANDARDS
- CONSTRUCT PROPERTY CONNECTIONS TO SEQ-SEW-1100 SERIES.
- 20. CONSTRUCT MAINTENANCE STRUCTURES TO SEQ-SEW-1300 SERIES. 21. CONSTRUCT BULKHEADS TO SEQ-SEW-1206-1.
- 22. INSTALL DETECTABLE MARKER TAPE ON ALL MAINS AND PROPERTY 23 CALCAREOUS CONCRETE IN MAINTENANCE HOLES REQUIRED IN
- ACCORDANCE WITH SEQ WS.&S D.&C CODE REQUIREMENTS.

 24. CCTV OF SEWER TO BE UNDERTAKEN AND SUPPLIED TO SUPPRINTENDENT.
- PRIOR TO , BUT NO GREATER THAN 2 WEEKS BEFORE, THE ON-SITE INSPECTION FOR OFF MAINTENANCE

VEGETATION PROTECTION

A TREES LOCATED ALONG THE FOOTPATH SHALL BE, TRANSPLANTED PRIOR TO CONSTRUCTION, OR REPLACED IF DESTROYED.

B. WHEN WORKING WITHIN 4m OF TREES, RUBBER OR HARDWOOD GIRDLES S HALL BE CONSTRUCTED WITH 1.8m BATTENS CLOSELY SPACED AND ARKANGED VERTICALLY FROM GROUND LEVEL GIRDLES SHALL BE STRAPPED TO TREES PRIOR TO CONSTRUCTION AND REMAIN UNTIL COMPLETION. C. TREE ROOTS SHALL BE TUNNELLED LINDER, RATHER THAN SEVERED IE ROOTS

ARE SEVERED THE DAMAGED AREA SHALL BE TREATED WITH A SUITABLE FUNGICIDE. CONTACT RELEVANT COUNCIL ARBORIST FOR FURTHER ADVICE.
D. ANY TREE LOPPING REQUIRED SHOULD BE UNDERTAKEN BY AN APPROVED ARBORIST

- A. TOPSOIL AND SUBSOIL SHALL BE STOCKPILED SEPARATELY. B. CARE SHALL BE TAKEN TO PREVENT SEDIMENT FROM ENTERING THE STORMWATER SYSTEM. THIS MAY INVOLVE PLACING APPROPRIATE SEDIMENT CONTROLS AROUND STOCKPILES
- C. IF ACID SULPHATE SOILS EXIST IN THE WORKS AREA, ACID SULPHATE SOILS ARE TO MANAGED IN ACCORDANCE WITH AN APPROVED ACID SULPHATE SOIL

CREEK CROSSINGS

- A SILTATION CONTROL MEASURES SHALL BE PLACED DOWNSTREAM OF ANY
- B. APPROPRIATE SEDIMENT CONTROLS SHALL BE USED TO PREVENT SEDIMENT FROM ENTERING THE CREEK
- C. NO SOIL SHALL BE STOCKPILED WITHIN 5m OF THE CREEK.

REHABILITATION

A. PREDISTURBANCE SOIL PROFILES AND COMPACTION LEVELS SHALL BE R PREDISTURBANCE VEGETATION PATTERNS SHALL BE RESTORED

A. THE DESIGN AND CONSTRUCTION OF THE WORKS SHALL COMPLY WITH ALL **OUEENSLAND LEGISLATION**

INDEMNITY - EXISTING SERVICES

NOT WITHSTANDING THAT EXISTING SERVICES MAY OR MAY NOT BE SHOWN ON THESE DRAWINGS NO RESPONSIBILITY IS TAKEN BY THE ENGINEER OR THE PRINCIPAL FOR THIS INFORMATION WHICH HAS BEEN SUPPLIED BY OTHERS. TO DETAILS ARE PROVIDED FOR INFORMATION ONLY. THE CONTRACTOR SHALL ASCERTAIN THE POSITION OF ALL UNDERGROUND SERVICES PRIOR TO EXCAVATION AND SHALL BE RESPONSIBLE FOR THE COST OF REPAIRS TO DAMAGES CAUSED AS A RESULT OF THE WORKS

ALL ENVIRONMENT PROTECTION MEASURES SHALL BE IMPLEMENTED PRIOR TO COMMENCING ANY CONSTRUCTION WORK, INCLUDING CLEARING

ALL SEWER CONSTRUCTION WORK UNDERTAKEN BY THE CONTRACTOR SHALL COMPLY WITH THE REQUIREMENTS O THE OUEENSLAND WORKPLACE HEALTH AND SAFETY ACT INFORMATION PHONE: 1300 369 915

CONTACT "DIAL BEFORE YOU DIG" ON 1100 FOR LOCATION OF EXISTING PUBLIC SERVICES PRIOR TO EXCAVATION

TRENCH EXCAVATION AND SPOIL

ALL TRENCH EXCAVATIONS SHALL INCLUDE TREATING, SIZING, CONDITIONING AND PROCESSING OF ALL TYPES OF ROCK. CONTRACTOR SHALL PLACE ALL EXCESS TRENCH SPOIL TO A LOCATION NOMINATED BY THE SUPERINTENDEN INCLUDING ALL LEVEL ONE COMPACTION REQUIREMENTS AND TESTING AND MUST BE FREE-DRAINING. THE PLACEMENT OF THE SPOIL SHALL MEET ALL REQUIREMENTS OF THE FILL SPECIFICATION PROVIDED WITHIN THESE

COMPLIANCE ENDORSEMENT referred to in the PDA DEVELOPMENT APPROVAL

Approval no: DEV2018/999/10

15 December 2020

NAME OF	ESTATE	EVERLEIGH SCHOOL SITE PACKAGE 3 - ANDERSON DRIVE			
SUBDIVIDER		MIRVAC			
APPLICATION N	0.	•			
SP DELEGATE A	PPROVAL DATE	16 APRIL 2019			
COUNCIL DA AP	PROVAL No.	DEV 2018 / 999			
DRAWING/PLAN	No.	C500-C504			
No. OF ALLOTM	ENTS	1			
AREA IN Ha.		104На			
LENGTH OF	DN150 uPVC SN8	399m			
SEWERS	DN150 DI	18m)			

		PRELIMINARY - FOR APPROVAL		
31/03/20	8	AMENDED TRENCH EXCAVATION AND SPOIL PRELIMINARY ISSUE NOT FOR CONSTRUCTION	MM MM	IC IC
DATE	REV	DESCRIPTION	REC	AP
		REVISIONS		



BRISBANE OFFICE

LEVEL 1, 100 BRUNSWICK STREE PO BOX 361 FORTITUDE VALLEY, QLD 4006 PH: (07) 3253 2222 WEB: www.premise.com.au

