PLANS AND DOCUMENTS referred to in the PDA DEVELOPMENT APPROVAL



Approval no:DEV2019/1087/1Date:25th June 2020

Conceptual Stormwater Management Plan Subdivision – 15 & 19-67 Pub Lane, Greenbank

Prepared for: Shopping Centres Australasia Property Group

Date: 9 April 2020

Prepared by: Anthony Raadschelders

Ref: 29875_CI_001_C

Wood & Grieve Engineers now part of Stantec 232 St Paul's Terrace, Fortitude Valley QLD 4006 Tel: +61 7 3811 4500 Email: brisbane@wge.com.au www.wge.com.au 200409 - 29875-CI SITE BASED STORMWATER MANAGEMENT PLAN - ROL_REV C.DOCX



Revision

Revision	Date	Comment	Prepared By	Approved By
А	31/10/19	Issued for Approval	BM/AR	AR
В	1/11/19	Minor updates	AR	AR
С	10/04/20	ROL changes	AR	AR

Site Address:	15 and 19-67 Pub Lane, Greenbank
Real Property Description:	Lot 5 on SP214051
Proposed Development:	Subdivision (1 into 2)

Client:

Shopping Centres Australasia Property Group (SCA)

Economic Development Queensland (EDQ)

Local Authority:

Authority Reference #:

Anthony Raadschelders RPEQ 19881 For and on behalf of

Wood & Grieve Engineers

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Contents

1.	Introduction	1
2.	Existing Site Characteristics	2
2.1 2.2 2.3 2.4	Property Detail Existing Site Conditions & Improvements Proposed Development Topography	2 3 3 3
3.	Flooding/ Overland Flow Impacts	4
3.1 3.2	Known Existing Flooding/ Overland Flow Paths External Catchment	4 4
4.	Stormwater Quantity	5
4.1 4.2 4.3	Existing Stormwater Regime Lawful Point of Discharge Proposed Stormwater Management Strategy	5 7 7
5.	Site-based Stormwater Quality Management Plan	12
5.1 5.2 5.3	Stormwater Management Strategy – Operational Phase Acid Sulphate Soils Erosion and Sediment Control (ESC) – Construction	12 12 12
6.	Conclusion	13
Appen	idix A - Existing Detailed Site Survey and ROL Layout	14
Appen	idix B - Authority Flood Mapping	15
Appen	idix C - Existing Operational Works Drawings	16
Appen	ndix D - Engineering Drawings	17
Appen	dix E - Stormwater Quantity Calculations	18



Design with community in mind

1. Introduction

Wood & Grieve Engineers have been commissioned by Shopping Centres Australasia Property Group (SCA) to prepare this Stormwater Management Plan (SMP) for the proposed 1 into 2 subdivision of the property situated at 19-67 Pub lane, Greenbank. The site's Real Property Description is 5 on SP214051.

This SMP outlines the Conceptual level stormwater servicing strategy to support the Development Application for the proposed subdivision being lodged with the with the Minister of Economic Development of Queensland (MEDQ).

It is noted that no new uses are proposed on the subject site as part of the current application. As such, subsequent discussion and reporting is based on maintaining the current stormwater quantity discharge regime and continuing to meet the applicable stormwater management obligations for the existing shopping centre that currently utilises the subject site for their stormwater management.

1.1.1 Purpose

The purpose of this SBSMP is to evaluate the quantity and quality of stormwater associated with the proposed development and relocation of the bio-retention basin, so as to demonstrate to MEDQ that an appropriate stormwater management strategy can be accommodated.

The SBSMP specifically addresses the following items for both the construction and operational phases of the development:

- An appropriate stormwater quality management strategy can be implemented that meets Water Sensitive Urban Design (WSUD) best management practices, state and local government planning and guideline requirements,
- An appropriate stormwater quantity management strategy can be implemented to that ensure that the developed site's stormwater runoff meets Council requirements, and
- Maintenance of water quality treatment devices.

It is noted that this report is specifically associated with demonstrating maintaining non-worsening of the stormwater condition of the subject site, associated with the subject application, ie a reconfiguration of a lot (ROL). As no uses or works are proposed as part of the subject development proposal, this report will demonstrate that only impacted measures will be relocated to accommodate the proposed development without impacting on the stormwater condition as it leaves the site. No additional measures or mitigations are required nor proposed as part of this applications.