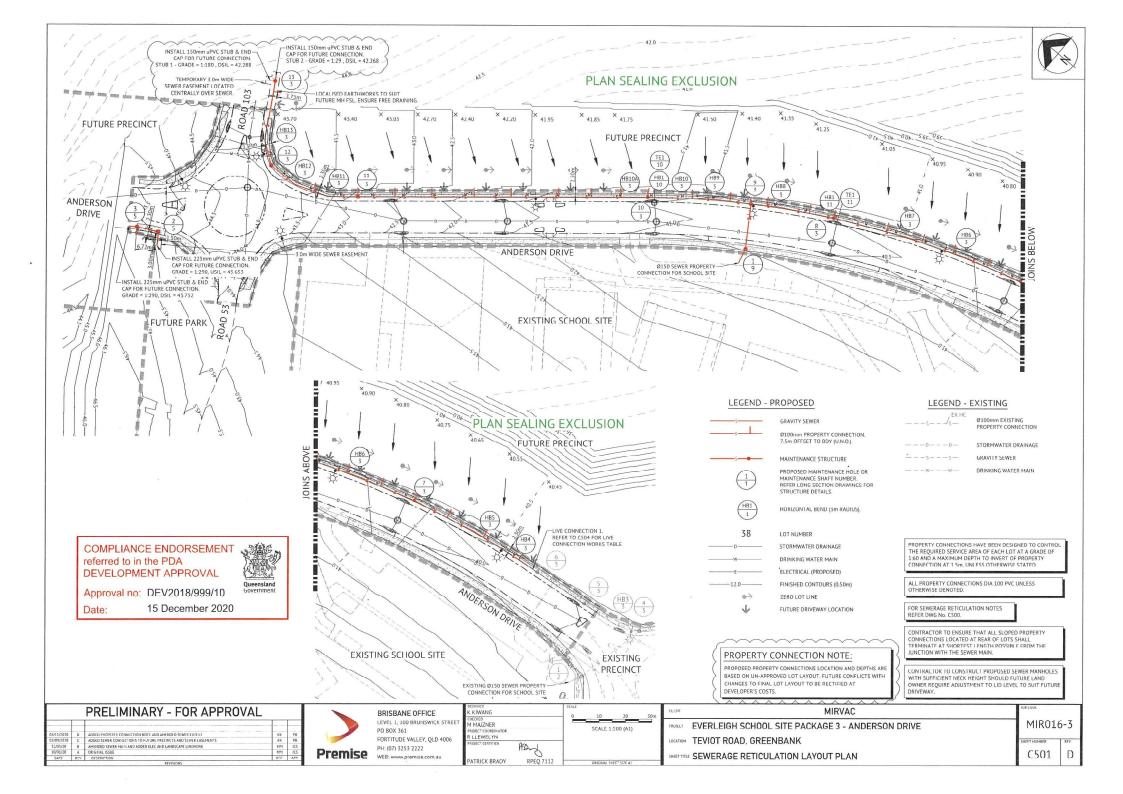
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CHECKED		7 —	100	200	30011
M MAJZNER			SCALE 1	5000 (A1)	
PROJECT COORDINATOR			SCALE I.	3000 (A1)	
R LLEWELYN					
PROJECT CERTIFIER	Prand				
DATRICK RRADY	PPEO 7112	_			_

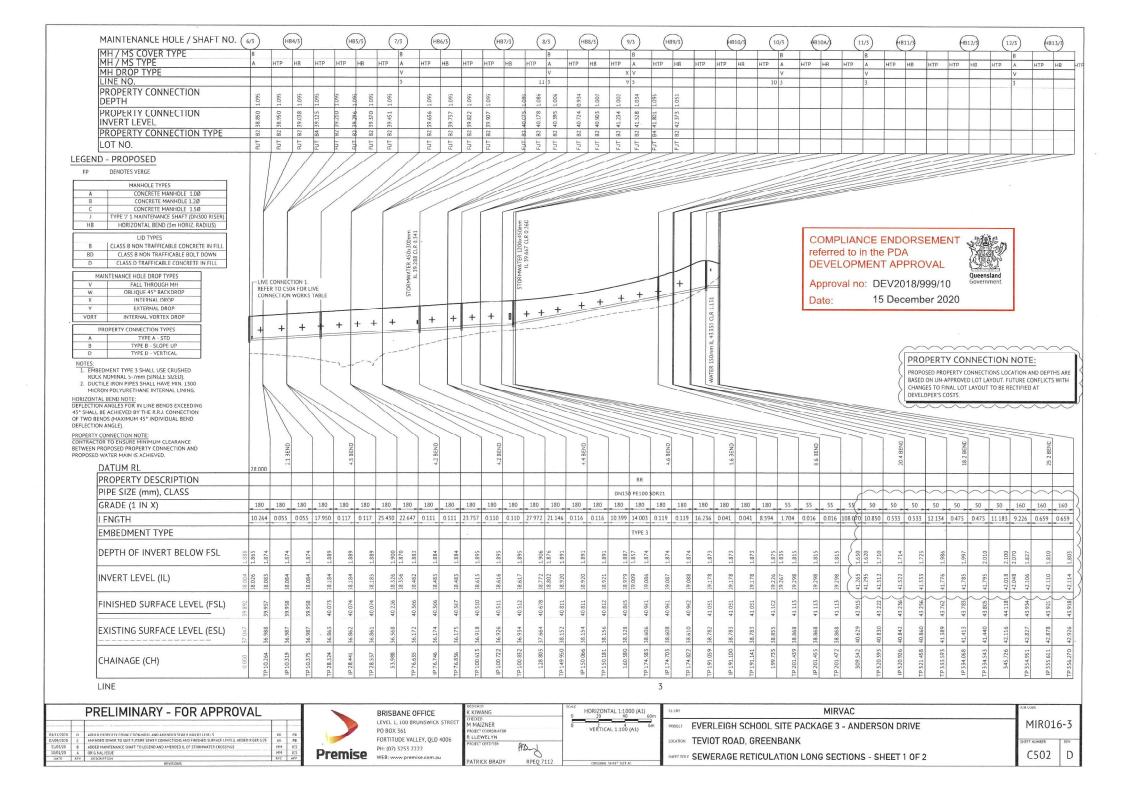
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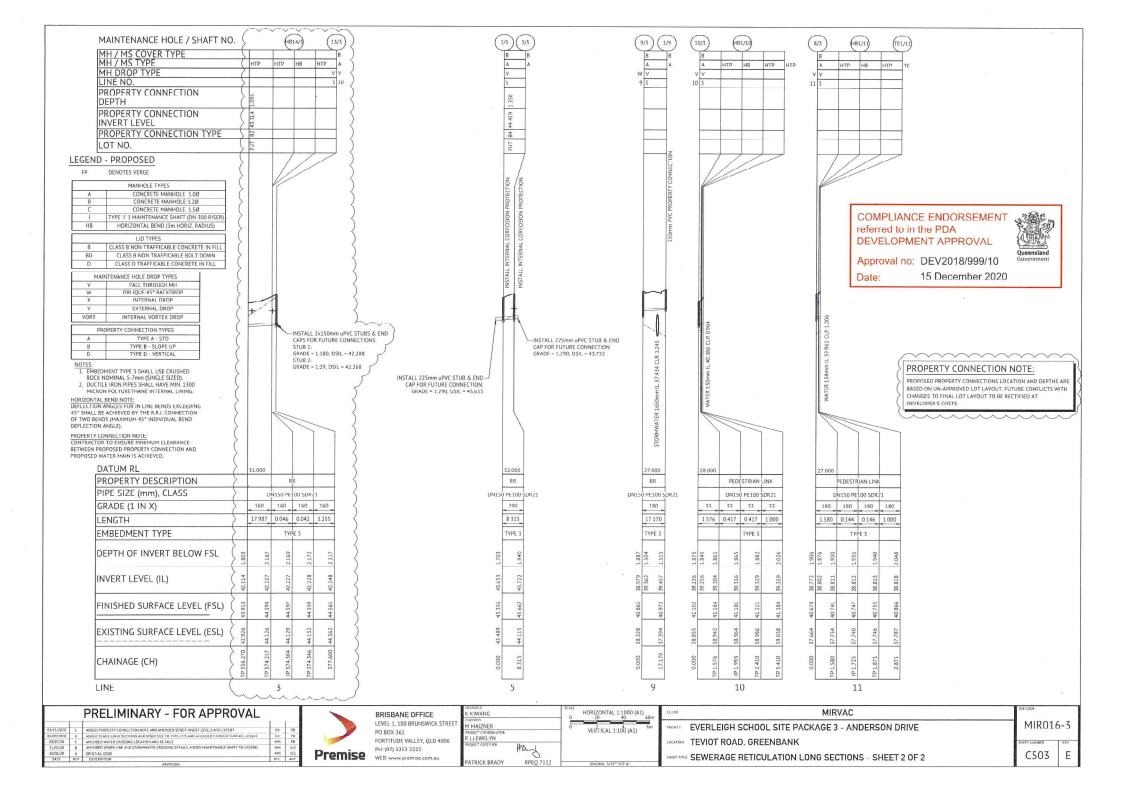
CLIENT	MIRVAC
PROJECT	EVERLEIGH SCHOOL SITE PACKAGE 3 - ANDERSON DRIVE

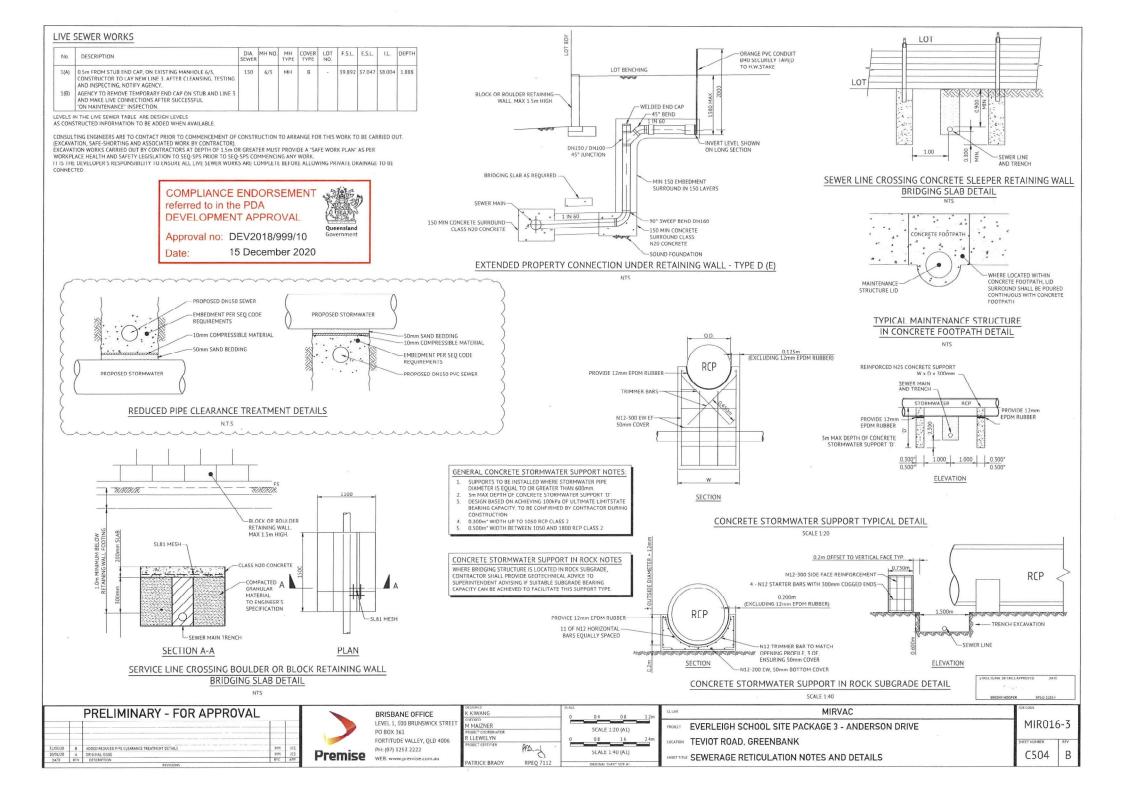
LOCATION TEVIOT ROAD, GREENBANK SHEET TITLE SEWERAGE RETICULATION LOCALITY PLAN & NOTES MIR016-3

C500









COMPLIANCE ENDORSEMENT referred to in the PDA DEVELOPMENT APPROVAL oproval no DEV2018/999/7 21 April 2020

MIRVAC EVERLEIGH STATE SCHOOL TEMPORARY SEWAGE PUMP STATION

*			DRAWING LIST
DRAWING NUMBER	REV	DATE	DESCRIPTION
d2020.02.03.00	C0	19/03/2020	TITLE & INDEX SHEET
d2020.02.03.01	C0	19/03/2020	SITE LAYOUT
d2020.02.03.02	C0	19/03/2020	PLAN, GENERAL NOTES & PUMP DETAILS
d2020.02.03.03	C0	19/03/2020	SECTION
d2020.02.03.04	C0	19/03/2020	BACKFILL DETAILS & CONSTRUCTION NOTES
d2020.02.03.05	C0		BILL OF MATERIALS