2. Existing Site Characteristics

2.1 Property Detail

Address:19-67 Pub Lane, GreenbankReal Property Description:Lot 5 on SP214051Total Site Area:9.964ha

As can be seen in the aerial photo below, the site is bounded by the existing shopping centre to the East, Pub Lane to the South and the Brisbane – Sydney Rail Line to the West. There are existing rural-residential properties along the northern boundary.



Figure 2-1: Site Location Plan (Source: Nearmap 2019)

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2.2 Existing Site Conditions & Improvements

The existing Shopping Centre is located on the adjacent Lot 1 east of the subject site against Teviot Rd. The subject site, located on Lot 5 is undeveloped, but has an on-site sewage treatment system, evapotranspiration area, and an existing stormwater detention basin which services the existing shopping centre located in the existing drainage easements.

2.3 Proposed Development

The development will consist of a Reconfiguring of a Lot (ROL) to create 2 Lots. The new Lot 8 is subject to further approvals for any future uses. It is noted that an existing Development Approval exists for the Development of proposed Lot 7 with EDQ (Ref: DEV2016/813) The proposed development can be seen in Appendix A.

2.4 Topography

A detailed surface survey was conducted by Lawson Surveys on 1 April 2016, which is included as a background to the development layout in Appendix A.

It shows that the surface generally grades away from the Teviot Rd/ Pub Lane intersection towards the basin in the northwestern corner of the site. The site is generally a platform for the existing shopping centre, from which it is battered down to the gently graded existing surface, which is on average about 2-3%.

3. Flooding/ Overland Flow Impacts

3.1 Known Existing Flooding/ Overland Flow Paths

Logan City Council (LCC) flood mapping indicates that the subject site is not affected by inundation overlays associated with a river, creek, tidal surge or overland flow path (attached in Appendix B). This has been previously confirmed as part of previous applications with Department of Infrastructure, Local Government and Planning (DILGP). Therefore, no further Flood Impact Study or investigation is suggested to be required as part of this application.

3.2 External Catchment

By examining contours of the surrounding area, it has been established that there are external catchments that impact on the proposed development site. The external catchment is limited to flows from the existing shopping centre and road batters in Pub Lane. It is reflected in the catchment plans in Appendix D. The catchment is approximately 4.187ha and arrives at the existing detention basin via overland flow and an existing swale drain running along the northern boundary of the site, which directs stormwater flow towards the existing detention basin. To accommodate these flows, it is proposed to utilise, and divert as necessary, the existing overland flow path to the existing discharge point at the rail corridor on the western boundary of the site.

4. Stormwater Quantity

4.1 Existing Stormwater Regime

The site survey demonstrates that the site drainage is towards the north-western corner of the site. This has been verified by a site visit on 10 June 2016. The site discharges as overland flow to the rail corridor on the western boundary of the site, which is then conveyed across the rail corridor via an existing pipe culvert.

There is an existing detention basin located at the north-western boundary of the site, which was constructed to mitigate the increase in peak discharges from the site resulting from the Greenbank Shopping Centre development. The Operational Works drawings for this basin are included in Appendix C.

4.1.1 Pre-Development Peak Stormwater Condition

An existing detention basin is currently located in the north-western corner of the site. It was constructed to mitigate the stormwater quantity impacts associated with the development comprising the existing shopping centre development. The subject application relates to subdividing Lot 5 on SP214051, for a future use unrelated to the shopping centre or its planned expansions. As the existing detention basin is located in Proposed Lot 8, it is proposed to relocate the facility to Proposed Lot 7, which is the proposed lot for the proposed shopping centre expansion development (DEV2016/813). As such the relocated detention basin will be to continue mitigate the increase of peak discharges from the site resulting in those flows associated with the <u>existing</u> shopping centre.

Therefore, for the purposes of this report, the pre-development condition is taken to refer to the undeveloped condition of the subject site <u>prior to the development of the existing shopping centre area</u>. The subsequent assessment will demonstrate that the relocated basin will maintain the development obligations required associated with the construction of the <u>existing shopping centre</u>.

Rational Method Calculations (in Appendix E) have been undertaken to provide peak flow rates to compare against the DRAINS model which has been utilised to calculate the pre-development peak flow rates for the catchment.

The rainfall intensities utilised in the stormwater calculations have been calculated for the site's coordinates using the ARR16 Very Frequent Design Rainfall Intensity, gathered from the Bureau of Meteorology. The 1hr rainfall intensity for a 10% AEP ($^{1}I_{10}$) for this site location is 57.7 mm/hr.