SIGNATURE	
MARIO DELA CUADRA	
RPEQ NO.	18461
DATED	18/03/2020

								_
_			_	-	_		_	
							_	
Cô	ISSUED FOR CONSTRUCTION			SL	IMS	IMS	19/03/2	0
REV	AMENDMENT			IRN	CKD	APP	DATE	Ξ
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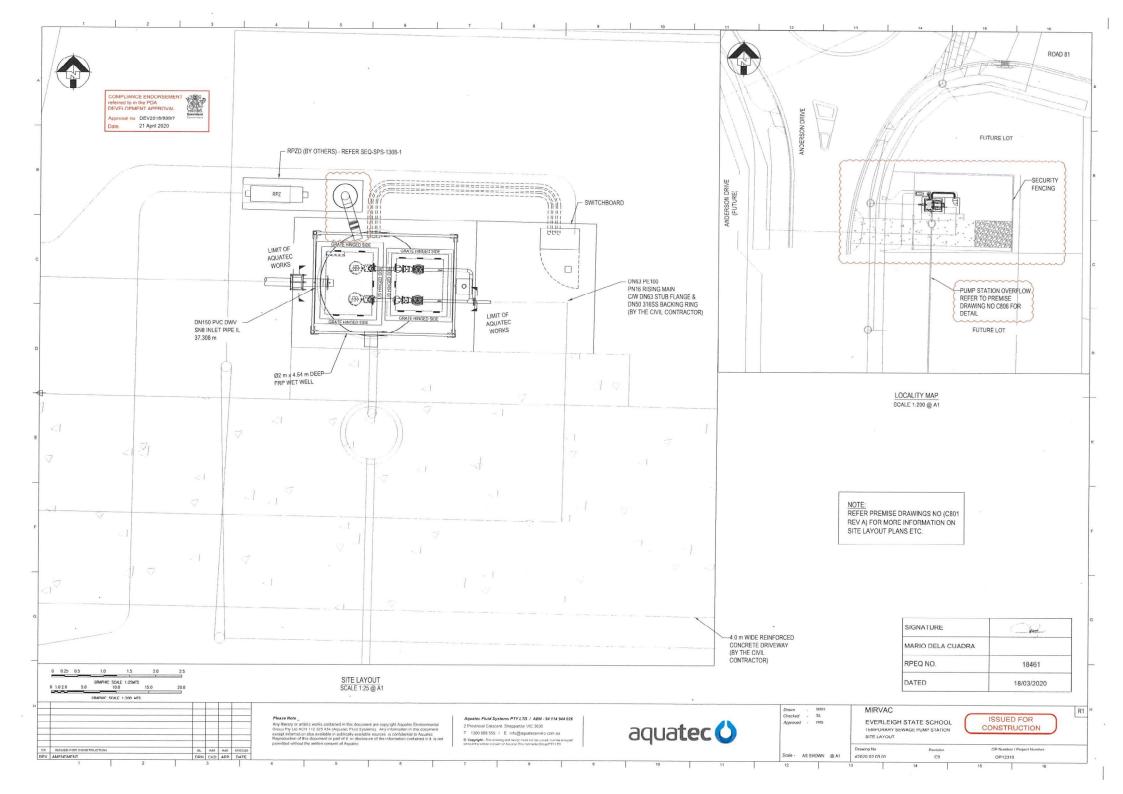
2 Provincial Crescent, Shepparton VIC 3630



Checked - SL Approved - IMS
Approved - IMS
No. of Contract of

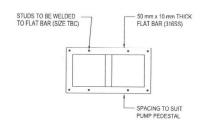
EVERLEIGH STATE SCHOOL TITLE BLOCK & INDEX SHEET

ISSUED FOR CONSTRUCTION





COMPLIANCE ENDORSEMENT referred to in the PDA DEVELOPMENT APPROVAL Approval no DEV2018/999/7 Date 21 April 2020

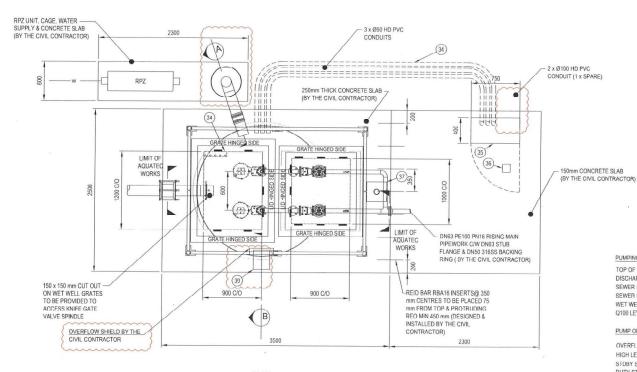




DETAIL "A"

TYPICAL PUMP PEDESTAL BASE PLAN

SCALE 1:10 @ A1



PLAN (COVERS REMOVED FOR CLARITY) SCALE 1:20 @ A1

PUMPING STATION DETAILS:

TOP OF SLAB LEVEL RL: 40 m DISCHARGE PIPE IL: 38.3 m SEWER INLET PIPE DIAMETER: DN150 (PVC DWV \$N8) SEWER INLET PIPE IL: 37.309 m WET WELL FLOOR IR: 35.46 m Q100 LEVEL: 38.90 m

PUMP OPERATING LEVELS:

OVERFLOW RL (ASSUMED): 38.8 m HIGH LEVEL ALARM (FLOAT) RL: 36.61 m STUBY START RL: 36.46 m DUTY START RL: 36.31 m PUMP STOP RL: 36.11 m LOW LEVEL: 36.01 m

PUMP DETAILS:

PUMP DISCHARGE: DN40

PUMP. FLYGT XYLEM
MODEL: MP 3090 HT 3 - 250 50Hz 4.3kW
IMPELLER MATERIAL: GREY CAST IRON
IMPELLER TYPE: SEMI-OPEN MULTI-CHANNEL
DESIGN DUTY. 2.90 I/s@ 41.29 m
PUMP OPERATION: DUTY / STDBY

GENERAL NOTES:

- ALL PVC PENETRATIONS TO BE GLASSED IN WITH THE FRP VESSEI
- 2. REINFORCEMENT TO COMPLY WITH AS 1302 & AS 1304
- 3. ALL HOLES TO BE PRE-CORED AND GLASSED
- 4. ALL FLANGES TO BE DRILLED TO AS4087 PN16 UNO
- FRP PIPE PENETRATION & 316SS FIXINGS TO THE FRP WALL TO BE PERFORMED IN ACCORDANCE WITH AS2634
- 6. SWITCHBOARD DOOR TO HAVE MIN 600mm CLEARANCE TO SURROUNDING ABOVE GROUND STRUCTURE AS PER AS/NZS 3000

SIGNATURE	()Q
MARIO DELA CUADRA	
RPEQ NO.	18461 .
DATED	18/03/2020

0 0.10.2 0.5 1.0 1.5 2.0

GRAPHIC SCALE 1:20MTS

14
09 ISSUEC POR CONSTRUCTION 05. MAS 0. MS 1900/20
09 ISSUEC POR CONSTRUCTION 05. MAS 0. MS 1900/20
09 OTH 05.00 APP 0.ATE

Aquatec Fluid Systems PTY LTD / ABN - 94 114 944 026 2 Provincial Crescent. Shepparton VIC 3630

T 1300 088 555 / E info@aquatecenviro com au

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without the written consent of Aquatec Environments Coup PTV LID



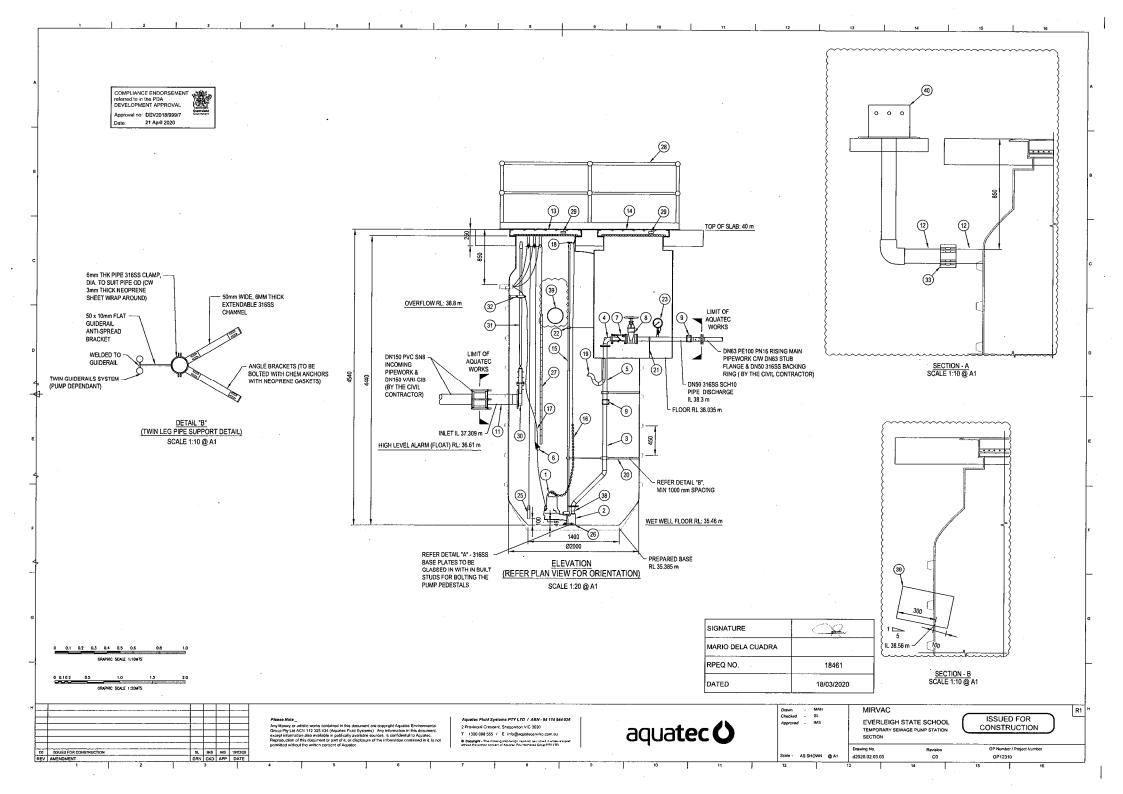
Drawn	MAH
Checked	SL
Approved	IMC

MIRVAC

EVERLEIGH STATE SCHOOL

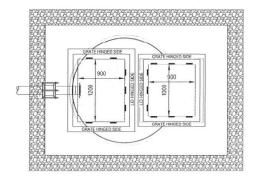
TEMPORARY SEWAGE PUMP STATION
PLAN, GENERAL NOTES & PUMP DETAILS

ISSUED FOR CONSTRUCTION



NON-TRAFFICABLE

COMPLIANCE ENDORSEMENT referred to in the PDA DEVELOPMENT APPROVAL Approval no DEV2018/999/7
Date 21 April 2020



BACKFILL PLAN SCALE 1:25 @ A1

CAUTION: HAND COMPACTION ONLY TO ALL IMPORTED BACKFILL WITHIN 1 m RADIUS OF PUMP STATION STRUCTURES.

> AQUATEC HAVE ASSUMED GWL AT FSL FOR WORST CASE FOR THE PUMP STATION BUOYANCY CALCULATIONS 250 mm THICK CONCRETE SLAB (SLAB & REINFORCING BARS TO BE DESIGNED & SUPPLIED BY THE CIVIL CONTRACTOR) -200 MM LAYER LIFT OF 20MM COMPACTED TYPE 2 5C ROAD BASE AROUND TANK TO A MINIMUM 95 % STANDARD COMPACTION AS PER AS1289 5 (DENSITY = 1600 kg/m3) CONCRETE BALLAST (2400 kg/m3, f 'c = 25 MPa), VOLUME OF CONCRETE CYLINDER = 14 45 m³ Ø3900 -200 mm TYPE 2.3 COMPACTED ROAD BASE (95% STANDARD COMPACTION), MIN ALLOWABLE SOIL BEARING CAPACITY TO BE 100kPa. BACKFILL ELEVATION GRAPHIC SCALE 1:25MTS TANK BASE FOUNDATION SHALL BE INSPECTED BY AN EXPERIENCED SCALE 1:25 @ A1 GEO-TECHNICAL ENGINEER TO CONFIRM MINIMUM BEARING REQUIRED

FIBRE-GLASS TANKS INSTALLATION PROCEDURE:

- EXCAVATION DEPTH IS TO BE A MINIMUM OF 200MM BELOW BASE AND MAY BE DEEPER AS REQUIRED (OR POURING ADDITIONAL BLINDING) TO ACHIEVE A MINIMUM FOUNDATION BEARING CAPACITY OF 100KPA, AND BASE TO BE LEVELED WITH 200MM THICK LAYER OF COMPACTED ROAD BASE AS PER GIVEN I EVELS
- LOWER UNIT IN HOLE MAKING SURE THAT NO SHARP OBJECTS COME NEAR UNIT.
- TO PREVENT VESSEL FROM FLOATATION DURING INSTALLATION, FILL VESSEL WITH WATER SUCH THAT IT IS HEAVIER THAN THE CONCRETE BALLAST. (INLET PIPE STUB TO BE PLUGGED TEMPORARY BY THE CIVIL CONTRACTOR PRIOR TO FILLING WATER)
- POUR CALCULATED VOLUME OF CONCRETE AS RETAINER BALLAST AROUND BASE OF UNIT & SHALL BE CONSTRUCTED TO THE DIMENSIONS SHOWN ON THE SECTION.
- PUMP STATION SHALL HAVE MINIMUM OF 3 RIBS LOCATED WITHIN THE CONCRETE BALLAST.
- 6. COMPLETE BACKFILL WITH COMPACTED ROAD BASE MATERIAL AS SHOWN ON THE SECTION.
- 7. BOX OUT AND POUR COVERSLAB TO ENGINEERS REQUIREMENT WITHOUT ANY LOADS BEING
- TRANSFERRED DIRECTLY ONTO THE TANK.

NOTE:

CONTRACTOR TO GAIN GEO-TECHNICAL ENGINEERS DIRECTION THAT THE PROPOSED BACKFILL DETAILED ON THIS DRAWING IS APPROPRIATE FOR ON-SITE CONDITIONS PRIOR TO COMMENCING CONSTRUCTION

SITE SPECIFIC RECOMMENDATIONS:

DE17/162, DATED: 14 JUNE 2017)

- CONTRACTORS TO LIAISE WITH RESPECTIVE GEOTECHNICAL ENGINEERS WHO HAVE CONDUCTED SITE SPECIFIC GEOTECHNICAL REPORTS, FOR TESTING REQUIREMENTS (I.E FIELD DENSITY TESTING FREQUENCYEXTENTS INSPECTION REQUIREMENTS II E. LEVEL OF SUPERVISION).
- CONTRACTORS TO ADHERE TO ANY EARTHWORK, EXCAVATION, BACKFILL, CONSTRUCTION, SITE SPECIFIC TREATMENT REQUIREMENT/SRECOMMENDATIONS STATED IN SITE SPECIFIC GEOTECHNICAL REPORTS (I.E. DRAINAGE MEASURES, DE-WATERING MEASURES, EXCAVATION SUPPORT REQUIREMENTS, MOISTURE CONTROL MEASURES, TREE REMOVAL/PLANTATION MEASURES, ROOT TREATMENTS, ASS MANAGEMENT MEASURES, ERGISON & SEDIMENT CONTROL MEASURES.
- CONTRACTORS TO ENSURE BEARING CAPACITY > 100 KPA IS AVAILABLE AT FOUNDATIONS?
 CONTRACTORS TO REMOVE ANY EXISTING SOIL (I.E FILL, TOPSOIL, DISTURBED/WEAKENED SOILS, ORGANIC/DELETER/IOUS/PERISHABLE MATTER) FROM THE PUMP STATION SITE, DENOTED IN SITE.
- STORMINGUELE INFORMATION FOR THE POWER THE POW

SIGNATURE

MARIO DELA CUADRA

RPEQ NO. 18461

DATED 18/03/2020

H CO ISSUED FOR CONSTRUCTION MAN INS INS 188323

Please No.