By undertaking an overall site investigation and looking at historical aerial photography, the undeveloped site can be generally categorised as rural. As such, a Fraction Impervious of 0.0 has been determined. The pre-development f_i and C_{10} values as per the QUDM have been evaluated and are listed below in Table 4-1.

Table 4-1: Catchment Un-developed Parameters

Catchment	Catchment's Development Category	Fraction Impervious (f _i)	Coefficient of Discharge (C ₁₀)
Undeveloped Site	Rural	0.0	0.7

The undeveloped peak flows for the Catchments for both DRAINS and the Rational Method are summarised in the following Table 4-2 and Table 4-3.

The rainfall temporal patterns from Australian Rainfall and Runoff (ARR16) were utilised in the DRAINS model. The ILSAX hydrological method has been used with 1mm storage or impervious surfaces and 5mm storage for pervious surfaces.

Table 4-2: Undeveloped Peak Flows – Rational Method

AEP (ARI yrs)	39% (2yr)	18% (5yr)	10% (10yr)	5% (20yr)	2% (50yr)	1% (100yr)
Total Catchment	1.457	2.264	2.828	4.567	5.755	6.625

Table 4-3: Pre-development Peak Flows – DRAINS Model

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AEP (ARI yrs)	39% (2yr)	18% (5yr)	10% (10yr)	5% (20yr)	2% (50yr)	1% (100yr)
Total Catchment	2.27	3.32	3.88	4.68	5.52	6.27

As demonstrated by Table 4-2 and Table 4-3 above, the Rational Method calculations and DRAINS model yield similar values and are considered comparable. As such, the DRAINS values shall be adopted as the peak flow rates for the undeveloped site condition for the purposes of the subsequent analysis.

4.2 Lawful Point of Discharge

It is a requirement that every development must have a lawful point of stormwater discharge. It is proposed to maintain the existing lawful point of discharge which is the overland flow path located on the western boundary that discharges to the adjacent rail corridor. Refer to the Conceptual Stormwater Management Plan in Appendix D for the locations.

4.3 Proposed Stormwater Management Strategy

4.3.1 Catchment Description

Similar to the Pre-development Stormwater Condition Assessment in Section 4.1, the proposed Stormwater condition that will subsequently be assessed relates to the developed condition of the <u>existing shopping centre development</u>. <u>No new</u> <u>uses</u> have been considered nor are proposed as part of the subject development application.

The pre and post-development catchment areas are summarised in Table 4-4 below and on the drawing within Appendix D.

Table 4-4: Pre & Post-development Catchments

Catchment Name	Pre-development (Ha)	Post-development (Ha)	Change (Ha)
Site Catchment	14.151	14.151	0
Total	14.151	14.151	0

The Coefficients of Discharge have been determined in accordance with QUDM, utilising the Development Layout Plan. The f_i and C_{10} values have been evaluated and are listed below in Table 4-5.

Table 4-5: Catchment Post-development Parameters

Catchment	Fraction Impervious (f _i)	Coefficient of Discharge (C ₁₀)
Existing Shopping Centre	0.85	0.84
Existing Undeveloped Site	0.0	0.7

The Coefficient of Runoff (C_y) for the various ARI events is evaluated by using the frequency factor and C_{10} values established above.

Rational Method Calculations (in Appendix E) have been undertaken to provide peak flow rates to compare against the DRAINS model which has been utilised to calculate the unmitigated post-development peak flow rates for the catchment. The unmitigated post-development peak flows for the Catchments for both DRAINS and the Rational Method are summarised in Table 4-6 and Table 4-7 following.

Table 4-6: Unmitigated Post-development Peak Flows – Rational Method

AEP	63%	39%	18%	10% (10yr)	5%	2%	1%
(ARI yrs)	(1yr)	(2yr)	(5yr)		(20yr)	(50yr)	(100yr)
Total Catchment	1.299	1.579	2.453	3.063	3.715	4.771	5.525

Table 4-7: Unmitigated Post-development Peak Flows – DRAINS Model

AEP	63%	39%	18%	10%	5%	2%	1%
(ARI yrs)	(1yr)	(2yr)	(5yr)	(10yr)	(20yr)	(50yr)	(100yr)
Total Catchment	2.58	3.57	4.74	5.42	6.38	7.13	8.03

As demonstrated by Table 4-6 and Table 4-7, the DRAINS model yields consistently greater values than the Rational Method calculations. This is owing to the partial area affects being considered in the DRAINS model. As such, the DRAINS model shall be utilised for subsequent analysis.