Aquatec Fluid Systems PTY LTD / ABN - 94 114 944 026

2 Provincial Crescent, Shepparton VIC 3630 T 1300 088 555 / E info@aquatecenviro.com.au aqua**tec** 🔾

Drawn - MAH Checked - SL Approved - IMS

Scale - AS SHOWN @ A1

EVERLEIGH STATE SCHOOL TEMPORARY SEWAGE PUMP STATION BACKFILL DETAILS & CONSTRUCTION NOT

MIRVAC

ISSUED FOR CONSTRUCTION

| Drawing No. | Revision | OP Number / Project Number | d2020 02 03 04 | C0 | OP 12310 |



BILL OF MATERIALS

ITEM				
NUMBER	DESCRIPTION	QUANTITY	MATERIAL	REMARKS
1	SUBMERSIBLE PUMP	2	CAST IRON	REFER PUMP DETAILS
2	DN40 DISCONNECTION BEND	2	CAST IRON	ISO G2
3	DN50 RISER PIPEWORK FL-FL C/W 2 x DN50 L/R 45" ELBOW BW	2	316SS SCH10	LENGTHS TO SUIT
4	DN50 90° ELBOW L/R FL-FL C/W DN15 ROUND SOCKET (TAPPING PORT FOR TESTING)	2 .	316SS SCH10	
5	DN50 FL-SP PIPEWORK	4	316SS SCH10	LENGTHS TO SUIT
6	FLOAT LEVEL SWITCH	1	RUBBER	NOLTA
7	DN50 SWING CHECK VALVE (RESILIENT SEATED)	2	DUCTILE IRON	BROOK VALVES: RSCK, FUSION COATED BLUE
8	DN80 GATE VALVE CW HAND-WHEEL, RESILIENT SEATED, CLOCKWISE CLOSE, PN16	2	DUCTILE IRON	AVFI MODE: RSGV - AS , FUSION COATED, DRILLED TO AS4087 PN
9	DN50 PIPE COUPLING	4	31688	NORMACONNECT® FLEX E
10	DN50 FL-SP-SP MANIFOLD CW DN50 LR 90° ELBOW BW & DN80 EQUAL TEE	1	316 SS SCH10	
11	DN150 INLET SP-SP PIPEWORK C/W DN150 STUB FLANGE & 316SS BACKING RING	1	PVC DWV SN8	MIN 600 mm. INLET INVERT TO MATCH INCOMING SEWER INVER
12	DN100 VENT PIPEWORK	2	PVC DWV SN8	ONE ITEM C/W 1 x 90° ELBOW
13	WET WELL ACCESS COVER - SPLIT HINGED SAFETY GRATE (CLASS B RATED) CLEAR OPENING: 1200 x 900mm	1	ALUMINIUM	McBERNS LFM, 150 SQUARE CUT-OUT TO BE PROVIDED TO ACCESS KGV SPINDLE, REFER LOGAN WIA STANDARD DRWG (PM001-01-S-DWG-CI-2010) - NOTE 2.B.d
14	VALVE CHAMBER ACCESS COVER - SINGLE OPENING, SPLIT HINGED SAFETY GRATE (CLASS B RATED) CLEAR OPENING: 1000 x 900mm	1	ALUMINIUM	McBERNS LFM
15	3 / 4* GUIDERAILS	4	316 SS '	
16	LIFTING CHAINS (LOAD RATED)	2	316 SS	10MM LIFTING CHAIN ABOUT 1 M LENGTH FROM PUMP LIFTING LUC CONNECTED WITH 6MM ROPE. THE ROPE IS EXTENDED TO TOP OF THE WELL
17	PUMP CABLE	2		TO SUIT PUMPS
18	FLOAT & CHAIN HOOKS	TO SUIT	316 SS	
19	DN50 FLOOR DRAIN WITH TRAP, FLAP SEAL AND FLAP VALVE	1	PVC DWV SN6	

20	FRP BRACKETING WITH 316 SS FIXINGS	TO SUIT	316 \$S/FRP	MIN 1000 mm CENTRES
21	PIPE SUPPORT BRACKETS (VERTICAL)	4	316SS	
22	ANTI - SPREAD BRACKETS FOR GUIDE-RAILS	4	316SS	
23	15 mm ROUND SOCKET (TAPPING POINT) CW 15mm BALL VALVE & PRESSURE GAUGE (FLOYD)	1	316 SS	
24	FLOAT BAR	TO SUIT	316SS	
25	LEVEL TRANSDUCER	1	316 SS	VEGAWELL 52
26	10 mm PUMP PEDESTAL BASE	. 2	316 SS	REFER DETAIL "A"
27	BACKUP "MULTITRODE" LEVEL SWITCH	1		1.5/10-30FS FAILSAFE LEVEL PROBE WITH 2M STICK AND 30M CABLE PN: 837775
28) HANDRAIL CW SELF CLOSING DOUBLE DOORS (MODULAR NO WELD HANDRAIL)	1	GALV. MS	MODDEX, REFER LOGAN WIA STANDARD DRWG (PM001-01-S-DWG-CI-2010) - NOTE 2.C.c
29	CONFINED SPACE SIGNS	2	PLASTIC	
30	DN150 KNIFE GATE VALVE (CLOCKWISE CLOSE)	-1	316SS	HMA VALVECO GENERAL PURPOSE (LUGGED)
31	EXTENSION SPINDLE .	1	316SS	
32	EXTENSION SPINDLE BRACKET	1	31688	
33	DN100 DEKS COUPLER	1		
34	ELECTRICAL CONDUITS (1 x Ø32, 3 x Ø50 & 2 x Ø100)	6	HDPVC	
35	SWITCHBOARD	1,		
36	EARTH STAKE PIT - 120 L x 120 W x 76 H mm	1	ALUMINIUM	ERB PART No. DULERB1
37	DAVIT BASE	1	316SS	SPANSET SPXTIN2007 (TBC)
38	DN40- DN50 PIPEWORK FL-BSP C/W DN40 BSP SOCKET & DN40-DN50 ECCENTRIC REDUCER	2	316SS SCH10	
39	DN225 OVERFLOW STUB	1	PVC DWV SN8	
40	GROUND MOUNT ODOUR FILTER	1	POLY	McBERNS GM150

SIGNATURE	(H)
MARIO DELA CUADRA	
RPEQ NO.	18461
DATED	18/03/2020

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	CO	ISSUED FOR CONSTRUCTION	SL	IMS	MS	19/03/20
	REV	AMENDMENT	DBN	CKO	APP	DATE

2 Provincial Crescent, Shepparton VIC 3630 T 1300 088 555 / E info@aquatecenviro.com.au

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Approved - IMS	Drawn Checked		MAH SL	
		:		

MIRVAC EVERLEIGH STATE SCHOOL TEMPORARY SEWAGE PUMP STATION BILL OF MATERIALS ISSUED FOR CONSTRUCTION



A.10 APPENDIX J – TEMPORARY SPS – LW SUPPORT COMMUNICATIONS

Simon Steinhofer

From: O'Brien, Daniel < DanielO'Brien@logan.qld.gov.au>

Sent: Thursday, 3 March 2022 1:50 PM

To: Simon Steinhofer

Cc: Herath, Kumara; WaterDA; Clint Thorp; Mark Clancy; Brendan Saur;

jason.augustine@mirvac.com; Marco Bonotto

Subject: RE: [#MIR-0800] Everleigh - School Site - Temporary sewage pump station -

Utilising remaining capacity

Simon,

Logan Water is supportive for the spare capacity in the temporary sewage pump station to be reassigned to service residential lots should the proposed childcare centre not proceed.

I have cc. Marco Bonotto from EDQ on this email.

Daniel O'Brien

Water Developer Services & Connections Program Leader Water Infrastructure Solutions Branch

RELIABLE - SUSTAINABLE - COMMITTED

danielo'brien@logan.qld.gov.au | 07 2899 7728 | 0401 256 668 | Teams Call / Chat

Connect with us: Website | Facebook | Twitter | LinkedIn





Logan City Council acknowledges the Traditional Custodians of the lands and waterways across the City of Logan. We pay our respects to Elders past, present and emerging.

From: Simon Steinhofer <simon.steinhofer@premise.com.au>

Sent: Wednesday, 2 March 2022 4:08 PM

To: O'Brien, Daniel < Daniel O'Brien@logan.qld.gov.au>

Cc: Herath, Kumara < KumaraHerath@logan.qld.gov.au>; WaterDA < WaterDA@logan.qld.gov.au>; Clint Thorp

<clint.thorp@premise.com.au>; Mark Clancy <mark.clancy@mirvac.com>; Brendan Saur

<bre><bre>dan.saur@mirvac.com>; jason.augustine@mirvac.com

Subject: [#MIR-0800] Everleigh - School Site - Temporary sewage pump station - Utilising remaining capacity

Hi Daniel,

We are in finalising the ROL design for both Precinct 8 & 10 at the Everleigh Development. In referencing earlier support from Logan Water of a proposed childcare centre to utilise the space capacity exiting in the temporary sewage pump station provided to service the Everleigh School site (see attached support correspondence), we would like to utilise this referenced spare capacity to service residential lots within the Everleigh development. The application of the childcare centre is not progressing as it will be catered for elsewhere in the development. Therefore, the remaining spare capacity within the temporary pump station is still not allocated.

We would like to seek your support for the remaining capacity of the temporary sewage pump station provided to service the Everleigh School site to be used to service residential lots.