4.3.2 Proposed Stormwater Management Strategy

The flow comparison in Section 4.3.1 demonstrates that peak flow rates are worsened from pre-development conditions as a result of the existing shopping centre development. Therefore, a detention basin facility is required to be retained on the site as part of the proposed subject development. As noted in Section 4.1, the existing detention basin is proposed to be relocated to Proposed Lot 7, immediately adjacent to the existing shopping centre. This is proposed to be an interim measure to ensure the site's current obligations are maintained as a result of the proposed ROL.

It is noted that subsequent developments, for example EDQ ref 2016/813, will require the further alteration of the stormwater detention facilities within the existing shopping centre and Proposed Lot 7. These future alterations are not the subject of this development and report. Further, it is acknowledged that this management strategy is different to the approved stormwater management strategy in the Development Permit for the shopping centre expansion. As such, prior to commencement of the development of the shopping centre, a Change of Approval application to accommodate this change to the existing approved Stormwater Management Strategy will be required. However, this shall form a separate application, and is not the subject of this report.

Therefore, as part of the subject development, relocate and modify the current detention basin to accommodate existing attenuation requirements as a result of the existing shopping complex.

The proposed Conceptual Stormwater Management Strategy has been prepared based on these investigations. The Stormwater Management Plan and Details have been included in Appendix D.

4.3.3 Proposed Temporary Stormwater Attenuation

A new temporary detention basin has been proposed directly adjacent to the north west boundary of the existing shopping complex development, in order to mitigate the stormwater flows resulting from the existing development. The basin's details are shown in the drawings in Appendix D and are summarised subsequently below. The subsequent design is preliminary only and is subject to further optimisation and design development as part of the operational works process.

A hydraulic assessment has been undertaken to evaluate stormwater detention and outlet control requirements for each storm event to demonstrate that pre-development flow rates as established in Section 4.1.1 have been achieved in the post-development site condition. The DRAINS model established in Section 4.3.1 for the unmitigated post-development condition has been utilised to undertake mitigated post-development scenario modelling.

The proposed basin is designed to collect all runoff up to a 1% AEP from the existing shopping complex development. The basin also incorporates some bio-retention area and its associated extended detention depth as outlined in Section 0. The basin has the following proposed properties:

Max Detention Volume:	1,753m³
Max Detention Depth:	1.19m (RL65.74m AHD)
Detention Base level:	RL 64.553m AHD
Min Bund Level:	RL 66.10m AHD
Min. Freeboard:	0.3m
Low level Outlet:	1/ 525mm RCP @ RL 64.55m AHD
High Level Spillway:	1 x 5m weir at RL 65.5m AHD
(Stepped Weir)	1 x 10m weir at RL 65.7m AHD

The proposed outlet configuration has the following modelled rating curve as shown in Figure 4-1.



Figure 4-1: Basin Outlet Rating Curve

The proposed detention basin has been modelled with a Storage Volume vs Height profile as shown in Figure 4-2 below. Please note that the below Volume vs Height graph does not include the storage available within the upstream pipe and pit system, and as such, it is a conservative approximation of the available total system storage thus providing a factor of safety for the system design.



Figure 4-2: Basins' Stage - Storage Relationships

The proposed basin has been designed such that the minimum freeboard of 0.3m can be achieved in the critical 1% AEP storm event. This is in accordance with QUDM's requirements.

4.3.4 Mitigated Post Development Condition

The proposed stormwater quantity management strategy was modelled using a DRAINS model as established in the earlier sections. The model has demonstrated that the mitigated post-development peak flow rates do not exceed the undeveloped condition's peak flow rates as established by Section 4.1.1 for each storm event between 39% to 1% AEP and standard duration from 1 min to 168 hours.

The peak undeveloped and post-development runoff hydrographs for the critical 1% AEP event as established by DRAINS can be seen following in Figure 4-3. The graph clearly shows the effect of the proposed detention device by illustrating the reduction of post-development inflow to outflow for the 100yr ARI event.



Figure 4-3: Total Site Hydrograph Comparison, 1% AEP (100yr ARI)

The results of the proposed detention basin and stormwater quantity management strategy have been summarised in Table 4-8 below, with the DRAINS model results for the critical duration for each event seen in Appendix E.