If you have any questions, please don't hesitate to call



SIMON STEINHOFER

Principal Civil Engineer

T 07 3253 2222 | **M** 0476 810 311 **E** simon.steinhofer@premise.com.au

A Level 11, 300 Adelaide St, Brisbane QLD 4000

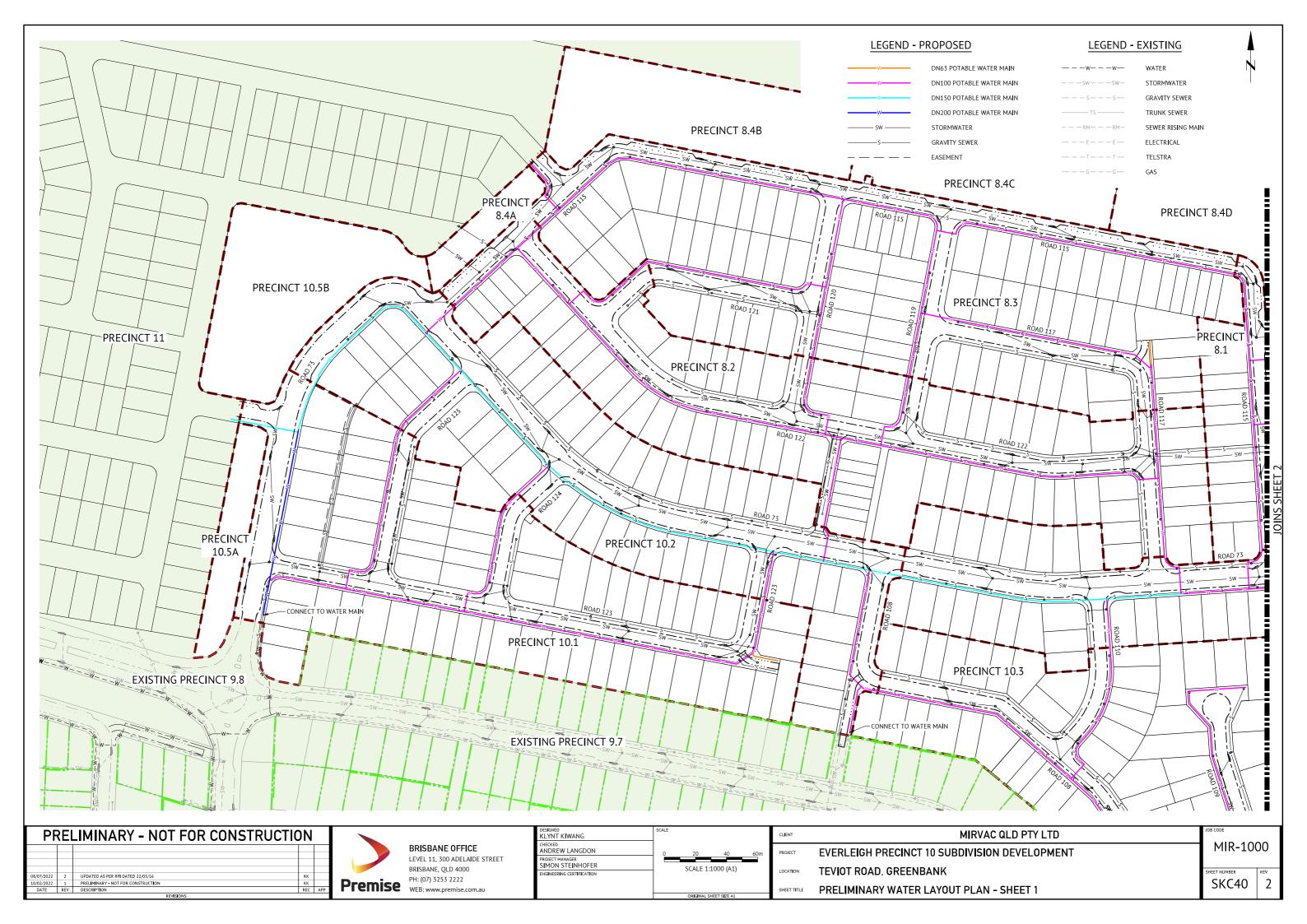


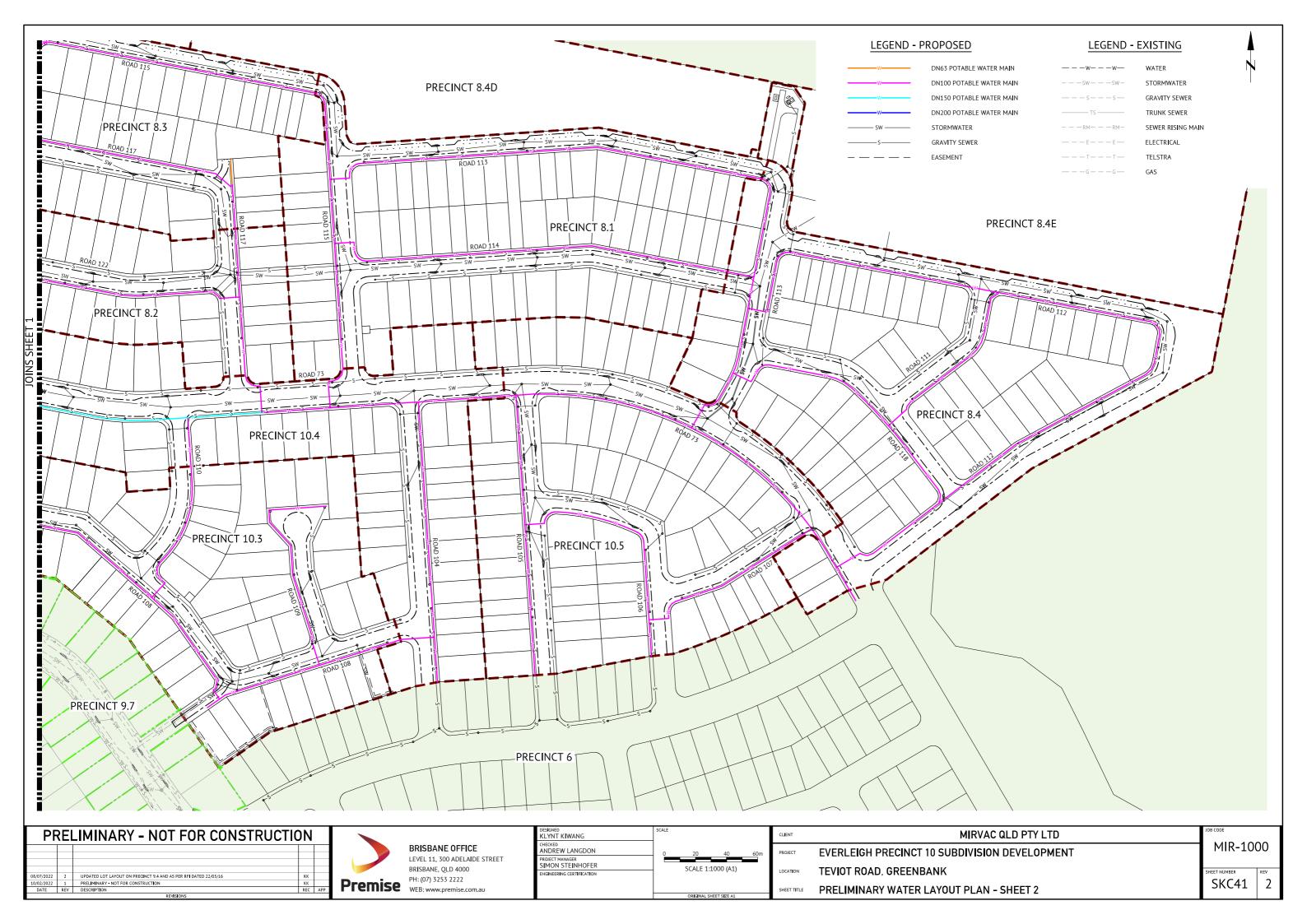
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A.11 APPENDIX K – CONCEPTUAL WATER RETICULATION PLANS







A.12 APPENDIX L— ELECTRICAL SERVICING STATEMENT



3 March 2022

Mirvac Queensland Pty Limited Box 10047 Brisbane Adelaide Street Qld 4000

Attention: Mr Mark Clancy

Robin Russell & ASSOCIATES PTY. LTD. ABN 78 010 589 661

Dear Sir,

EVERLEIGH – PRECINCTS 8 & 10: ELECTRICAL SERVICING STATEMENT

As electrical engineering consultants who have previously been engaged to undertake design services for multiple stages of Everleigh Precincts (1, 9 & 12), we can confirm the following in relation to Everleigh – Precincts 8 & 10:

- Energex electrical network infrastructure, NBN telecommunications & gas reticulation services have been constructed and/or designed for multiple stages of Everleigh, Precinct 9, adjacent to proposed Precincts 8 &10,
- Preliminary investigations including consideration of proposed PMT site locations for Precincts 8 & 10, have commenced,
- Sufficient network capacity exists in the existing electrical network infrastructure, following completion of Precinct 9.8 and the associated 11kV tie cable, to cater for the increased electrical load of the proposed precincts:
 - Refer to Figure 1 below, showing significant spare capacity at the adjacent Energex Zone Substation - North Maclean (SSNMC)
- Final arrangements will be confirmed during the detailed design phase for each stage of the precinct.

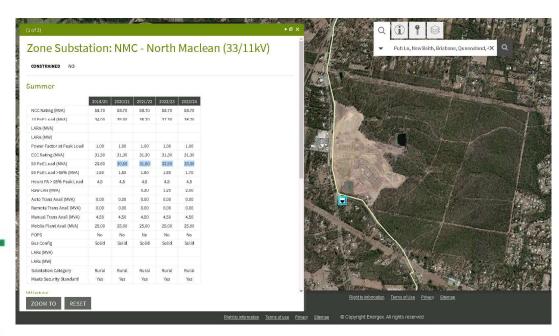


Figure 1: Zone Substation North Maclean - No Constraints

Robin Russell BE, BCom, FIEAust, CPEng RPEQ 1546

Consulting Electrical Engineers

Subdivision Electrical Services

204/6 Babarra St. Stafford Queensland 4053 Australia Head Office

> Ph (07) 3872 5555 Fax (07) 3872 5566 Email rr@robrus.com.au

www.robrus.com.au

Please feel free to contact the undersigned if you require any further details.

Yours faithfully,

Robin Rumela

ROBIN RUSSELL & ASSOCIATES PTY. LTD.

Robin Russell

(RPEQ 1546)

MIRVAC ROL10 - PRECINCT 8 & 10, EVERLEIGH ENGINEERING SERVICES REPORT