Avg Exceedance Probability (AEP) (ARI yrs)	39% (2yr)	18% (5yr)	10% (10yr)	5% (20yr)	2% (50yr)	1% (100yr)
Peak Undeveloped Flows (m³/s)	2.03	3.00	3.54	4.28	5.10	5.76
Peak Mitigated Post- development Flows (m³/s)	1.84	2.63	3.2	4.01	4.93	5.66
Total Increase†	-0.19	-0.37	-0.34	-0.27	-0.17	-0.10

Table 4-8: Total Site Mitigated Results Summary for Various ARI Events, Critical Durations

† negative denotes reduction in mitigated post-development peak flow rates

As such, it has been demonstrated that the proposed stormwater quantity management strategy as depicted in the drawings in Appendix D adequately meets the requirements in relation to stormwater quantity for the site.



5. Site-based Stormwater Quality Management Plan

5.1 Stormwater Management Strategy – Operational Phase

The subject development is associated with a ROL only, and no uses are proposed. The stormwater quality management objectives of the site are:

- a. Maintain the current development permit obligations associated with the existing shopping centre
- b. Demonstrate that the water quality objectives for the proposed development can be achieved.

The existing shopping centre did not have any stormwater quality obligations that were required to be met with on-site facilities. While the Development Permit could not be sourced due to its age, the Operational Works drawings for the Roads and Drainage component were. These are included in Appendix C. It demonstrates that the existing basin had no bioretention facilities incorporated into it. As such, it is not proposed to incorporate any stormwater quality treatment measures associated with the existing shopping centre development.

As noted in Section 2.3, no new uses are proposed as part of the subject application. These future developments are subject of separate applications. Specifically:

- Proposed Lot 7 The proposed lot for the shopping centre expansion. The shopping centre expansion is the subject of an existing EDQ Development Approval (Ref: DEV2016/813). The stormwater quality measures associated with this development will be constructed as part of this development in accordance with its approvals. It is acknowledged that a Change Application is required to the existing Development Approval to accommodate the stormwater quality management within Proposed Lot 7 (instead of the currently documented location within the Proposed Lot 8 footprint).
- Proposed Lot 8 No new uses are proposed as part of the subject development. These shall be by separate application by others. It is therefore proposed that as part of the future development application over Proposed Lot 8, that any Stormwater Quality Management requirements associated with this future development are assessed and mitigated as part of its application by others.

Therefore, no stormwater quality measures are required, nor proposed as part of the subject proposed development.

5.2 Acid Sulphate Soils

Acid Sulphate Soils are typically encountered in Holocene sediment and below 5m AHD. The lowest area of the proposed works associated with the development is at an approximate RL 61m AHD, with the deepest excavation expected to be to approximately RL 60m AHD.

The deepest excavation is not expected to be below RL 5m AHD, the natural surface is not below RL 20m AHD, and the site is not subject to Council's or Qld Government's ASS mapping. As such, acid sulphate soils are not expected to be a development issue.

5.3 Erosion and Sediment Control (ESC) – Construction

An Erosion and Sediment Control (ESC) Management Plan has been prepared by the Contractor as part of their Construction Environmental Management Plan. It will need to demonstrate that the proposed development can accommodate the necessary devices to mitigate the sediment and erosion risks associated with the construction phase of the development. The plan has been prepared with reference to the International Erosion Control Association (IECA) Best Practice Erosion and Sediment Control. Prior to works commencement on-site, the ESC Plans will be reviewed, amended and endorsed by a Certified Professional in Erosion and Sediment Control (CPESC).



6. Conclusion

This Site Based Stormwater Management Plan has been prepared for the proposed subdivision of the the property situated at 15-67 Pub Lane, Greenbank, Qld.

This report has demonstrated that the the existing stormwater detention basin can be relocated into Proposed Lot 7 and continue to meet the stormwater quantity development permit obligations of the existing shopping centre.

It has further been demonstrated that no stormwater quality treatment measures are required to either:

- Maintain the current development permit obligations associated with the existing shopping centre, or
- Achieve the water quality objectives for future developments on Proposed Lot 7 or 8. These shall be constructed as required as part of their respective approvals.

We therefore request that MEDQ supports the Development Application for this site.

Appendix A - Existing Detailed Site Survey and ROL Layout

A2 1070 Rev A by DTS dated 15/10/19





Appendix B - Authority Flood Mapping LCC Flood search results



Logan City Council - Logan Planning Scheme 2015

Logan City Council © The State of Queensland, 2017. Includes material © Planet Labs

Appendix C -	Existing	Operational	Works
Drawings			



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Stormwater Drawings

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Appendix D - Engineering Drawings





Appendix E - Stormwater Quantity Calculations

Rational Method Calculation

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		ing Cel	,		racterist	ומרוכוואו	gory/ :tion ious (fi)		ace / Pa	ace / Pa		0.85	ace / Pa	0.26		
-	lteo	Shopp			ient Cha		Cate Frac impervi		Open Sr	Open Sp			Open Sp			
DW PART OF	star	enbank			Catchm		ia (Ha)		4.284	9.927	14.211	4.284	9.927	14.211		
ž		Gree	_				Are			rre		nt)	rei			
						Descriptio		ndev	Indev (Cu	ase Case	ev (curre	Indev (cui				
2		ct:	Descriptio				ment		<u>را</u>	<2 U	Jndev B	<u>د</u>	K2 U	l Dev		
Projec				Catchn				Ĩ	Û	Total L	ũ	Û	Total			

					ARI	Q ₁₀₀ (m ³ /s)			1.670	3.660		6.653	000	2.969	3.660	5.554			
	3	3M	//2019		EP/ 100y	l₁ _{00yr,t} ₀ (mm/hr)			166.91	157.87		200.48		249.33	157.87	157.85			
e Civil 1 4500	Ň.	ш	2/10		1% A	C100			0.84	0.84		0.84		-	0.84	0.891			
Brisbane (07) 381	Sheet				ARI	Q ₅₀ (m³/s)			1.441	3.160	0	9.779		2.585	3.160	4.796			
	5	By:	Date:		EP/ 50yr	l _{50yr, te} mm/hr)			150.34	142.25		181./2		224.67	142.25	142.24			
					2% A	C ₅₀			0 805	0.805		GU8.U		0.966	0.805	0.854			
				RI)	ARI	Q ₂₀ (m ³ /s)			1.120	2.461		4.58/		2.006	2.461	3.735			
				erval (A	EP/ 20yr /	l _{20yr, te} mm/hr)			127.99	121.32		157.96		191.00	121.32	121.31			
				nce Inte	5% AI	C ₂₀ (0.735	0.735		0.735		0.882	0.735	0.779			
				scurrer	ARI	Q ₁₀ (m ³ /s)			0.927	2.029		2.840		1.657	2.029	3.079			
tion		9875		age Re	EP/ 10yr	l _{10yr, te} nm/hr)			111.20	105.01		102.69		165.67	105.01	105.00			
lculat		3	A	oy Avel	10% A	C ₁₀ (1			0.7	0.7	1 0	0.7		0.84	0.7	0.742			
d Cal		Project No:	Revision:	ak Flow Rates I	ARI	Q5 (m³/s)			0.743	1.625	100	2.2/4		1.327	1.625	2.466			
Aetho					AEP/ 5yr .	l _{5yr, te} (mm/hr)			93.81	88.53		86.54		139.67	88.53	88.52			
nal N			Pea	18% /	ů			0.665	0.665		0.665		0.798	0.665	0.705				
Ratio		sion			ARI	Q2 (m³/s)			0.479	1.046	1 100	1.463		0.855	1.046	1.588			
		Centre Extens			AEP/ 2yr	l _{2yr, te} mm/hr)			67.56	63.70		QZ:Z9		100.53	63.70	63.69			
					39% /	C ₂			0.595	0.595		0.595		0.714	0.595	0.631			
	S S S S S S S S S S S S S S S S S S S	oppinç			ARI	Q ₁ (m ³ /s)			0.394	0.861		1.204		0.705	0.861	1.306			
ART OF	änt	ank Sh			\EP/ 1yr .	I _{1yr, te} mm/hr)			59.07	55.69		54.42		88.03	55.69	55.69			
MON	2	Greent			63% /	Ċ.			0.56	0.56		0990		0.672	0.56	0.594			
						ription			hdev	(Current		e Case		current)	(current				
	ENGINEER		iption:			t Desd			'n	Indev		v Basi		Dev (Jndev				
WOOD & GRIEVE		Project:	Title / Descri			Catchmen			EX1	EX2		I otal Under		EX1	EX3	Total Dev			

Design with community in mind

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